

# Chapter 10

# Heat Transfer



# Energy Balance for a Closed System

- *First Law of Thermodynamics for a closed system* (a fixed volume or space with no streams entering or leaving the system)

$$\Delta E = Q + W \quad (10.1)$$

$E$  = total energy of a system

$Q$  = heat transferred into the system  
(e.g. through the boundaries)

$W$  = work done on the system

# Energy Balance for an Open System

- Open system
  - a system with streams entering and leaving
- For a steady-state open system

$$\sum_{\substack{\text{output} \\ \text{streams}}} \left\{ \dot{m} \hat{E} \right\}_{out} - \sum_{\substack{\text{input} \\ \text{streams}}} \left\{ \dot{m} \hat{E} \right\}_{in} = \dot{Q} + \dot{W} \quad (10.2)$$

$\dot{m}$  = mass flow rate of a stream (units of mass per time)

$\hat{E}$  = energy per mass of a stream of flowing material

$\dot{Q}$  = rate of transfer of energy across the boundaries of a stream into the system (units of energy per time)

$\dot{W}$  = rate that work is done on a system (units of energy per time)

# Energy Balance for an Open System

$$\hat{E}_{total} = \hat{E}_{internal} + \hat{E}_{kinetic} + \hat{E}_{potential} = \hat{U} + \frac{1}{2}\alpha v^2 + gz \quad (10.3)$$

$$\sum_{\substack{\text{output} \\ \text{streams}}} \left\{ \dot{m} \hat{E} \right\}_{out} - \sum_{\substack{\text{input} \\ \text{streams}}} \left\{ \dot{m} \hat{E} \right\}_{in} = \dot{Q} + \dot{W} \quad (10.2)$$

$$\sum_{\substack{\text{output} \\ \text{streams}}} \dot{m} \left[ \hat{U} + \frac{1}{2}\alpha v^2 + gz \right]_{out} - \sum_{\substack{\text{input} \\ \text{streams}}} \dot{m} \left[ \hat{U} + \frac{1}{2}\alpha v^2 + gz \right]_{in} = \dot{Q} + \dot{W} \quad (10.4)$$

# Heat Transfer

- Conduction
  - through a stationary medium
  - by temperature difference
- Convection
  - through a moving medium
- Radiation
  - As electromagnetic waves
  - without a medium (even through a vacuum)
  - e.g. sun radiating its heat to the earth

# Conduction

- Fourier's Law of Heat Conduction

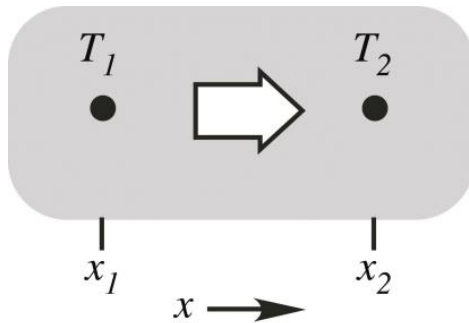


Figure 10.1  
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$$\dot{Q}_{cond,x} = -k A \frac{T_2 - T_1}{x_2 - x_1}$$

$k$  = thermal conductivity

$A$  = cross-sectional area  
through which the heat  
conducts

- cf. Fick's Law of Diffusion

$$\dot{N}_A = -D_{AB} A \frac{C_{A,2} - C_{A,1}}{x_2 - x_1}$$

# Conductivity (k)

<i>k (W/m °C) @25 °C</i>	
<i>air</i>	<i>.026</i>
<i>water</i>	<i>.61</i>
<i>glass</i>	<i>1.4</i>
<i>aluminum</i>	<i>237</i>

Which has the lowest k, gas or solid?

What are the best insulations?

Why is a double-pane window an effective thermal barrier?

# Convection

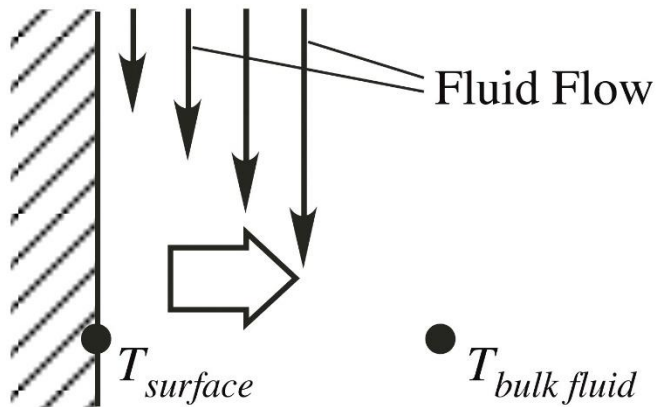


Figure 10.2  
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$$\dot{Q}_{conv} = h A (T_{surface} - T_{bulk\ fluid})$$

$h$  = heat-transfer coefficient  
(depends on geometry  
and flow)

$A$  = cross-sectional area

cf. Mass Transfer Rate:  $\dot{N}_A = h_m A (c_{A,1} - c_{A,2})$



# Radiation

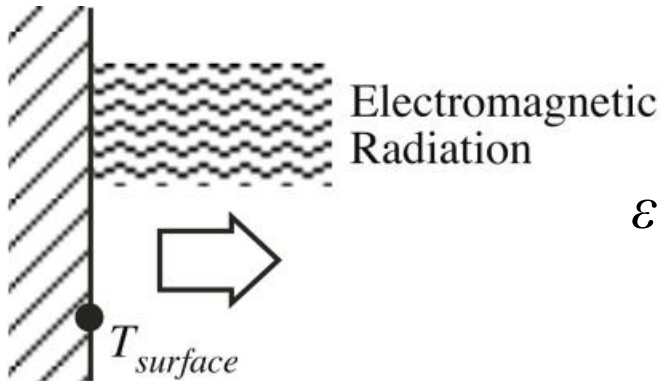


Figure 16.3  
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$$\dot{Q}_{rad} = \varepsilon \sigma A (T_{surface})^4$$

$\varepsilon$  = emissivity, which indicates how well the surface emits radiation compared with a “perfect” radiator (unit-less)

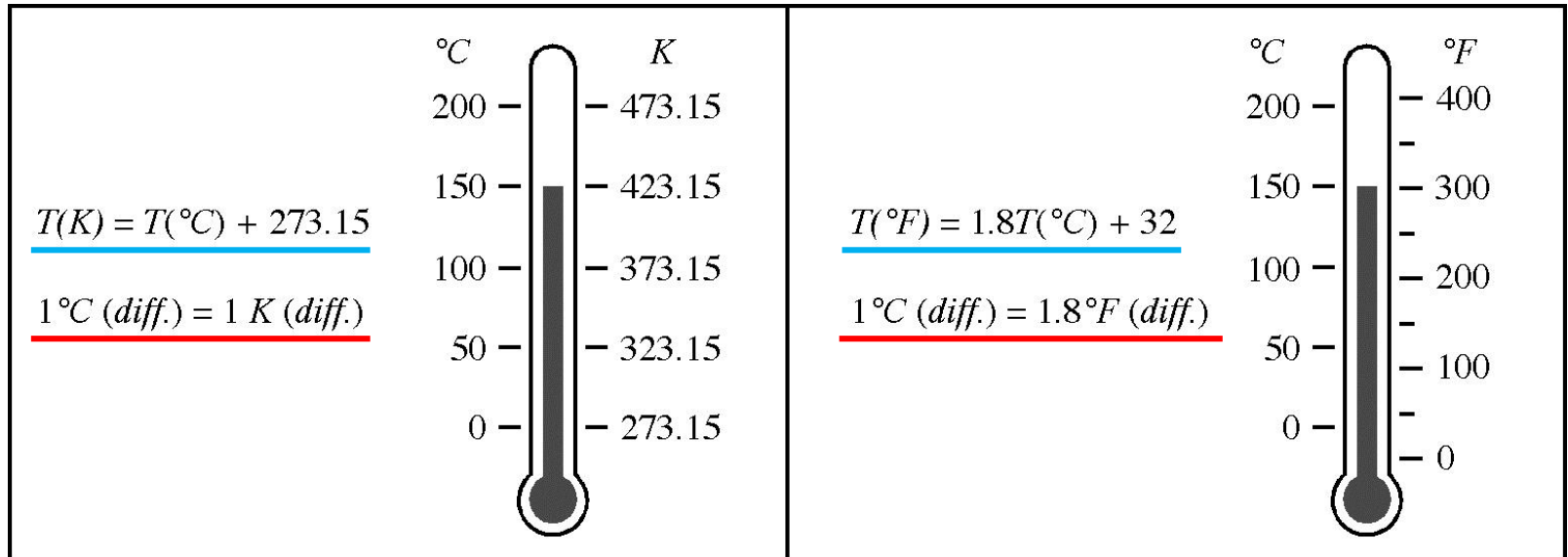
$\sigma$  = Stefan-Boltzmann constant  
( $5.67 \times 10^{-8} \text{ W} / \text{m}^2 \text{ K}^4$ )

$A$  = area of the radiating surface

$T$  = absolute surface temperature (K)

$$\dot{Q}_{rad,net} = \varepsilon_1 \sigma A_1 (T_{surface,1})^4 - \varepsilon_2 \sigma A_2 (T_{surface,2})^4$$

# Temperature & Temp. Difference



Ex. 10.1. A typical value for the thermal conductivity of steel is  $53 \text{ W/m K}$ . What is the corresponding value in unit of  $\text{Btu/hr ft } ^{\circ}\text{F}$ ?

$\Delta T$

# Rate of Work

- Rate of shaft work ( $\dot{W}_s$ )
  - Energy per time
  - Positive when work is done on the system (such as in a pump, “push” the fluid)
  - Negative when work is done by the fluid (such as in turbine)
- Rate of flow work ( $\dot{W}_{PV}$ )
  - Work resulting from the displacement of fluid during flow
  - Similar to the pressure-volume work associated with the compression or expansion of a closed system

# Energy Balance

$$\dot{W}_{PV} = \sum_{\substack{\text{input} \\ \text{streams}}} (P\dot{V})_{in} - \sum_{\substack{\text{output} \\ \text{streams}}} (P\dot{V})_{out} = \sum_{\substack{\text{input} \\ \text{streams}}} (\dot{m}P\hat{V})_{in} - \sum_{\substack{\text{output} \\ \text{streams}}} (\dot{m}P\hat{V})_{out} \quad (10.8)$$

$$\dot{W} = \dot{W}_s + \dot{W}_{PV} \quad (10.9)$$

$$\sum_{\substack{\text{output} \\ \text{streams}}} \dot{m} \left[ \hat{U} + \frac{1}{2} \alpha v^2 + gz \right]_{out} - \sum_{\substack{\text{input} \\ \text{streams}}} \dot{m} \left[ \hat{U} + \frac{1}{2} \alpha v^2 + gz \right]_{in} = \dot{Q} + \dot{W} \quad (10.4)$$

$$\sum_{\substack{\text{output} \\ \text{streams}}} \left\{ \dot{m} \left[ \hat{U} + \frac{1}{2} \alpha v^2 + gz \right] \right\}_{out} - \sum_{\substack{\text{input} \\ \text{streams}}} \left\{ \dot{m} \left[ \hat{U} + \frac{1}{2} \alpha v^2 + gz \right] \right\}_{in} = \dot{Q} + \dot{W}_s + \dot{W}_{PV} \quad (10.10)$$

# Energy Balance

$$\sum_{\substack{\text{output} \\ \text{streams}}} \left\{ \dot{m} \left[ \hat{U} + P\hat{V} + \frac{1}{2}\alpha v^2 + gz \right] \right\}_{out} - \sum_{\substack{\text{input} \\ \text{streams}}} \left\{ \dot{m} \left[ \hat{U} + P\hat{V} + \frac{1}{2}\alpha v^2 + gz \right] \right\}_{in} = \dot{Q} + \dot{W}_s \quad (10.11)$$

Compare Eq. 10.11 with mechanical energy balance.

$$\left( \frac{P}{\rho} + \frac{1}{2}\alpha v_{ave}^2 + gz \right)_{out} - \left( \frac{P}{\rho} + \frac{1}{2}\alpha v_{ave}^2 + gz \right)_{in} = w_s - w_f \quad (7.8a)$$

# Energy Balance

$$\hat{H} = \hat{U} + P\hat{V} \quad (10.12)$$

Most common form of the steady-state open-system energy balance.

$$\sum_{\text{output streams}} \left\{ \dot{m} \left[ \hat{H} + \frac{1}{2} \alpha v^2 + gz \right] \right\}_{out} - \sum_{\text{input streams}} \left\{ \dot{m} \left[ \hat{H} + \frac{1}{2} \alpha v^2 + gz \right] \right\}_{in} = \dot{Q} + \dot{W}_s$$

$$(10.13)$$

# Energy Balance

Steady-state energy balance  
with negligible change in kinetic and potential energies  
and with no shaft work

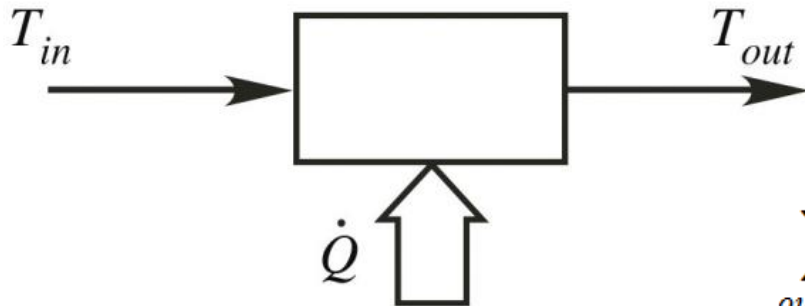
$$\sum_{\text{output streams}} \left\{ \dot{m} \left[ \hat{H} + \frac{1}{2} \alpha v^2 + gz \right] \right\}_{\text{out}} - \sum_{\text{input streams}} \left\{ \dot{m} \left[ \hat{H} + \frac{1}{2} \alpha v^2 + gz \right] \right\}_{\text{in}} = \dot{Q} + \dot{W}_s$$

(10.13)

$$\sum_{\text{output streams}} (\dot{m} \hat{H})_{\text{out}} - \sum_{\text{input streams}} (\dot{m} \hat{H})_{\text{in}} = \dot{Q}$$

(10.14)

# Energy Balance



$$\sum_{\text{output streams}} (\dot{m} \hat{H})_{out} - \sum_{\text{input streams}} (\dot{m} \hat{H})_{in} = \dot{Q} \quad (10.14)$$

Figure 10.5  
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(i) **Sensible Heating/Cooling:**  $\sum_{out} \dot{m} \bar{C}_p (T - T_{ref}) - \sum_{in} \dot{m} \bar{C}_p (T - T_{ref}) = \dot{Q}$   
 $T_{out} > T_{in}$  (No phase change) (10.16)

(ii) **Phase Change:**  $\dot{m}_{\text{phase change}} \Delta \hat{H}_{\text{phase change}} = \dot{Q}$   
 $T_{out} = T_{in}$  (Phase change) (10.18)

(iii) **Chemical Reaction:**  $r_{\text{consumption},A} \Delta \tilde{H}_{\text{reaction},A} = \dot{Q}$   
 $T_{out} = T_{in}$  (10.20)



# Heat-Exchangers

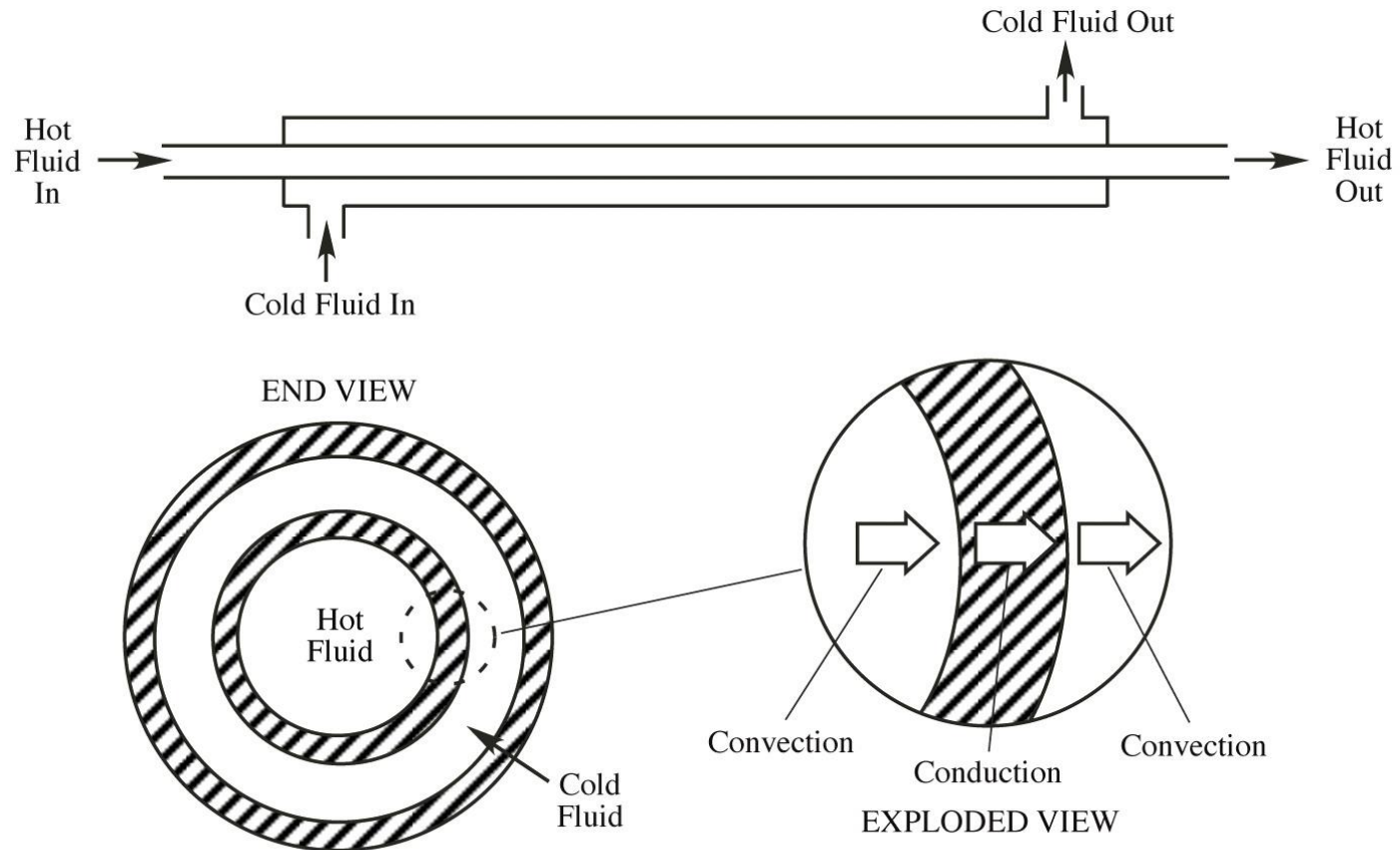


Figure 10.10  
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## Concentric-Cylinder Heat Exchanger

# Heat-Exchangers

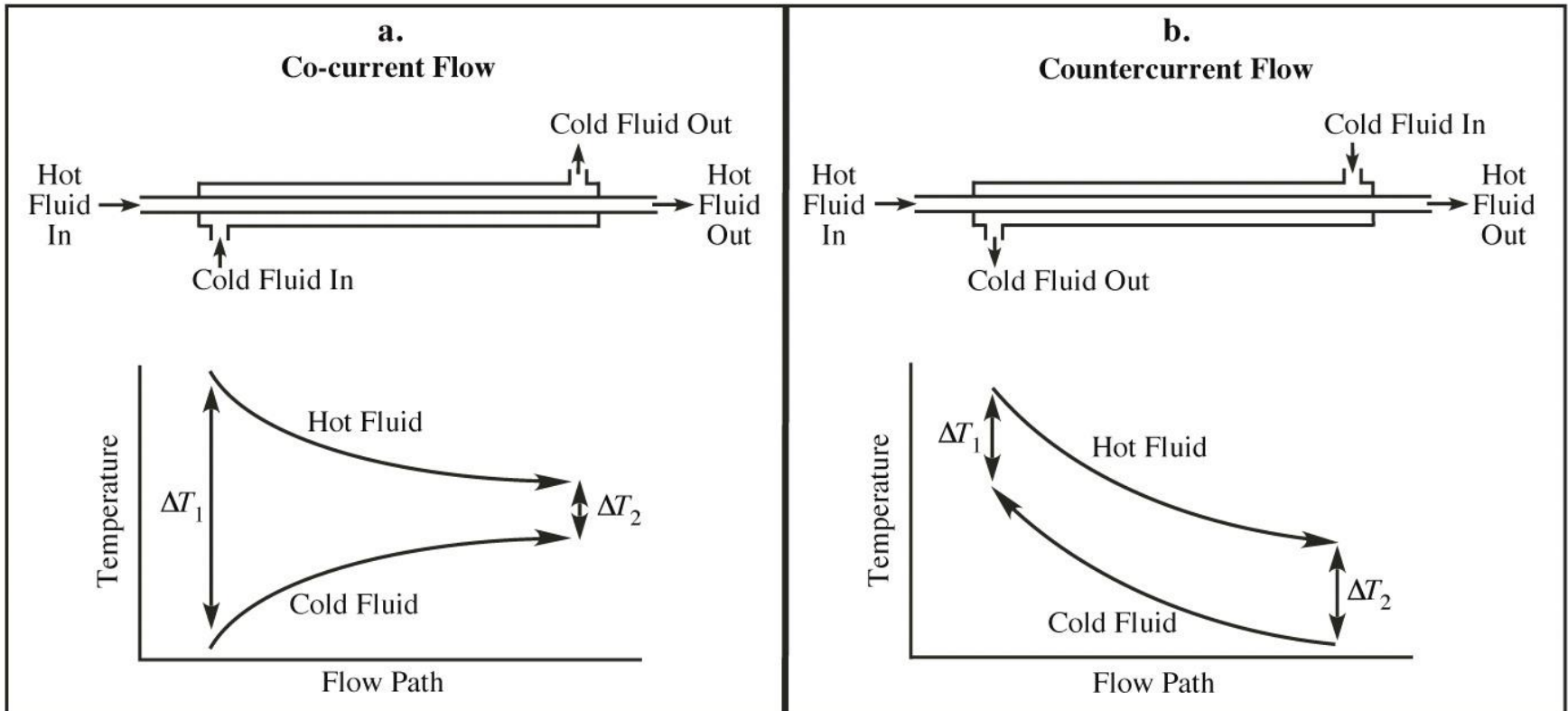


Figure 10.11

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# Heat-Exchangers

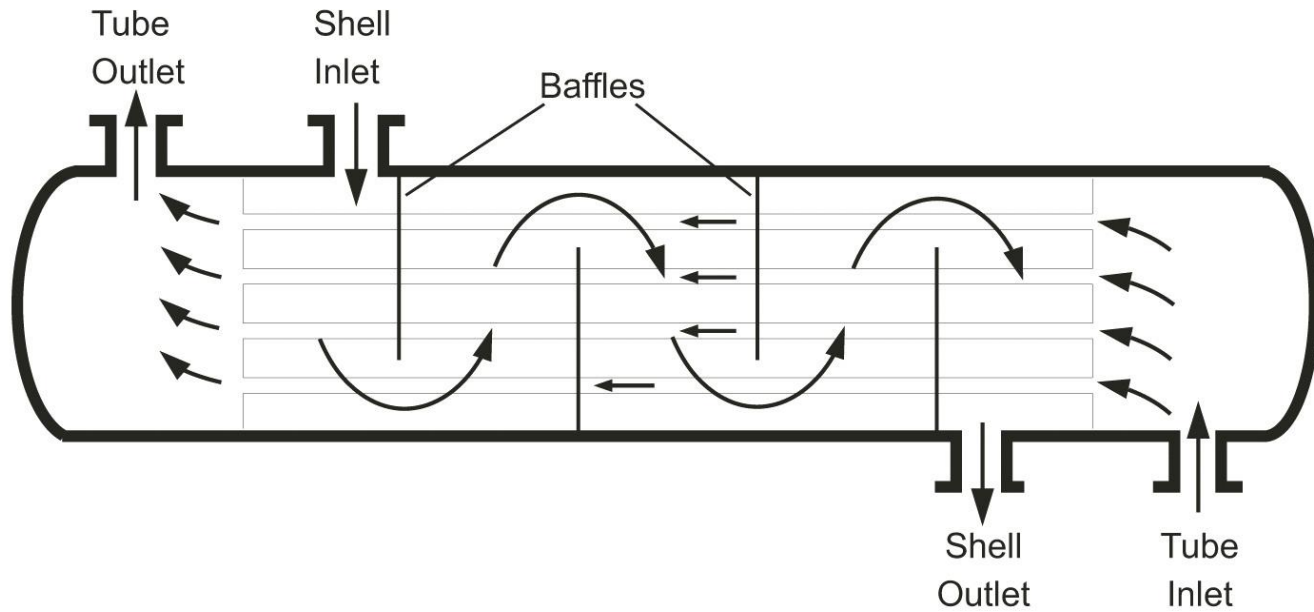


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## Shell-and-Tube Heat Exchanger

# Heat-Exchangers

(i) Sensible Heating/Cooling:

$$\left[ \dot{m} C_p (T_{out} - T_{in}) \right]_{hot} = -\dot{Q}_{duty} \quad (10.24a)$$

$$\left[ \dot{m} C_p (T_{out} - T_{in}) \right]_{cold} = \dot{Q}_{duty} \quad (10.24b)$$

(ii) Phase Change:

$$\left[ \dot{m} \Delta \hat{H}_{phase\ change} \right]_{hot} = -\dot{Q}_{duty} \quad (10.24c)$$

$$\left[ \dot{m} \Delta \hat{H}_{phase\ change} \right]_{cold} = \dot{Q}_{duty} \quad (10.24d)$$

(iii) Chemical Reaction:

$$\left[ r_{consumption,A} \Delta \tilde{H}_{reaction,A} \right]_{hot} = -\dot{Q}_{duty} \quad (10.24e)$$

$$\left[ r_{consumption,A} \Delta \tilde{H}_{reaction,A} \right]_{cold} = \dot{Q}_{duty} \quad (10.24f)$$

# Heat-Exchangers

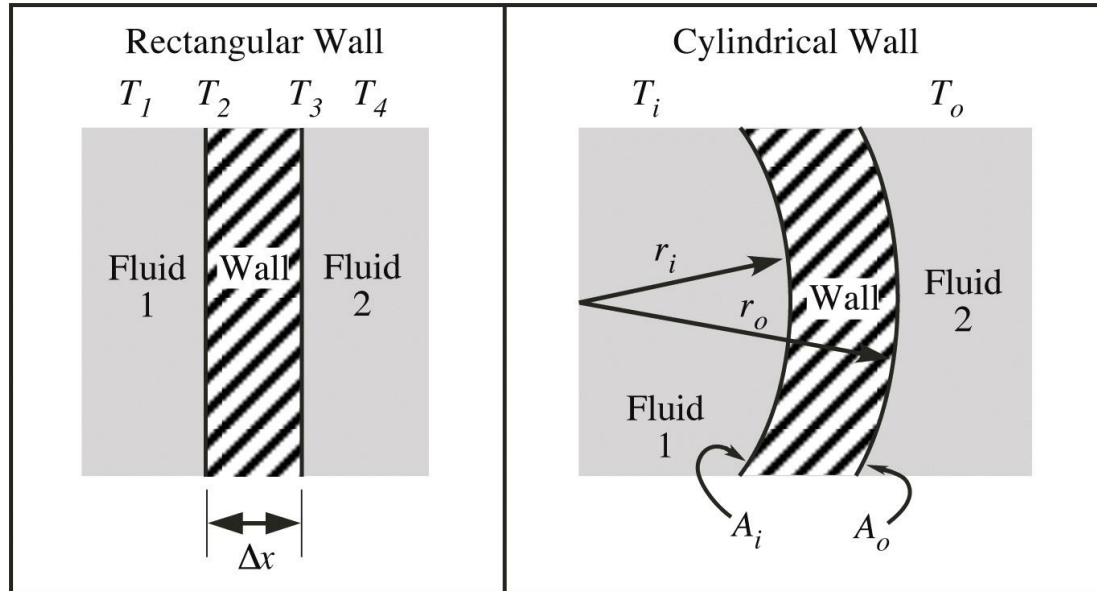


Figure 10.15  
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$$\dot{Q} = h_1 A (T_1 - T_2) = kA \frac{T_2 - T_3}{\Delta x} = h_2 A (T_3 - T_4) \quad (10.25)$$

# Homework

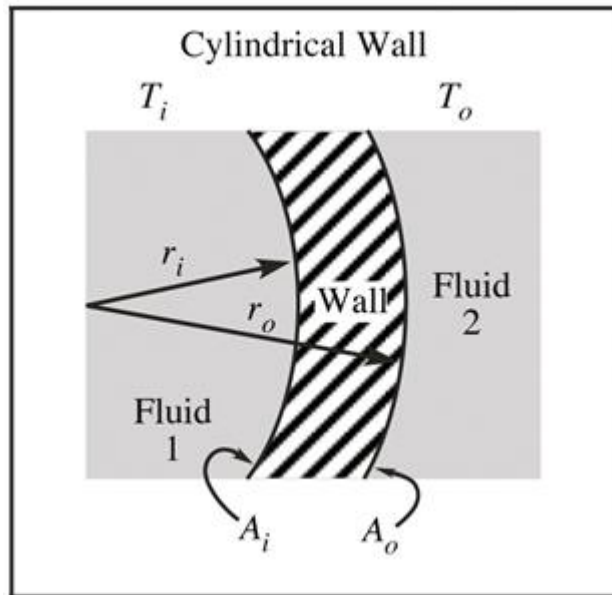
- Derive following equations.

$$\dot{Q} = \frac{T_1 - T_4}{\frac{1}{h_1 A} + \frac{\Delta x}{kA} + \frac{1}{h_2 A}} \quad (10.26)$$

$$\dot{Q} = \frac{T_i - T_o}{\frac{1}{h_i A_i} + \frac{\ln(r_o / r_i)}{2\pi kL} + \frac{1}{h_o A_o}} \quad (10.27)$$

# Heat-Exchangers

- $T_i$  and  $T_o$  change along the length of the device.
- The prediction of the values of  $h_i$  and  $h_o$  is complex.



$$\dot{Q}_{duty} = U_o A \Delta T_{ave} \quad (10.28)$$

$U_o$  : overall heat transfer coefficient

$$\Delta T_{\log mean} = \frac{\Delta T_1 - \Delta T_2}{\ln \frac{\Delta T_1}{\Delta T_2}} \quad (10.29)$$

log mean temperature difference