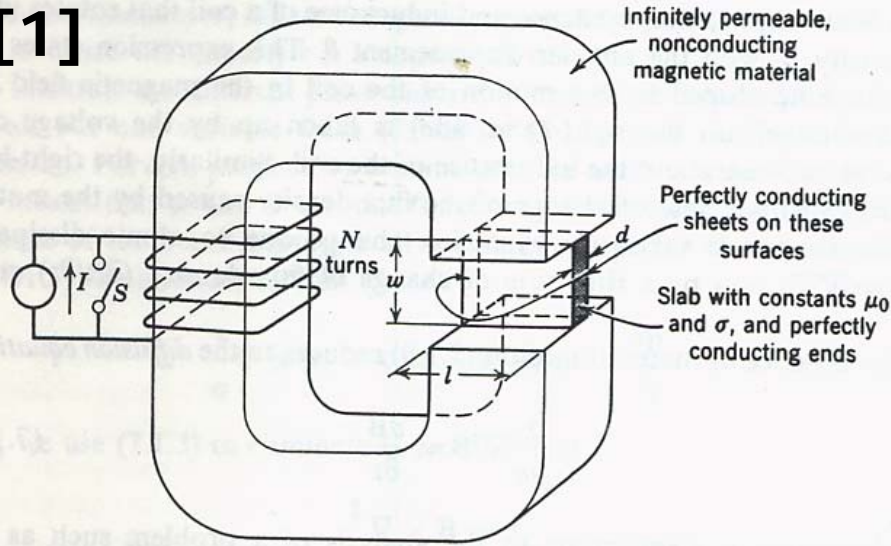


[1]



스위치가 열리는 순간 I 가 가해지고
 자장 B_0 가 가해진다. 이 때 물건
(block) 안의 자계 분포를 구하라.
 자계는 x 방향으로만 존재한다고 생
 각하고 z, t 만의 함수로 가정한다 (25 점).

(a) B_0 를 구하라 (B_0 는 공간의 자속밀도) (3 점).

(b) $B_x(z, t)$ at $0 < z < d$ (10 점)

(c) 기본 시정수 τ 를 구하라 (2 점).

(d) 그래프를 그려라 (2 점).

(e) Eddy current 를 구하고 그래프를 그려라 (4 점).

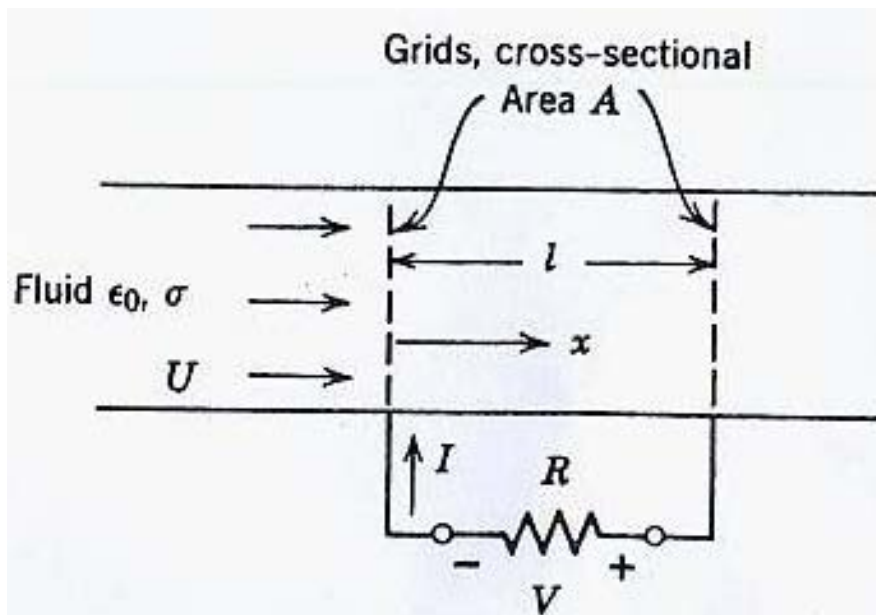
(f) Block 을 one turn coil 로 생각하고 집중정수상수 G, L 을 구하라. 이 때
 시정수는 (c) 에서 구한 τ 를 사용하라 (4 점).

[2] 도전성 유체(s)가 단면적 A 인 절연파이프 안을 x 방향으로 흐르고 있다. 유체는 일정한 속도 U 로 흐르고 있다. 이온은 $x = 0$ 에 있는 전원으로부터 전하밀도 ρ_0 로 주입되고 있다 (25점).

(a) 두 전극 사이에서의 전하 밀도 분포를 구하라 (10점).

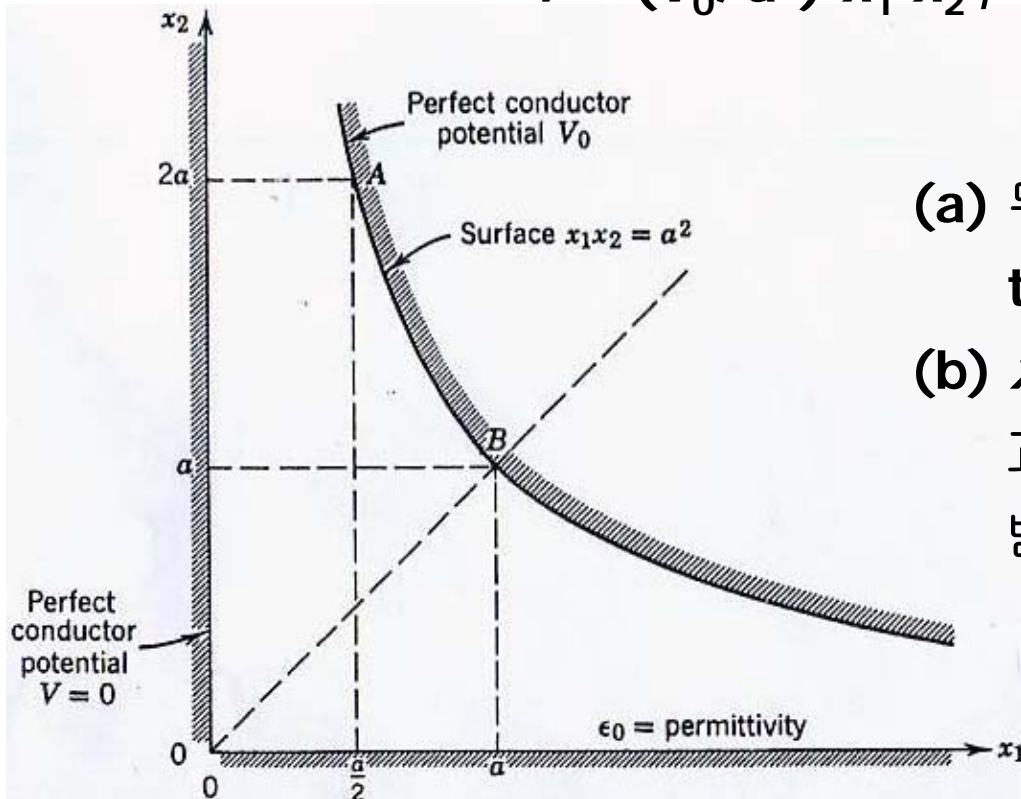
(b) 전극 사이의 전기의 세기를 구하라 (10점).

(c) 저항 R 사이에 인가되는 전압을 구하라 (5점).



[3] 그림과 같이 두 개의 등전위 전극이 있다. x_3 방향으로는 무한히 길다. 두 전극 사이의 포텐셜은 다음 식과 같고 전계의 세기는 아래의 식으로 규정한다 (25 점).

$$f = (V_0/a^2) x_1 x_2, \quad E = - \text{grad } f$$

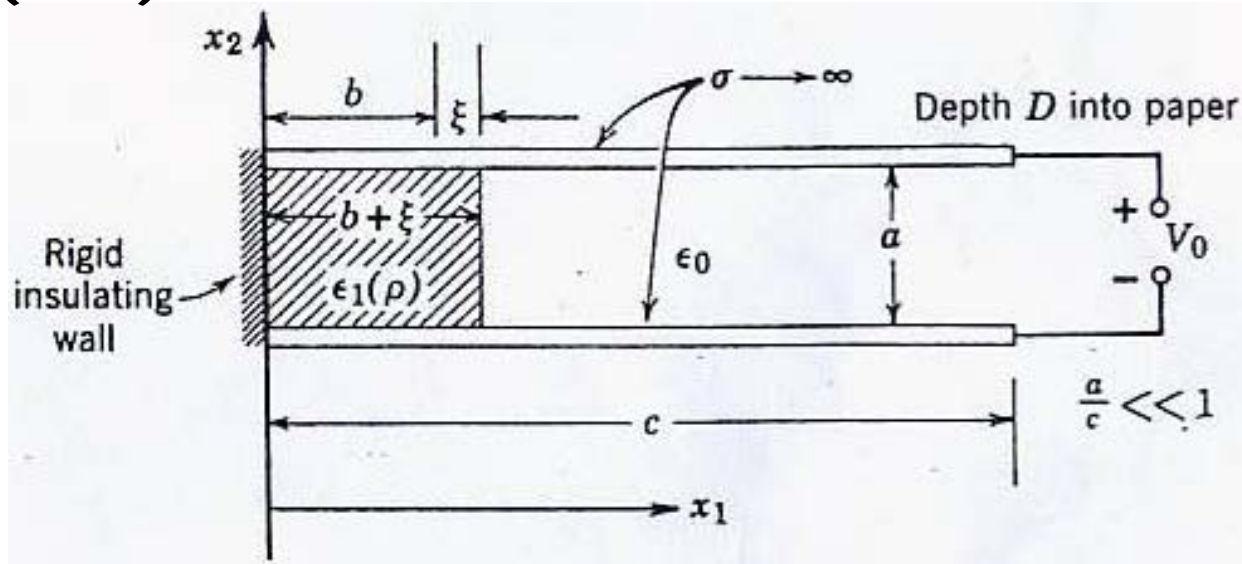


- (a) 두 전극 사이의 모든 방향의 **stress tensor** 성분을 구하라 (10점).
- (b) x_3 방향으로는 길이가 D 이고 A 점과 B 점 사이의 전극의 곡면 부분이 받는 전체 힘을 구하라 (15 점).

[4] 탄성 물질이 왼쪽이 고정되어 있고 두 전극 사이에 놓여 있다. 오른쪽은 자유롭게 놓여 있고 유전율은 밀도의 함수이다. $\epsilon_1 = \epsilon_1(\rho)$. 두 전극에는 일정 전압이 걸려있다 (25점).

(a) 분극 물질에 적용하는 **Maxwell stress tensor**를 이용하여 두 전극 사이의 물질의 오른쪽 면에 가해지는 전체 힘을 구하라 (15점).

(b) **Energy method**(가상 변위법)를 이용해서 (a)의 결과를 확인하라 (10점).



[1]

(a) $\oint_C \vec{H} \cdot d\vec{l} = NI$

$$H_0 w = NI \rightarrow H_0 = \frac{NI}{w}$$

$$\therefore B_0 = \mu_0 H_0 = \frac{\mu_0 NI}{w}$$

(b) $-\frac{1}{\mu_0 \sigma} \nabla^2 \vec{B} + \frac{\partial \vec{B}}{\partial t} = \vec{v} \times (\vec{v} \times \vec{B}) \quad \vec{v} = 0 \text{ 이므로}$

$$\Rightarrow -\frac{1}{\mu_0 \sigma} \nabla^2 \vec{B} + \frac{\partial \vec{B}}{\partial t} = 0 \quad \text{x, y, z 각각에 대해} \quad \frac{1}{\mu_0 \sigma} \frac{\partial^2 B_x}{\partial z^2} = \frac{\partial B_x}{\partial t}$$

$$\text{초기조건} \quad \begin{cases} t=0^+ \rightarrow B_x=0 \\ t \rightarrow \infty \rightarrow B_x=B_0 \end{cases}$$

$$\text{일반해} \quad B_x = \hat{B}(z) \cdot e^{-\alpha t} + B_0$$

$$\Rightarrow \frac{1}{\mu_0 \sigma} \frac{d^2 \hat{B}}{dz^2} = -\alpha \hat{B}$$

$$\Rightarrow \hat{B} = C_1 \sin \sqrt{\mu_0 \sigma \alpha} z + C_2 \cos \sqrt{\mu_0 \sigma \alpha} z$$

$$\therefore B_x = (C_1 \sin \sqrt{\mu_0 \sigma \alpha} z + C_2 \cos \sqrt{\mu_0 \sigma \alpha} z) e^{-\alpha t} + B_0$$

$$C_2 = 0 \text{ 임을 } \rightarrow \sqrt{\mu_0 \sigma \alpha} d = n\pi \Rightarrow d_n = \frac{n\pi d^2}{\mu_0 \sigma d^2}$$

* $t=0^+$ 일 때,

$$0 = \sum_{n=1}^{\infty} a_n \sin \frac{n\pi z}{d} + B_0$$

$$\Rightarrow \int_0^d -B_0 \sin \frac{m\pi z}{d} dz = \int_0^d \sum_{n=1}^{\infty} a_n \sin \frac{n\pi z}{d} \cdot \sin \frac{m\pi z}{d} dz.$$

$m \neq n$ or right term = 0 or Bz.

$$\therefore \int_0^d -B_0 \sin \frac{m\pi z}{d} dz = \int_0^d a_m \sin^2 \frac{m\pi z}{d} dz.$$

$$\text{Hence } \begin{cases} a_m = -\frac{4}{m\pi} B_0 & m \text{ odd.} \\ a_m = 0 & m \text{ even} \end{cases}$$

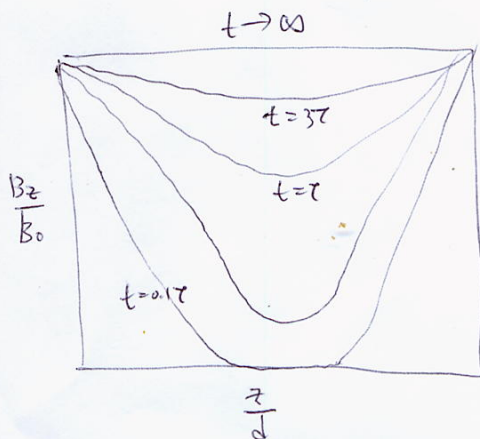
$$\therefore B_x = B_0 \left(1 - \sum_{n \text{ odd}} \frac{4}{n\pi} \sin \frac{n\pi z}{d} e^{-n\pi t/\tau} \right)$$

$$\tau = \frac{l}{\alpha} = \frac{\mu_0 d^2}{\pi^2}$$

$$\therefore B_x = B_0 \left(1 - \sum_{n \text{ odd}} \frac{4}{n\pi} \sin \frac{n\pi z}{d} e^{-n^2 t/\tau} \right)$$

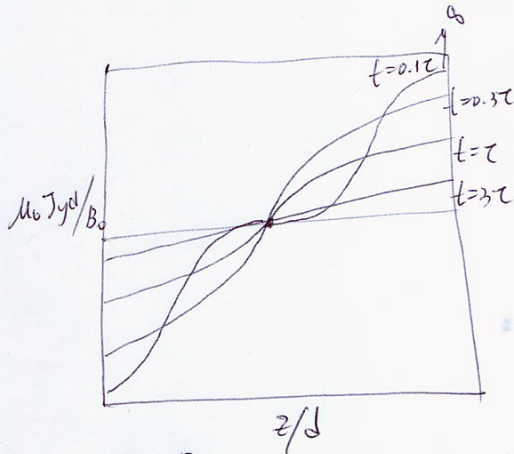
(c) $\tau = \frac{\mu_0 d^2}{\pi^2}$

(d)

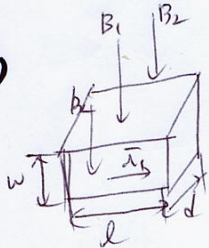


$$(c) \mu_0 \vec{J} = \vec{\nabla} \times \vec{B}$$

$$\Rightarrow J_y = \frac{1}{\mu_0} \frac{dB_x}{dz} = - \frac{B_0}{\mu_0 d} \sum_{n \text{ odd}} \left(\cos \frac{n\pi z}{d} \right) e^{-n^2 t/\tau}$$



(f)



$$B_2 = \frac{\mu_0 N \bar{i}_2}{w}$$

$$B_1 = \frac{\mu_0 N \bar{i}_2}{w} - \frac{\mu_0 \bar{i}_1}{w}$$

$$\lambda_1 = -dI B_1 = L \bar{i}_1 - M \bar{i}_2$$

$$\therefore L = \frac{dI \mu_0}{w}, \quad M = \frac{dI \mu_0 N}{w}$$

$$GL \frac{d\bar{i}_1}{dt} + \bar{i}_1 = GM \frac{d\bar{i}_2}{dt}$$

$$\bar{i}_1 = I N e^{-t/GL} \quad (\bar{i}_2 \text{ is magnitude } I \text{ of step function})$$

$$t > 0, \text{ outside the conductors } = B = B_2 = \frac{\mu_0 N I}{w}$$

$$\text{between the conductors } = B = B_1 = \frac{\mu_0 N I}{w} (1 - e^{-t/GL})$$

$$\therefore G = \frac{\sigma (2d/\pi^2) w}{2l}$$

$$GL = \frac{\mu_0 d^2}{c^2}$$

[2]

(a) $x=0$ 에서 ρ_0 가 주어진 ($\rho_0 = \text{constant}$)

$$\frac{\sigma}{\epsilon_0} \rho_f + U \frac{d\rho_f}{dx} = 0.$$

$$\Rightarrow \rho_f(x) = \rho_0 e^{-\frac{\sigma}{\epsilon_0 U} x} = \rho_0 e^{-\frac{1}{R_e} x} \quad (0 \leq x \leq l)$$

(여기서 $R_e = \frac{\epsilon_0 U}{\sigma}$)

(b) $\vec{J}_f = \sigma \vec{E} + \rho_f \vec{U}$ 이기 때문에 x 방향으로 J_x 이다.

$$J_x = \sigma E_x + \rho_f U, \quad J_x = \frac{I}{A}$$

$$\begin{aligned} E_x &= \frac{1}{\sigma} (J_x - \rho_f U) \\ &= \frac{I}{\sigma A} - \frac{\rho_0}{\sigma} U e^{-\frac{1}{R_e} x} \\ &= \frac{I}{\sigma A} - \frac{\rho_0 U}{\sigma} e^{-\frac{\sigma}{\epsilon_0 U} x} \end{aligned}$$

\Rightarrow open circuit 상태 Van de Graaff Generator 와 동일

$$\begin{aligned} (I=0) \quad V_x &= - \int_0^l E_x dx = \int_0^l \frac{\rho_0 U}{\sigma} e^{-\frac{1}{R_e} x} dx \\ &= \left[-\frac{\rho_0}{\sigma} R_e e^{-\frac{1}{R_e} x} \right]_0^l = \frac{\rho_0}{\sigma} R_e (1 - e^{-\frac{l}{R_e}}) \\ &= \frac{\rho_0 \epsilon_0}{\sigma^2} U^2 (1 - e^{-\frac{l}{R_e}}) \\ &= \rho_0 \cdot R_e^2 \cdot \frac{U^2}{\epsilon_0} (1 - e^{-\frac{l}{R_e}}) = V_{oc} \end{aligned}$$

(C) 저항이 생길때만,

$$I = \frac{V}{R}$$

$$Z_x = \frac{V}{\sigma A R} - \frac{\rho_0}{\sigma} u e^{-\frac{1}{R\epsilon} x} \quad (R' = \frac{1}{\sigma A})$$

$$= \frac{R' V}{R l} - \frac{\rho_0}{\sigma} u e^{-\frac{1}{R\epsilon} x}$$

$$= \frac{R' V}{R l} + Z_{oc}$$

$$V = - \int_0^l \left(\frac{R' V}{R l} \right) dx + \int_0^l \frac{\rho_0}{\sigma} e^{-\frac{1}{R\epsilon} x} dx$$

$$= - \frac{R'}{R} V + V_{oc} \quad (V_{oc} = \frac{\rho_0 \epsilon_0}{\sigma} u (1 - e^{-\frac{l}{R\epsilon}}))$$

$$V = \left(\frac{R}{R+R'} \right) V_{oc} = \frac{\frac{\rho_0 \epsilon_0}{\sigma} u^2 (1 - e^{-\frac{l}{R\epsilon}})}{(1 + \frac{l}{\sigma A R})} = \frac{\frac{\rho_0 \epsilon_0}{\sigma} u^2 (1 - e^{-\frac{\sigma l}{\epsilon_0 u}})}{1 + \frac{l}{\sigma A R}}$$

$$\Sigma, Z_x = \frac{R'}{R} \frac{1}{l} \cdot \frac{R}{R+R'} V_{oc} + Z_{oc} = \frac{R'}{R+R'} \frac{V_{oc}}{l} + Z_{oc},$$



open circuit 이면 $R \rightarrow \infty$ $V = V_{oc}$, $Z_x = Z_{oc}$.

short circuit 이면 $R \rightarrow 0$, $V = 0$, $Z_x = \frac{V_{oc}}{l} + Z_{oc} = 0$.

$I = V +$ 따라서 $I_x = \rho_0 u$ 가 되어 모든 저항이 외부로 나가므로
 $\rho_0 u$ 이므로 $V = 0$ 이 된다.

인양 $R \rightarrow \infty$ 이면,

$$Z_{oc} = \lim_{R \rightarrow \infty} - \frac{R l}{\epsilon_0} \rho_0 e^{-\frac{1}{R\epsilon} x} = \infty \quad \left(\frac{1}{R\epsilon} = x \right)$$

$$V_{oc} = \lim_{R \rightarrow \infty} R \rho_0 \frac{l^2}{\epsilon_0} (1 - e^{-\frac{l}{R\epsilon}}) = \lim_{x \rightarrow 0} \frac{\rho_0 l^2 (1 - e^{-x})}{\epsilon_0 x^2} = \infty$$

$R \rightarrow 0$ 이면

$$Z_{oc} = \lim_{R \rightarrow 0} - \frac{l \rho_0}{\epsilon_0} R e^{-\frac{1}{R\epsilon} x} = 0$$

$$V_{oc} = \lim_{R \rightarrow 0} R \rho_0 \frac{l^2}{\epsilon_0} (1 - e^{-\frac{l}{R\epsilon}}) = 0.$$

[3]

(a) $\phi = \frac{V_0}{a^2} x_1 x_2$, $\varepsilon_1 = -\frac{V_0}{a^2} x_2$, $\varepsilon_2 = -\frac{V_0}{a^2} x_1$, $\varepsilon_3 = 0$, $\frac{\partial}{\partial x_3} = 0$.

$$T_{11} = \frac{\varepsilon_0}{2} \left(\frac{V_0^2}{a^4} x_2^2 - \frac{V_0^2}{a^4} x_1^2 \right) = \frac{\varepsilon_0}{2} \frac{V_0^2}{a^4} (x_2^2 - x_1^2)$$

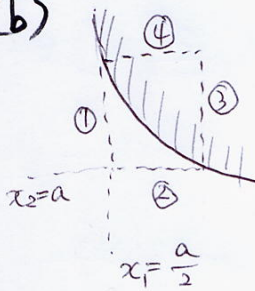
$$T_{22} = -T_{11}$$

$$T_{12} = T_{21} = \varepsilon_0 \frac{V_0^2}{a^4} x_1 x_2$$

$$T_{33} = -\frac{\varepsilon_0}{2} \left(\frac{V_0^2}{a^4} \right) (x_1^2 + x_2^2)$$

$$T_{13} = T_{31} = T_{23} = T_{32} = 0$$

(b)



$$\begin{aligned} f_1 &= -\int_{\text{①}} T_{11} da + \int_{\text{②}} -T_{12} da \\ &= -\int \frac{\varepsilon_0 V_0^2}{2a^4} (x_2^2 - \frac{a^2}{4}) da - \int \varepsilon_0 \frac{V_0^2}{a^4} (a) \cdot x_1 da \\ &= -D \left[\frac{\varepsilon_0 V_0^2}{2a^4} \left[\frac{1}{3} x_2^3 - \frac{a^2}{4} x_2 \right]_a^{2a} + \varepsilon_0 \frac{V_0^2}{a^3} \left[\frac{1}{2} x_1^2 \right]_{\frac{a}{2}}^a \right] \\ &= -D \frac{\varepsilon_0 V_0^2}{2a^3} \left[\frac{1}{a} \left(\frac{8a^3}{3} - \frac{a^3}{2} - \frac{a^3}{3} + \frac{a^3}{4} \right) + (a^2 - \frac{a^2}{4}) \right] \\ &= -\frac{17}{12} \frac{D}{a} \varepsilon_0 V_0^2 \end{aligned}$$

$$f_2 = -\int_{\text{①}} T_{21} da - \int_{\text{②}} T_{22} da$$

$$T_{21} (x_1 = \frac{a}{2}) = \frac{\varepsilon_0 V_0^2}{2a^3} x_2$$

$$T_{22} (x_2 = a) = -\frac{\varepsilon_0 V_0^2}{2a^4} (a^2 - x_1^2) = \frac{\varepsilon_0 V_0^2}{2a^4} (x_1^2 - a^2)$$

$$\begin{aligned}
 f_2 &= -D \left\{ \frac{\epsilon_0 V_0^2}{2a^3} \int_a^{2a} x_2 dx_2 + \frac{\epsilon_0 V_0^2}{2a^4} \int_{\frac{a}{2}}^a (x_1^2 - a^2) dx_1 \right\} \\
 &= -D \frac{\epsilon_0 V_0^2}{2a^3} \left\{ \frac{1}{2} \{ (2a)^2 - a^2 \} + \frac{1}{a} \left[\frac{1}{3} \left(a^3 - \frac{a^3}{8} \right) - a^2 \left(a - \frac{a}{2} \right) \right] \right\} \\
 &= -D \frac{\epsilon_0 V_0^2}{2a^3} a^2 \left\{ \frac{3}{2} + \frac{7}{24} - \frac{1}{2} \right\} \\
 &= -\frac{31}{48} \frac{D}{a} \epsilon_0 V_0^2
 \end{aligned}$$

$$f_3 = 0.$$

i) $V_0 = 10^5 \text{ V}$, $a = 0.1 \text{ m}$, $D = 0.1 \text{ m}$.

$$f_1 = -0.125 \text{ N}, \quad f_2 = -0.057 \text{ N}$$

ii) $V_0 = 1 \text{ MV}$, $a = 0.1 \text{ m}$, $D = 0.1 \text{ m}$.

$$f_1 = -12.5 \text{ N}, \quad f_2 = -5.7 \text{ N}.$$

[4]:

(a) $q \delta V = \delta W' - \delta \mathcal{E}$

$\Rightarrow q \delta V = \int_V \delta w' dV - \int_V \vec{F} \cdot \delta \xi dV$

here $q \delta V = - \int_S \epsilon \vec{\nabla} \phi \cdot n \delta \phi da$

$= \int_V \vec{\nabla} \cdot [(\epsilon \vec{\nabla} \phi) \cdot (\delta \phi)] dV$

$= \int_V \frac{1}{2} \epsilon \delta (\vec{\nabla} \phi)^2 dV$

$\Rightarrow \int_V \frac{1}{2} \epsilon \delta (\vec{\nabla} \phi)^2 dV = \int_V \delta w' dV - \int_V \vec{F} \cdot \delta \xi dV$

or $\int_V \delta \left[\frac{1}{2} \epsilon (\vec{\nabla} \phi)^2 \right] dV = \int_V \delta w' dV$

$\Rightarrow \delta w' = \delta \left[\frac{1}{2} \epsilon (\vec{\nabla} \phi)^2 \right] = \frac{1}{2} (\vec{\nabla} \phi)^2 \delta \epsilon + \frac{1}{2} \epsilon \delta (\vec{\nabla} \phi)^2$

$\epsilon \vec{\nabla} \phi \cdot \vec{\nabla} (\delta \phi) = \vec{\nabla} \cdot (\delta \phi \epsilon \vec{\nabla} \phi) - \delta \phi \vec{\nabla} \cdot (\epsilon \vec{\nabla} \phi) = 0$

$\Rightarrow \delta w' = \frac{1}{2} (\vec{\nabla} \phi)^2 \delta \epsilon$

$\therefore \int_V \left(\frac{1}{2} \vec{\nabla} \cdot \vec{\nabla} \delta \epsilon - \vec{F} \cdot \delta \xi \right) dV = 0 \quad \text{--- } \textcircled{1}$

$\delta \epsilon = \frac{\partial \epsilon}{\partial \rho} \delta \rho, \quad - \delta \rho = \rho \vec{\nabla} \cdot \delta \xi$

अतः $\textcircled{1}$ के लिये $\delta \epsilon$ term है.

$\int_V \frac{1}{2} \vec{\nabla} \cdot \vec{\nabla} \delta \epsilon dV = \int_V -\frac{1}{2} \vec{\nabla} \cdot \vec{\nabla} \frac{\partial \epsilon}{\partial \rho} \rho \vec{\nabla} \cdot \delta \xi dV$

$$= - \int_V \vec{\nabla} \cdot \left(\frac{1}{2} \vec{E} \cdot \vec{E} \cdot \frac{\partial \epsilon}{\partial \rho} \rho \delta \rho \right) dV + \int_V \vec{\nabla} \cdot \left(\frac{1}{2} \vec{E} \cdot \vec{E} \cdot \frac{\partial \epsilon}{\partial \rho} \rho \right) \cdot \delta \rho dV$$

재배열하여 0 식을 다시 재배열하면

$$\int_V \left[-\frac{1}{2} \vec{E} \cdot \vec{E} \cdot \vec{\nabla} \epsilon + \vec{\nabla} \left(\frac{1}{2} \vec{E} \cdot \vec{E} \cdot \frac{\partial \epsilon}{\partial \rho} \rho \right) - \vec{F} \right] \cdot \delta \rho dV = 0.$$

$$\Rightarrow \vec{F} = -\frac{1}{2} \vec{E} \cdot \vec{E} \cdot \vec{\nabla} \epsilon + \vec{\nabla} \left(\frac{1}{2} \vec{E} \cdot \vec{E} \cdot \frac{\partial \epsilon}{\partial \rho} \rho \right)$$

$$\therefore \vec{F} = \rho \vec{E} - \frac{1}{2} \vec{E} \cdot \vec{E} \cdot \vec{\nabla} \epsilon + \vec{\nabla} \left(\frac{1}{2} \vec{E} \cdot \vec{E} \cdot \frac{\partial \epsilon}{\partial \rho} \rho \right)$$

이것은 Maxwell stress tensor 을 이용해서 재배열하면,

$$F_m = \frac{d}{dx_n} (\epsilon E_m E_n) - \frac{\epsilon}{2} \frac{d}{dx_m} (E_k E_k) \\ - \frac{1}{2} E_k E_k \cdot \frac{\partial \epsilon}{\partial x_m} + \frac{d}{dx_m} \left(\frac{1}{2} E_k E_k \cdot \frac{\partial \epsilon}{\partial \rho} \rho \right)$$

재배열하면,

$$F_m = \frac{\partial T_{mn}}{\partial x_n} = \frac{d}{dx_n} \left[\underbrace{\epsilon E_m E_n}_{T_{mn}} - \frac{1}{2} \delta_{mn} E_k E_k \left(\epsilon - \frac{\partial \epsilon}{\partial \rho} \rho \right) \right]$$

$$(b) \quad \delta W' = \int \delta v' - f \delta \xi$$

$$W' = \int \delta v', \quad W' = \frac{1}{2} v^2 C(\xi)$$

$$\Rightarrow \left(\frac{1}{2} v^2 \frac{\partial C(\xi)}{\partial \xi} - f \right) \delta \xi = 0$$

$$\Rightarrow f = \frac{1}{2} v^2 \frac{\partial C(\xi)}{\partial \xi}$$

$$C(\xi) = \epsilon_1(\rho) \frac{(b+\xi) \cdot D}{a} + \epsilon_0 \frac{(c-(b+\xi)) \cdot D}{a}$$

$$\Rightarrow \frac{\partial C(\xi)}{\partial \xi} = \frac{b \cdot D}{a} \frac{\partial \epsilon_1(\rho)}{\partial \xi} + \frac{D}{a} \epsilon_1(\rho) + \frac{\xi \cdot D}{a} \frac{\partial \epsilon_1(\rho)}{\partial \xi} - \frac{D}{a} \epsilon_0$$

$$= \frac{D}{a} \left[(\epsilon_1(\rho) - \epsilon_0) + (b+\xi) \frac{\partial \epsilon_1(\rho)}{\partial \xi} \right]$$

$$\frac{\partial \rho}{\partial \xi} = -\frac{\rho}{\xi} \text{ (BZ)}$$

$$\Rightarrow \frac{D}{a} \left[(\epsilon_1(\rho) - \epsilon_0) + (b+\xi) \frac{\partial \epsilon_1(\rho)}{\partial \rho} \left(-\frac{\rho}{\xi} \right) \right]$$

$$= \frac{D}{a} \left[(\epsilon_1(\rho) - \epsilon_0) - \frac{\rho}{\xi} (b+\xi) \frac{\partial \epsilon_1(\rho)}{\partial \rho} \right]$$

$$\therefore f = \frac{1}{2} v^2 \frac{D}{a} \left[(\epsilon_1(\rho) - \epsilon_0) - \frac{\rho}{\xi} (b+\xi) \frac{\partial \epsilon_1(\rho)}{\partial \rho} \right]$$

$$= a \cdot D \cdot \frac{1}{2} \bar{\epsilon} \left[(\epsilon_1(\rho) - \epsilon_0) - \frac{\rho}{\xi} (b+\xi) \frac{\partial \epsilon_1(\rho)}{\partial \rho} \right]$$