Lecture Note of Naval Architectural Calculation

# **Ship Stability**

# Ch. 9 Numerical Integration Method in Naval Architecture

Spring 2018

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- ☑ Ch. 2 Review of Fluid Mechanics
- ☑ Ch. 3 Transverse Stability Due to Cargo Movement
- ☑ Ch. 4 Initial Transverse Stability
- ☑ Ch. 5 Initial Longitudinal Stability
- ☑ Ch. 6 Free Surface Effect
- ☑ Ch. 7 Inclining Test
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- ☑ Ch. 9 Numerical Integration Method in Naval Architecture
- ☑ Ch. 10 Hydrostatic Values and Curves
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- ☑ Ch. 12 Deterministic Damage Stability
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# Ch. 9 Numerical Integration Method in Naval Architecture

- 1. Simpson's Rule
- 2. Gaussian Quadrature
- 3. Green's Theorem
- 4. Calculation of Hydrostatic Values by Using Simpson's Rule
- 5. Calculation of Hydrostatic Values by Using Gaussian Quadrature and Green's Theorem

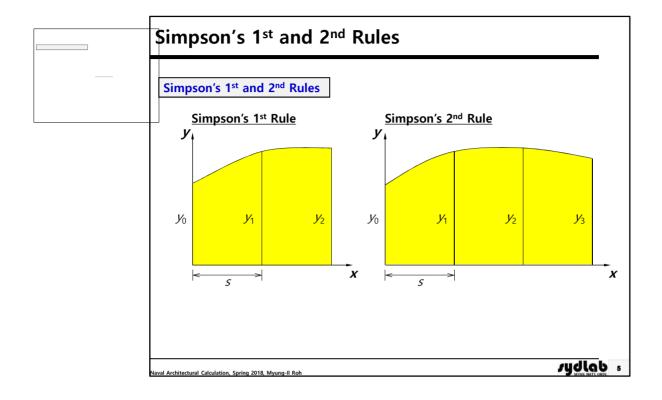
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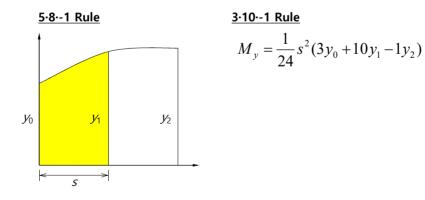
# 1. Simpson's Rule

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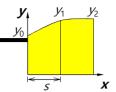


# 5.8.-1, 3.10.-1, and 7.36.-3 Rules



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# Derivation of Simpson's 1st Rule (1/4)





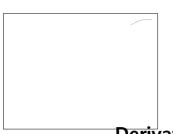
te the function  $\underline{y}$  by a parabola ( s the form

polynomial curve) whose

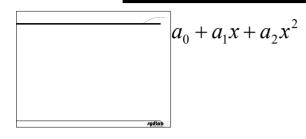
$$y = a_0 + a_1 x + a_2 x^2$$

 $y=a_0+a_1x+a_2x^2$  pla is represented by three points defining this curve. So points  $(y_0,y_1,y_2)$  are obtained by dividing the given interval into equal  $y_0$ ,  $y_1$ ,  $y_2$ ,  $y_3$ ,  $y_4$ ,  $y_5$ ,  $y_5$ ,  $y_5$ ,  $y_6$ ,  $y_7$ ,  $y_8$ ,  $y_9$ 

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# Derivation of Simpson's 1st Rule (3/4)



Integrate the area A from 0 to 2s. (Definite Integral



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# Derivation of Simpson's 2<sup>nd</sup> Rule (1/4)

Simpson's 2<sup>nd</sup> rule:

e the function by a

polynomial curve whose equation has the

$$y = a_0 + a_1 x + a_2 x^2 + a_3 x^3$$

polynomial curve is represented by four points defining this curve. Sints  $(y_0, y_1, y_2, y_3)$  are obtained by dividing the given interval into equal "s"

Cubic polynomial curve

The relation between the coefficients  $a_0$ ,  $a_1$ ,  $a_2$ ,  $a_3$  ("Find") and  $y_0$ ,  $y_1$ ,  $y_2$ , and  $y_3$  are

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The unknown coefficients,  $a_{\mu}$   $a_{\mu}$ ,  $a_{\mu}$  and  $a_{\mu}$  lead

# Derivation of Simpson's 2<sup>nd</sup> Rule (3/4)



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Integrate the area A from 0 to 3s

	y, y <sub>1</sub> _y <sub>2</sub> _y <sub>3</sub>	]
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# Derivation of 5.8.-1 Rule (1/4)

$$y = a_0 + a_1 x + a_2 x$$

te the function y by a parabola whose equation has the form  $y = a_0 + a_1 x + a_2 x^2$  pla is represented by three points defining this curve. Doints  $(y_0, y_1, y_2)$  are obtained by dividing the given interval into equal  $y_0, y_1, y_2, y_3$  are obtained by dividing the given interval into equal



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# Derivation of 5·8·-1 Rule (3/4) $a_0 + a_1 x + a_2 x^2$

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Integrate the area A from 0 to s.





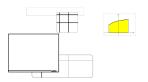
### Derivation of 3·10·-1 and 7·36·-3 Rules

$$M_{y} = M_{L} = \int_{0}^{s} x dA = \int_{0}^{s} xy dx = \int_{0}^{s} a_{0}x + a_{1}x^{2} + a_{2}x^{3} dx$$

$$= \frac{1}{24} s_{\frac{110}{100}}^{2} \left( 3 \underbrace{y_{0} + 10y_{0}}_{\frac{1}{100} \text{ total point of a low about } - y_{2}}_{\frac{1}{100} \text{ total point of a low about } - y_{2}} \right)$$

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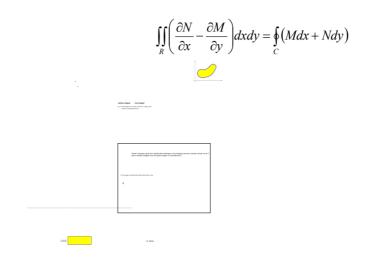
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				Since bending $M$ . The boundary of $g$ is a given boundary of $M$ as a given bound $\{X_i^{(k)}\}$	
Canada	an quadraturs:				C_MINISTER C_MINISTER A_MINISTER
Calculation of Area by U ${\cal N}$	Jsing Gaussian Quadrature	Node $t_j$			
3		$t_1 = -0.7745966692$ $t_2 = 0$			
		t <sub>3</sub> = 0.7745966692	Coefficients		
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# Calculation of Area by Using Green's Theorem



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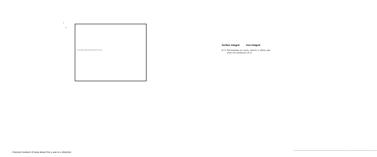
# Calculation of First Moment of Area by Using Green's Theorem (2/2)



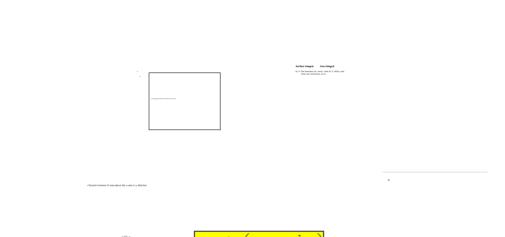
$$\therefore 2M_{A,x} = \oint_C \left( xy dy - \frac{y^2}{2} dx \right)$$

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[Example] Calculation of Area, First Moment of Area, an Centroid with Respect to the Inertial Frame (2/10)

# Segment ②:

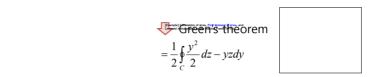
$$\frac{1}{2} \int_{\mathcal{Q}} y dz - z dy = \frac{1}{2} \int_{0}^{\sqrt{2}} \left( y \frac{dz}{dt} - z \frac{dy}{dt} \right) dt$$







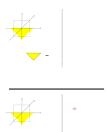




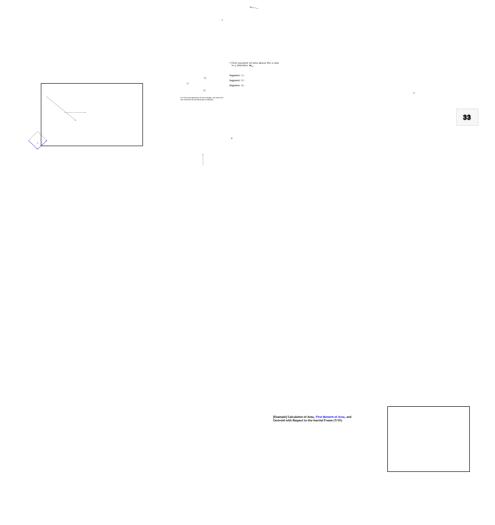








(Comple) Collidation of Jones, Front Remove of Jones, and Control with Respect to the Instructions (4/16): 
$$\frac{1}{2}\int_{\mathbb{D}}\frac{y^2}{2}dz-yzdy=-\frac{\sqrt{2}}{3}$$







[Example] Calculation of Area, First Moment of Area, at Centroid with Respect to the Inertial Frame (8/10)

$$= \frac{1}{2} \int_0^{\sqrt{2}} \left( t(t - \sqrt{2}) \cdot 1 - \frac{(t - \sqrt{2})^2}{2} \cdot 1 \right) dt$$



\_\_





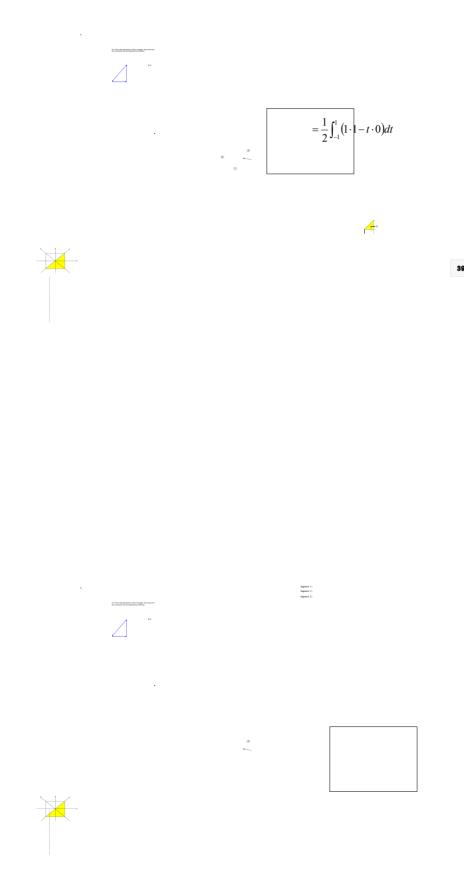
[Example] Calculation of Area, First Moment of Area, an Centroid with Respect to the Inertial Frame (10/10)

$$M_{A,z} = \frac{1}{2} \oint_{C} \frac{y^{2}}{2} dz - yz dy = 0$$

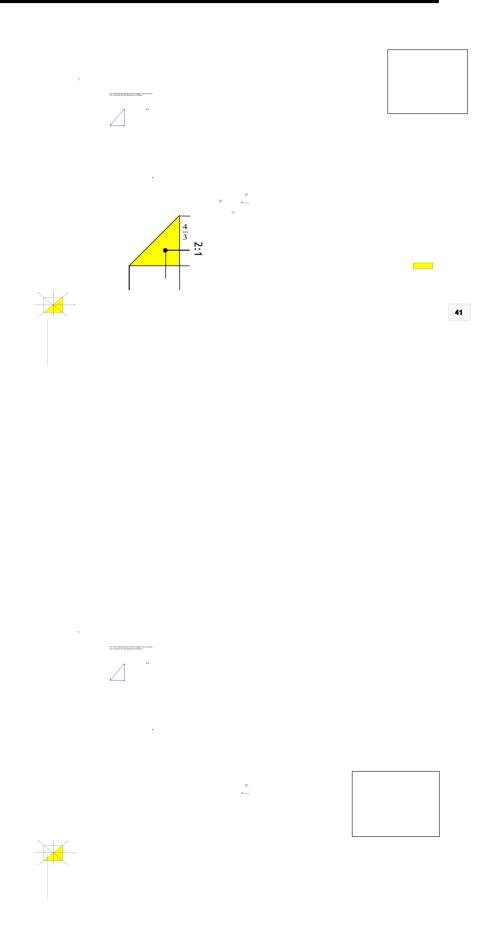




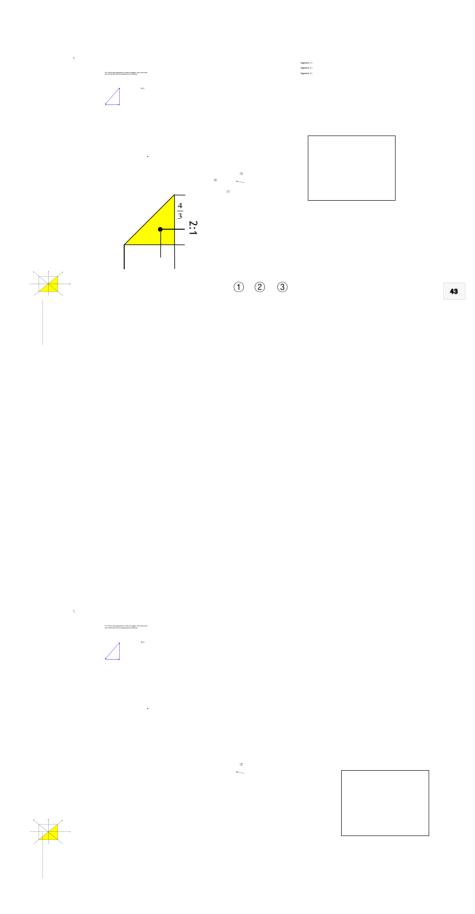
# [Example] Calculation of Area, First Moment of Area, and Centroid with Respect to the Body Fixed Frame (2/10)



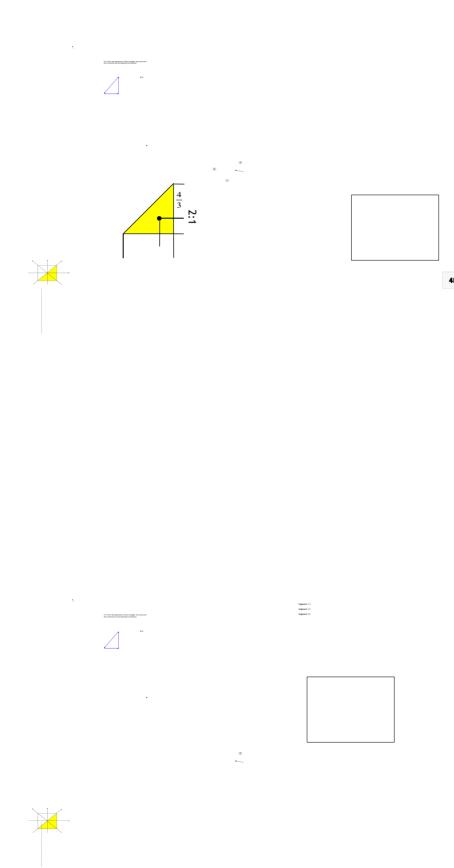
# [Example] Calculation of Area, First Moment of Area, and Centroid with Respect to the Body Fixed Frame (4/10)



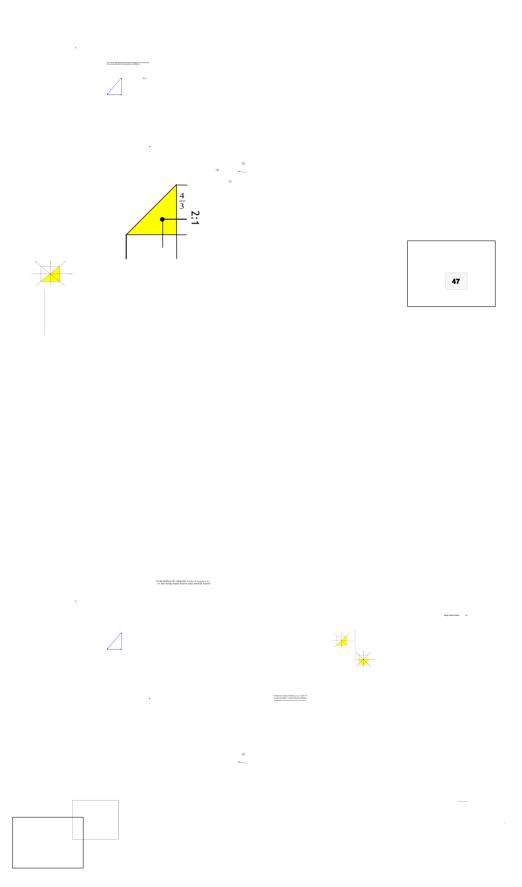
# [Example] Calculation of Area, First Moment of Area, and Centroid with Respect to the Body Fixed Frame (6/10)



# [Example] Calculation of Area, First Moment of Area, and Centroid with Respect to the Body Fixed Frame (8/10)



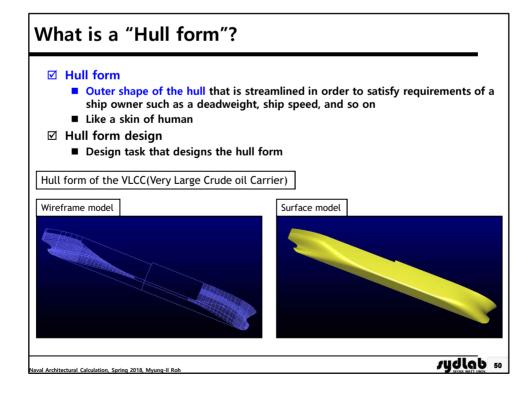
# [Example] Calculation of Area, First Moment of Area, and Centroid with Respect to the Body Fixed Frame (10/10)

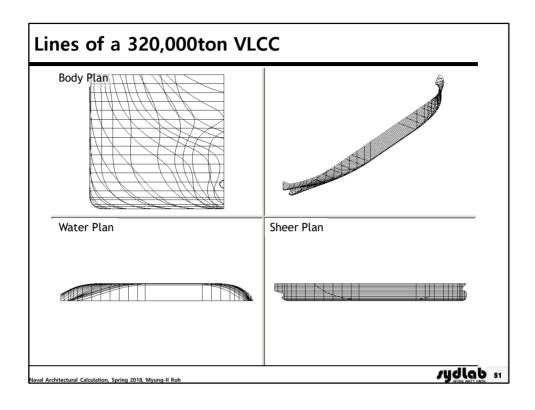


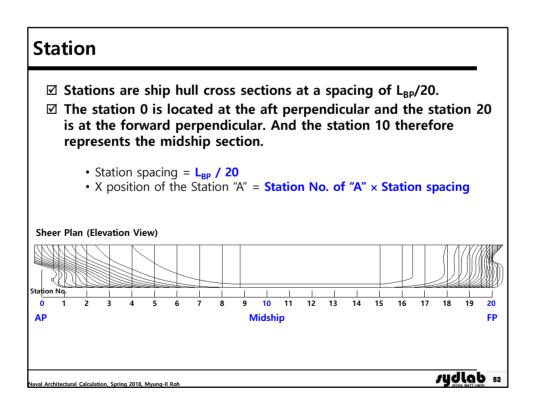
# 4. Calculation of Hydrostatic Values by Using Simpson's Rule

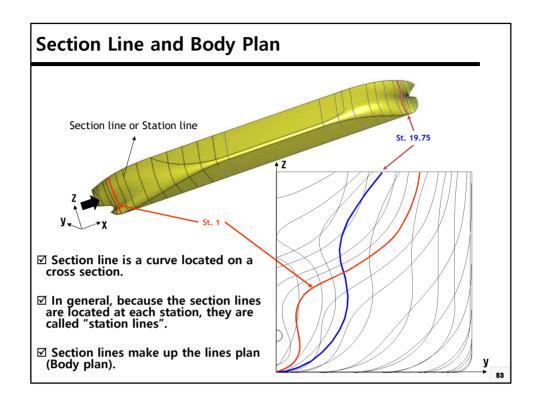
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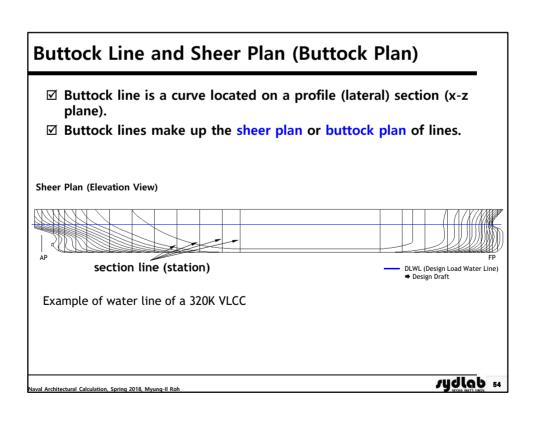
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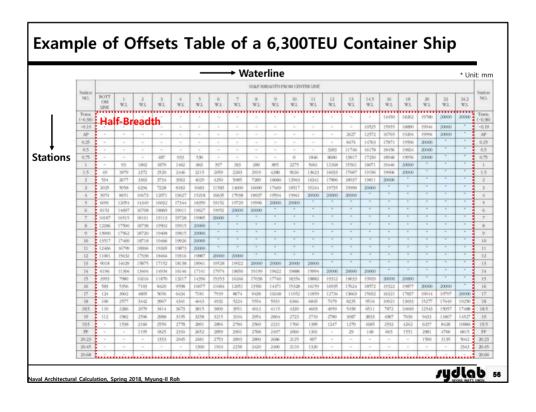


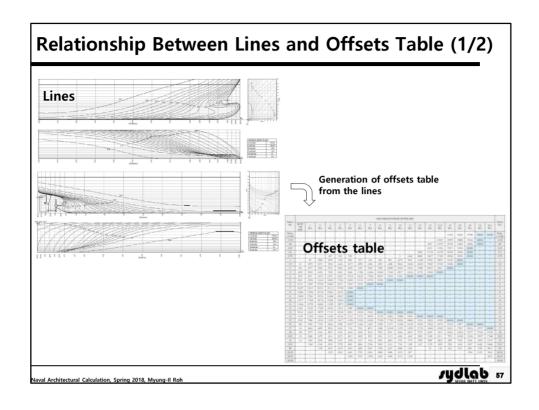


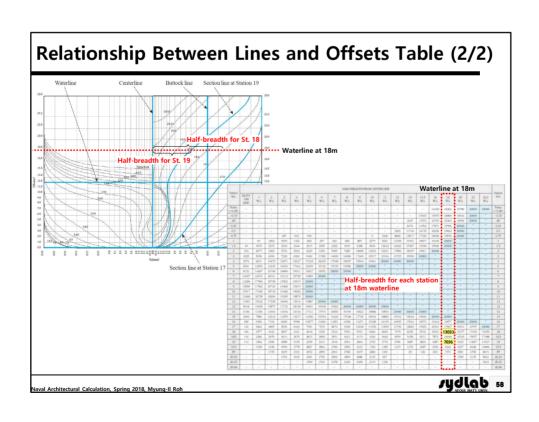




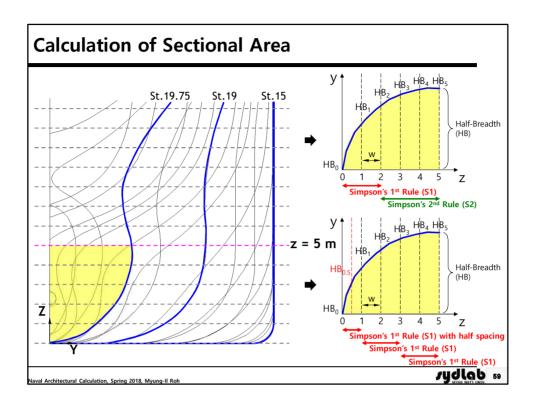
# Water Line and Water Plan (Half-Breadth Plan) ✓ Water line is a curve located on a water plane (vertical) section (x-y plane). ✓ Water lines make up the water plan or half-breadth plan of lines. Water Plan (Plan View) — DLWL (Design Load Water Line) Design Draft Example of water line of a 320K VLCC











### **Calculation of the First Moment of Sectional Area**

$$Area_1 = \int dA = \frac{1}{3}s(y_0 + 4y_1 + y_2) = \frac{1}{3}w(HB_0 + 4HB_1 + HB_2)$$

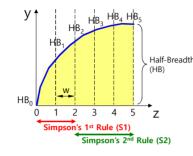
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### **Calculation of the First Moment of Sectional Area**

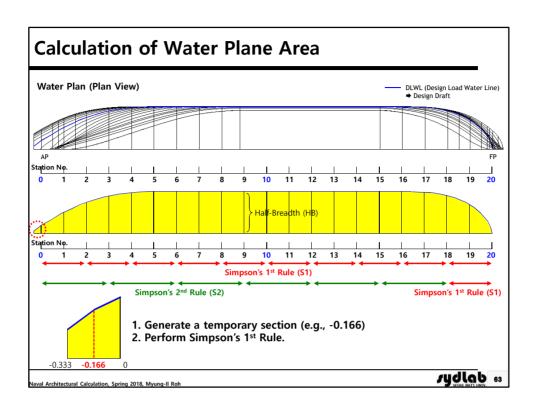
### Calculation of the First Moment of Sectional Area (about z axis)



$$\begin{split} M_{z,1} &= \int z dA = \frac{1}{3} s(Y_0 + 4Y_1 + Y_2) \\ &= \frac{1}{3} s \left( 1 \cdot ((y_0 / 2) \cdot y_0) + 4 \cdot ((y_1 / 2) \cdot y_1) + 1 \cdot ((y_2 / 2) \cdot y_2) \right) \\ &= \frac{1}{3} w \left( 1 \cdot ((HB_0 / 2) \cdot HB_0) + 4 \cdot ((HB_1 / 2) \cdot HB_1) + 1 \cdot ((HB_2 / 2) \cdot HB_2) \right) \end{split}$$

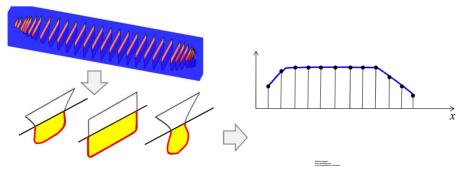
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### **Calculation of Displacement Volume**

☑ The displacement volume (underwater volume) at a certain draft can be calculated by integrating sectional areas in the longitudinal direction.



☑ In addition, the volume can be calculated by integrating water plane areas in the vertical direction. There can be a difference between two volumes due to approximation.

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### **Calculation for Wetted Surface Area**

- ☑ The wetted surface area means ship's area which contacts with water.
- ☑ This area can be calculated with the following approximate formula.

$$S = \mathcal{S}z \int_{Sta. \, 6}^{Sta. \, 6} \sqrt{1 + \left(\frac{dy}{dx}\right)^2 + \left(\frac{dy}{dz}\right)^2} dx$$

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 $\delta z = (6-3) = 3 \, m$ 67 10 MeV hadro make 10, MeV hadro make 10, MeV hadro make 10, MeV hadro make 10 MeV hadro make MeV 10, MeV 10





(1)	(1.1)	(1.2)	(2)	(3)	(4)	(4.1)	(4.2)	(5)	(5.1)	(5.2)	(6)	(7)	(8)	(9)	(10)	(11)
Sta.	HB 6m	HB 3m	δу/δz	(δy/δz) <sup>2</sup>	Sta. Ford.	HB 6m	HB 3m	Sta. Aft.	HB 6m	HB 3m	Mean δy/δx	(δy/δx) <sup>2</sup>	Sum	(Sum) <sup>1/2</sup>	S.M	Prod.
5	19,66	18.41	0.42	0.17	6	20,12	19.84	4	17.56	15,56	-0.12 (2)	0.01	1,18	1.09	1	1.09
4	17.56	15,47	0.70	0.49	5	19.66	18.41	3	13,38	11.16	-0.24	0,06	1.55	1.24	3	3.72
3	13,38	11,16	0,74	0,55	4	17,56	15,47	2	8,14	6,64	-0,33	0,11	1,66	1,29	3	3,87
2	8.14	6,64	0.50	0,25	3	13,38	11.16	1	2,62	2,16	-0,35	0,13	1,38	1.17	1, 444	1.69
11/2	5,43	4,39	0,35	0.12	2	8,14	6,64	1 (3)	2,62	2,16	-0,36	0,13	1,25	1,12	1,778	1,99
1	2.62	2,16	0.15	0.02	11/2	5,43	4,39	1/2	-0.22+	-0.28+	-0.37	0.14	1,16	1,08	0, 444	0.48
															Σ =	12.84

### 2. Substituting 1) and 2) into the formula.

$$S \approx \delta z \int_{Sta.5}^{Sta.5} \sqrt{1 + \left(\frac{\delta y}{\delta x}\right)^2 + \left(\frac{\delta y}{\delta z}\right)^2} dx$$

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(1)	(1.1)	(1.2)	(2)	(3)	(4)	(4.1)	(4.2)	(5)	(5.1)	(5.2)	(6)	(7)	(8)	(9)	(10)	(11)
Sta.	HB 6m	HB 3m	δу/δz	(δy/δz) <sup>2</sup>	Sta. Ford.	HB 6m	HB 3m	Sta. Aft.	HB 6m	HB 3m	Mean δy/δx	(δy/δx) <sup>2</sup>	Sum	(Sum) <sup>1/2</sup>	S.M	Prod.
5	19,66	18,41	0.42	0.17	6	20,12	19.84	4	17.56	15,56	-0.12 (2)	0.01	1,18	1.09	1	1.09
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3	13,38	11,16	0,74	0,55	4	17,56	15,47	2	8,14	6,64	-0,33	0,11	1,66	1,29	3	3,87
2	8.14	6,64	0.50	0,25	3	13,38	11.16	1	2,62	2,16	-0,35	0,13	1,38	1.17	1, 444	1.69
11/2	5,43	4,39	0,35	0,12	2	8,14	6,64	1 (3)	2,62	2,16	-0,36	0,13	1,25	1,12	1,778	1,99
1	2,62	2,16	0.15	0.02	11/2	5,43	4,39	1/2	-0.22+	-0.28+	-0,37	0.14	1,16	1.08	0, 444	0.48
															Σ =	12,84



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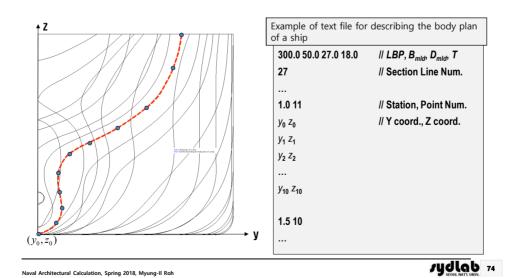
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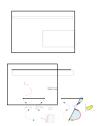


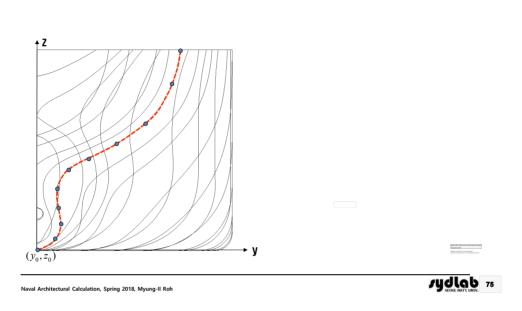
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# **Description of Section Lines (1/2)**









Given: B-spline curve, the intersection points between the B-spline curve and water plane, and B-spline parameter "u" at each end point of the line segments Find: Sectional area and 1st moment of section

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 $u = \frac{(t+1)(u_{\text{max}} - u_{\text{min}})}{2} + u_{\text{min}}$ 





**X** Method to check whether the line segments are located under the water plane or not

 $\mathbf{n} \cdot (\mathbf{X} - \mathbf{O}) > 0$ 







# Calculation of Water Plane Area, 1<sup>st</sup> and 2<sup>nd</sup> Moment of Water Plane Area

Given: Intersection points between the water plane and the section lines Find: Water plane area, 1st moment and 2nd moment of the water plane area

