

# Chap.6 The Impulse–Momentum Principle

- So far, we have studied the flow characteristics (velocity, pressure, etc.) in a fluid. In this chapter, we study the force acting on a structure by fluid in a flow. As for the force acting on a structure in quiescent fluid, we studied it in Chapter 2.
- Newton's 2nd law (in a vector form):

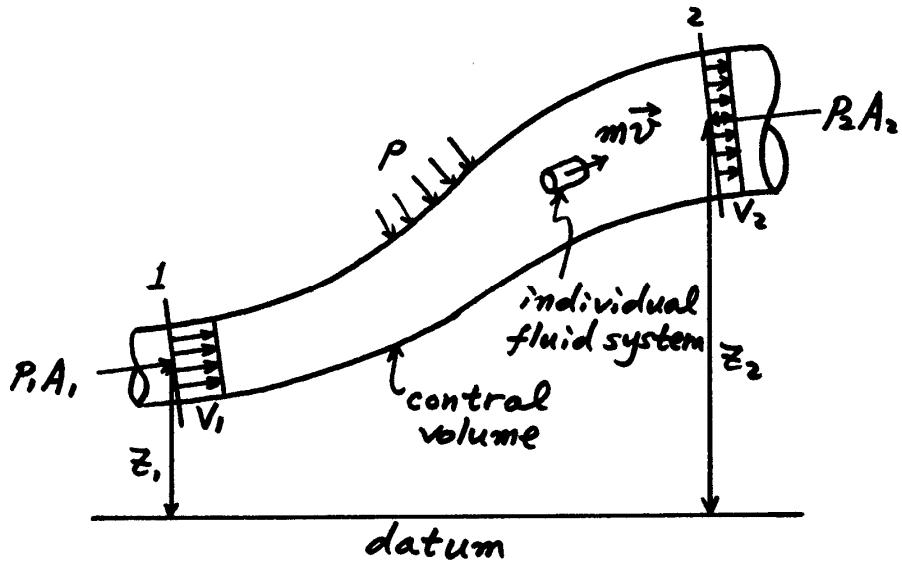
$$\sum \vec{F} = m\vec{a}_c = \frac{d}{dt}(\vec{m}\vec{v}_c)$$

where  $\vec{v}_c$  = velocity of the center of mass of the system

$$\underbrace{\left( \sum \vec{F} \right) dt}_{\substack{\text{impulse in} \\ \text{the time } dt}} = d \underbrace{\left( \vec{m}\vec{v}_c \right)}_{\substack{\text{linear} \\ \text{momentum}}}$$

- Linear impulse–momentum equation
  - magnitude and direction of resultant forces exerted on fluid by structures (or on structures by fluid)
- Angular impulse–momentum equation
  - line of action of the resultant force

## 6.1 Linear Impulse-Momentum Equation



For the individual fluid system,

$$\sum \vec{F} = \vec{ma} = \frac{d}{dt}(\vec{mv}) = \frac{d}{dt}(\rho \vec{v} dV)$$

Summation over the whole flow system:

$$\begin{aligned}\sum \vec{F}_{\text{ext}} &= \iiint_{\text{system}} \frac{d}{dt}(\rho \vec{v} dV) = \frac{d}{dt} \iiint_{\text{system}} \rho \vec{v} dV \\ &= \iint_{\text{CS}_{\text{out}}} \rho \vec{v} (\vec{v} \cdot \vec{n} dA) + \iint_{\text{CS}_{\text{in}}} \rho \vec{v} (\vec{v} \cdot \vec{n} dA) \\ &= \rho_2 \vec{V}_2 Q_2 - \rho_1 \vec{V}_1 Q_1 = Q \rho (\vec{V}_2 - \vec{V}_1)\end{aligned}$$

where  $\sum \vec{F}_{\text{ext}} = \text{body force} + \text{forces on C.S.}$

( $\because$  all the internal forces b/w individual fluid systems are cancelled out)

$$\therefore \sum \vec{F}_{\text{ext}} = Q\rho(\vec{V}_2 - \vec{V}_1)$$

In a 2-D flow ( $x$  and  $z$ ),

$$\left. \begin{aligned} (\sum F_{\text{ext}})_x &= Q\rho(V_{2_x} - V_{1_x}) \\ (\sum F_{\text{ext}})_z &= Q\rho(V_{2_z} - V_{1_z}) \end{aligned} \right\}$$



Magnitude and direction of  $\sum \vec{F}_{\text{ext}}$ .

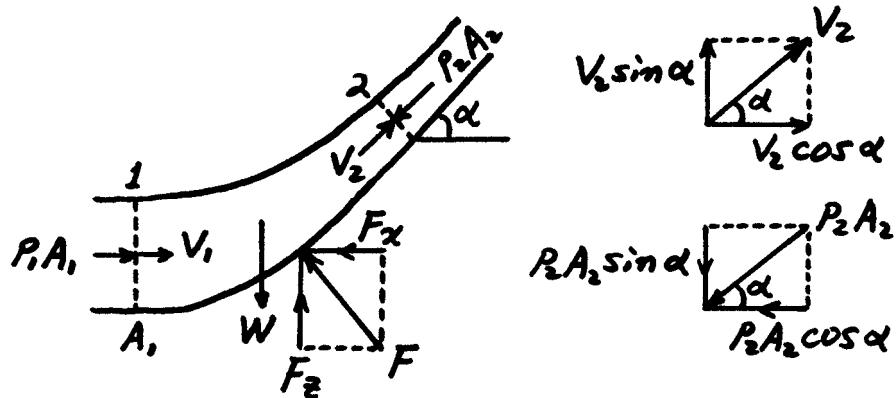
But line of action is not known yet.

If the flow enters and leaves at more than one location,

$$\sum \vec{F}_{\text{ext}} = \left( \sum Q\rho \vec{V} \right)_{\text{out}} - \left( \sum Q\rho \vec{V} \right)_{\text{in}}$$

## 6.2 Pipe Flow Applications

### (1) Force acting on pipe bend



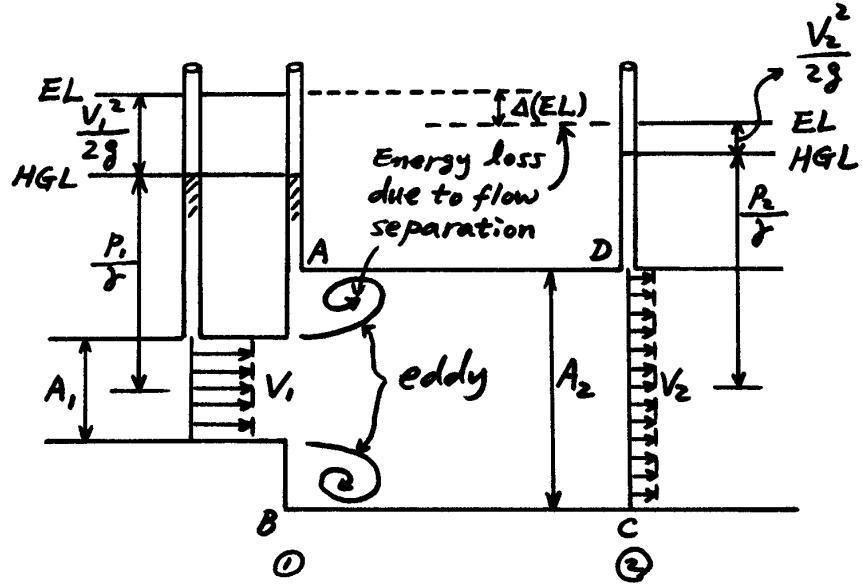
$$x: p_1 A_1 - p_2 A_2 \cos \alpha - F_x = Q\rho(V_2 \cos \alpha - V_1)$$

$$F_x = p_1 A_1 - p_2 A_2 \cos \alpha - Q\rho(V_2 \cos \alpha - V_1)$$

$$z: -W - p_2 A_2 \sin \alpha + F_z = Q\rho(V_2 \sin \alpha - 0)$$

$$F_z = W + p_2 A_2 \sin \alpha + Q\rho V_2 \sin \alpha$$

## (2) Energy loss at abrupt expansion of a passage



Impulse-momentum equation on C.V. ABCD:

$$\sum F_x \approx p_1 A_2 - p_2 A_2 = Q \rho (V_2 - V_1) = A_2 V_2 \rho (V_2 - V_1)$$

Note:  $p$  may be different from  $p_1$  in eddy area.

$$\therefore \frac{p_1 - p_2}{\gamma} = \frac{V_2(V_2 - V_1)}{g}$$

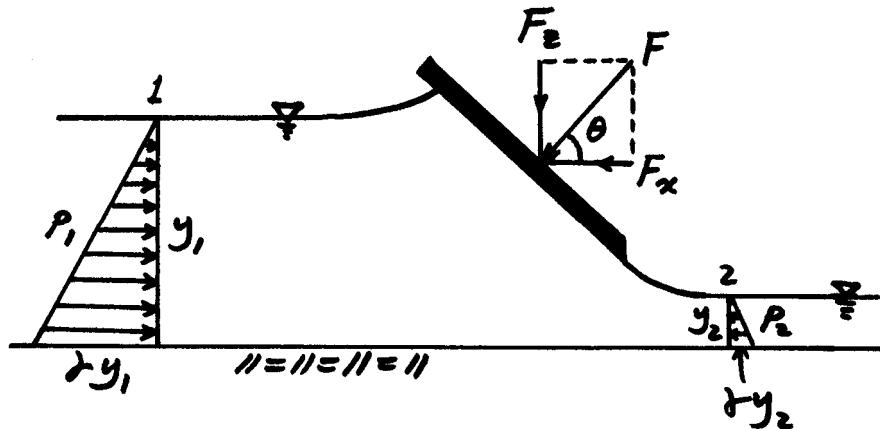
Work-energy equation:

$$\frac{p_1}{\gamma} + \frac{V_1^2}{2g} - \Delta(\text{EL}) = \frac{p_2}{\gamma} + \frac{V_2^2}{2g}$$

$$\begin{aligned} \therefore \Delta(\text{EL}) &= \frac{p_1 - p_2}{\gamma} + \frac{V_1^2 - V_2^2}{2g} = \frac{V_2(V_2 - V_1)}{g} + \frac{V_1^2 - V_2^2}{2g} \\ &= \frac{(V_1 - V_2)^2}{2g} : \text{Borda-Carnot head loss} \end{aligned}$$

## 6.3 Open Channel Flow Applications

### (1) Force acting on a sluice gate



$$\left( \sum F_{\text{ext}} \right)_x = \frac{\gamma y_1^2}{2} - \frac{\gamma y_2^2}{2} - F_x = Q\rho(V_2 - V_1) = q\rho \left( \frac{q}{y_2} - \frac{q}{y_1} \right)$$

$$\therefore F_x = \frac{\gamma}{2} (y_1^2 - y_2^2) - q^2 \rho \left( \frac{1}{y_2} - \frac{1}{y_1} \right)$$

$\vec{F} \perp$  gate ( $\because$  no shear force for ideal fluid)

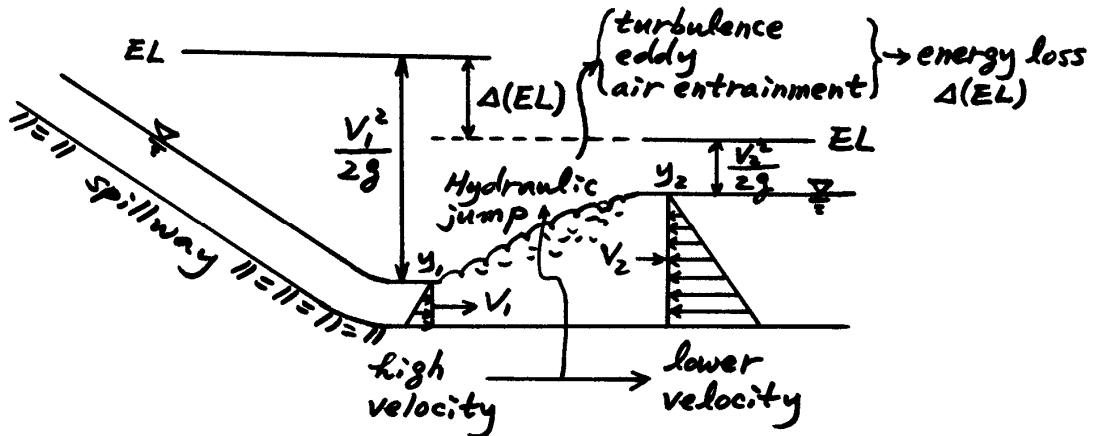
$$\therefore F \cos \theta = F_x \rightarrow F = \frac{F_x}{\cos \theta}$$

$$F_z = F \sin \theta$$

No need for impulse-momentum equation in  $z$ -direction.

See IP 6.2 (p 197) for horizontal force acting on an overflow structure (same principle).

## (2) Energy loss due to hydraulic jump



Impulse-momentum equation:

$$\left(\sum F_{\text{ext}}\right)_x = \frac{\gamma_1^2}{2} - \frac{\gamma_2^2}{2} = q\rho(V_2 - V_1) \quad \leftarrow \text{no structure}$$

no external force by structure

$$\text{Continuity: } q = V_1 y_1 = V_2 y_2 \rightarrow V_1 = \frac{q}{y_1}, \quad V_2 = \frac{q}{y_2}$$

$$\therefore \frac{\rho g}{2} \left( y_1^2 - y_2^2 \right) = q^2 \rho \left( \frac{1}{y_2} - \frac{1}{y_1} \right)$$

$$y_2^2 - y_1^2 = \frac{2q^2}{g} \left( \frac{1}{y_1} - \frac{1}{y_2} \right)$$

$$(y_2 + y_1)(y_2 - y_1) = \frac{2q^2}{g} \frac{y_2 - y_1}{y_1 y_2}$$

$$\left( \frac{y_2}{y_1} \right)^2 + \frac{y_2}{y_1} - \frac{2q^2}{gy_1^3} = 0$$

$$\therefore \frac{y_2}{y_1} = \frac{1}{2} \left( -1 + \sqrt{1 + \frac{8q^2}{gy_1^3}} \right) = \frac{1}{2} \left( -1 + \sqrt{1 + \frac{8V_1^2}{gy_1}} \right)$$

(a)  $\mathbf{F}_1^2 = \frac{V_1^2}{gy_1} = 1 \rightarrow \frac{y_2}{y_1} = 1$ ; no hydraulic jump

(b)  $\mathbf{F}_1^2 = \frac{V_1^2}{gy_1} > 1 \rightarrow \frac{y_2}{y_1} > 1$ ; hydraulic jump occurs

(c)  $\mathbf{F}_1^2 = \frac{V_1^2}{gy_1} < 1 \rightarrow \frac{y_2}{y_1} < 1$ ; physically impossible

Note:  $\mathbf{F} = \frac{V}{\sqrt{gy}}$  = Froude number

$$\Delta(\text{EL}) = \left( y_1 + \frac{V_1^2}{2g} \right) - \left( y_2 + \frac{V_2^2}{2g} \right) = \left( y_1 + \frac{q^2}{2gy_1^2} \right) - \left( y_2 + \frac{q^2}{2gy_2^2} \right)$$

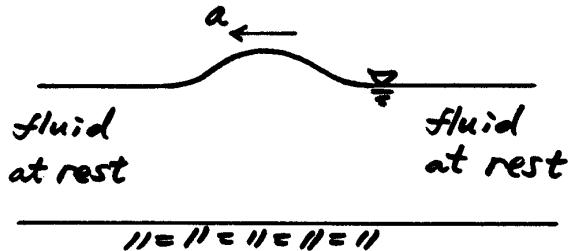
Using  $q^2 = \frac{g}{2} y_1 y_2 (y_1 + y_2)$

$$\Delta(\text{EL}) = \frac{(y_2 - y_1)^3}{4y_1 y_2} > 0 \text{ for energy loss}$$

$\therefore y_2 > y_1 \rightarrow \frac{y_2}{y_1} > 1$

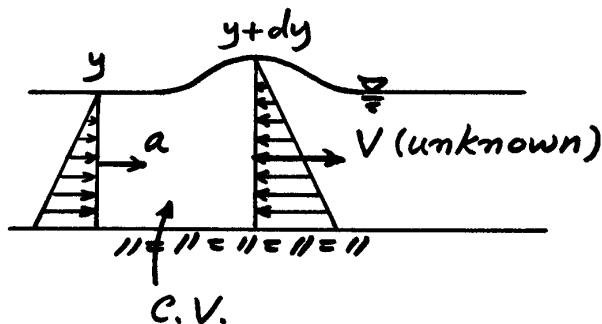
### (3) Velocity of small gravity waves

↳ not fluid velocity but propagating speed of waves



Under the wave, fluid velocity is unknown except that it is constant over depth for a small gravity wave (or long wave).

For a stationary observer, it is an unsteady problem. For an observer moving with speed  $a$ , however, it is a steady problem.



Continuity:  $ay = V(y + dy) = q$

$$\text{Impulse-momentum: } \frac{\gamma y^2}{2} - \frac{\gamma(y + dy)^2}{2} = q\rho(V - a)$$

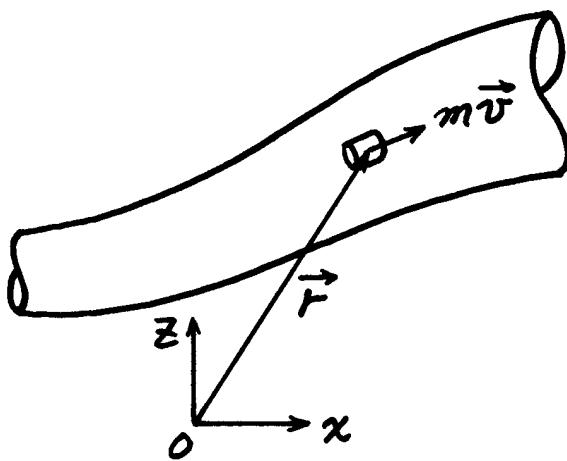
$$\therefore a^2 = g \left( 1 + \frac{dy}{y} \right) \left( y + \frac{1}{2} dy \right)$$

If  $y \gg dy$ , then  $a \approx \sqrt{gy}$  ←  $a$  depends only on  $y$ .

## 6.4 Angular Impulse-Momentum Principle

→ line of action of resultant forces

$$(\sum \vec{F} = m\vec{a})_{\text{moment}} \rightarrow \text{moment of momentum} = \text{angular momentum}$$



$$\sum (\vec{r} \times \vec{F}) = \vec{r} \times m\vec{a} = \frac{d}{dt} (\vec{r} \times m\vec{v}) = \frac{d}{dt} (\vec{r} \times \vec{v} \rho dV)$$

Summation over the whole flow system:

$$\begin{aligned} \sum (\vec{r} \times \vec{F}_{\text{ext}}) &= \frac{d}{dt} \iiint_{\text{sys}} (\vec{r} \times \vec{v}) \rho dV \\ &= \iint_{\text{CS}_{\text{out}}} (\vec{r} \times \vec{v}) \rho (\vec{v} \cdot \vec{n} dA) + \iint_{\text{CS}_{\text{in}}} (\vec{r} \times \vec{v}) \rho (\vec{v} \cdot \vec{n} dA) \\ &= \iint_{\text{CS}_{\text{out}}} (\vec{r} \times \vec{v}) \rho dQ - \iint_{\text{CS}_{\text{in}}} (\vec{r} \times \vec{v}) \rho dQ \\ &= Q\rho (\vec{r}_{\text{out}} \times \vec{V}_{\text{out}}) - Q\rho (\vec{r}_{\text{in}} \times \vec{V}_{\text{in}}) \\ &= Q\rho [(\vec{r} \times \vec{V})_{\text{out}} - (\vec{r} \times \vec{V})_{\text{in}}] \end{aligned}$$

$$\therefore \sum (\vec{r} \times \vec{F}_{\text{ext}}) = \sum \vec{M}_0 = Q\rho [(\vec{r} \times \vec{V})_{\text{out}} - (\vec{r} \times \vec{V})_{\text{in}}]$$

Note:  $\vec{r} = x\vec{i} + y\vec{j} + z\vec{k}$ ,  $\vec{V} = V_x\vec{i} + V_y\vec{j} + V_z\vec{k}$

$$\vec{r} \times \vec{V} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ x & y & z \\ V_x & V_y & V_z \end{vmatrix} = (yV_z - zV_y)\vec{i} + (zV_x - xV_z)\vec{j} + (xV_y - yV_x)\vec{k}$$

In 2-D problem ( $x, z$ ),

$$\vec{r} \times \vec{V} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ x & 0 & z \\ V_x & 0 & V_z \end{vmatrix} = (zV_x - xV_z)\vec{j}$$

Similarly,  $\vec{r} \times \vec{F} = (zF_x - xF_z)\vec{j}$

$$\therefore \sum (zF_{ext_x} - xF_{ext_z}) = Q\rho [(z_2V_{2_x} - x_2V_{2_z}) - (z_1V_{1_x} - x_1V_{1_z})]$$

where 1=CS<sub>in</sub> and 2=CS<sub>out</sub>.

For the resultant force, use  $F_{\text{ext}} \times r$ , where  $F_{\text{ext}}$  is known from linear impulse-momentum equation. For other external forces (i.e. body force and pressure forces at 1 and 2), we know the point of action (i.e.  $x$  and  $z$ ).

