Lecture Notes 414.341

선박해양유체역학

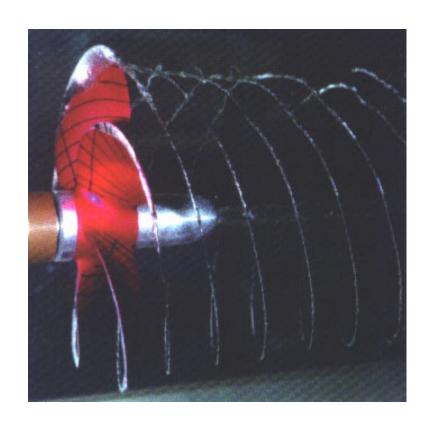
MARINE HYDRODYNAMICS

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선박해양유체역학 MARINE HYDRODYNAMICS



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Contents

0. OUTLINE OF COURSE	1
0.1 Course Description	1
0.2 References	2
0.3 Course Contents	2
1. INTRODUCTION	5
1.1 Continuum Mechanics	6
1.1.1 Definition of Fluid	6
1.1.2 Assumptions and Axioms	7
1.1.3 Basic Equations	10
1.2 Characteristics of Hydrodynamics	12
1.2.1 Types of Fluid Flow	12
1.2.2 Various Characteristic Effects	14
1.2.3 Characteristics of Ship/Marine Hydrodynamics	14
1.2.4 Ocean Environment	16
1.3 Mathematical Prerequisites: Vector Analysis	24
1.3.1 Fundamental Function Analysis	24
1.3.2 Vector Calculus	25
1.3.3 Expansion Formulas	30
1.3.4 Divergence Theorem (Gauss Theorem)	31

ii Contents

1.3.5 Stokes' Theorem	 32
1.3.6 Dyadic Products	 33
1.3.7 Reynolds Transport Theorem	 34
1.3.7.1 Example of the Reynolds transport theorem in 1-D	 35
1.3.8 Moving Coordinate Systems	 37
2. MODEL TESTING	39
2.1 Introduction	 41
2.1.1 Dimensional Analysis	 41
2.1.2 Flow Similarity and Model Studies	 42
2.1.3 Nature of Dimensional Analysis: Example	 43
2.1.4 Significant Dimensionless Numbers	 44
2.1.5 Error Estimates in Uncertainty Analysis	 45
2.1.6 Flow Visualization	 45
2.2 Drag Force on a Sphere	 46
2.2.1 Dimensional Analysis	 46
2.2.2 Pressure Drag Variation with Reynolds Numbers	 48
2.3 Viscous Drag on a Flat Plate	 50
2.3.1 Dimensional Analysis for Frictional Drag	 50
2.3.2 Transition Range of Reynolds Numbers	 52
2.4 Viscous Drag on General Bodies	 54
2.4.1 Infeasible Tests of Geosims	 54
2.4.2 Frictional Drag and Pressure Drag	 54
2.5 Hydrofoil Lift and Drag	 58
2.5.1 Lifting Surfaces	 58
2.5.2 Lift and Drag on Hydrofoil	 61
2.5.3 Remarks: Induced Drag for 3-D Lifting Surfaces	 63

<u>Contents</u> iii

2.6 Screw Propeller	63
2.7 Drag on a Ship Hull	71
2.8 Propeller-Hull Interactions	77
2.8.1 Propeller and Ship Powering	80
2.9 Unsteady Force on an Accelerating Body	85
2.9.1 Added Mass	87
2.10 Vortex Shedding	87
2.11 Water Waves	93
2.11.1 Dispersion Relation of a Progressive Wave in Infinite Depth	93
2.11.2 Secondary Effects: Viscosity, Air, Surface tension, Nonlinear Effects	96
2.11.3 Solutions for Finite Depth	100
2.11.4 Shallow Water Limit	101
2.11.5 Superposition of Waves: Group Velocity	106
2.11.6 Wave Force on a Stationary Body	108
2.11.7 Body Motions in Waves	110
2.11.8 Ship Motions in Waves	111
3. KINEMATICS	115
3.1 Description of Fluid Motion	116
3.1.1 Definition of Fluid Particle	116
3.1.2 Lagrangian Description: Path Lines	116
3.1.3 Eulerian Description	117
3.1.3.1 Local derivative	117
3.1.3.2 Material derivative	118
3.1.4 Particle Tracing Lines	119
3.1.4.1 Streamlines	119
3.1.4.2 Streaklines	120

iv Contents

3.1.5 Example of Particle Tracing Lines	120
3.1.5.1 Velocity field	120
3.1.5.2 Pathlines	121
3.1.5.3 Streamlines	122
3.1.5.4 Streaklines	123
3.2 Conservation of Mass: Continuity Equation	124
3.2.1 Material Volume Approach	124
3.2.2 Control Volume Approach	125
3.2.3 Special Cases: Steady Motion and Incompressible Flow	128
3.3 Vorticity and Circulation	129
3.3.1 Definition of Vorticity	129
3.3.2 Vortex Line and Vortex Tube	130
3.3.3 Circulation and Vorticity Flux	131
2.2.4.77 (0) (1	
3.3.4 Vortex Strength	132
	132 135
	135
4. DYNAMICS	135 136
4. DYNAMICS 4.1 Forces	135 136 136
4. DYNAMICS 1 4.1 Forces 1 4.1.1 Body Forces 1	135 136 136 137
4. DYNAMICS 1 4.1 Forces 1 4.1.1 Body Forces 1 4.1.2 Surface Forces 1	135 136 136 137
4. DYNAMICS 1 4.1 Forces 1 4.1.1 Body Forces 1 4.1.2 Surface Forces 1 4.1.3 Stress and Stress Tensor 1	136 136 137 138
4. DYNAMICS 1 4.1 Forces 1 4.1.1 Body Forces 1 4.1.2 Surface Forces 1 4.1.3 Stress and Stress Tensor 1 4.1.4 Surface Tension 1	135 136 136 137 138 139
4. DYNAMICS 1 4.1 Forces 1 4.1.1 Body Forces 1 4.1.2 Surface Forces 1 4.1.3 Stress and Stress Tensor 1 4.1.4 Surface Tension 1 4.2 Equations of Motion: Navier-Stokes Equations 1	135 136 137 138 139 141
4. DYNAMICS 1 4.1 Forces 1 4.1.1 Body Forces 1 4.1.2 Surface Forces 1 4.1.3 Stress and Stress Tensor 1 4.1.4 Surface Tension 1 4.2 Equations of Motion: Navier-Stokes Equations 1 4.2.1 Newton's Second Law for Material Volume 1	135 136 136 137 138 139 141 141
4. DYNAMICS 1 4.1 Forces 1 4.1.1 Body Forces 1 4.1.2 Surface Forces 1 4.1.3 Stress and Stress Tensor 1 4.1.4 Surface Tension 1 4.2 Equations of Motion: Navier-Stokes Equations 1 4.2.1 Newton's Second Law for Material Volume 1 4.2.2 Surface Forces for Differential Control Volume 1	135 136 136 137 138 139 141 141 142

<u>Contents</u> v

	4.2.5 Navier-Stokes Equations in a Moving Frame	150
	4.2.5.1 Kinematic description	150
	4.2.5.2 Representation of velocity field	151
	4.2.5.3 Governing equations	152
	4.2.6 Boundary Conditions	153
4.3	Example: Low Reynolds Number Flows	153
	4.3.1 Velocity Field: Solution of the Simplified Navier-Stokes Equations	154
	4.3.2 Stress Tensor and Drag	157
4.4	Simple Problems for Viscous Flows	158
	4.4.1 Flow between Two Parallel Walls (Plane Couette Flow)	158
	4.4.2 Flow through a Pipe(Poiseuille Flow)	160
	4.4.3 External Flow Past One Flat Plate: Unsteady Motion of a Flat Plate	160
	4.4.3.1 Stokes 1st problem	161
	4.4.3.2 Stokes 2nd problem	162
4.5	Boundary Layer Theory	164
	4.5.1 Introduction	164
	4.5.2 Laminar Boundary Layer: Flat Plate	165
	4.5.3 Laminar Boundary Layer: Steady 2-D Flow	171
	4.5.3.1 Von Karman integral relation	174
	4.5.3.2 Laminar boundary layers: Closing remarks	175
4.6	Turbulent Flows: General Aspects	17 6
	4.6.1 Introduction	176
	4.6.2 Analysis of Turbulent Flows	178
	4.6.3 Turbulent Boundary Layer on a Flat Plate	181
	4.6.4 Turbulent Boundary Layers: Closing Remarks	187

vi Contents

5. POTENTIAL FLOWS	195
5.1 Euler Equations for Inviscid Flows	196
5.1.1 General Aspects	196
5.1.2 Conservation of Circulation: Kelvin's Theorem	199
5.1.2.1 Inroduction	199
5.1.2.2 Time rate of circulation for barotropic fluids	199
5.1.2.3 Case of inviscid flows	201
5.1.2.4 Another derivation of Kelvin's theorem	202
5.1.2.5 Circulation generation: Kutta condition	203
5.1.3 Irrotational Flow and Velocity Potential	204
5.2 Energy Equation: Bernoulli Equation	205
5.2.1 Integration of Euler Equations for Inviscid Fluids	205
5.2.2 Case 1: Inviscid Steady (possibly Rotational) Incompressib along Streamline	
5.2.2.1 Steady barotropic flows	207
5.2.3 Case 2: Inviscid Unsteady Irrotational Incompressible Flow	209
5.2.3.1 Irrotational barotropic flows	209
5.3 Boundary Conditions	210
5.3.1 Kinematic Boundary Condition	210
5.3.1.1 Alternate form	211
5.3.2 Dynamic Boundary Condition: Free Surface Condition	212
5.4 Simple Potential Flows	213
5.4.1 Irrotational Inviscid Flows: Potential Flows	213
5.4.1.1 Uniqueness of Laplace equation	215
5.4.2 Techniques for Solving the Laplace Equation	215
5.4.3 Source/Sink/Dipole/Vortex in Free Stream (Uniform Flow)	216
5.4.3.1 Flow past a sphere	220

<u>Contents</u> vii

	5.4.4 Flow around a Circular Cylinder	221
	5.4.4.1 Circular cylinder with circulation	222
	5.5 Stream Function	223
	5.5.1 Various Singularity and Simple Potential Flows	225
	5.6 Separation of Variables	227
	5.6.1 Fixed Bodies and Moving Bodies	230
	5.7 Method of Images	231
	5.8 Green's Theorem and Distributions of Singularities	236
	5.8.1 Scalar Identity	236
	5.9 Hydrodynamics Pressure Forces: Forces and Moments Acting on a Body	239
	5.10 Force on a Moving Body in an Unbounded Fluid	242
	5.10.1 Far-field Behavior of Velocity Potential	242
	5.10.2 Decomposition of Velocity Potential: 6 Degrees of Freedom	243
	5.11 Added Mass	245
	5.11.1 General Properties of Added-Mass Coefficients	246
	5.11.2 Added Mass of Simple Forms	249
	5.12 Body-Mass Force: Equations of Motion	251
A.	VECTOR ANALYSIS	255
	A.1 Introduction	257
	A.1.1 Vector and Tensor Notation	257
	A.1.2 Fundamental Function Analysis	258
	A.2 Vector Calculus	260
	A.2.1 Definition of Vector Quantity	260
	A.2.2 Basic Unit Tensors	263
	A.2.2.1 Kronecker delta tensor	263
	A.2.2.2 Permutation tensor	263
	A.2.2.3 Multiplication of basic tensors	264
	A.2.2.4 Example of permutation tensor	265

viii Contents

A.2.3 Multiplication of Vectors	O
A.2.4 Vector Derivatives	7
A.2.4.1 Gradient	7
A.2.4.2 Divergence	8
A.2.4.3 Curl	9
A.2.4.4 Laplacian	9
A.2.4.5 Differential operators	0
A.2.4.6 Directed derivative	0
A.2.5 Expansion Formulas	1
Integral Theorems	2
A.3.1 Divergence Theorem	2
A.3.2 Stokes' Theorem	4
A.3.3 Volume Integrals of a Vector	6
Curvilinear Orthogonal Coordinates	8
A.4.1 Line element	8
A.4.2 Gradient	0
A.4.2 Gradient	
	1
A.4.3 Divergence	1
A.4.3 Divergence	1 1 2
A.4.3 Divergence	1 1 2 3
A.4.3 Divergence 28 A.4.4 Curl. 28 A.4.5 Laplacian 28 A.4.6 Convection term 28	1 1 2 3
A.4.3 Divergence 28 A.4.4 Curl. 28 A.4.5 Laplacian 28 A.4.6 Convection term 28 Tensors of Second Order 28	1 1 2 3 4
A.4.3 Divergence 28 A.4.4 Curl. 28 A.4.5 Laplacian 28 A.4.6 Convection term 28 Tensors of Second Order 28 A.5.1 Dyadic Products 28	1 1 2 3 4 5
A.4.3 Divergence 28 A.4.4 Curl. 28 A.4.5 Laplacian 28 A.4.6 Convection term 28 Tensors of Second Order 28 A.5.1 Dyadic Products 28 A.5.2 Gradient of a Vector 28	1 1 2 3 4 5
	A.2.4 Vector Derivatives 26 A.2.4.1 Gradient 26 A.2.4.2 Divergence 26 A.2.4.3 Curl 26 A.2.4.4 Laplacian 26 A.2.4.5 Differential operators 27 A.2.4.6 Directed derivative 27 A.2.5 Expansion Formulas 27 Integral Theorems 27 A.3.1 Divergence Theorem 27 A.3.2 Stokes' Theorem 27 A.3.3 Volume Integrals of a Vector 27 Curvilinear Orthogonal Coordinates 27 A.4.1 Line element 27

<u>Contents</u> ix

A.7	Moving Coordinate Systems	291
	A.7.1 Velocity due to Rigid Body Rotation	291
	A.7.2 Transformations of Moving Coordinates	293
A.8	Mathematical Identities	295
	A.8.1 Green's Scalar Identity	295
	A.8.2 Uniqueness of Scalar Identity	298
	A.8.3 Type of Boundary Conditions	299
	A.8.4 Vector Identity	301
	A.8.5 Integral Expression of Helmholtz Decomposition	305
	A.8.6 Uniqueness of Vector Identity	307
	A.8.7 Improper Integrals	308
	A 8 8 Green Functions	310

List of Figures

1.1	Behavior of a solid and a fluid, under the action of constant shear force	6
1.2	Definition of density	8
1.3	Measured data to define density with variation of length scale	9
1.4	Possible classification of fluid mechanics	13
1.5	Schematic diagram of various types of fluid flow	13
1.6	Variation of density with salinity and temperature at atmospheric pressure	17
1.7	Typical variation od depth versus density for different global latitudes	19
1.8	Variation of surface temperature, salinity and density with latitude–average for all oceans	20
1.9	Typical viscous velocity gradient	21
1.10	Molecular explanation of surface tension	22
1.1	1 Sequential change of the interval of the integral (1.106)	35
1.12	2 Moving coordinate system	38
2.1	The drag coefficient of a sphere	44
2.2	Definition of bias and precision error	45
2.3	Probability error estimates	46
2.4	Typical PIV system for cavitation tunnel	47
2.5	The drag coefficient of a sphere	48
2.6	The drag coefficient of a sphere for moderate Reynolds number	49
2.7	Wake of a sphere for moderate Reynolds number	49

xii List of Figures

2.8	The drag coefficient of a sphere at critical Reynolds number	50
2.9	Wake of a sphere at critical Reynolds number	51
2.10	Wake of a sphere at critical Reynolds number	51
2.11	Schoenherr's flat-plate frictional drag coefficient	52
2.12	Transition from laminar to turbulent flow for a flat plate drag coefficient	53
2.13	Flow over a flat plate normal to inflow	55
2.14	Drag coefficient for two-dimensional cylinders	56
2.15	Drag on a strut: Contributions of frictional drag and pressure drag to total drag as a function of thickness-length ratio	56
2.16	Drag coefficient for a circular cylinder	57
2.17	Drag coefficient for a sphere.	57
2.18	Three-dimensional lifting surface	58
2.19	Geometry of a hydrofoil section	59
2.20	Flow past a hydrofoil section	60
2.21	Flow past a foil without circulation	60
2.22	Assumed flow past a foil with circulation	60
2.23	Lift coefficient for a two-dimensional hydrofoil	61
2.24	Lift characteristics of hydrofoils	62
2.25	Drag coefficient for a two-dimensional hydrofoil	64
2.26	Trailing vortex system of a wing	65
2.27	Downwash distribution for trailing vortex system on a wing	65
2.28	Derivation of induced drag on a wing	66
2.29	Propeller coordinate system	67
2.30	Propeller blade geometry in 3 coordinate systems	68
2.31	Perspective view of a propeller and its shaft	69
2.32	2 2-D view of a propeller blade section	70
2.33	Experimental setup for propeller open water test in towing tank	70

List of Figures xiii

2.34	Components of a typical marine propulsion system	71
2.35	Decomposition of ship resistance	72
2.36	Components of ship resistance	72
2.37	Froude's hypothesis for prediction of resistance of a full-scale ship	73
2.38	Calculation of model and full scale frictional drag coefficients	74
2.39	Total drag coefficients of geosim models	75
2.40	Total drag coefficients of geosim models: Validation check on Froude hypothesis	76
2.41	Total drag coefficients of geosim models: Viscous form drag	77
2.42	Frictional drag coefficients	78
2.43	Total drag coefficients of geosim models: Larger models effect	79
2.44	Extrapolation using form factor k	79
2.45	Schematic diagram of propeller-hull interaction	80
2.46	Thrust identity condition between open-water propeller test and self-propulsion test	81
2.47	Components of a typical marine propulsion system	81
2.48	Schematic diagram of propeller and ship powering	82
2.49	Transmission efficiency of mechanical drives and electric drives	83
	Development of unsteady flows about an impulsively started circular cylinder	86
2.51	Force coefficient for an impulsively started circular cylinder	88
2.52	Karman vortex street	88
2.53	Karman vortex street in nature	89
2.54	Lateral lift force and shedding frequency	89
2.55	Strouhal number for a circular cylinder at low Reynolds numbers	90
2.56	Drag coefficient and Strouhal number for a circular cylinder at moderate and high Reynolds numbers	91
2.57	Lock-in phenomena between the lateral lift force and vortex-shedding frequency	91

xiv List of Figures

2.58	Example of VIV(Vortex Induced Vibration) phenomena: Collapse of the Tacoma bridge
2.59	Sketch of a periodic progressive wave in a fluid of mean depth h
2.60	Velocity field of a plane progressive wave in deep water
2.61	Surface tension for two stationary fluids in 2-dimensions
2.62	Surface tension for a stationary spherical bubble
2.63	The "steepest wave" profile of nonlinear waves
2.64	Velocity field of a plane progressive wave in finite depth
2.65	Particle trajectories of a plane progressive wave in finite depth 102
2.66	Phase velocity, wave length, and depth ratios of a plane progressive wave in finite depth
2.67	Propagation of plane progressive waves into shallow water
2.68	Propagation of the Indian Ocean Tsunami of 26 December 2004 105
2.69	Wave group resulting from the superposition of two nearly equal plane waves
2.70	Phase velocity and group velocity ratios for a plane progressive wave as a function of the water depth
2.71	Sequence of photograpghs showing the phase velocity and the group velocity for a plane progressive wave system advancing into calm water 107
2.72	Heave response of slender spar buoy in regular waves
2.73	Ship motions in 6 degrees of freedom
2.74	Roll and pitch response of a 319 m ship
3.1	Example of various flow lines
3.2	Material surface of interface between two fluids
3.3	Differential control volume in Cartesian coordinates
3.4	Differential control volume in cylindrical coordinates
	Viscous shearing and vorticity generation by no-slip boundary condition at wall boundary

List of Figures xv

3.6	Line and surface integrals for Stokes'theorem	131
3.7	Circulation about a vortex tube	132
3.8	Vortex filament approximation of a vortex tube	133
11	Street Association Contaction and Instance	120
4.1	Stress tensor in Cartesian coordinates	138
4.2	Stress vector at surface	138
4.3	Force diagram for a spherical bubble with surface tension	140
4.4	Stresses in the <i>x</i> -direction on a differential control volume in Cartesian coordinates	142
4.5	Motion of a fluid particle	143
4.6	Deformation of fluid element in 2-D flows	144
4.7	Rotational motion of a fluid particle	144
4.8	Squeeze motion of a fluid particle	145
4.9	Pressure diagram of a fluid	146
4.10	O Stress and strain for simple shear flow of a Newtonian fluid	148
4.1 1	1 Moving coordinate system	150
4.12	Notation for low Reynolds number flow about a spherical body in uniform flow	154
4.13	3 Viscous flow around a foil	158
4.14	4 Plane Couette flow between two parallel walls	159
4.15	5 Stokes 1st problem: Sinusoidal motion of flat plate	162
4.16	6 Velocity profile near an impulsively started flat plate (Stokes 2nd problem).	163
4.17	7 Boundary layer thickness in Stokes 2nd problem for an impulsively started flat plate	164
4.18	8 Variation of boundary layer thickness with Reynolds numbers	165
4.19	9 Boundary layer on a flat plate	166
4.20	Velocity profile in a Blasius laminar boundary layer	168
4.21	1 Boundary layer thickness definition	169

xvi List of Figures

4.22	Development of laminar boundary layer along a flat plate 169
4.23	Flat-plate frictional resistance coefficient: Blasius laminar boundary layer solution
4.24	Laminar boundary layer: Steady 2-D flow
4.25	Boundary layer flow with pressure gradient
4.26	Flow past a body with separation
4.27	Boundary layer equations with pressure gradient
4.28	Velocity profiles and growth of the boundary layer near the leading edge of a foil
4.29	Attached and separated flows about a foil
4.30	Flow visualization of laminar, transition and turbulent flows in pipe 177
4.31	Decomposition of turbulent quantities into an average and a fluctuating part. 179
4.32	Comparison of laminar and mean turbulent velocity profiles
4.33	Mean velocity profile of turbulent flow close to a smooth wall 184
4.34	Logarithmic form of the velocity defect law for a turbulent boundary layer of a smooth wall
4.35	Boundary layers of turbulent flows with wall regions
4.36	Schoenherr's flat plate frictional resistance coefficient (ATTC line) 186
4.37	Eddy Structure of turbulent boundary layers near a flat plate 188
4.38	Turbulent viscous flows generated on body surface
4.39	Comparison of laminar and turbulent separation on a body surface 189
4.40	Flow over sphere: Effect of Reynolds number
4.41	Modification of boundary layer flows
4.42	Control of flow separation on a sphere by turbulence stimulator 191
4.43	Examples of simulation by CFD
4.44	Examples of flow over bodies
4.45	Examples of coupled solid-fluid interaction
4.46	Pattern of the turbulent kinetic energy spectrum

List of Figures xvii

4.47	Measurements of turbulent flows
5.1	Schematic view of the Hele-Shaw flow for visualization of inviscid potential flow
5.2	Initial development of the circulatory flow past a hydrofoil by Kutta condition
5.3	Open and closed line integrals in region of an irrational flow: Path independent integrals of velocity potential
5.4	Semi-infinite half-body generated by a point source at the origin in free stream
5.5	Rankine ovoid generated by a point source and sink combination in free stream
5.6	Schematic concept of dipole singularity by approach of source and sink 219
5.7	Spherical coordinate system for showing the flow about a sphere
5.8	Pressure distribution over the surface of a sphere
5.9	Measure of flux across a contour: Stream function
5.10	Streamlines about a Rankine ovoid
5.11	Streamlines about a ship forebody
5.12	2 Method of images: Source above a wall
5.1 3	Method of images: Circular cylinder above a wall
5.1 4	Method of images: Vortex above a wall
5.15	Method of images: Circular cylinder and vortex inside an L-corner 234
5.16	Method of images: Circular cylinder in two parallel walls
5.17	Surfaces of integration for Green's theorem
5.18	Fixed control surface S_C surrounding the moving body surface S_B
5.19	Position vectors in inertial coordinate system fixed in space and moving system fixed in a body
5.20	Approximation of added mass for a square by using the inscribed circle and the circumscribed circle
5.21	Added mass for a spheroid or an ellipsoid of revolution

xviii List of Figures

A.1 Two Cartesian coordinate systems rotated with respect to one another	261
A.2 Cylindrical and spherical coordinate systems	279
A.3 Change of material volume in transport of physical quantity	290
A.4 Rotation of a rigid body	292
A.5 Moving coordinate system	293
A.6 Two-dimensional drawing of a simply connected region for deriving the scalar identity.	296
A.7 Small sphere region containing a singular point.	297

List of Tables

1.1	Density variations with temperature (salinity 3.5%)	18
1.2	Density variations with temperature (fresh water)	18
1.3	Viscosity of sea water with temperature (salinity 3.5%)	22
1.4	Viscosity of fresh water with temperature	22
1.5	Saturation vapour pressure p_v for fresh and sea water	22
1.6	Typical values of surface tension for sea and fresh water with temperature	23
2.1	Dimensions of fluid properties	42
2.2	Dispersive relation of deep water ocean waves	95
2.3	Relative effect of nonlinear waves	l 00
4.1	Boundary layers of turbulent flows with wall regions	183
4.2	Comparison between laminar and turbulent boundary layers	188
5.1	Velocity potential versus stream function	225
5.2	Various singularity and simple potential flows	227
	Comparison of flows for fixed bodies and moving bodies: circle and sphere of radius r_0	231
5.4	Far-field behavior of singularities	242
5.5	Added mass of various simple 2-D bodies	250

1

INTRODUCTION

1.1	Continuum Mechanics	6
	1.1.1 Definition of Fluid	6
	1.1.2 Assumptions and Axioms	7
	1.1.3 Basic Equations	10
1.2	Characteristics of Hydrodynamics	12
	1.2.1 Types of Fluid Flow	12
	1.2.2 Various Characteristic Effects	14
	1.2.3 Characteristics of Ship/Marine Hydrodynamics	14
	1.2.4 Ocean Environment	16
1.3	Mathematical Prerequisites: Vector Analysis	24
	1.3.1 Fundamental Function Analysis	24
	1.3.2 Vector Calculus	25
	1.3.3 Expansion Formulas	30

1.3.4 Divergence Theorem (Gauss Theorem)	31
1.3.5 Stokes' Theorem	32
1.3.6 Dyadic Products	33
1.3.7 Reynolds Transport Theorem	34
1.3.8 Moving Coordinate Systems	37

1.1 Continuum Mechanics

1.1.1 Definition of Fluid

- Fluid can not withstand shearing forces when a shear stress is applied: Fluids continuously deform and Solids deform or bend.
- While solid can be in stable equilibrium under shear stress oblique to the surface separating any two parts, fluid cannot be in stationary equilibrium.

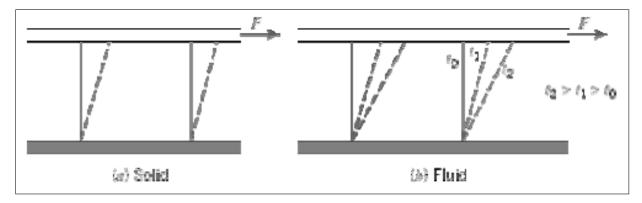


Figure 1.1 Behavior of a solid and a fluid, under the action of constant shear force. Solid (*left*); Fluid (*right*). (From Fox, McDonald & Pritchard 2004)

• Resistance to rate of shear deformation from viscosity gives rise to drag for bodies. We can easily recognize that such shear stresses do exist in fluids: e.g., consider how the fluid in a rotating circular vessel takes on the rotating motion of the vessel eventually.

- Other observed properties of fluids are:
 - resistance to volumetric compression and tension in general,
 - no shape or preferred orientation (Solids: definite shape; Fluids: no preferred shape),
 - homogeneous matter in general, and
 - has mass.
- There are two kinds of fluids depending on bulk elasticity (compressibility): 1
 - Liquid forms a free surface(density $\rho \approx 0$ above free surface).
 - Gas expands to fill container.

1.1.2 Assumptions and Axioms

• Continuum Viewpoint: Fluid as a continuum in macroscopic scale compared with molecules.

We assume that the fluid is continuous and homogeneous in structure.

- Actually this is not so since matter is ultimately made up of molecules and atoms, but in many applications the dimensions we are concerned with are large compared to the molecular structure, and the smallest sample of fluid that concerns us contains a very great number of molecules (i.e., number of about $2.687 \times 10^{19}/cm^3$). ²
- In such cases, the properties of any sample are the average values over many molecules, and the approximation of a continuum is found to be acceptable and useful.
 - * Measurable smallest scale: length $l \sim O(10^{-5}) \, m$, volume $V \sim O(10^{-15}) \, m^3$.

¹On the mechanism of formation of liquid and vapor, see Brennen, C. (1995), *Cavitation and Bubble Dynamics*, Oxford University Press, pp. 1–6.

 $^{^2}$ Avogadro no./1 mol = $6.02214 \times 10^{23}/22.414$ liter. This number is about 10 times as many as the total no. of stars in the known universe, and about 100 times as many as grains of sand on all beaches and deserts. (See Garrison, T. (2007), *Oceanography: An Invitation to Marine Science*, 6th ed., Thomson Brooks/Cole.) Suppose a supercomputer can count at the rate of one billion molecules per second. For a cubic centimeter of a fluid we would take a very long time for counting the occupied molecules: $2.687 \times 10^{10} \, \mathrm{sec} \approx 850 \, \mathrm{yr}$.

- · Nano scale devices: $l \sim O(10^{-8}) \, m$
- · Ocean current diameter: $l \sim O(10^6) \, m$
- * No. of air molecules in the volume at standard pressure: $\sim 3\times 10^{10}.$
- * No. of water molecules in the volume at standard pressure: $\sim 10^{13}$.

Example: definition of density at a point (see Figures 1.2 and 1.3)

$$\rho \equiv \lim_{\delta V \to \delta V'} \frac{\delta m}{\delta V} = \rho(x, y, z, t) \tag{1.1}$$

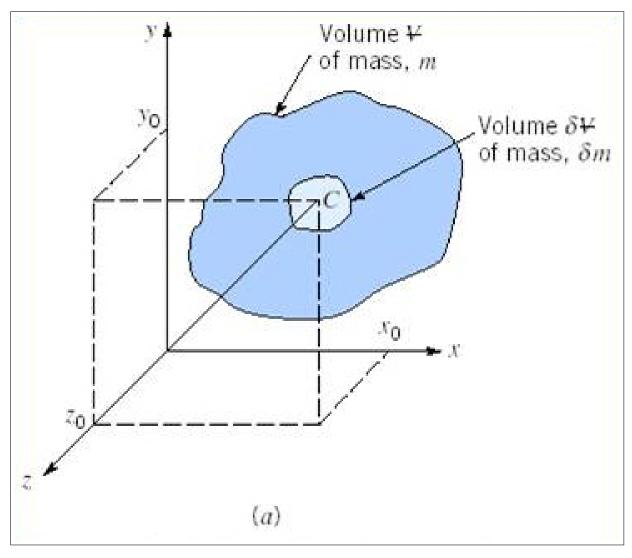


Figure 1.2 Definition of density. (From Fox, McDonald & Pritchard 2004)

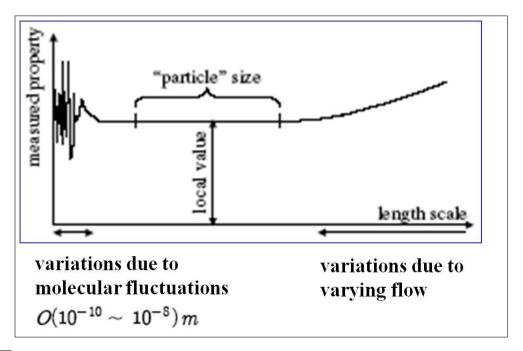


Figure ton 1984)

- **1.3** Measured data to define density with variation of length scale. (From Pan-
- Nevertheless, results obtained on the assumption of a continuum may be erroneous whenever the molecular structure dimensions are relatively large.
 - For example, at very high altitudes (low pressures), the molecular spacing is so great that air is not even approximately a continuum in its contact with a body.
 - Failures of the continuum assumption occur probably in the cases of that body size compares with molecular dimensions (e.g., a very small body in a fluid) or with distances between molecules (e.g., a body in a rarefied gas).
- Other acceptable and useful assumptions are those as follows:
 - (1) that physical laws are independent of the coordinate system used to express them (frame indifference),
 - (2) that natural laws are independent of the dimensions of physical quantities that occur in the expressions (dimensional homogeneity),
 - (3) that derivations of physical quantities with respect to space and time exist to the required order (smoothness of quantities), and

(4) that the present motion is a function of its history and not the future (memory of history).

1.1.3 Basic Equations

- Fundamental Laws of Continuum Mechanics:
 - Conservation of mass: Continuity equation
 - Conservation of momentum (Newton's law of motion)
 - * Principle of momentum and angular momentum
 - * Navier-Stokes equations for viscous flow
 - * Euler's equation for inviscid flow
 - * Bernoulli equation as an energy equation from integration of Euler's equation
 - Conservation of energy (First law of thermodynamics)
 - * The First Law of Thermodynamics: Energy conservation for heat and work interactions
 - * The Second Law of Thermodynamics: Heat flow in direction of entropy increase

We postulate that mass, momentum and energy are conserved: Conservation of mass, Conservation of momentum, Conservation of energy. Since these notes tend to deal mostly with incompressible flows, we do not examine the conservation of energy.

• Newton's equations of motion are derived from rigid body mechanics:

$$\underline{F} = m \frac{d^2 \underline{x}}{dt^2} \tag{1.2}$$

where m = mass of particle or body, $\underline{F} = \text{sum}$ of external forces, $\underline{x} = \text{position vector}$, and t = time.

Three differential equations

- Applicable to mass particle or system of mass particles, differential element or whole part of continuum
- Concept of dynamic and static equilibrium for given external forces
- General equations of motion applicable to arbitrary elements of bodies in concern:

$$\underline{F} = \frac{d\underline{M}}{dt}, \quad \underline{L} = \frac{d\underline{H}}{dt}$$
 (1.3)

where \underline{M} = linear momentum, \underline{L} = sum of moment in action, \underline{H} = angular momentum.

• Our use of these laws are based on continuum hypothesis. Equations of motion for continuum:

$$\rho \, \frac{d^2 \underline{x}}{dt^2} = \rho \, \underline{b} + \nabla \cdot \underline{\underline{T}} \tag{1.4}$$

where $\underline{\underline{T}}$ = stress tensors (internal or surface forces), \underline{b} = body force per unit mass.

- Constitutive Laws
 - Solids: Hooke's law, stress = f (strain) force/area \sim relative displacement/length
 - Fluids: stress = f (rate of strain)
 force/area ~ velocity gradient

We need the <u>constitutive equations</u> which are a sort of relationships between the stress tensor and the strain tensor, under some assumptions such as homogeneous, isotropic, continuous, elastic (Newtonian) continuum. Relation to the strain in solid and the strain rate in fluid:

$$F \propto \triangle \ell, \quad F \propto \triangle u$$
 (1.5)

where the proportional factors are the <u>elasticity</u> and the <u>viscosity</u> coefficients, respectively.

• Isotropic stress tensors having linear relationship with strain tensor and

strain rate tensor, respectively: ³

$$\underline{T} = \lambda' (\nabla \cdot \underline{d}) \underline{I} + \lambda \left[\nabla \underline{d} + (\nabla \underline{d})^T \right]$$
 (1.6)

$$\underline{T} = \left[-p + \mu' \left(\nabla \cdot \underline{u} \right) \right] \underline{I} + \mu \left[\nabla \underline{u} + \left(\nabla \underline{u} \right)^T \right]$$
 (1.7)

where d and u are, respectively, the displacement and the velocity, λ' , λ , μ' and μ are the proportional factors.

The differential equations for displacement and velocity, respectively:

$$\rho \frac{\partial^2 \underline{d}}{\partial t^2} = \rho \underline{f}_{body} + (\lambda' + \lambda) \nabla (\nabla \cdot \underline{d}) + \lambda \nabla^2 \underline{d}$$
 (1.8)

$$\rho \frac{\partial^{2} \underline{d}}{\partial t^{2}} = \rho \underline{f}_{body} + (\lambda' + \lambda) \nabla (\nabla \cdot \underline{d}) + \lambda \nabla^{2} \underline{d}$$

$$\rho \frac{\partial^{2} \underline{u}}{\partial t^{2}} = \rho \underline{f}_{body} - \nabla p + (\mu' + \mu) \nabla (\nabla \cdot \underline{u}) + \mu \nabla^{2} \underline{u}$$
(1.8)

- Liquids and gases depending on compressibility (bulk elasticity).
 - Liquids: 'Hydrodynamics' (Hydrodynamic flows are treated as incompressible.)
 - Gases: 'Aerodynamics' (Aerodynamic flows are treated as compressible.)
- Classification of fluid mechanics

1.2 **Characteristics of Hydrodynamics**

1.2.1 **Types of Fluid Flow**

With the principal types of fluid flow and their associated phenomena, it is possible to make up practically any flow combination in nature, even the complex system around a moving ship:

Potential Flow

³For detailed information on difference and similarity among various fields in continuum mechanics and their historical background, see the article: 이승준 (1992), "재료역학과 고체역학: 유체역학자의 관점에서", 대한 조선학회지, 제29권, 제3호.

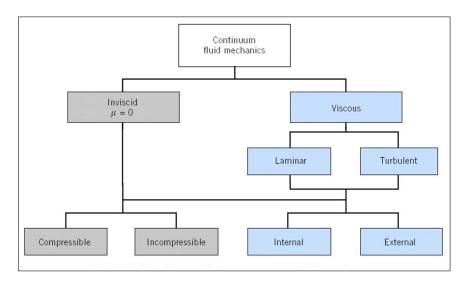


Figure 1.4 Possible classification of fluid mechanics. (From Fox, McDonald & Pritchard 2004)

- Viscous Flow
- Turbulent Flow
- Separation of Flow from a Surface
- Cavitation
- Wavemaking
- Circulatory or Vortical Flow
- Elastic or Compressible Flow

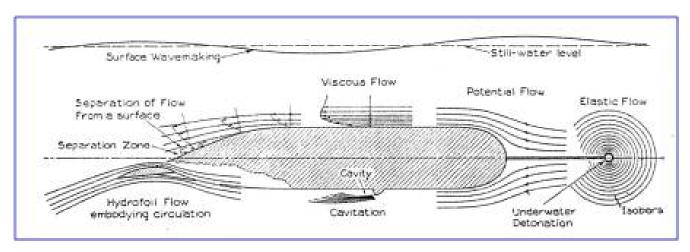


Figure 1.5 Schematic diagram of various types of fluid flow. (From Saunders 1957)

1.2.2 Various Characteristic Effects

Such flow phenomena can be characterized by several principal effects which constitute the basis for important relationships in the form of non-dimensional numbers:

- <u>Velocity effects</u> have the phenomena which are function of the rate at which a body moves in a fluid (e.g. denotation wave around a torpedo exploded).
- Acceleration effects is associated with the acceleration imparted to fluid particles by differences in pressure and other causes (e.g. flow around a propeller blade section).
- <u>Force effects</u> are the application of forces of special nature which is closely related to accelerative effects (e.g. dynamic lift developed by a planning form).
- <u>Inertia effects</u> involve the mass density of the fluid, the velocity of the moving fluid particles, and the necessity for changing their direction (e.g. dynamic pressure on the blunt face).
- Gravity effects result in the changes in potential energy under the influence of the gravity, which occur at an interface with gas (e.g. wavemaking).
- <u>Viscous effects</u> are due to the internal resistance of the fluid to deformation in the shear forces (e.g. flow past a solid surface).
- Elastic effects are due to the compressibility of the fluid (e.g. acoustic wave traveling through water).
- <u>Surface tension effects</u> appear as the attraction between the surface molecules of the real fluid (e.g. air bubbles in water).

1.2.3 Characteristics of Ship/Marine Hydrodynamics

 Ship/Marine Hydrodynamic Aspects: Applicable to naval architecture and ocean engineering

- Many Separate Topics: Propulsion/steering, behavior in waves of a moored buoy or oil-drilling platform
- Related Applications of the General Field of Hydrodynamics
 - Lifting Surfaces: Propellers, Rudders, Anti-rolling fins, Yacht keels,
 Sails
 - Equations of Motion: Unsteady ship, Buoy, or Platform motions in waves, Maneuvering of ships or submarines in non-straight paths.
- Broad Level of Sophistication: From empirical design methodology to theoretical research activities (as well as intuition and experiment)
 - Diverse Fields of Technology: Fluid mechanics, solid mechanics, control theory, statistics, random process, data acquisition
- Necessary Background
 - Intelligent evaluation and application of empirical procedure
 - Introduction to specialized study on the advanced research
 - Continuum Mechanics: Force and motion in smooth and continuous manner
- Complicated Force Mechanisms
 - 3 Principal Types: Inertial, Gravitational, Viscous
 - Secondary Effects: Surface tension, Elastic, Cavitation
- Physical Parameters: Length, Velocity, Density, Gravity, Viscosity, Pressure

- Inertial forces
$$\sim$$
 mass \times acceleration $\sim (\rho l^3) \left(\frac{U^2}{l}\right) = \rho U^2 l^2$ (1.10)

- Viscous forces
$$\sim$$
 shear stress $\left(\mu \frac{\partial u}{\partial y}\right) \times \text{area} \sim \left(\mu \frac{U}{l}\right)(l^2) = \mu U l$ (1.11)

- Gravitational forces \sim mass \times gravity $\sim (\rho l^3)g$ (1.12)
- Pressure forces \sim pressure \times area $\sim (p p_0)l^2$ (1.13)

Dynamical Similarity

$$\frac{\text{Inertial Force}}{\text{Gravitational Force}} = \frac{\rho U^2 l^2}{\rho g l^3} = \frac{U^2}{g l} = (\text{Froude No.})^2 \quad (1.14)$$

$$\frac{\text{Inertial Force}}{\text{Viscous Force}} = \frac{\rho U^2 l^2}{\mu U l} = \frac{\rho U l}{\mu} = \text{Reynolds No.} \quad (1.15)$$

$$\frac{\text{Inertial Force}}{\text{Viscous Force}} = \frac{\rho U^2 l^2}{\mu U l} = \frac{\rho U l}{\mu} = \text{Reynolds No.}$$
 (1.15)

$$\frac{\text{Gravitational Force}}{\text{Viscous Force}} = \frac{\rho g l^3}{\mu U l} = \frac{\rho g l^2}{\mu U}$$
 (1.16)

- Simultaneous scaling is not possible. Scaling dilemma!
- Cavitation: Change of physical state below vapor pressure at very high speeds

Cavitation No.:
$$\sigma = \frac{p_0 - p_v}{\frac{1}{2}\rho U^2}$$
 (1.17)

- Difficulty of Navier-Stokes Equations: System of coupled nonlinear P.D.E.
 - Inviscid Assumptions: Mathematical solutions (with free surface effects).
 - Froude's Hypothesis: Total resistance = frictional + residual resistance.
 - Boundary Layer: Viscous effect within thin viscous layer at large Reynolds number.
 - CFD: Numerical simulation by using discretization and approxiamtion of governing equations with physical modelling.

Ocean Environment 1.2.4

- Density of Water
 - Dependence on temperature and salinity.
 - * Greater influence of temperature at a given salinity in a higher temperature regions.
 - * Greater effect of salinity in a lower temperature regions.

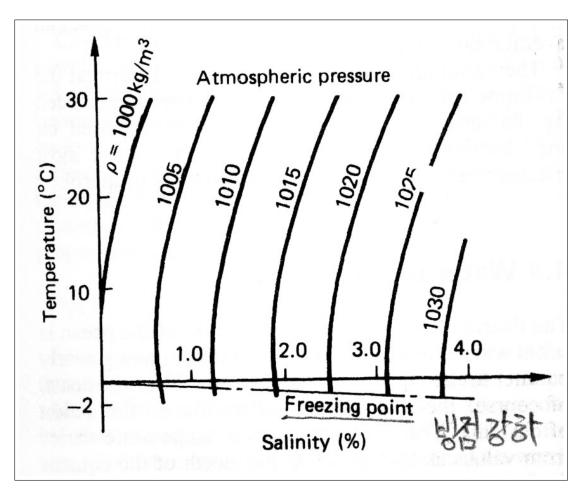


Figure 1.6 Variation of density with salinity and temperature at atmospheric pressure. (From Carlton 1994)

Table 1.1 Density variations with temperature (salinity 3.5%). (Adapted from Carlton 1994)

Temperature $({}^{0}C)$	0	5	10	15	20	25	30
Density (kg/m^3)	1028.1	1027.7	1026.8	1025.9	1024.7	1023.3	1021.7

Table 1.2 Density variations with temperature (fresh water). (Adapted from Carlton 1994)

Temperature (^{0}C)	0	4	5	10	15	20	25	30
Density (kg/m^3)	999.8	1000	999.9	999.6	999.0	998.1	996.9	995.6

- Increase with depth.

Sea water: $\rho = 1,026 \, kg/m^3$ at $15^{\circ}C$.

• Salinity = 3.47% at sea surface:

Salinity =
$$1.80655 \times$$
 Chlorinity in % (1.18)

- Water Temperature
 - From $T=28^{o}\,C$ at equator to $T=-2^{o}\,C$ near ice in high latitudes.
 - Three thermal layers:
 - * Upper layer between $D=50\,m$ and $D=200\,m$ below surface: $T=20^o\,C$ at surface
 - * Transition layer to $D=1,000\,m$: $T=8^o\,C$ at $D=500\,m$ and $T=5^o\,C$ at $D=1,000\,m$
 - * Deep ocean region: $T = 2^{\circ} C$ at D = 4,000 m.
- Viscosity

$$\tau_{yx} = \mu \frac{\partial u}{\partial y} \tag{1.19}$$

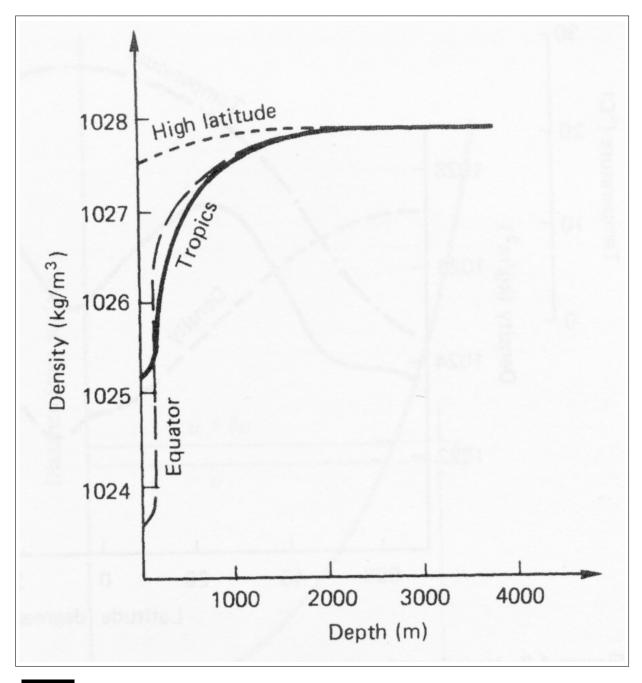


Figure 1.7 Typical variation od depth versus density for different global latitudes. (From Carlton 1994)

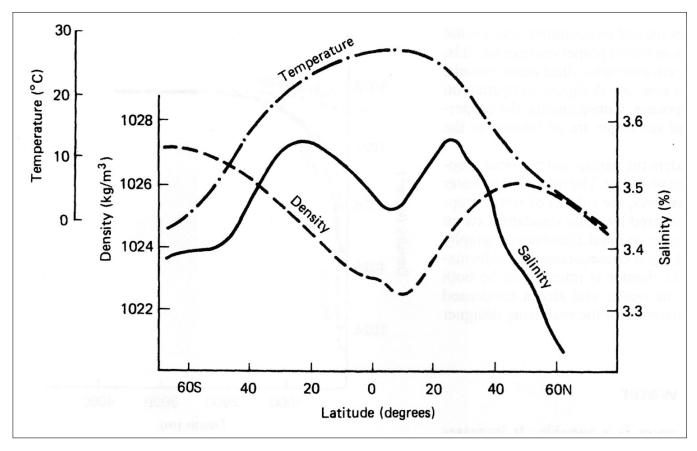


Figure 1.8 Variation of surface temperature, salinity and density with latitude–average for all oceans. (From Carlton 1994)

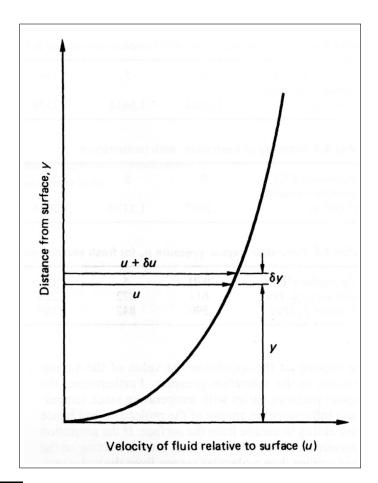


Figure 1.9 Typical viscous velocity gradient. (From Carlton 1994)

Table 1.3 Viscosity of sea water with temperature (salinity 3.5%). (Adapted from Carlton 1994)

Temperature $({}^{0}C)$	0	5	10	15	20	25	30
Kinematic Viscosity							
$\times 10^6 \ (m^2/s)$	1.8284	1.5614	1.3538	1.1883	1.0537	0.9425	0.8493

Table 1.4 Viscosity of fresh water with temperature. (Adapted from Carlton 1994)

Temperature (^{0}C)	0	5	10	15	20	25	30
Kinematic Viscosity							
$\times 10^6 \ (m^2/s)$	1.7867	1.5170	1.3064	1.1390	1.0037	0.8929	0.8009

• Vapour Pressure

Table 1.5 Saturation vapour pressure p_v for fresh and sea water. (Adapted from Carlton 1994)

Temperature $({}^{0}C)$	0.01	5	10	15	20	25	30
Sea Water $p_v(Pa)$	590	842	1186	1646	2296	3058	4097
Fresh Water $p_v(Pa)$	611	872	1228	1704	2377	3166	4241

• Surface Tension

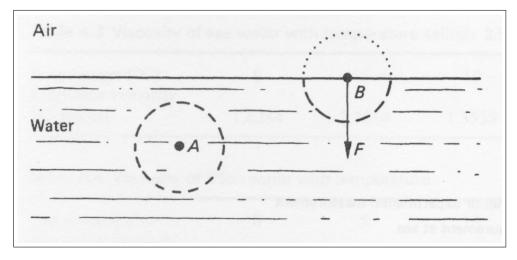


Figure 1.10 Molecular explanation of surface tension. (From Carlton 1994)

Table 1.6 Typical values of surface tension for sea and fresh water with temperature. (Adapted from Carlton 1994) Note: $1 \, dyne = 10^{-5} \, Newton$.

Temperature $({}^{0}C)$	0	5	10	15	20	25	30
Sea Water (dynes/cm)	76.41	75.69	74.97	74.25	73.55	72.81	72.09
Fresh Water (dynes/cm)	75.64	74.92	74.20	73.48	72.76	72.04	71.32

- Incompressibility of Water ⁴
 - The elastic force in a fluid is

Elastic force
$$\sim p l^3 \sim \rho C^2 l^2$$
 (1.20)

since the speed of sound C in a fluid is related to pressure and density: $C = \frac{p}{\rho}$. Then

(1.21)

 Mach number: ratio of characteristic fluid velocity in a flow to speed of sound in the medium:

Mach number
$$M = \frac{\text{inertia force}}{\text{elastic force}} = \sqrt{\frac{\rho U^2 l^2}{\rho C^2 l^2}} = \frac{U}{C}$$
 (1.22)

where U is the characteristic fluid velocity.

- The average speed of sound in air and water is: $C_{air} \sim 350 m/s$, $C_{water} \sim 1,500 m/s$ Therefore the average ratio of the speed of sound in water to air is $C_{water}/C_{air} \sim 4$.
- Because the average water to air density ratio is 1,000, it is 'harder' to move in water and therefore, typically, it is $U_{water} \ll U_{air}$ giving thus typical values of Mach numbers in the order of:

$$M_{air} \sim O(1) \Rightarrow \text{Compressible flow}$$
 (1.23)

$$M_{water} \ll 1 \Rightarrow \text{Incompressible flow}$$
 (1.24)

 Only 0.4 % change under 100 atmospheric pressure (at 1 km depth in sea water).

- Note: An incompressible flow does not mean constant density.

1.3 Mathematical Prerequisites: Vector Analysis

1.3.1 Fundamental Function Analysis

- If $\lim_{x\to c} \phi(x) = \phi(c)$, the function $\phi(x)$ is said to be continuous at the point x=c.
- \bullet The base of natural logarithm e,

$$e = \lim_{n \to \infty} \left(1 + \frac{1}{n} \right)^n = 2.7182818285 \cdots$$
 (1.25)

Euler formula: $e^{i\theta} = \cos \theta + i \sin \theta$

Hyperbolic sine and cosine functions:

$$\sinh x = \frac{e^x - e^{-x}}{2}, \quad \cosh x = \frac{e^x + e^{-x}}{2} \tag{1.26}$$

• A definite integral in the sense of Riemann sum:

$$\int_{a}^{b} f(x) dx = \lim_{N \to \infty} \sum_{i=1}^{N} f\left(a + i\frac{b-a}{N}\right) \frac{b-a}{N}$$
 (1.27)

• The rule for change of variable :

$$\int_{x_1}^{x_2} f(x) \, dx = \int_{u_1}^{u_2} f(x(u)) \frac{dx}{du} \, du \tag{1.28}$$

The integral for functions of two variables

$$\iint_{\Omega_{xy}} f(x,y) \, dxdy = \iint_{\Omega_{uv}} f(x(u,v),y(u,v)) |J| \, dudv, \qquad (1.29)$$

where Jacobian
$$J \equiv \frac{\partial(x,y)}{\partial(u,v)} = \frac{\partial x}{\partial u} \frac{\partial y}{\partial v} - \frac{\partial x}{\partial v} \frac{\partial y}{\partial u}$$
.

• Leibnitz's rule in 1-D:

$$\frac{d}{dt} \int_{a(t)}^{b(t)} f(x,t) \, dx =
f [b(t),t] b'(t) - f [a(t),t] a'(t) + \int_{a(t)}^{b(t)} \frac{\partial f}{\partial t} \, dx$$
(1.30)

The Reynolds' Transport Theorem for 2-D and 3-D region.

- Tensor notation in 3D space
 - Range convention:

$$x_i \ (i = 1, 2, 3) \to x_1, x_2, x_3$$
 (1.31)

- Summation convention:

$$a_i b_i = a_1 b_1 + a_2 b_2 + a_3 b_3 \quad (i = 1, 2, 3)$$
 (1.32)

- For example, $a_i = x_{ij} n_j$ denotes three equations, one for each i = 1, 2, 3 and j is the dummy index.
- Tensors.
 - A scalar is called a zero-order tensor.
 - A vector is a first-order tensor.
 - Dyads are second-order tensors: a 3×3 matrix form. (e.g. stress tensor)
 - The alternating tensor ϵ_{ijk} is a special third-order tensor.

1.3.2 Vector Calculus

• The simplest vector: *line vectors*.

A line vector is transformed from one coordinate system to another.

Consider two Cartesian coordinate systems rotated with respect to one another.

- a_{11} , a_{21} , a_{31} : the direction cosines of the x'_1 axis, with respect to the x_1 , x_2 , x_3 axes, respectively.
- Transform between 2 coordinates in a summation notation:

$$x_i' = \sum_{j=1}^{3} a_{ji} x_j \quad i = 1, 2, 3$$
 (1.33)

$$x_i = \sum_{j=1}^{3} a_{ij} x'_j \quad i = 1, 2, 3$$
 (1.34)

• A vector is defined as:

$$u_i' = \sum_{j=1}^{3} a_{ji} u_j \quad i = 1, 2, 3$$
(1.35)

- Example (a) Velocity of a point, dx_i/dt .

$$\frac{dx_i'}{dt} = \frac{d}{dt} \sum_{j=1}^{3} a_{ji} x_j = \sum_{j=1}^{3} a_{ji} \frac{dx_j}{dt}.$$
 (1.36)

– Example (b) Gradient of a scalar function, $\partial u/\partial x_i$. Let $w_i \equiv \partial u/\partial x_i$; and $w_i' \equiv \partial u/\partial x_i'$.

$$w_i' = \sum_{j=1}^3 \frac{\partial u}{\partial x_j} \frac{\partial x_j}{\partial x_i'} = \sum_{j=1}^3 \frac{\partial u}{\partial x_j} a_{ji} = \sum_{j=1}^3 a_{ji} w_j$$
 (1.37)

- *Unit base vectors*: $\underline{i}, \underline{j}$, and \underline{k} . For curvilinear coordinate systems, $\underline{e}_1, \underline{e}_2$, and \underline{e}_3 .
- Any vector \underline{a} as the sum of its components :

$$\underline{a} = a_1 \, \underline{i} + a_2 \, \underline{j} + a_3 \, \underline{k}. \tag{1.38}$$

The position vector \underline{x} :

$$\underline{x} = x\,\underline{i} + y\,j + z\,\underline{k}.\tag{1.39}$$

The distance of \underline{x} from the origin as $r \equiv |\underline{x}| = \sqrt{x^2 + y^2 + z^2}$.

• Tensor notation:

Example) Kronecker delta:

$$\delta_{ij} = 1 \text{ if } i = j; \quad \delta_{ij} = 0 \text{ if } i \neq j$$
 (1.40)

Example) Alternating tensor of permutation symbol:

$$\begin{cases}
\epsilon_{ijk} = 0 & \text{if any } i, j, k \text{ equal} \\
\epsilon_{ijk} = 1 & \text{if } (ijk) = (123), (231), (312) \\
\epsilon_{ijk} = -1 & \text{if } (ijk) = (132), (213), (321)
\end{cases}$$
(1.41)

The basic formulas:

$$\delta_{ii} = 3, \quad \delta_{ij} u_{klmi} = u_{klmj}, \quad \delta_{ij} \epsilon_{ijk} = 0,$$
 (1.42)

$$\epsilon_{ijk} \, \epsilon_{klm} = \delta_{il} \, \delta_{jm} - \delta_{im} \, \delta_{jl}, \quad \epsilon_{ijk} \, \epsilon_{ijk} = 6,$$
 (1.43)

$$\epsilon_{ijk}\,\epsilon_{ljk} = 2\,\delta_{il}.\tag{1.44}$$

• Scalar product:

$$\underline{a} \cdot \underline{b} = a \, b \, \cos(\underline{a} \cdot \underline{b}) \tag{1.45}$$

or,

$$\underline{a} \cdot \underline{b} = a_1 \, b_1 + a_2 \, b_2 + a_3 \, b_3 \tag{1.46}$$

or,

$$\underline{a} \cdot \underline{b} = \delta_{ij} \, a_i \, b_j = a_i \, b_i$$
, (summation convention) (1.47)

• Vector product:

$$\underline{c} = \underline{a} \times \underline{b}; \quad w = a b \sin(\underline{a}, \underline{b}).$$
 (1.48)

In a form of tensor-notation, $\underline{a} \times \underline{b} = \epsilon_{ijk} a_j b_k$.

• Scalar triple product:

$$\underline{a} \cdot (\underline{b} \times \underline{c}) = a_i \, \epsilon_{ijk} \, b_j \, c_k \tag{1.49}$$

$$\underline{a} \cdot \underline{b} \times \underline{c} = \underline{a} \times \underline{b} \cdot \underline{c} = \underline{b} \cdot \underline{c} \times \underline{a} \text{ etc.}$$
 (1.50)

• *Vector triple product*:

$$\underline{a} \times (\underline{b} \times \underline{c}) = (\underline{a} \cdot \underline{c}) \, \underline{b} - (\underline{a} \cdot \underline{b}) \, \underline{c} \tag{1.51}$$

i.e.,

$$\underline{a} \times (\underline{b} \times \underline{c}) = \epsilon_{mli} a_l \epsilon_{ijk} b_j c_k$$

$$= (\delta_{mj} \delta_{lk} - \delta_{mk} \delta_{lj}) a_l b_j c_k$$

$$= a_k b_j c_k - a_j b_j c_k. \tag{1.52}$$

The basic formula:

$$\underline{a} \times (\underline{b} \times \underline{c}) + \underline{b} \times (\underline{c} \times \underline{a}) + \underline{c} \times (\underline{a} \times \underline{b}) = 0 \tag{1.53}$$

• Gradient:

$$\nabla u \equiv \lim_{V \to 0} \frac{1}{V} \oint_{S} u \, \underline{n} \, dS \tag{1.54}$$

where S is the area enclosing the volume V, dS is the element of area, and \underline{n} is the unit vector normal to the surface.

In limit,

$$\nabla u = \underline{i} \, \frac{\partial u}{\partial x} + \underline{j} \, \frac{\partial u}{\partial y} + \underline{k} \, \frac{\partial u}{\partial z} \tag{1.55}$$

Symbol: ∇u , grad u, or $\frac{\partial u}{\partial x_i}$.

• Divergence:

$$\nabla \cdot \underline{v} = \lim_{V \to 0} \frac{1}{V} \oint_{S} \underline{n} \cdot \underline{v} \, dS \tag{1.56}$$

$$\nabla \cdot \underline{v} = \frac{\partial v_1}{\partial x} + \frac{\partial v_2}{\partial y} + \frac{\partial v_3}{\partial z}$$
 (1.57)

Symbol: $\nabla \cdot \underline{v}$, div \underline{v} , or $\frac{\partial v_i}{\partial x_i}$.

• Curl:

$$\nabla \times \underline{v} \equiv \lim_{V \to 0} \frac{1}{V} \oint_{S} \underline{n} \times \underline{v} \, dS \tag{1.58}$$

$$\nabla \times \underline{v} = \left(\frac{\partial v_3}{\partial y} - \frac{\partial v_2}{\partial z}\right) \underline{i} + \left(\frac{\partial v_1}{\partial z} - \frac{\partial v_3}{\partial x}\right) \underline{j} + \left(\frac{\partial v_2}{\partial x} - \frac{\partial v_1}{\partial y}\right) \underline{k} \quad (1.59)$$

or,

$$\nabla \times \underline{v} = \begin{vmatrix} \underline{i} & \underline{j} & \underline{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ v_1 & v_2 & v_3 \end{vmatrix}$$
 (1.60)

Symbol: curl \underline{v} , $\nabla \times \underline{v}$, or $\epsilon_{ijk} \frac{\partial v_k}{\partial x_i}$.

• Laplacian:

$$\nabla^2 u \equiv \nabla \cdot (\nabla u) = \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2}$$
 (1.61)

The Laplacian of a vector function

$$\nabla^2 \underline{v} = \underline{i} \ \nabla^2 v_1 + j \ \nabla^2 v_2 + \underline{k} \ \nabla^2 v_3 \tag{1.62}$$

• Differential operator: $dr \cdot \nabla$

$$du = d\underline{r} \cdot \nabla u \tag{1.63}$$

where \underline{r} is the position vector and $d\underline{r}$ is any directed line element.

- This means that du is the increment of u corresponding to a position increment dr.
- In rectangular Cartesian coordinates,

$$du = \frac{\partial u}{\partial x} dx + \frac{\partial u}{\partial y} dy + \frac{\partial u}{\partial z} dz = (d\underline{r} \cdot \nabla)u \tag{1.64}$$

- Similarly, for a vector function $\underline{v}(x, y, z)$,

$$d\underline{v} \equiv \underline{i} dv_1 + \underline{j} dv_2 + \underline{k} dv_3$$

$$= \left(dx \frac{\partial}{\partial x} + dy \frac{\partial}{\partial y} + dz \frac{\partial}{\partial z} \right) (\underline{i} v_1 + \underline{j} v_2 + \underline{k} v_3)$$

$$= (d\underline{r} \cdot \nabla)\underline{v}$$
(1.65)

– The symbol ∇ is a vector operator:

$$\nabla = \underline{i} \, \frac{\partial}{\partial x} + \underline{j} \, \frac{\partial}{\partial y} + \underline{k} \, \frac{\partial}{\partial z}. \tag{1.66}$$

1.3.3 Expansion Formulas

• ϕ : any differentiable scalar function of x, y, z. $\underline{u}, \underline{v}, \underline{w}$: any such vector functions.

$$\nabla \cdot (\phi \, \underline{u}) = \underline{u} \cdot \nabla \phi + \phi \, \nabla \cdot \underline{u} \tag{1.67}$$

$$\nabla \times (\phi \, \underline{u}) = (\nabla \phi) \times \underline{u} + \phi \, \nabla \times \underline{u} \tag{1.68}$$

$$\nabla \cdot (\underline{v} \times \underline{w}) = \underline{w} \cdot \nabla \times \underline{v} - \underline{v} \cdot \nabla \times \underline{w}$$
 (1.69)

$$\nabla \times (\underline{v} \times \underline{w}) = \underline{w} \cdot \nabla \underline{v} + \underline{v} \nabla \cdot \underline{w} - \underline{w} \nabla \cdot \underline{v} - \underline{v} \cdot \nabla \underline{w}$$
 (1.70)

$$\nabla(\underline{v} \cdot \underline{w}) = \underline{v} \cdot \nabla \underline{w} + \underline{w} \cdot \nabla \underline{v} + \underline{v} \times (\nabla \times \underline{w}) + \underline{w} \times (\nabla \times \underline{v}) \quad (1.71)$$

$$\nabla \cdot (\nabla \times \underline{v}) = 0 \tag{1.72}$$

$$\nabla \times (\nabla \phi) = 0 \tag{1.73}$$

$$\nabla \times (\nabla \times v) = \nabla(\nabla \cdot v) - \nabla^2 v \tag{1.74}$$

• The position vector: $\underline{x} = x_1 \underline{i} + x_2 \underline{j} + x_3 \underline{k}$.

Magnitude of the position vector $r = |\underline{x}| = \sqrt{\underline{x} \cdot \underline{x}}$ and a constant vector \underline{a} :

$$\nabla r = \underline{x}/r \tag{1.75}$$

$$\nabla \cdot \underline{x} = 3 \tag{1.76}$$

$$\nabla \times x = 0 \tag{1.77}$$

$$\nabla r^n = n \, r^{n-2} \, \underline{x} \tag{1.78}$$

$$\nabla \cdot (r^n \underline{x}) = (n+3) r^n \tag{1.79}$$

$$\nabla \times (r^n \underline{x}) = 0 \tag{1.80}$$

$$\nabla^2(r^n) = n(n+1) \, r^{n-2} \tag{1.81}$$

$$\nabla \cdot (\underline{a} \times \underline{x}) = 0 \tag{1.82}$$

$$\nabla(\underline{a} \cdot \underline{x}) = \underline{a} \tag{1.83}$$

$$\nabla \times (\underline{a} \times \underline{x}) = 2\,\underline{a} \tag{1.84}$$

$$\nabla \cdot (\underline{a} \times \nabla r) = 0 \tag{1.85}$$

$$\nabla \cdot (r \underline{a}) = (\underline{x} \cdot \underline{a})/r \tag{1.86}$$

$$\nabla \times (r \underline{a}) = (\underline{x} \times \underline{a})/r \tag{1.87}$$

1.3.4 Divergence Theorem (Gauss Theorem)

• Consider the surface integral $\oint_S u \ \underline{n} \ dS$. If the volume V is subdivided into small volume V_i ,

$$\oint_{S} u \, \underline{n} \, dS = \sum \oint_{S_{i}} u \, \underline{n} \, dS \tag{1.88}$$

In the limit,

$$\oint_{S_i} u \ \underline{n} \ dS = \int_{V_i} \nabla u \ dV.$$

Definition of the gradient, eq. (1.54),

$$\oint_{S} u \, \underline{n} \, dS = \int_{V} \nabla u \, dV \tag{1.89}$$

• Use the definitions of the divergence and curl,

$$\oint_{S} \underline{n} \cdot \underline{v} \, dS = \int_{V} \nabla \cdot \underline{v} \, dV \tag{1.90}$$

$$\oint_{S} \underline{n} \times \underline{v} \, dS = \int_{V} \nabla \times \underline{v} \, dV \tag{1.91}$$

General form:

$$\oint_{S} (\underline{n} * f) \ dS = \int_{V} (\nabla * f) \ dV$$
 (1.92)

• An example,

$$\int_{V} \nabla^{2} u \, dV = \int_{V} \nabla \cdot (\nabla u) \, dV$$

$$= \oint_{S} \underline{n} \cdot \nabla u \, dS = \oint_{S} \frac{\partial u}{\partial n} \, dS$$
(1.93)

where $\partial u/\partial n$ is the directed derivative in the outward direction.

1.3.5 Stokes' Theorem

• From our definitions for ∇u and $\nabla \times \underline{v}$

$$\underline{n} \times \nabla u \approx \frac{1}{S} \oint_C u \, d\underline{r} \tag{1.94}$$

$$\underline{n} \cdot \nabla \times \underline{v} \approx \frac{1}{S} \oint_{C} \underline{v} \cdot d\underline{r} \tag{1.95}$$

where S denotes a very small surface element in the fluid, C is the small contour that forms the boundary of S, and \underline{n} is a unit normal to S.

• The transformation theorems relate certain surface integrals to contour in-

tegrals:

$$\int_{S} \underline{n} \times \nabla u \ dS = \oint_{C} u \ d\underline{r} \tag{1.96}$$

$$\int_{S} \underline{n} \cdot \nabla \times \underline{v} \, dS = -\int_{S} (\underline{n} \times \nabla) \cdot \underline{v} \, dS$$

$$= \oint_{C} \underline{v} \cdot d\underline{r} \tag{1.97}$$

The unified form of Stokes' theorem:

$$\left| \int_{S} (\underline{n} \times \nabla) * f \ dS = \oint_{C} d\underline{r} * f \right|$$
 (1.98)

1.3.6 Dyadic Products

• The dyadic product: a special form of second-order tensor $\underline{u} \ \underline{v}$:

• The gradient of a vector, $\nabla \underline{v}$, in the Navier-Stokes equations: If the vector \underline{v} is a velocity resolved into a symmetric and antisymmetric form:

$$\nabla \underline{v} = \frac{1}{2} \left[\left(\nabla \underline{v} + \nabla \underline{v}^T \right) + \left(\nabla \underline{v} - \nabla \underline{v}^T \right) \right]$$

$$= \frac{1}{2} de f(\underline{v}) + \frac{1}{2} rot(\underline{v})$$
(1.100)

- A second-order tensor to be a 3×3 matrix.
- The superscript T stand for transpose of the matrix.
- The first term causes stress: (i) normal strain rate and (ii) shear strain rate.
- The second term: rigid body rotation of a fluid element.

1.3.7 Reynolds Transport Theorem

• The rate of change of an integral taken over a volume moving through a field $F(\underline{x},t)$

$$\frac{d}{dt} \iiint\limits_{V(t)} F(\underline{x}, t) \ dV \tag{1.101}$$

The path of points in V(t):

$$\underline{x} = \underline{x}(\xi, t) \tag{1.102}$$

where ξ is the initial point of \underline{x} .

• The Reynolds transport theorem

$$\frac{d}{dt} \iiint_{V(t)} F \ dV = \iiint_{V} \left[\frac{\partial F}{\partial t} + \nabla \cdot (\underline{v} F) \right] dV \tag{1.103}$$

or

$$\boxed{\frac{d}{dt} \iiint\limits_{V(t)} F \ dV = \iiint\limits_{V(t)} \frac{\partial F}{\partial t} \ dV + \iint\limits_{S(t)} \underline{n} \cdot (\underline{v} F) \ dS}$$
(1.104)

- Here \underline{v} is the velocity of the point \underline{x} , and \underline{n} is the outward unit vector normal to the boundary S(t).
- The first integral is the rate of change in volume, and the second integral is the rate of change associated with motion of surface bounding volume.
- Similar to Leibnitz's rule for 1-dimensional region:

$$\frac{d}{dt} \int_{a(t)}^{b(t)} f(x,t) \, dx =
\int_{a(t)}^{b(t)} \frac{\partial f}{\partial t} \, dx + f[b(t),t] \, b'(t) - f[a(t),t] \, a'(t) \quad (1.105)$$

1.3.7.1 Example of the Reynolds transport theorem in 1-D

• Consider an integral with a(t) = t + 1, b(t) = 2t + 2, F(x,t) = xt, and $x(\xi,t) = \xi t + \xi$:

$$I(t) = \int_{a(t)}^{b(t)} F(x,t) \, dx, \quad \frac{dI(t)}{dt} = \frac{d}{dt} \int_{a(t)}^{b(t)} F(x,t) \, dx$$
 (1.106)

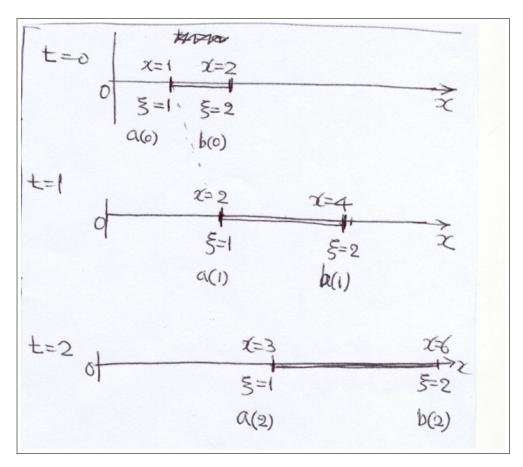


Figure 1.11 Sequential change of the interval of the integral (1.106).

• Lagrangian variable $\xi = \frac{x}{t+1}$ from the given relation $x(\xi,t) = \xi\,t + \xi$, then the integrand

$$F^*(\xi, t) = (\xi t + \xi)t \tag{1.107}$$

• Velocity and divergence of velocity:

$$\underline{v}^*(\xi,t) = \frac{\partial \underline{x}}{\partial t}\Big|_{\xi=\text{const.}} = \xi \,\underline{i} \equiv v^*\underline{i}$$
 in Lagrangian manner

(1.108)

$$\underline{v}(x,t) = \frac{x}{t+1} \underline{i} \equiv v \underline{i}$$
 in Eulerian manner (1.109)

$$\nabla \cdot \underline{v}(x,t) = \frac{1}{t+1} \equiv \frac{\partial v}{\partial x}$$
 in 1-dimensions (1.110)

• Chain rule (i.e., Jacobian)

$$\frac{\partial x}{\partial \xi} = t + 1 \equiv J \text{ (Jacobian)} \tag{1.111}$$

• The time derivative of the integral

$$\frac{dI(t)}{dt} = \frac{d}{dt} \int_{a(t)}^{b(t)} F(x,t) dx$$

$$= \frac{d}{dt} \int_{a(0)}^{b(0)} F^*(\xi,t) \frac{\partial x}{\partial \xi} d\xi \quad \text{(by change of variable)}$$

$$= \frac{d}{dt} \int_{a(0)}^{b(0)} \left\{ (\xi t + \xi)t \right\} J d\xi \quad \text{(with Jacobian)}$$

$$= \int_{a(0)}^{b(0)} \left[\frac{\partial \left\{ (\xi t + \xi)t \right\}}{\partial t} \Big|_{\xi = \text{const.}} J + \left\{ (\xi t + \xi)t \right\} \underbrace{\frac{\partial J}{\partial t}}_{A} \right] d\xi$$
(1.112)

where \boxed{A} is equivalent to

$$\frac{\partial J}{\partial t} = \frac{\partial}{\partial t} \left(\frac{\partial x}{\partial \xi} \right) = \frac{\partial}{\partial \xi} \left(\frac{\partial x}{\partial t} \right) \qquad \text{(interchanging the differential order)}$$

$$= \frac{\partial v^*}{\partial \xi} = \frac{\partial v}{\partial x} \frac{\partial x}{\partial \xi} \qquad \text{(by chain rule)}$$

$$= (\nabla \cdot \underline{v})J \implies \left(\frac{1}{t+1} \right) (t+1) \qquad (1.113)$$

• Rearranging the terms of the integrand and then converting the integral with respect to the variable ξ into one with respect to the original variable x, we have

$$\frac{dI(t)}{dt} = \int_{a(0)}^{b(0)} \left[\frac{\partial}{\partial t} (xt) + \underbrace{\frac{\partial x}{\partial t}}_{\xi = \text{const.}} \frac{\partial}{\partial x} (xt) + \underbrace{(xt) \left(\frac{1}{t+1}\right)}_{F \nabla \cdot \underline{v}} \right] \underbrace{(t+1)}_{J} d\xi$$

$$= \int_{a(t)}^{b(t)} \left[\frac{\partial F}{\partial t} + \nabla \cdot (\underline{v}F) \right] dx$$

$$= \int_{a(t)}^{b(t)} \left[\frac{\partial F}{\partial t} + \frac{\partial}{\partial x} (vF) \right] dx$$

$$= \int_{a(t)}^{b(t)} \frac{\partial F}{\partial t} dx + [vF(x,t)]\Big|_{x=b(t)} - [vF(x,t)]\Big|_{x=a(t)}$$

$$= \int_{a(t)}^{b(t)} \frac{\partial F}{\partial t} dx + F[b(t),t] b'(t) - F[a(t),t] a'(t) \tag{1.114}$$

1.3.8 Moving Coordinate Systems

• Two coordinate systems: The position vector \underline{x}' in the space-fixed system is related to the position vector x in the moving system:

$$\underline{x}' = \underline{x} + \underline{R} \tag{1.115}$$

where \underline{R} is the distance vector between the origins of two coordinate systems.

• The derivative (d'/dt) observed in the space-fixed system and the derivative (d/dt) observed in the moving system:

$$\frac{d'}{dt} = \frac{d}{dt} + \underline{\Omega} \times \tag{1.116}$$

where Ω is the angular velocity of the moving system.

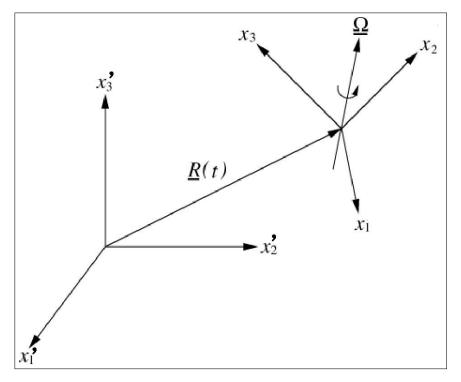


Figure 1.12 Moving coordinate system.

• The velocity vectors in the two coordinate systems:

$$\underline{q}' = \underline{q} + \underline{\Omega} \times \underline{x} + \underline{\dot{R}} \tag{1.117}$$

where $\underline{\dot{R}}$ represents the translation velocity of the moving frame.

• Acceleration vectors \underline{a} in the space-fixed system :

$$\underline{a}' \equiv \frac{d^2 \underline{x}'}{dt^2} = \underline{a} + 2\underline{\Omega} \times \underline{q} + \frac{d\underline{\Omega}}{dt} \times \underline{x} + \underline{\Omega} \times (\underline{\Omega} \times \underline{x}) + \underline{\ddot{R}}$$
 (1.118)

- The first term: the acceleration viewed in the moving system.
- The second term: the Coriolis acceleration.
- The fourth term: the generalized centripetal acceleration, since

$$|\underline{\Omega} \times (\underline{\Omega} \times \underline{x})| = \Omega^2 \underline{x} \sin(\underline{\Omega}, \underline{x}) \tag{1.119}$$

 For the self-rotation of earth with constant angular speed, its effect (a form of gradient of a scalar function) is already included in gravitational acceleration values.