

### P6.4-5

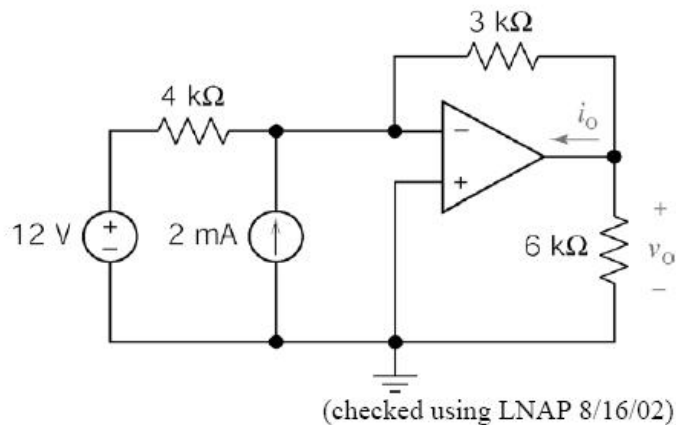
The voltages at the input nodes of an ideal op amp are equal so  $v_a = 0$  V. Apply KCL at node  $a$ :

$$-\left(\frac{v_o - 0}{3000}\right) - \left(\frac{12 - 0}{4000}\right) - 2 \cdot 10^{-3} = 0$$

$$\Rightarrow v_o = -15 \text{ V}$$

Apply KCL at the output node of the op amp:

$$i_o + \frac{v_o}{6000} + \frac{v_o}{3000} = 0 \Rightarrow i_o = 7.5 \text{ mA}$$



### P6.4-8

The node voltages have been labeled using:

1. The currents into the inputs of an ideal op amp are zero and the voltages at the input nodes of an ideal op amp are equal.

2. KCL

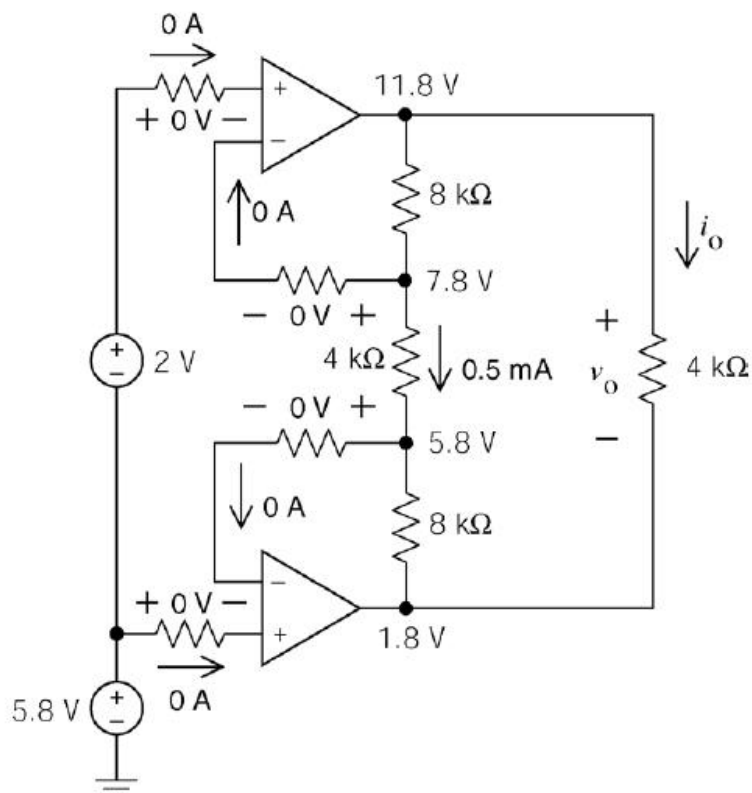
3. Ohm's law

Then

$$v_o = 11.8 - 1.8 = 10 \text{ V}$$

and

$$i_o = \frac{10}{4000} = 2.5 \text{ mA}$$



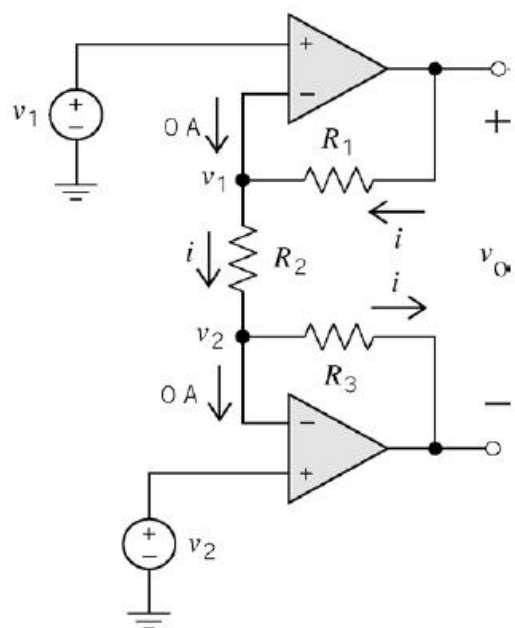
**P6.5-4**

Ohm's law:

$$i = \frac{v_1 - v_2}{R_2}$$

KVL:

$$v_0 = (R_1 + R_2 + R_3)i = \frac{R_1 + R_2 + R_3}{R_2}(v_1 - v_2)$$



**P6.5-7**

Apply KCL at the inverting input node of the op amp

$$-\left(\frac{v_a - 0}{10000}\right) + 0 - \left(\frac{(v_a + 6) - 0}{30000}\right) = 0$$

$$\Rightarrow v_a = -1.5 \text{ V}$$

Apply KCL to the super node corresponding the voltage source:

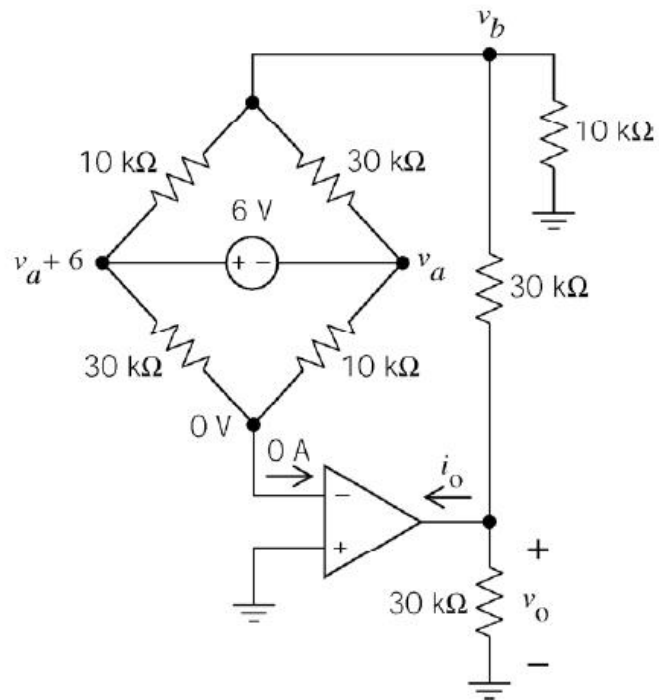
$$\frac{v_a - 0}{10000} + \frac{v_a + 6 - 0}{30000}$$

$$+ \frac{v_a - v_b}{30000} + \frac{(v_a + 6) - v_b}{10000} = 0$$

$$\Rightarrow 3v_a + v_a + 6 + v_a - v_b$$

$$+ 3[(v_a + 6) - v_b] = 0$$

$$\Rightarrow v_b = 2v_a + 6 = 3 \text{ V}$$



Apply KCL at node  $b$ :

$$\frac{v_b}{10000} + \frac{v_b - v_o}{30000} - \left(\frac{v_a - v_b}{30000}\right) - \left(\frac{(v_a + 6) - v_b}{10000}\right) = 0$$

$$\Rightarrow 3v_b + (v_b - v_o) - (v_a - v_b) - 3[(v_a + 6) - v_b] = 0$$

$$\Rightarrow v_o = 8v_b - 4v_a - 18 = \underline{12 \text{ V}}$$

Apply KCL at the output node of the op amp:

$$i_o + \frac{v_o}{30000} + \frac{v_o - v_b}{30000} = 0 \Rightarrow i_o = -0.7 \text{ mA}$$

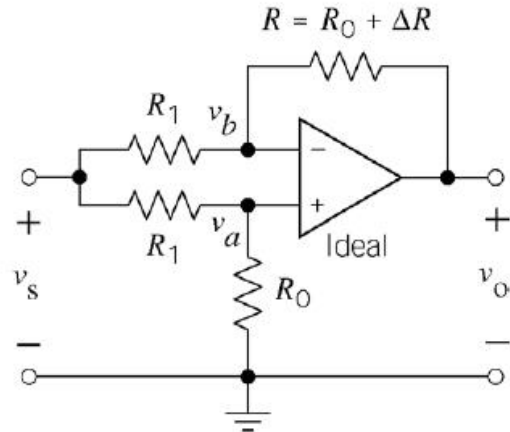
**P6.5-10**

By voltage division (or by applying KCL at node  $a$ )

$$v_a = \frac{R_0}{R_1 + R_0} v_s$$

Applying KCL at node  $b$ :

$$\begin{aligned} \frac{v_b - v_s}{R_1} + \frac{v_b - v_0}{R_0 + \Delta R} &= 0 \\ \Rightarrow \frac{R_0 + \Delta R}{R_1} (v_b - v_s) + v_b &= v_0 \end{aligned}$$

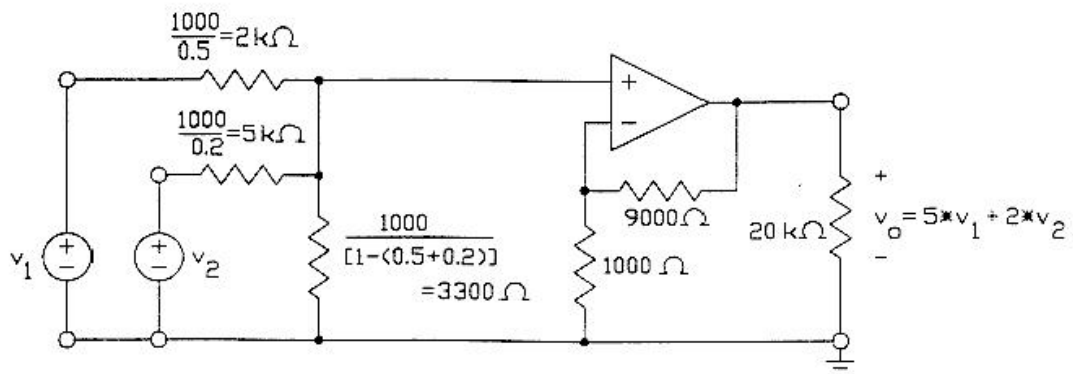


The node voltages at the input nodes of an ideal op amp are equal so  $v_b = v_a$ .

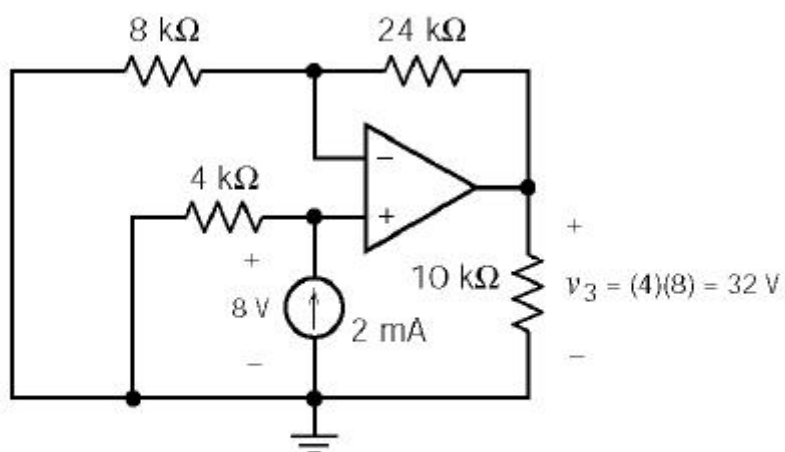
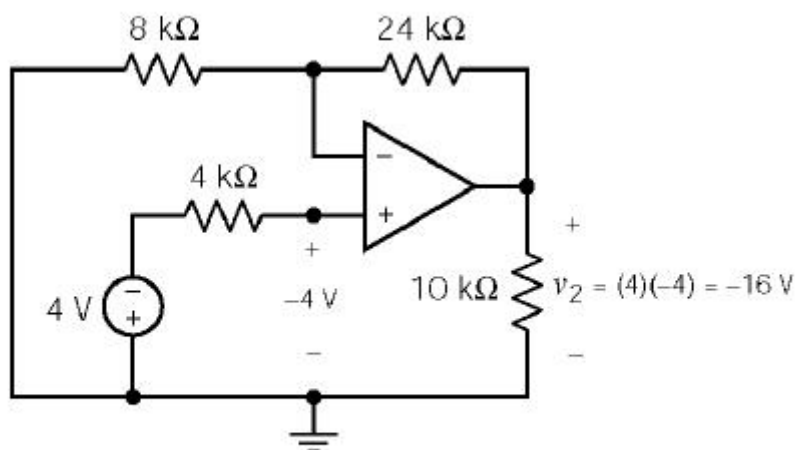
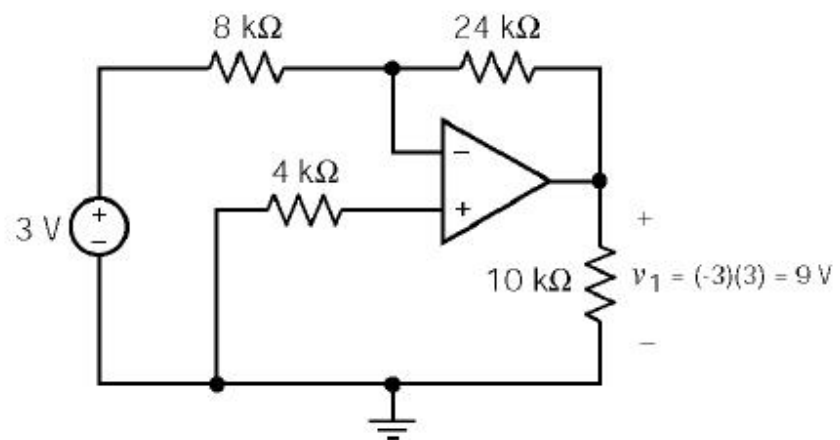
$$v_0 = \left[ \left( \frac{R_0 + \Delta R}{R_1} + 1 \right) \frac{R_0}{R_1 + R_0} \frac{R_0 + \Delta R}{R_1} \right] v_s = -\frac{\Delta R}{R_1 + R_0} v_s = \left( -v_s \frac{R_0}{R_1 + R_0} \right) \frac{\Delta R}{R_0}$$

**P6.6-3**

Use the noninverting summing amplifier, entry (e) in Figure 6.6-1.



**P6.6-9**



Using superposition,  $v_o = v_1 + v_2 + v_3 = -9 - 16 + 32 = 7 \text{ V}$

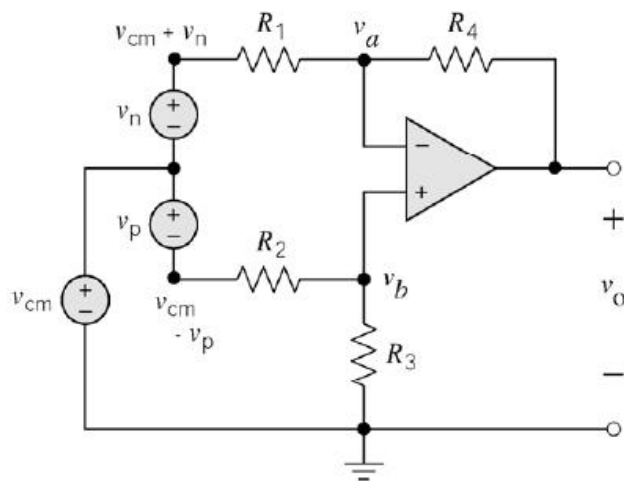
**P6.8-4**

a) 
$$\frac{v_o}{v_{in}} = -\frac{R_2}{R_1} = -\frac{49 \times 10^3}{5.1 \times 10^3} = \underline{-9.6078}$$

b) 
$$\frac{v_o}{v_{in}} = \frac{(2 \times 10^6)(75 - (200,000)(50 \times 10^3))}{(5 \times 10^3 + 2 \times 10^6)(75 + 50 \times 10^3) + (5 \times 10^3)(2 \times 10^6)(1 + 200,000)} = \underline{-9.9957}$$

c) 
$$\frac{v_o}{v_{in}} = \frac{2 \times 10^6(75 - (200,000)(49 \times 10^3))}{(5.1 \times 10^3 + 2 \times 10^6)(75 + 49 \times 10^3) + (5.1 \times 10^3)(2 \times 10^6)(1 + 200,000)} = \underline{-9.6037}$$

**P6.8-5**



Apply KCL at node  $b$ :

$$v_b = \frac{R_3}{R_2 + R_3}(v_{cm} - v_p)$$

Apply KCL at node  $a$ :

$$\frac{v_a - v_o}{R_4} + \frac{v_a - (v_{cm} + v_n)}{R_1} = 0$$

The voltages at the input nodes of an ideal op amp are equal so

$$v_a = v_b.$$

$$v_o = -\frac{R_4}{R_1}(v_{cm} + v_n) + \frac{R_4 + R_1}{R_1}v_a$$

$$v_o = -\frac{R_4}{R_1}(v_{cm} + v_n) + \frac{(R_4 + R_1)R_3}{R_1(R_2 + R_3)}(v_{cm} - v_p)$$

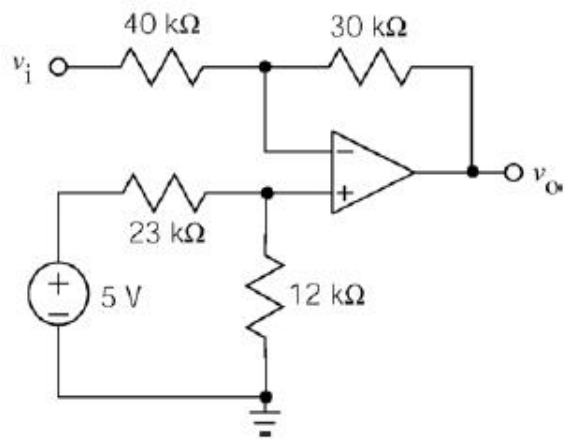
when  $\frac{R_4}{R_1} = \frac{R_3}{R_2}$  then  $\frac{(R_4 + R_1)R_3}{R_1(R_2 + R_3)} = \frac{\frac{R_4}{R_1} + 1}{\frac{R_3}{R_2} + 1} \times \frac{R_3}{R_2} = \frac{R_4}{R_1}$

so

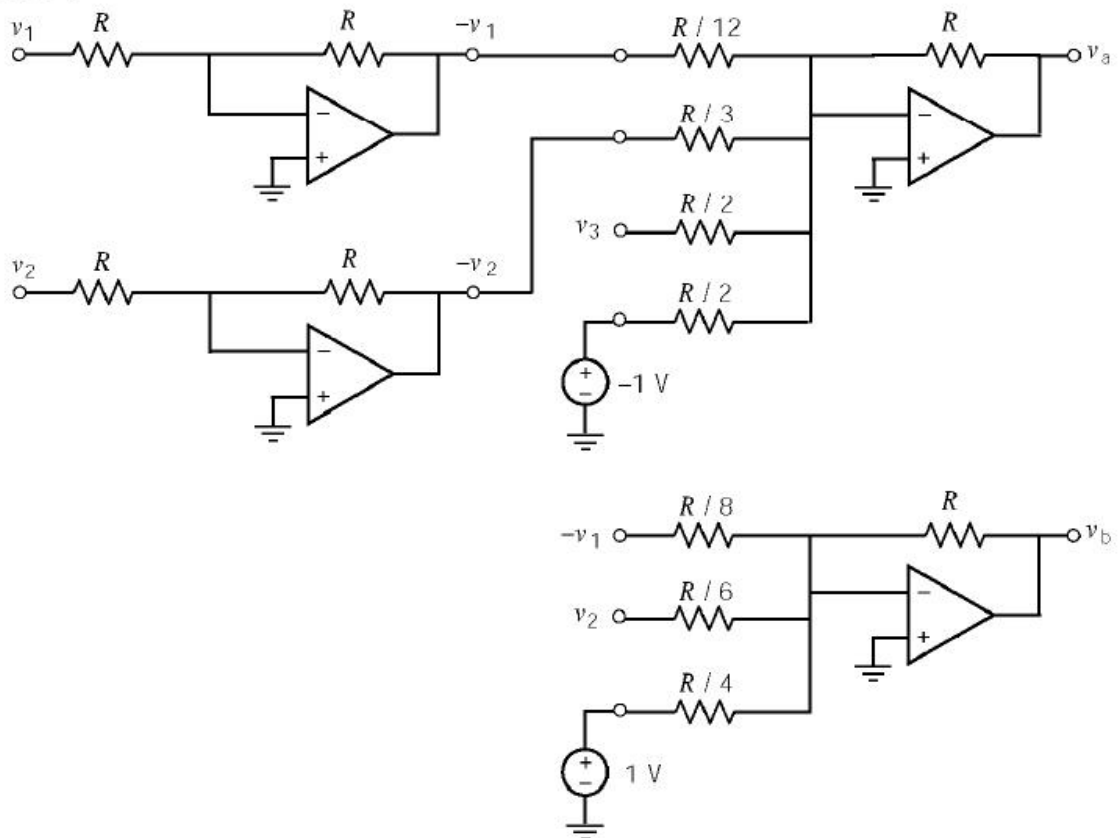
$$v_o = -\frac{R_4}{R_1}(v_{cm} + v_n) + \frac{R_4}{R_1}(v_{cm} - v_p) = -\frac{R_4}{R_1}(v_n + v_p)$$

**DP6-2**

$$v_o = -\frac{3}{4}v_i + 3 = -\frac{3}{4}v_i + \left(1 + \frac{3}{4}\right)\left(\frac{12}{35}\right)5 = -\frac{3}{4}v_i + \left(1 + \frac{3}{4}\right)\left(\frac{12}{12+23}\right)5$$

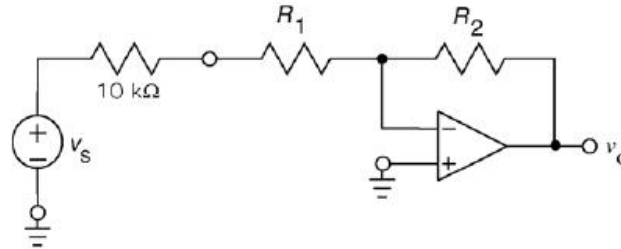


**DP6-4**

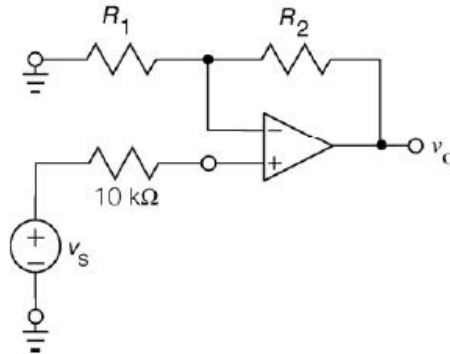


**DP6-5**

We require a gain of  $\frac{4}{20 \times 10^{-3}} = 200$ . Using an inverting amplifier:



Here we have  $200 = \left| -\frac{R_2}{10 \times 10^3 + R_1} \right|$ . For example, let  $R_1 = 0$  and  $R_2 = 1 \text{ M}\Omega$ . Next, using the noninverting amplifier:



Here we have  $200 = 1 + \frac{R_2}{R_1}$ . For example, let  $R_1 = 1 \text{ k}\Omega$  and  $R_2 = 199 \text{ k}\Omega$ .

The gain of the inverting amplifier circuit does not depend on the resistance of the microphone. Consequently, the gain does not change when the microphone resistance changes.