

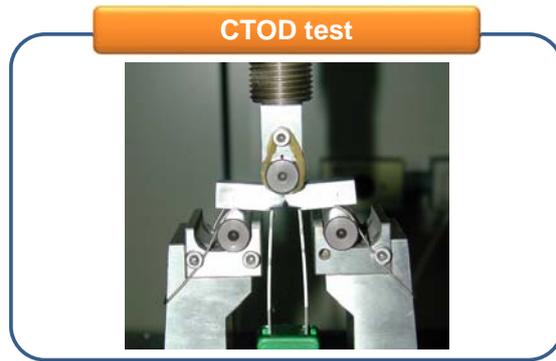
Instrumented Indentation Technique

(Tensile strength, Residual stress)

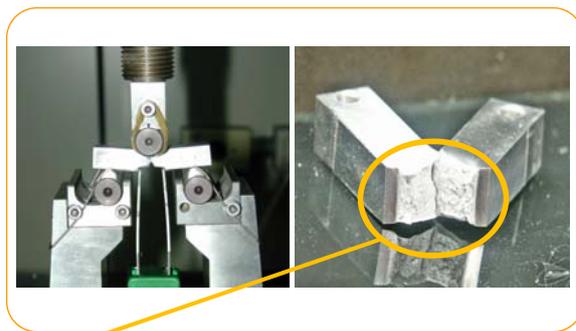
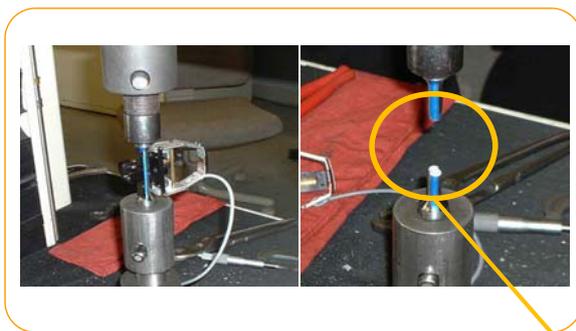
2014. 04. 29.
Jong hyoung Kim

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1. Instrumented Indentation Technique
 2. Strength
 3. Residual Stress

Mechanical Testing Methods



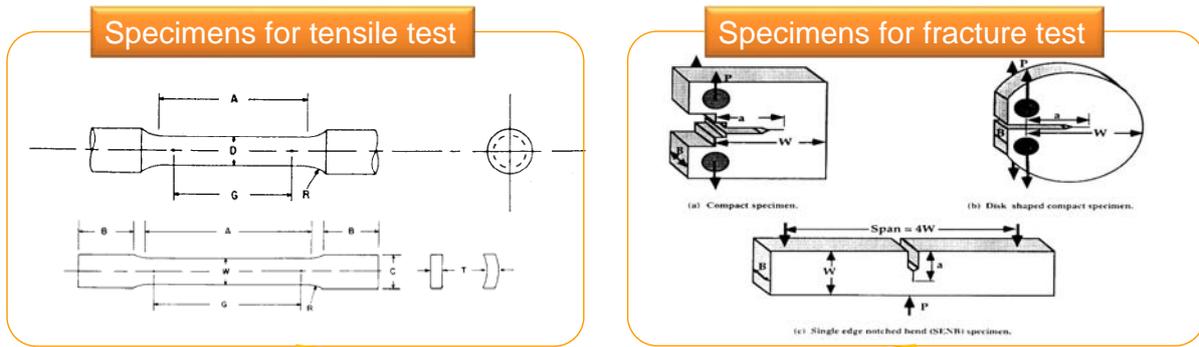
Limitation (1) - Destructive



Destructive !!!



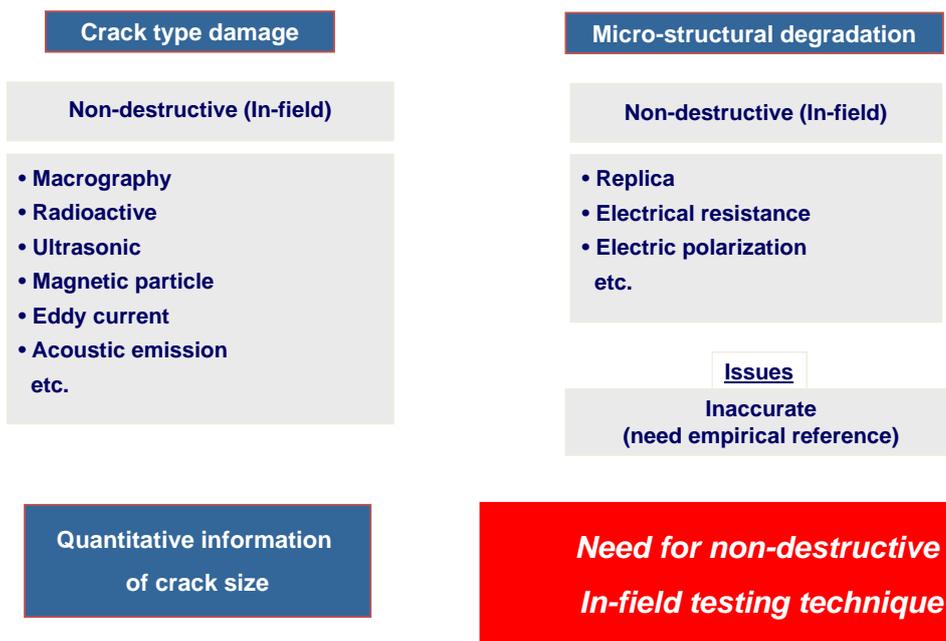
Limitation (2) – Large Scale



Large scale testing!!!



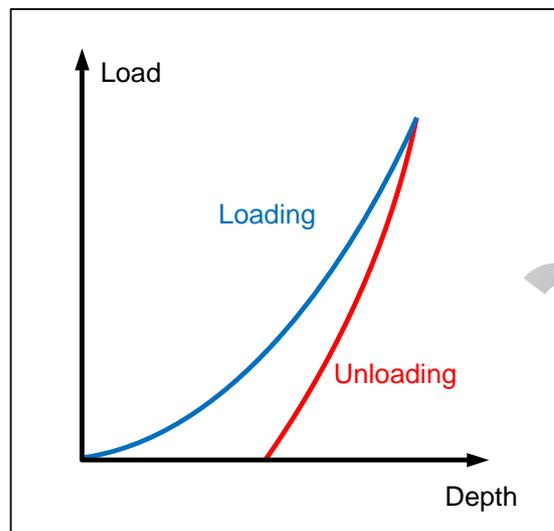
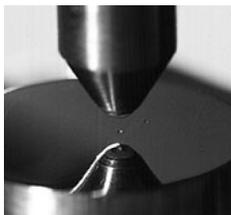
Conventional Non-destructive Tests



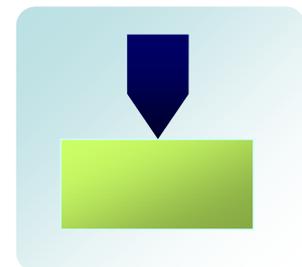
What is IIT?

Instrumented Indentation Test (1)

A novel method to characterize mechanical properties

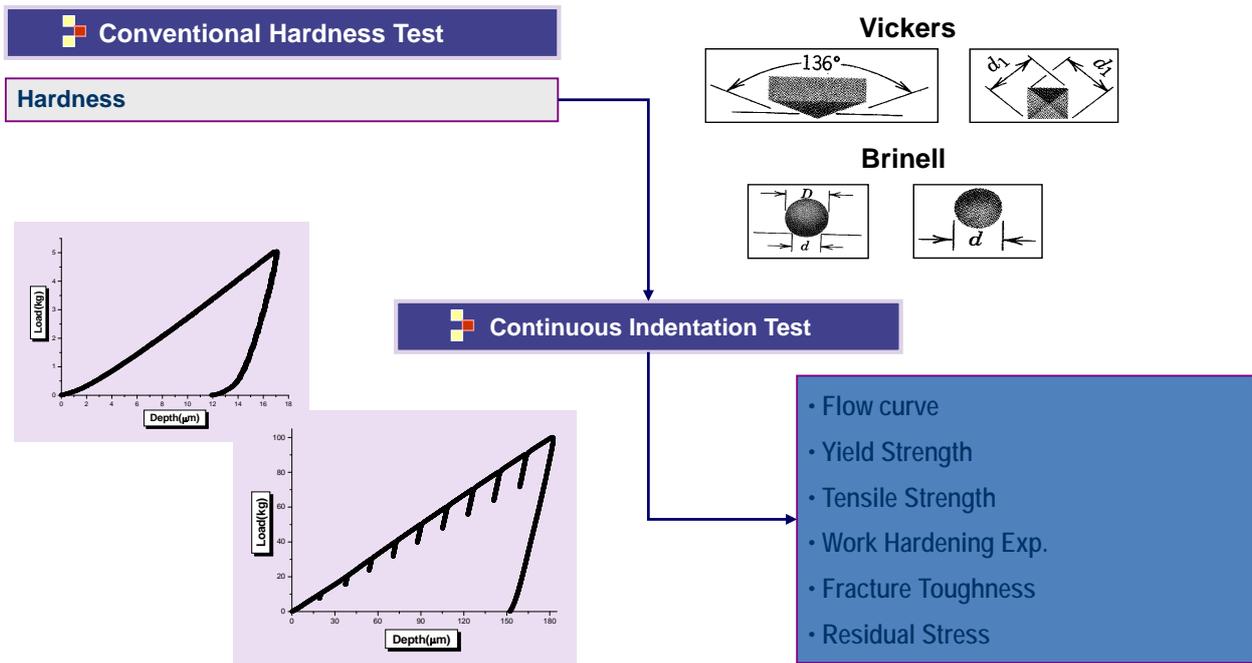


Indentation load-depth curve

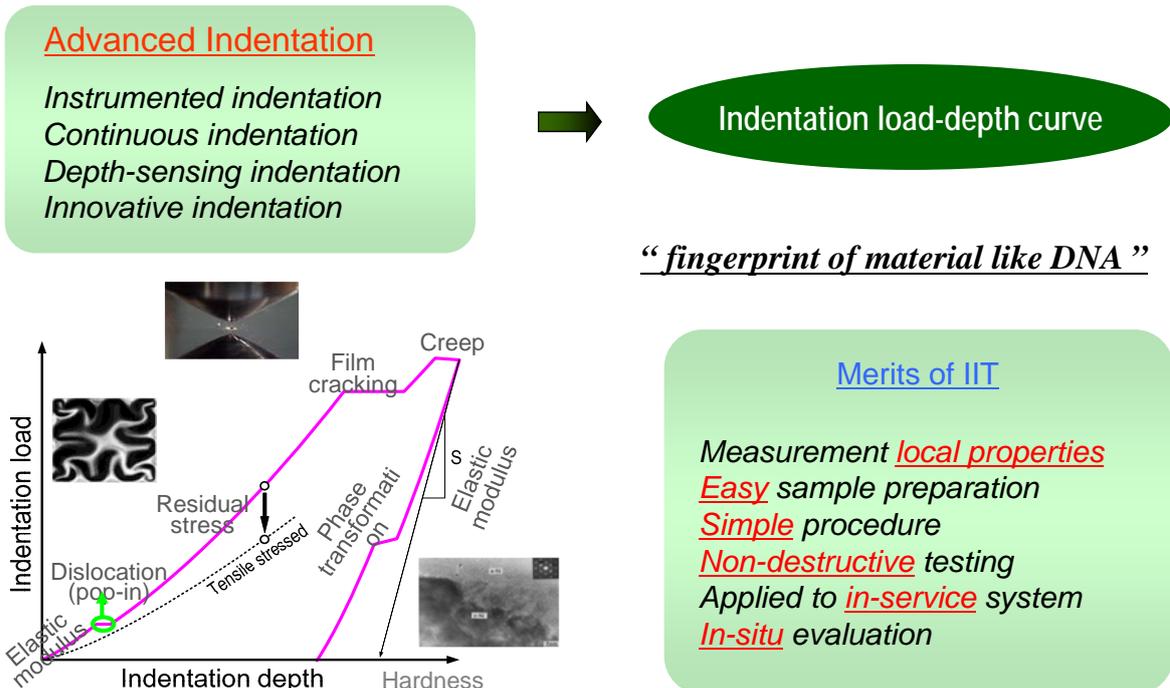


Hardness
Elastic modulus
Tensile properties
Residual stress
Fracture toughness

Instrumented Indentation Test (2)



Instrumented Indentation Test (3)



In-field & Nondestructive Test

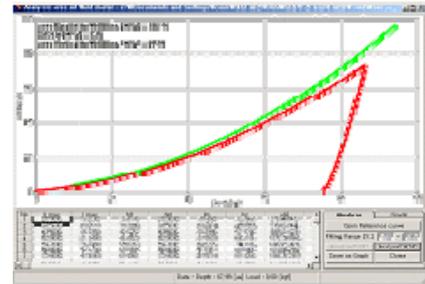
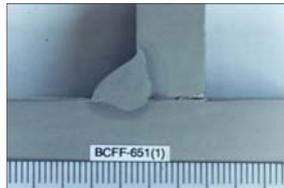
In-situ & In-field system



Simple & Fast

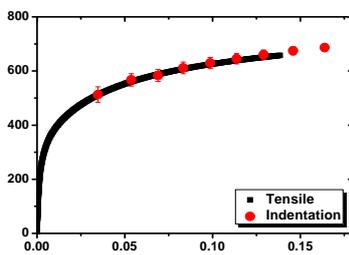
Convenient

Non-destructive & Local test



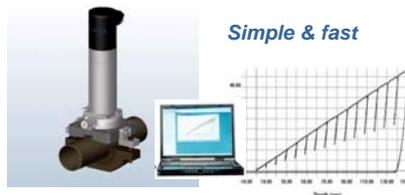
Various Properties

Tensile property



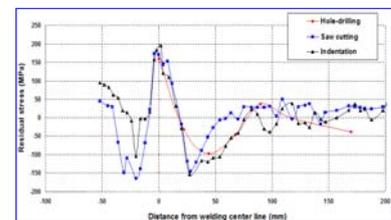
Uniaxial tensile test

Instrumented Indentation



Simple & fast

Residual stress



Hole drilling
Saw cutting
X-ray diffraction

Strength

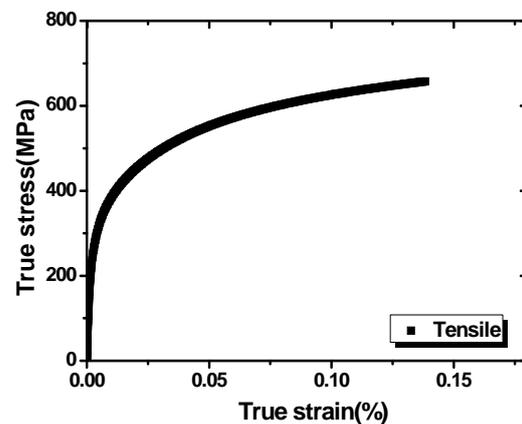
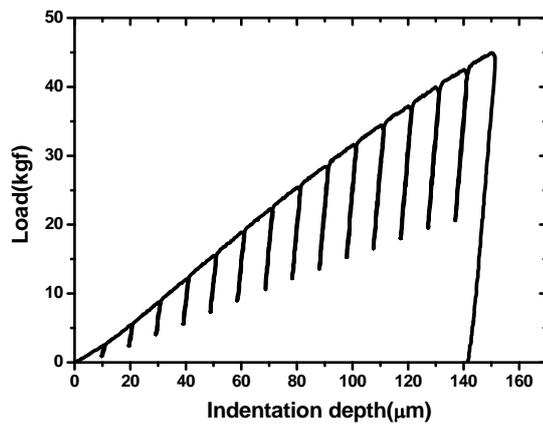
Evaluation of Strength using IIT

Can you imagine this?

Indentation curve



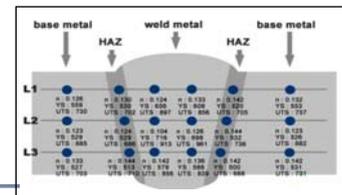
Tensile curve



(ISO/TR29381, 2008)

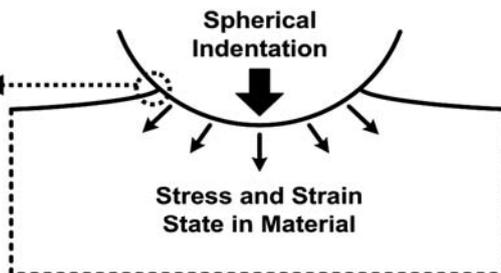


	Tensile Test	IIT
Property Characterized	Bulk (average)	Local (surface)
Testing Nature	Destructive	Non-destructive
Sample Preparation	Machining	Surface polishing
Potential Examples	Laboratory (conventional) Large volume	In-field Small volume



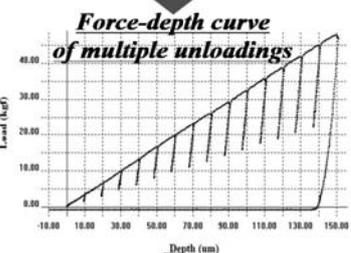
Algorithm for Strength Evaluation

◆ **Step 1**
Determining contact area
taking into consideration plastic pile-up/sink-in

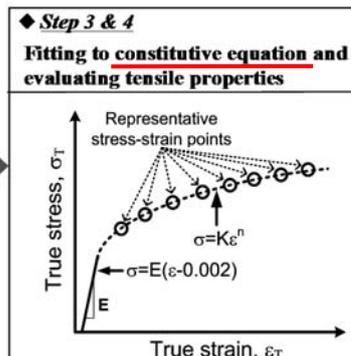
$$\frac{h_{pile}}{h_c^*} = f\left(n_{IT}, \frac{h_{max}}{R}\right)$$


[ISO/TR 29381, 2008]

Instrumented indentation test with a spherical indenter



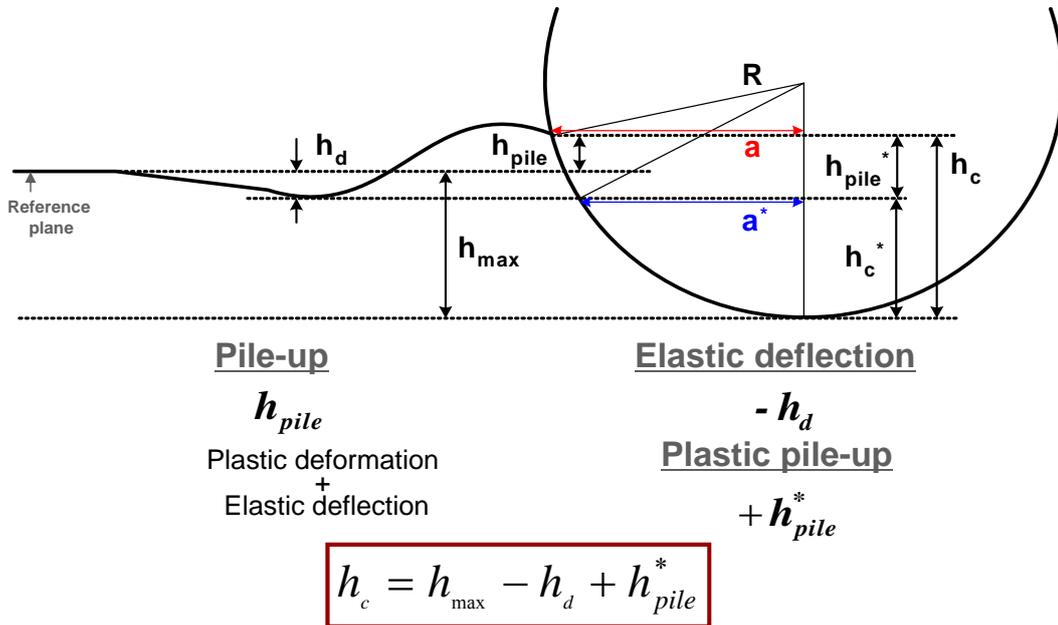
◆ **Step 2**
Defining stress and strain state
in materials underneath spherical indenter as representative stress and strain

$$\sigma_T = \frac{l}{\Psi} \frac{F_{max}}{A_c}, \quad \varepsilon_T = \alpha \tan \theta$$


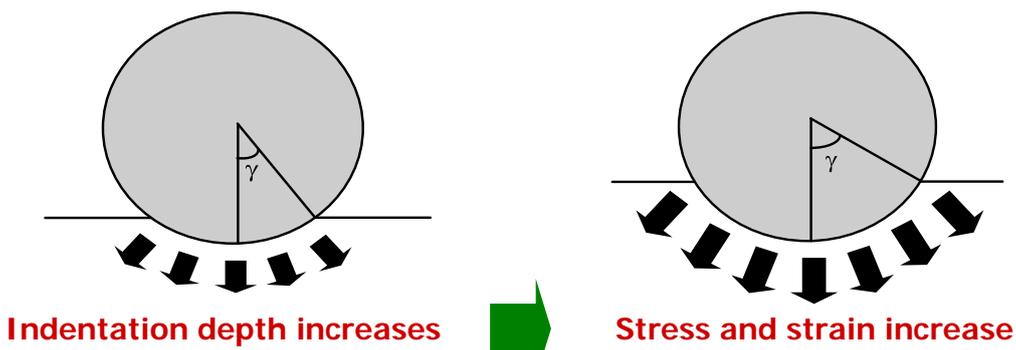
Tensile properties
 $\sigma_{y, IT}, \sigma_{u, IT}, n_{IT}, E_{IT}$

Step 1_Determination of Contact Area

Plastic pile-up & elastic deflection



Step 2_Representation of Stress & Strain



Representative Stress Definition

$$\sigma = \frac{1}{\Psi} \frac{L_{max}}{\pi a_c^2}$$

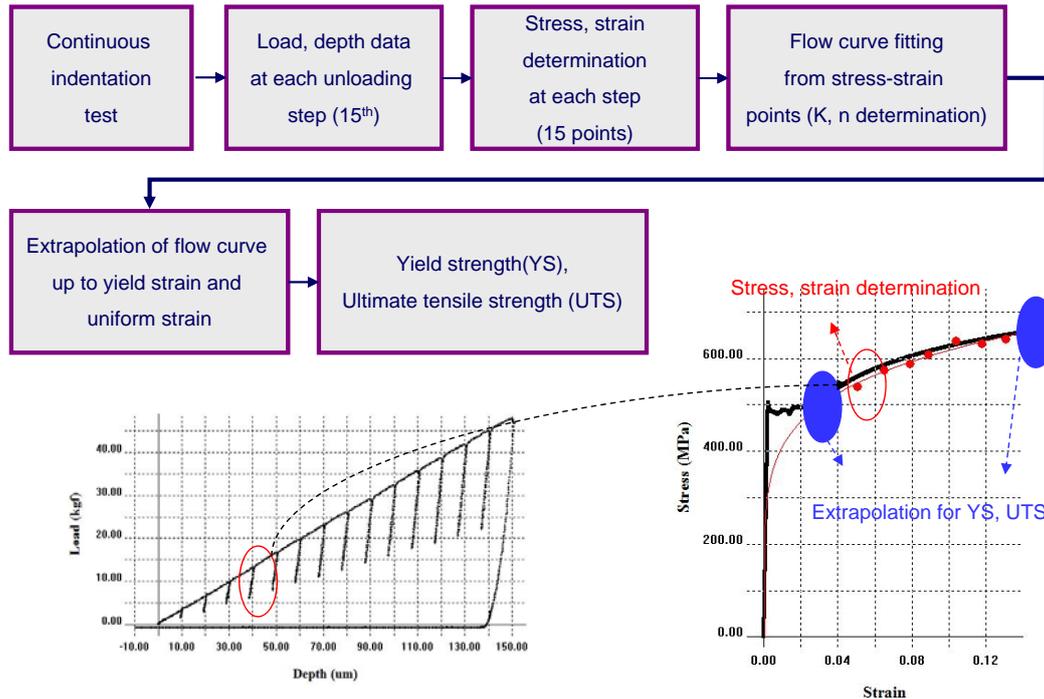
Ψ=3 for metallic material
(by D. Tabor)

Representative Strain Definition

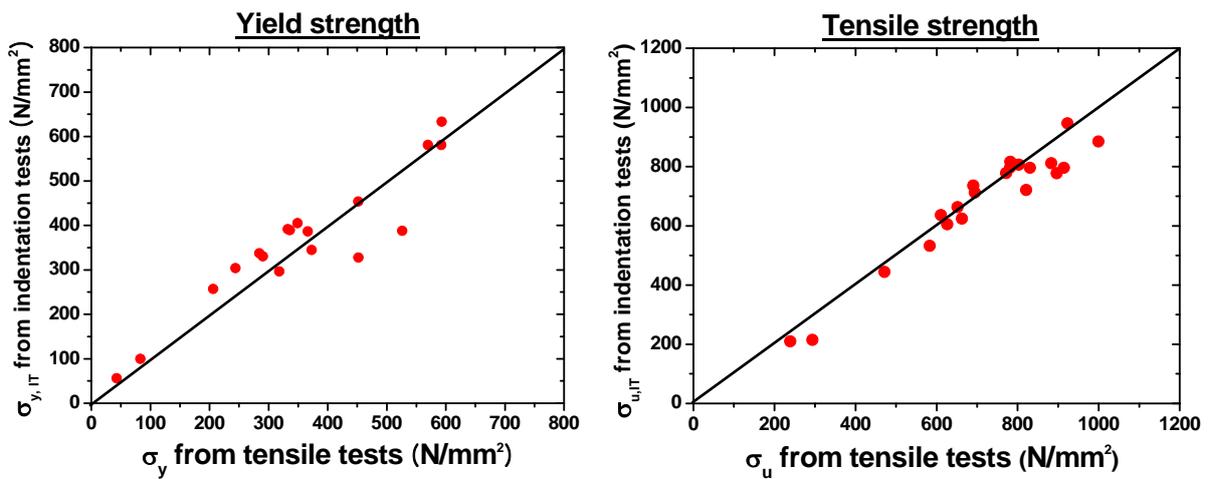
$$\varepsilon = f(a_c / R)$$

- Power-law hardening material
: 0.14tany
- Linear hardening material
: 0.3siny

Flow Chart for Tensile Curve Derivation Using IIT

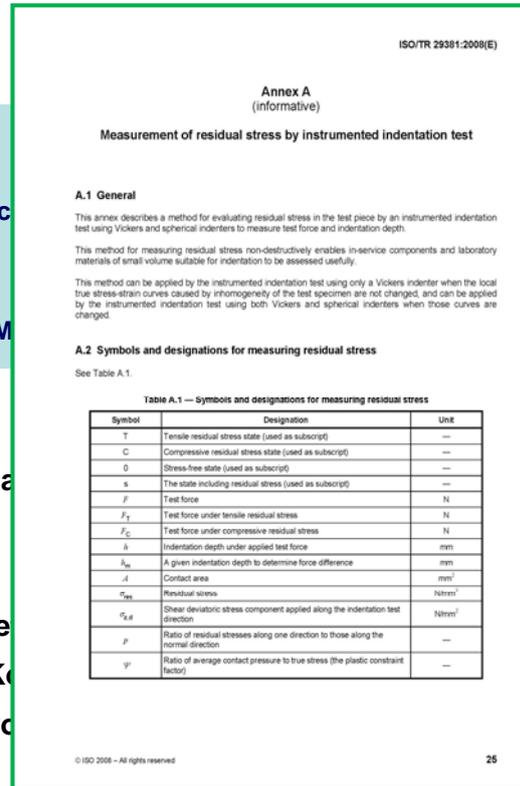
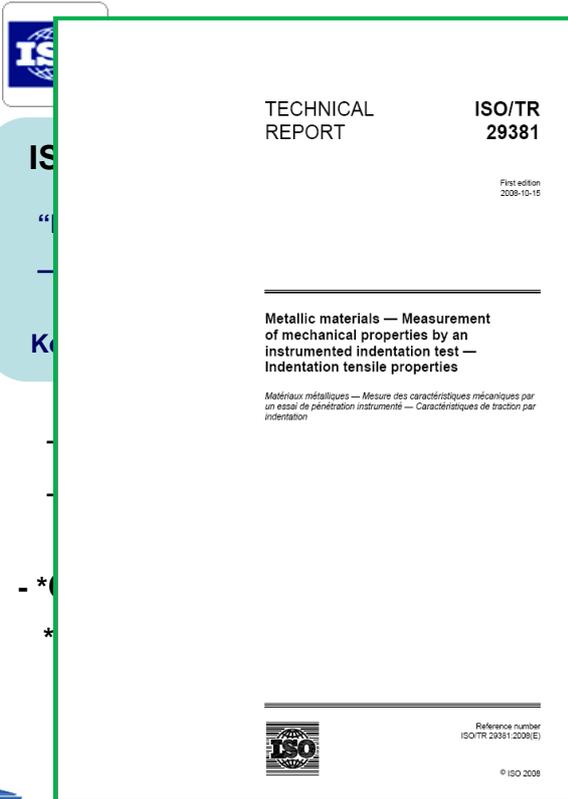


Results



Good agreement with results from tensile test

International Standardization Works (ISO)



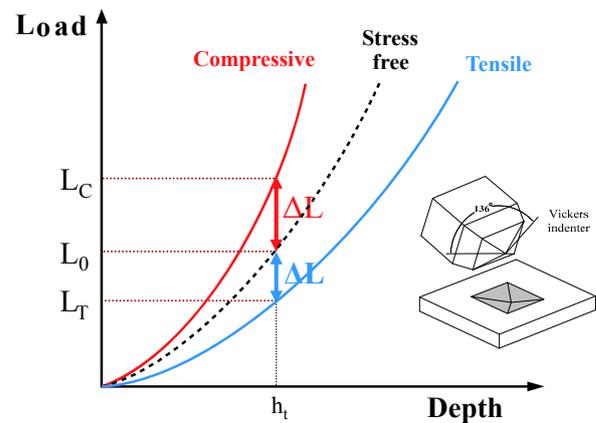
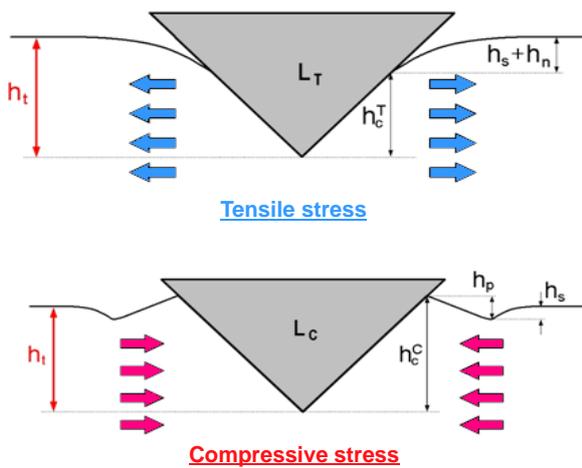
Residual Stress

Merits of IIT

	Method	Merit	Limitation
Mechanical Methods	Hole-Drilling	- Quantitative & mechanical analysis	- Destructive
	Saw-Cutting		
Physical Methods	X-Ray Diffraction	- Non-destructive	- Only crystalline materials - Sensitive to environment
	Neutron Diffraction		

Merit		
IIT	- <u>Quantitative & mechanical analysis</u>	- <u>Any materials possible</u>
	- <u>Non-destructive, can be used in field</u>	- <u>Microstructure not influenced</u>

Basic Principle

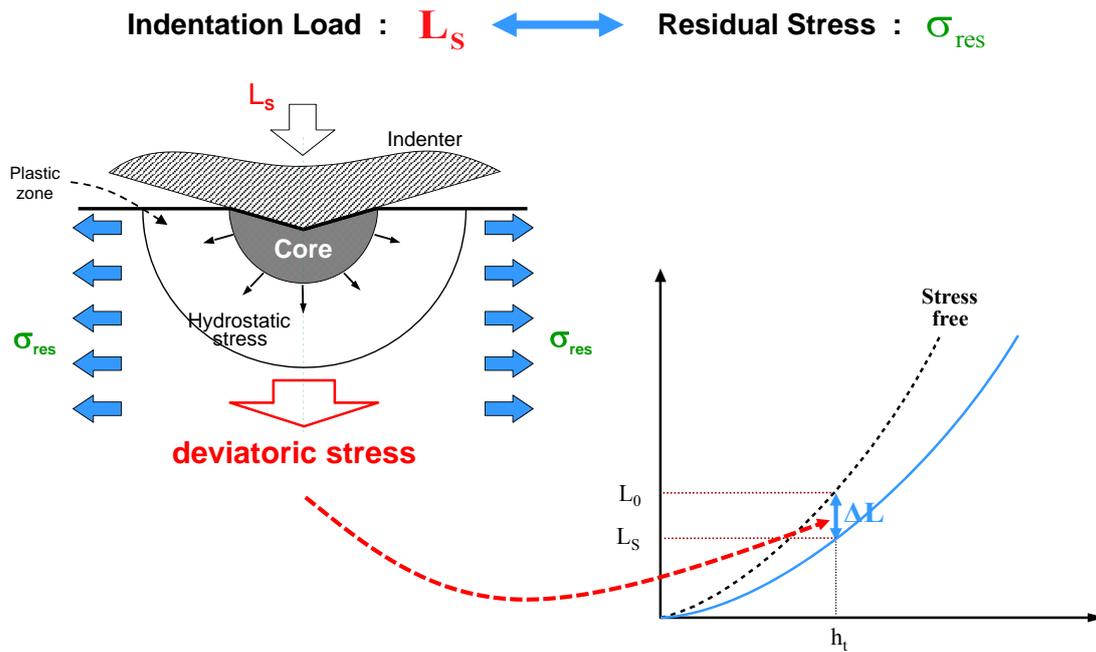


Indentation Load-Depth Curves

$$\Delta L = L_S - L_0$$

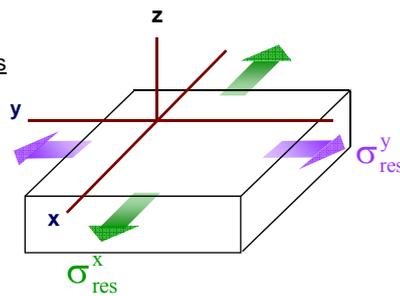
$$(L_S = L_T \text{ or } L_C)$$

Stress Interaction



Stress Tensor

Non-equibiaxial residual stress



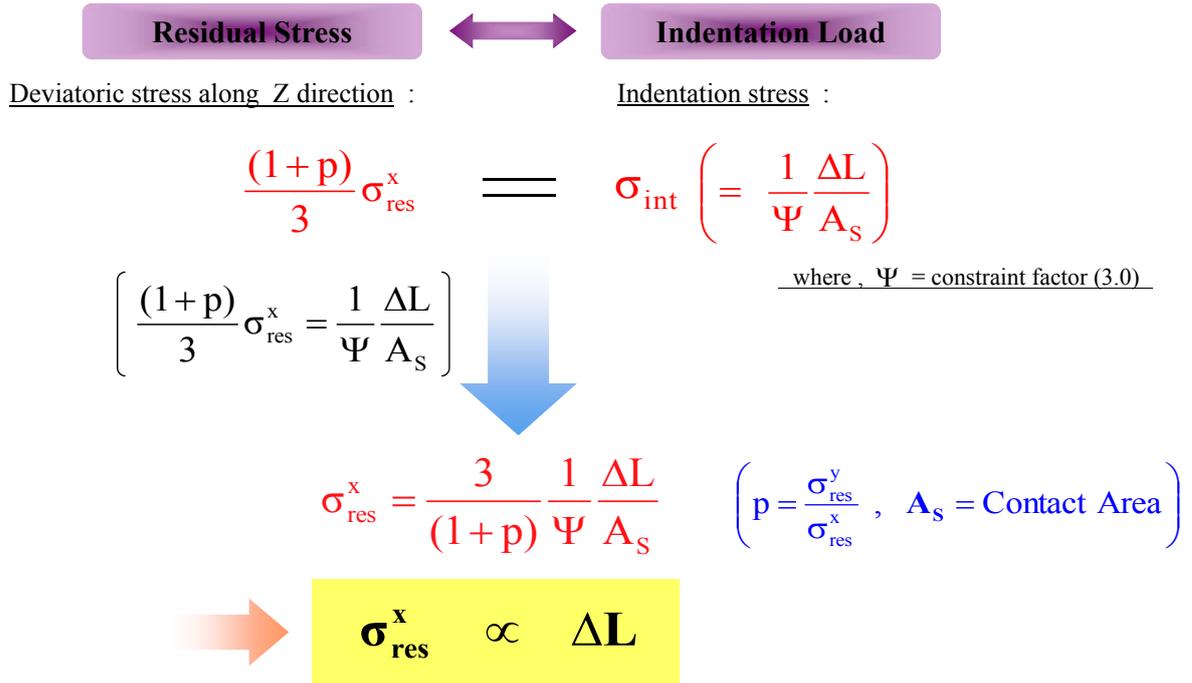
$$\text{Stress Ratio : } p = \frac{\sigma_{res}^y}{\sigma_{res}^x}$$

$$\begin{pmatrix} \sigma_{res}^x & 0 & 0 \\ 0 & \sigma_{res}^y & 0 \\ 0 & 0 & 0 \end{pmatrix} = \begin{pmatrix} \sigma_{res}^x & 0 & 0 \\ 0 & p\sigma_{res}^x & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

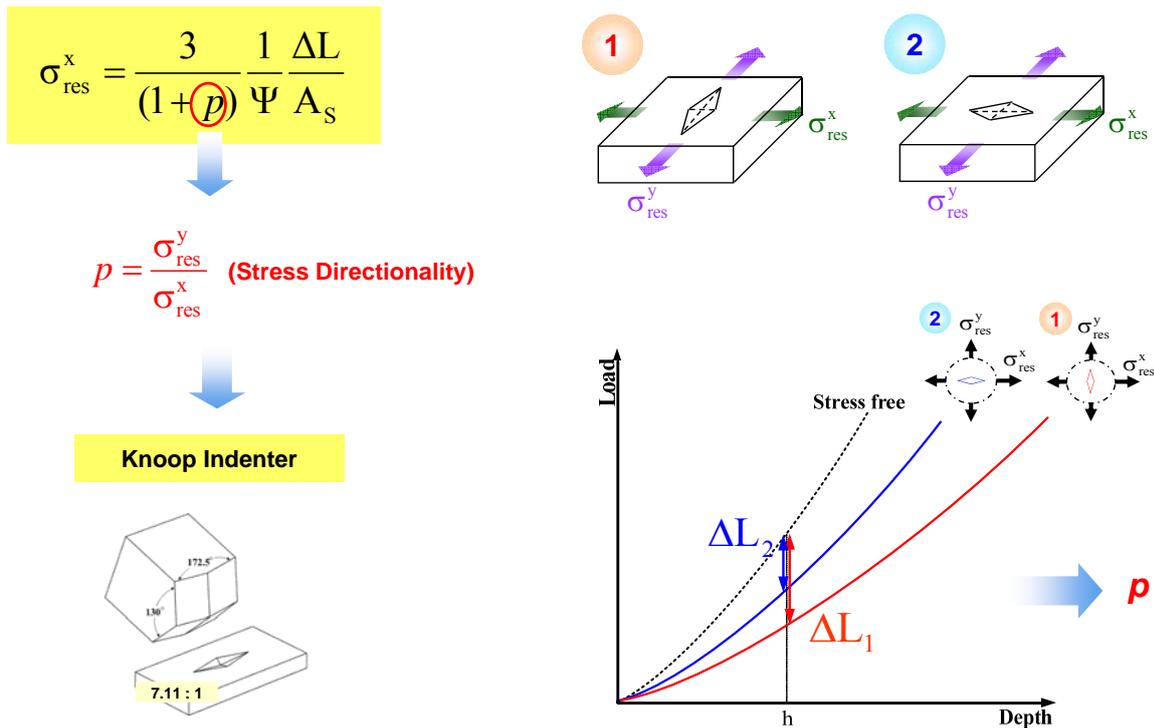
$$= \begin{pmatrix} \frac{(1+p)}{3}\sigma_{res}^x & 0 & 0 \\ 0 & \frac{(1+p)}{3}\sigma_{res}^x & 0 \\ 0 & 0 & \frac{(1+p)}{3}\sigma_{res}^x \end{pmatrix} + \begin{pmatrix} \frac{(2-p)}{3}\sigma_{res}^x & 0 & 0 \\ 0 & \frac{(2p-1)}{3}\sigma_{res}^x & 0 \\ 0 & 0 & -\frac{(1+p)}{3}\sigma_{res}^x \end{pmatrix}$$

hydrostatic stress
deviatoric stress

Evaluation of Residual Stress by IIT

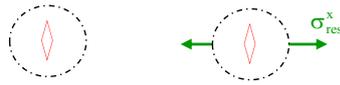


Directionality using Knoop Indenter



Determination of Conversion Factors

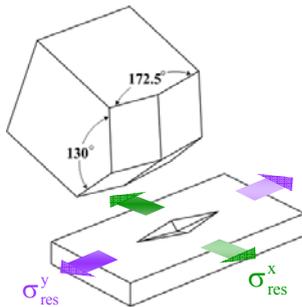
Stress-free Uni-axial stress



Comparison of indentation curves

$$\Delta L \approx \alpha_{\perp} \sigma_{res}^x$$

conversion factor in normal direction



Stress-free Uni-axial stress



Comparison of indentation curves

$$\Delta L \approx \alpha_{//} \sigma_{res}^y$$

conversion factor in parallel direction

α_{\perp} , $\alpha_{//}$ are conversion factors that are depth variables relating the residual stress to the indentation load difference

It can be proved that the ratio of conversion factors is constant.

$$\frac{\alpha_{//}}{\alpha_{\perp}} \approx 0.34 \quad (\text{from experiments})$$

Direct Summation

$$\begin{array}{c}
 \begin{array}{ccc}
 \begin{array}{c} \sigma_{res}^y \\ \uparrow \\ \text{---} \\ \downarrow \\ \sigma_{res}^y \end{array} & & \begin{array}{c} \sigma_{res}^x \\ \rightarrow \\ \text{---} \\ \leftarrow \\ \sigma_{res}^x \end{array} \\
 \text{---} & & \text{---} \\
 \leftarrow & & \rightarrow \\
 \text{---} & & \text{---} \\
 \downarrow & & \downarrow \\
 \sigma_{res}^y & & \sigma_{res}^y
 \end{array}
 \end{array}
 =
 \begin{array}{c}
 \begin{array}{c} \sigma_{res}^x \\ \rightarrow \\ \text{---} \\ \leftarrow \\ \sigma_{res}^x \end{array} \\
 \text{---} \\
 \leftarrow \\
 \text{---} \\
 \downarrow \\
 \sigma_{res}^y
 \end{array}
 +
 \begin{array}{c}
 \begin{array}{c} \sigma_{res}^y \\ \uparrow \\ \text{---} \\ \downarrow \\ \sigma_{res}^y \end{array} \\
 \text{---} \\
 \leftarrow \\
 \text{---} \\
 \downarrow \\
 \sigma_{res}^y
 \end{array}
 \end{array}$$

$$\Delta L_1 = \alpha_{\perp} \sigma_{res}^x + \alpha_{//} \sigma_{res}^y$$

$$\begin{array}{c}
 \begin{array}{ccc}
 \begin{array}{c} \sigma_{res}^y \\ \uparrow \\ \text{---} \\ \downarrow \\ \sigma_{res}^y \end{array} & & \begin{array}{c} \sigma_{res}^x \\ \rightarrow \\ \text{---} \\ \leftarrow \\ \sigma_{res}^x \end{array} \\
 \text{---} & & \text{---} \\
 \leftarrow & & \rightarrow \\
 \text{---} & & \text{---} \\
 \downarrow & & \downarrow \\
 \sigma_{res}^y & & \sigma_{res}^y
 \end{array}
 \end{array}
 =
 \begin{array}{c}
 \begin{array}{c} \sigma_{res}^x \\ \rightarrow \\ \text{---} \\ \leftarrow \\ \sigma_{res}^x \end{array} \\
 \text{---} \\
 \leftarrow \\
 \text{---} \\
 \downarrow \\
 \sigma_{res}^y
 \end{array}
 +
 \begin{array}{c}
 \begin{array}{c} \sigma_{res}^y \\ \uparrow \\ \text{---} \\ \downarrow \\ \sigma_{res}^y \end{array} \\
 \text{---} \\
 \leftarrow \\
 \text{---} \\
 \downarrow \\
 \sigma_{res}^y
 \end{array}
 \end{array}$$

$$\Delta L_2 = \alpha_{//} \sigma_{res}^x + \alpha_{\perp} \sigma_{res}^y$$

Knopp Indentation Modeling

$$\frac{\Delta L_2}{\Delta L_1} = \frac{\alpha_{//} \sigma_{res}^x + \alpha_{\perp} \sigma_{res}^y}{\alpha_{\perp} \sigma_{res}^x + \alpha_{//} \sigma_{res}^y} \Rightarrow \frac{\alpha_{//} + \frac{\sigma_{res}^y}{\sigma_{res}^x}}{\alpha_{\perp} + \frac{\sigma_{res}^y}{\sigma_{res}^x}} = \frac{\alpha_{//} + p}{\alpha_{\perp} + p}$$

$$1 + \frac{\alpha_{//} \sigma_{res}^y}{\alpha_{\perp} \sigma_{res}^x} = 1 + \frac{\alpha_{//} p}{\alpha_{\perp}}$$

$$\frac{\Delta L_2}{\Delta L_1} = \frac{\alpha_{//} + p}{\alpha_{\perp} + \frac{\alpha_{//}}{\alpha_{\perp}} p}$$

$$\frac{\alpha_{//}}{\alpha_{\perp}} \approx 0.34$$

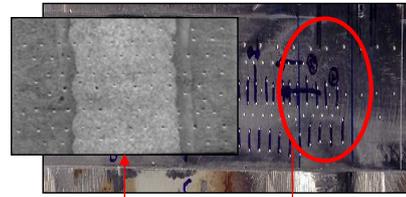
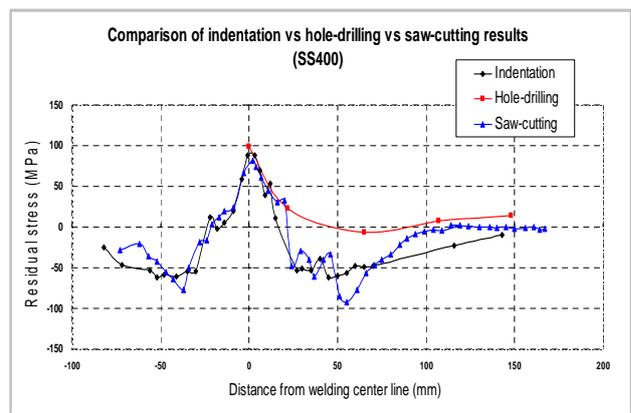
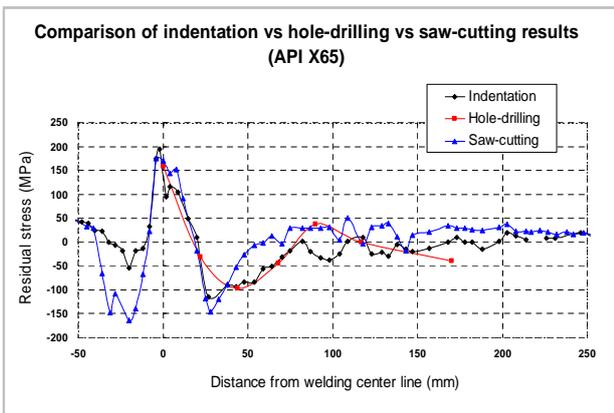
$$p = \frac{\sigma_{res}^y}{\sigma_{res}^x} = \frac{\frac{\Delta L_2}{\Delta L_1} - 0.34}{1 - 0.34 \frac{\Delta L_2}{\Delta L_1}}$$

Experimental data

Experimental Verification

API X65

SS400





**Thank You
for Your Attention**

