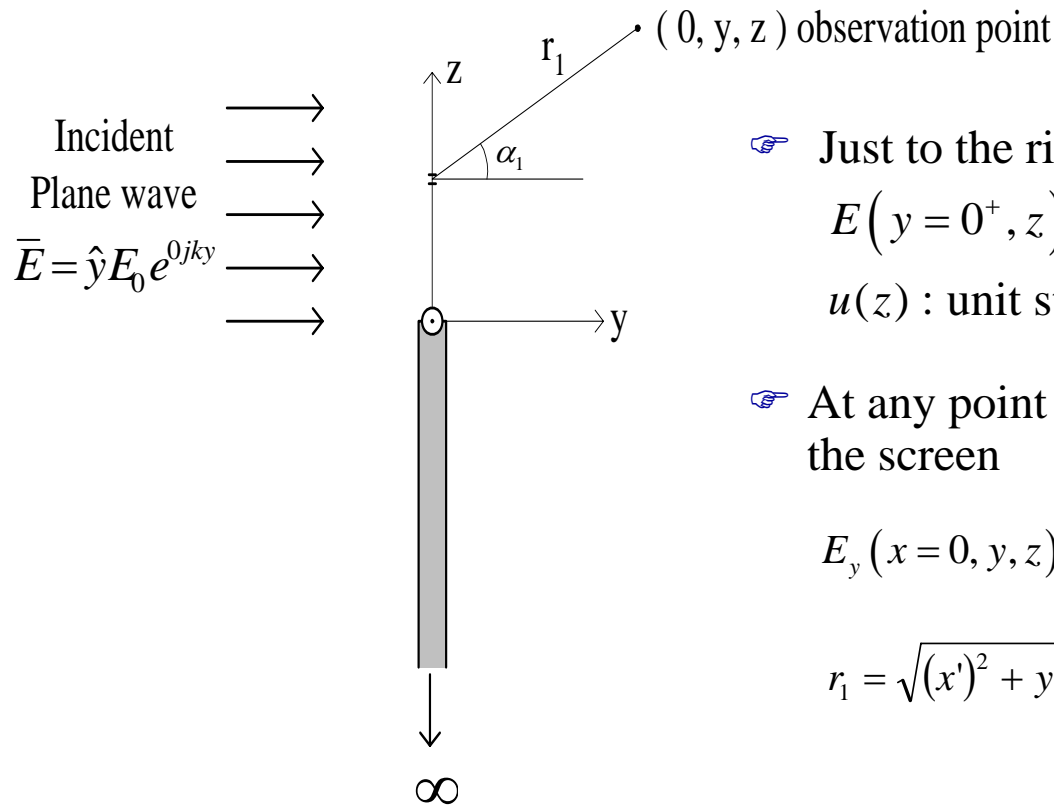


Plane Wave Diffraction

- Consider a plane wave propagation along y and incident on an absorbing half-screen



☞ Just to the right of the screen,

$$E(y = 0^+, z) = E_0 u(z)$$

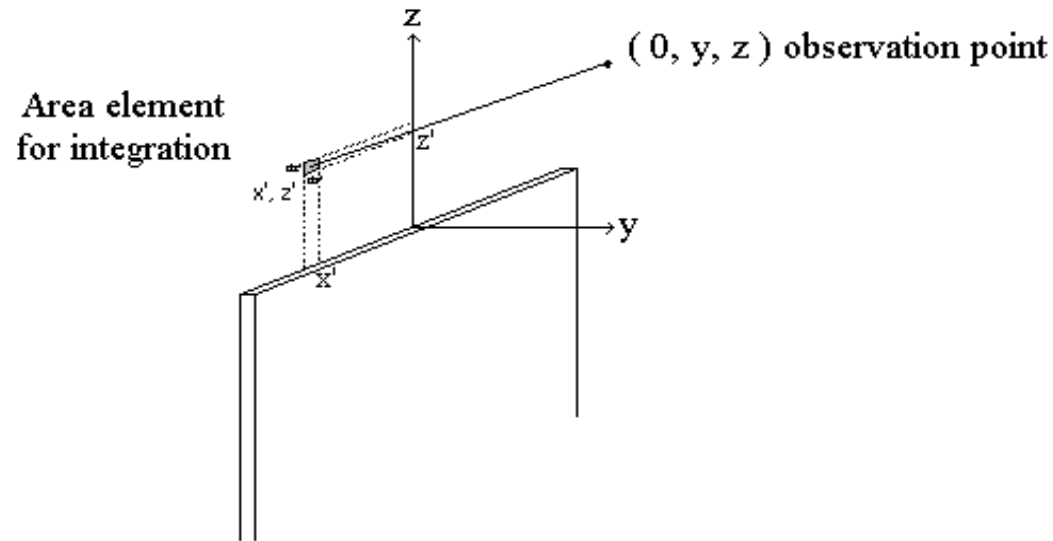
$u(z)$: unit step function

☞ At any point in the y-z plane to the right of the screen

$$E_y(x = 0, y, z) = \frac{jkE_0}{4\pi} \int_0^\infty \int_{-\infty}^\infty (1 + \cos \alpha_1) \frac{e^{-jk r_1}}{r_1} dx' dz'$$

$$r_1 = \sqrt{(x')^2 + y^2 + (z - z')^2}$$

Plane Wave Diffraction



- ☞ In order to carry out the x' integration, recognize that for $y \gg \lambda$, the area giving a significant contribution will have width along x that is small compared to y .

$$r_1 \approx \rho_1 + \frac{1}{2} \frac{(x')^2}{\rho_1} \quad \text{where} \quad \rho_1 = \sqrt{y^2 + (z - z')^2}$$

Plane Wave Diffraction

$$E_z(0, y, z) = \frac{jkE_0}{4\pi} \int_0^\infty \left[\frac{1 + \cos \alpha_1}{\rho_1} e^{-jk\rho_1} \int_{-\infty}^\infty e^{-j\frac{k(x')^2}{2\rho_1}} dx' \right] dz'$$

$$\begin{aligned} \int_{-\infty}^{+\infty} e^{\frac{jk}{2\rho} x'^2} dx' &= 2 \int_0^{+\infty} e^{\frac{jk}{2\rho} x'^2} dx' \\ &= 2 \left[\int_0^\infty \cos\left(\frac{k}{2\rho} x'^2\right) dx' - j \int_0^\infty \sin\left(\frac{k}{2\rho} x'^2\right) dx' \right] \\ &= 2 \sqrt{\frac{2\rho}{k}} \frac{1}{2} \sqrt{\frac{\pi}{2}} (1 - j) \\ &= \sqrt{\frac{2\pi\rho}{k}} e^{-j\frac{\pi}{4}} \end{aligned}$$

$$E_z(0, y, z) = \frac{je^{-j\frac{\pi}{4}}}{2\sqrt{2\pi}} \sqrt{k} E_0 \int_0^\infty \frac{1 + \cos \alpha_1}{\sqrt{\rho_1}} e^{-jk\rho_1} dz'$$

< cf >

$$\sqrt{-j} = \left(e^{-j\frac{\pi}{2}} \right)^{1/2} = e^{-j\frac{\pi}{4}}$$

$$\int_0^\infty \cos x^2 dx = \int_0^\infty \sin x^2 dx = \frac{1}{2} \sqrt{\frac{\pi}{2}}$$

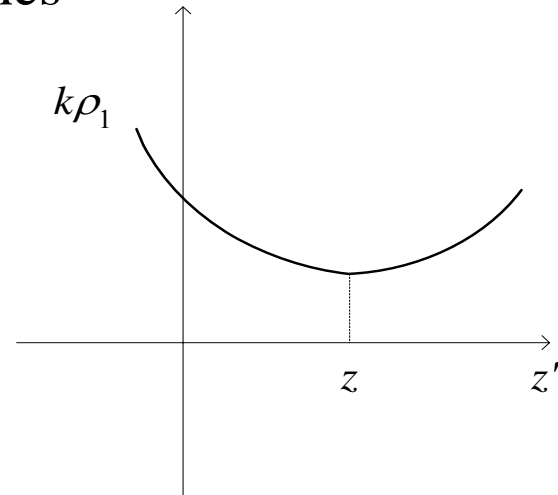
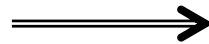
Plane Wave Diffraction

- In order to carry out the integration in the above equation, we observe that $\rho_1 = \sqrt{y^2 + (z - z')^2}$ will have a stationary point when the derivative of ρ_1 with respect to z' vanishes

$$0 = \frac{d\rho_1}{dz'} = \frac{-(z - z')}{\sqrt{y^2 + (z - z')^2}}$$

at $z = z'$

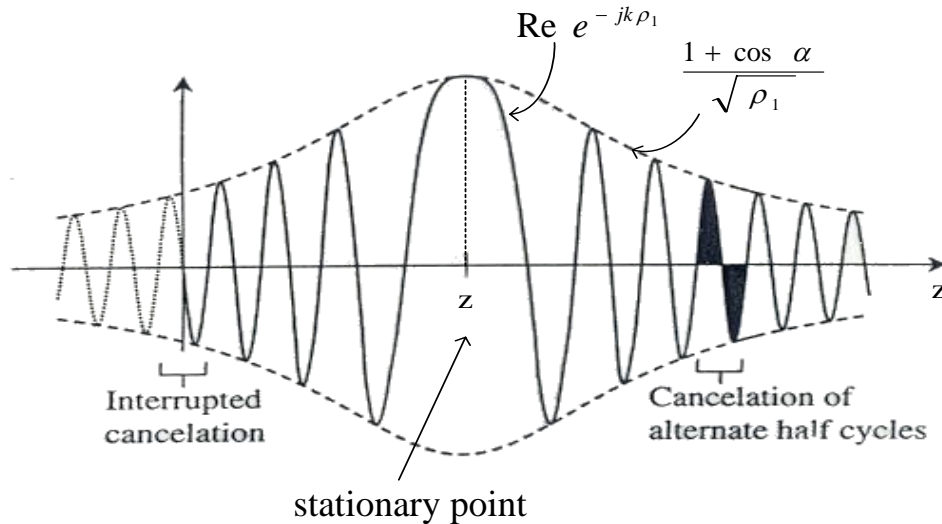
$$\rho_1 \approx y + \frac{1}{2y}(z - z')^2$$



- We identify three cases
- (1) The stationary point is well above the end point $z' = 0$ of the integral
 - (2) The stationary point is well below the end point
 - (3) The stationary point is near the end point

Plane Wave Diffraction

➤ Case 1. $z > 0$ by a large amount



☞ The imaginary part of the integrand will have a similar variation. To account for the interrupted cancellation of alternate $\frac{1}{2}$ cycle at $z'=0$, we will compute an end point contribution in the following way.

$$\int_0^{\infty} \frac{(1 + \cos \alpha_1)}{\sqrt{\rho_1}} e^{-jk\rho_1} dz' = \underbrace{\int_{-\infty}^{\infty} \frac{1 + \cos \alpha_1}{\sqrt{\rho_1}} e^{-jk\rho_1} dz}_{\text{First term}} - \underbrace{\int_{-\infty}^0 \frac{1 + \cos \alpha_1}{\sqrt{\rho_1}} e^{-jk\rho_1} dz}_{\text{Second term}}$$

Plane Wave Diffraction

☞ The first integral gives the stationary point contribution, which can be found using the approximation

☞ At the stationary point, $\alpha_1 = 0$ and $\sqrt{\rho_1} = \sqrt{y}$ in the denominator.

$$\begin{aligned} \int_{-\infty}^{\infty} \frac{1 + \cos \alpha_1}{\sqrt{\rho_1}} e^{-jk\rho_1} dz' &= \frac{2}{\sqrt{y}} e^{-jky} \int_{-\infty}^{\infty} e^{-j\frac{k}{2y}(z-z')^2} dz' \\ &= \left(\frac{2}{\sqrt{y}} e^{-jky} \right) \left(e^{-j\frac{\pi}{4}} \sqrt{\frac{2\pi y}{k}} \right) \end{aligned}$$

Plane Wave Diffraction

☞ The second integral comprises the end point contribution.

$$\rho_1 = \sqrt{y^2 + z^2 - 2zz' + (z')^2} \quad (z')^2 \rightarrow 0$$

$$\approx \sqrt{(y^2 + z^2) - 2zz'} = \sqrt{(y^2 + z^2)} - \frac{zz'}{\sqrt{y^2 + z^2}}$$

$$\text{let } \rho \equiv \sqrt{y^2 + z^2}, \cos \alpha \equiv \frac{y}{\rho}, \sin \alpha \equiv \frac{z}{\rho}$$

and then

$$-\int_{-\infty}^0 \frac{1 + \cos \alpha_1}{\sqrt{\rho_1}} e^{-jk\rho_1} dz' \approx -\frac{1 + \cos \alpha}{\sqrt{\rho}} e^{-jk\rho} \int_{-\infty}^0 e^{\frac{jkz}{\rho} z'} dz'$$

$$= -\frac{1 + \cos \alpha}{\sqrt{\rho}} e^{-jk\rho} \left. \frac{e^{\frac{jkz}{\rho} z'}}{jkz/\rho} \right|_{-\infty}^0$$

$$= -\frac{1 + \cos \alpha}{\sqrt{\rho}} e^{-jk\rho} \frac{1}{jkz/\rho} = j \frac{(1 + \cos \alpha) e^{-jk\rho}}{k\sqrt{\rho} \sin \alpha}$$

< cf >

$$\int_{-\infty}^{\infty} e^{j\alpha x} dx = 2\pi\delta(x)$$

$$\int_{-\infty}^0 e^{j\alpha x} dx = \pi\delta(x) + P \frac{1}{j\alpha}$$

P : excluding singular point i.e. x=0

Plane Wave Diffraction

Stationary + end point contribution

$$= \int_0^\infty \frac{1 + \cos \alpha}{\sqrt{\rho_1}} e^{-jk\rho_1} dz' \approx \underbrace{\frac{2\sqrt{2\pi}}{\sqrt{k}} e^{-j\pi/4} e^{-jky}}_{\text{Stationary point contribution}} + \underbrace{j \frac{1 + \cos \alpha}{k \sin \alpha} \frac{e^{-jk\rho}}{\sqrt{\rho}}}_{\text{End point contribution}}$$

for $z > 0$

$$E_z(0, y, z) = \frac{je^{-j\pi/4}}{2\sqrt{2\pi}} \sqrt{k} E_0 \left[\frac{2\sqrt{2\pi}}{\sqrt{k}} e^{-j\pi/4} e^{-jky} + j \frac{1 + \cos \alpha}{k \sin \alpha} \frac{e^{-jk\rho}}{\sqrt{\rho}} \right]$$

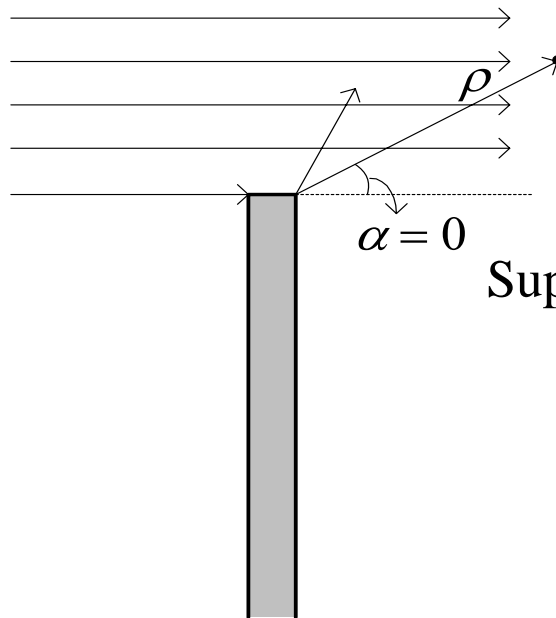
$$= E_0 e^{-jky} - E_0 \frac{e^{-j\pi/4}}{\sqrt{2\pi k}} \frac{1 + \cos \alpha}{2 \sin \alpha} \frac{e^{-jk\rho}}{\sqrt{\rho}}$$

$\frac{e^{-jk\rho}}{\sqrt{\rho}}$: cylindrical wave form

$\frac{1 + \cos \alpha}{2 \sin \alpha}$: singular at $\alpha=0$ (w.r.t $z=z_0$) i.e. on shadow boundary

Plane Wave Diffraction

- ☞ First term : incident plane wave
- ☞ Second term : cylindrical wave emitting from the edge

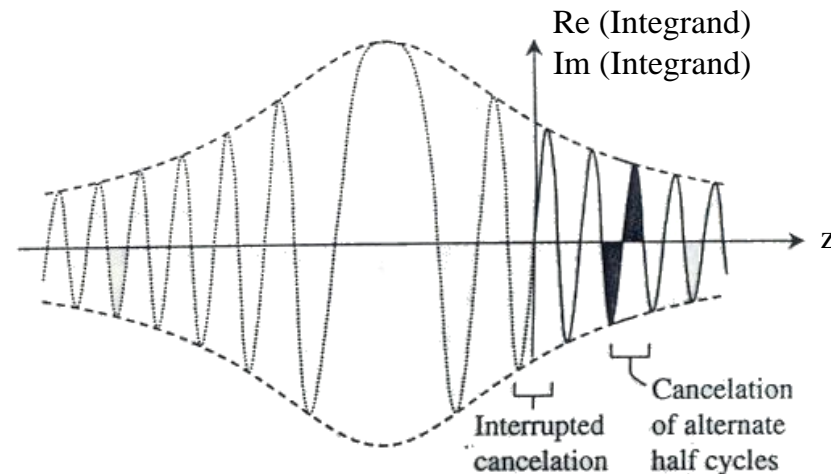


Superposition of incident and diffracted wave

Plane Wave Diffraction

- Case 2. $z < 0$ by a large amount

$$E_z(0, y, z) = \frac{je^{-j\pi/4}}{2\sqrt{2\pi}} \sqrt{k} E_0 \int_0^\infty \frac{1 + \cos \alpha_1}{\sqrt{\rho_1}} e^{-jk\rho_1} dz'$$



In this case, we have only the end point contribution.

Plane Wave Diffraction

$$\rho_1 \approx \sqrt{y^2 + z^2} - \frac{zz'}{\sqrt{y^2 + z^2}}$$

$$\int_0^\infty \frac{1 + \cos \alpha_1}{\sqrt{\rho_1}} e^{-jk\rho_1} dz' \approx \frac{1 + \cos \alpha}{\sqrt{\rho}} e^{-jk\rho} \int_0^\infty e^{j\frac{kz}{\rho}z'} dz'$$

$$= \frac{1 + \cos \alpha}{\sqrt{\rho}} e^{-jk\rho} \cdot \left. \frac{e^{j\frac{kz}{\rho}z'}}{jkz/\rho} \right|_0^\infty$$

$$= \frac{1 + \cos \alpha}{\sqrt{\rho}} e^{-jk\rho} \frac{(-1)}{jkz/\rho} = j \frac{1 + \cos \alpha}{k \sin \alpha} \frac{e^{-jk\rho}}{\sqrt{\rho}} \left(\because \sin \alpha = \frac{z}{\rho} \right)$$

$$\rho \equiv \sqrt{y^2 + z^2} \cos \alpha \equiv \frac{y}{\rho} \sin y \equiv \frac{z}{\rho}$$

$$\therefore E_z \approx -E_0 \frac{e^{-j\pi/4}}{\sqrt{2\pi k}} \frac{1 + \cos \alpha}{2 \sin \alpha} \frac{e^{-jk\rho}}{\sqrt{\rho}}$$

☞ Cylindrical wave emanating from the edge.

☞ The plane wave is blocked for $z < 0$.

Plane Wave Diffraction

➤ Case 3. z near 0

For this case, z and z' are both small compared to y so that $\alpha = 0$ on $\sqrt{\rho} \cong \sqrt{y}$

$$\rho_1 \cong y + \frac{1}{2y}(z - z')^2$$

$$E_z = \frac{e^{j\pi/4}}{\sqrt{2\pi}} E_0 \sqrt{\frac{k}{y}} e^{-jky} \int_0^\infty e^{-j\frac{k}{2y}(z-z')^2} dz'$$

$$t = -\sqrt{\frac{k}{2y}}(z - z')^2$$

$$E_z = \frac{e^{j\pi/4}}{\sqrt{\pi}} E_0 e^{-jky} \int_{-\sqrt{\frac{k}{2y}z}}^\infty e^{-jt^2} dt$$

(1) For $z < 0$,

$$\int_{-\sqrt{\frac{k}{2y}z}}^\infty e^{-jt^2} dt = \int_{\sqrt{\frac{k}{2y}|z|}}^\infty e^{-jt^2} dt$$

(2) For $z > 0$,

$$\begin{aligned} \int_{-\sqrt{\frac{k}{2y}z}}^\infty e^{-jt^2} dt &= \int_{-\infty}^\infty e^{-jt^2} dt - \int_{-\infty}^{-\sqrt{\frac{k}{2y}|z|}} e^{-jt^2} dt \\ &= \sqrt{\pi} e^{-j\pi/4} - \int_{\sqrt{\frac{k}{2y}z}}^\infty e^{-ju^2} du \quad (u = -t) \end{aligned}$$

$$E_z = E_0 e^{-jky} u(z) - E_0 e^{-jky} f\left(\sqrt{\frac{k}{2y}|z|}\right) \text{sgn}(z)$$

$$\text{sgn}(z) = \begin{cases} +1 & \text{for } z > 0 \\ -1 & \text{for } z < 0 \end{cases}$$

$$f(x) = \frac{e^{j\pi/4}}{\sqrt{\pi}} \int_x^\infty e^{-ju^2} du$$

Plane Wave Diffraction

For small z ,

$$\rho = \sqrt{y^2 + z^2} \approx y \pm \frac{1}{2} \frac{z^2}{y}$$

$$E_z = E_0 e^{-jky} U(z) - E_0 e^{-jk\rho} \left[e^{j\frac{k}{2y}z^2} f\left(\sqrt{\frac{k}{2y}}|z|\right) \right] \text{sgn}(z)$$

$$\text{Let } \xi = \frac{1}{2} \sqrt{\frac{k}{y}} |z|$$

$$F(\xi) = 2e^{j\frac{k}{2y}z^2} f\left(\sqrt{\frac{k}{2y}}|z|\right) = \frac{2}{\sqrt{\pi}} e^{j2\xi^2} e^{j\pi/4} \int_{\sqrt{2}\xi}^{\infty} e^{-ju^2} du$$

$$\therefore E_z = E_0 e^{-jky} U(z) - E_0 e^{-jk\rho} \frac{1}{2} F(\xi) \text{sgn}(z)$$

Fresnel Integral

cf)

$$\begin{aligned} & \int_x^{\infty} e^{-ju^2} du \\ &= \int_0^{\infty} e^{-ju^2} du - \int_0^x e^{-ju^2} du \\ &= \frac{\sqrt{\pi}}{2} e^{-j\pi/4} - \left[\int_0^x \cos u^2 du - \int_0^x \sin u^2 du \right] \\ &= \frac{\sqrt{\pi}}{2} e^{-j\pi/4} - \frac{\sqrt{\pi}}{2} [C_1(x) - jS_1(x)] \end{aligned}$$

$$\text{where } \begin{cases} C_1(x) = \sqrt{\frac{2}{\pi}} \int_0^x \cos t^2 dt \\ S_1(x) = \sqrt{\frac{2}{\pi}} \int_0^x \sin t^2 dt \end{cases}$$

Fresnel Integral

☞ The above equation applies for $|z|$ within some region about the shadow boundary $y > 0, z = 0$.

☞ We anticipate that this region will be the Fresnel zone. $|z| = \sqrt{y\lambda}$ in width.

Plane Wave Diffraction

$$|z| = \sqrt{y\lambda}$$

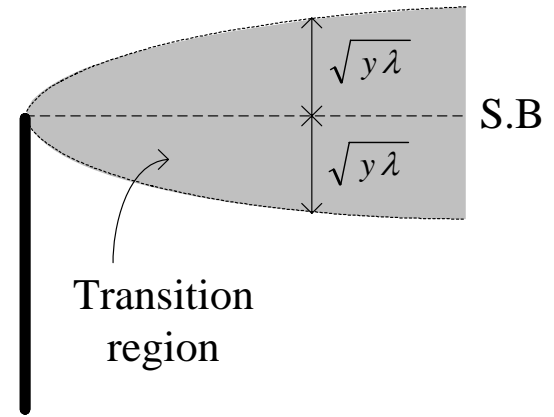
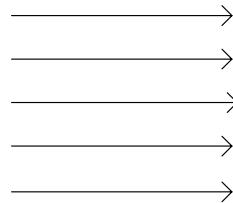
$$\xi = \frac{1}{2} \sqrt{\frac{k}{y}} |z| = \frac{1}{2} \sqrt{\frac{k}{y}} \sqrt{y\lambda} = \sqrt{\frac{\pi}{2}}$$

Outside the transition,

$$E_z = E_0 e^{-jky} - E_0 \frac{e^{-j\pi/4}}{\sqrt{2\pi k}} \frac{1 + \cos \alpha}{2 \sin \alpha} \frac{e^{-jk\rho}}{\sqrt{\rho}}$$

$$\text{or } E_z = -E_0 \frac{e^{-j\pi/4}}{\sqrt{2\pi k}} \frac{1 + \cos \alpha}{2 \sin \alpha} \frac{e^{-jk\rho}}{\sqrt{\rho}} \quad (\sin \alpha < 0 \because z < 0)$$

$$\bar{E}_z = E_0 e^{-jky} u(z) - E_0 \frac{e^{-j\pi/4}}{\sqrt{2\pi k}} \frac{1 + \cos \alpha}{2 \sin \alpha} \frac{e^{-jk\rho}}{\sqrt{\rho}}$$



- ☞ The first term : the incident field E_{in} in the illuminated region $z > 0$, and is zero in the shadow region $z < 0$, as would be given by geometric optics.
- ☞ The second term : the cylindrical wave emanating from the edge with pattern function $\frac{1 + \cos \alpha}{2 \sin \alpha}$

Diffraction coefficient

➤ Diffraction coefficient

$$D(\alpha) = -\frac{1}{\sqrt{2\pi k}} \frac{1 + \cos \alpha}{2 \sin \alpha}$$

$$E = E_{in} U(z) + E_0 \frac{e^{-j\pi/4} e^{-jk\rho}}{\sqrt{\rho}} D(\alpha)$$

➤ Inside the transition region

$$E = E_{in} U(z) + E_0 \frac{e^{-j\pi/4} e^{-jk\rho}}{\sqrt{\rho}} D_T(\alpha)$$

$$D_T(\alpha) = -\frac{1}{2} e^{j\pi/4} \sqrt{\rho} F(\xi) \operatorname{sgn}(z)$$

$$F(\xi) = \frac{2}{\sqrt{\pi}} e^{j2\xi^2} e^{j\pi/4} \int_{\sqrt{2\xi}}^{\infty} e^{-ju^2} du$$

$$\therefore D_T(\alpha) = -\frac{-j\sqrt{\rho}}{\sqrt{\pi}} e^{j2\xi^2} \left[\int_{\sqrt{2\xi}}^{\infty} e^{-ju^2} du \right] \operatorname{sgn}(z)$$

Diffraction coefficient

➤ Outside transition region

$$u^2 = 2\xi^2 + v, \quad u = \sqrt{2\xi^2 + v}$$

$$du = \frac{1/2}{\sqrt{2\xi^2 + v}} dv$$

$$\int_{2\xi}^{\infty} e^{-ju^2} du = \int_0^{\infty} e^{-j2\xi^2} e^{-jv} \frac{dv}{2\sqrt{2\xi^2 + v}}$$

$$\frac{1}{\sqrt{2\xi^2 + v}} = \frac{1}{\sqrt{2}\xi} - \frac{1}{2(\sqrt{2}\xi^2)^3} v + \dots \quad \text{By Taylor series}$$

$$\begin{aligned} \therefore \int_{2\xi}^{\infty} e^{-ju^2} du &= \frac{1}{2\sqrt{2}\xi} e^{-j2\xi^2} \left[\int_0^{\infty} e^{-jv} dv - \frac{1}{4\xi^2} \int_0^{\infty} v e^{-jv} dv + \dots \right] \\ &= \frac{1}{2\sqrt{2}\xi} e^{-j2\xi^2} \left[\frac{1}{j} + \frac{1}{4\xi^2} + \dots \right] \end{aligned}$$

$$\text{at } |z| = \sqrt{\lambda y}, \quad \xi = \sqrt{\frac{\pi}{2}} \text{ and } \frac{1}{4\xi^2} = \frac{1}{\pi}$$

☞ So that outside the Fresnel zone the term and higher decreases rapidly leaving only the first term in the series.

Diffraction coefficient

➤ For large $|z|$,

$$D_T(\alpha) \cong -\frac{j\sqrt{\rho}}{\sqrt{\pi}} e^{j2\xi^2} \cdot \frac{1}{j2\sqrt{2}\xi} e^{-j2\xi^2} \operatorname{sgn}(z)$$

$$\xi = \frac{1}{2} \sqrt{\frac{k}{y}} |z|$$

$$D_T(\alpha) \cong -\frac{\sqrt{\rho y} \operatorname{sgn}(z)}{\sqrt{\pi} \cdot 2\sqrt{2}} \cdot \frac{2}{\sqrt{k} |z|} = -\frac{1}{\sqrt{2\pi k}} \frac{\operatorname{sgn}(z)}{|z|/\sqrt{\rho y}}$$

➤ For small $|z|$,

$y \cong \rho$ and

$$\frac{\operatorname{sgn}(z)}{|z|/\sqrt{\rho y}} \cong \frac{\operatorname{sgn}(z)}{|z|/\rho} = \frac{1}{\sin \alpha} \Rightarrow \frac{1 + \cos \alpha}{2 \sin \alpha} \cong \sin \alpha$$

Diffraction coefficient

$$D(\alpha) = -\frac{1}{\sqrt{2\pi k}} \frac{1 + \cos \alpha}{2 \sin \alpha} \Leftrightarrow D_T(\alpha) = -\frac{1}{\sqrt{2\pi k}} \frac{\text{sgn}(z)}{|z|/\sqrt{\rho y}} \quad \text{for } |z| \text{ small}$$

$$D_T(\alpha) = -\frac{1}{2} e^{j\pi/4} \sqrt{\rho} F(\xi) \text{sgn}(z) \Leftrightarrow D_T(\alpha) = -\frac{1}{\sqrt{2\pi k}} \frac{\text{sgn}(z)}{|z|/\sqrt{\rho y}} \quad \text{for } |z| \text{ large}$$

$\hat{D}(\alpha)$: new diffraction coefficient that is uniformly valid for all z

$$\hat{D}(\alpha) = D(\alpha) + D_T(\alpha) + \frac{1}{\sqrt{2\pi k}} \frac{\text{sgn}(z)}{|z|/\sqrt{\rho y}}$$

For z (or α) large : the last two terms cancel $\Rightarrow \hat{D}(\alpha) = D(\alpha)$

For z (or α) small : the first and last cancel $\Rightarrow \hat{D}(\alpha) = D_T(\alpha)$

$$\therefore \bar{E} = E_{in} U(z) + E_0 \frac{e^{-j\pi/4} e^{-jk\rho}}{\sqrt{\rho}} \hat{D}(\alpha)$$

Diffraction coefficient

- More rigorous treatments of diffraction lead to the same result as the above equation with somewhat different value of $D(\alpha)$.
- A useful solution for an absorbing screen given by Felson is

$$D(\alpha) = \frac{-1}{\sqrt{2\pi k}} \left[\frac{1}{\alpha} + \frac{1}{2\pi - \alpha} \right]$$

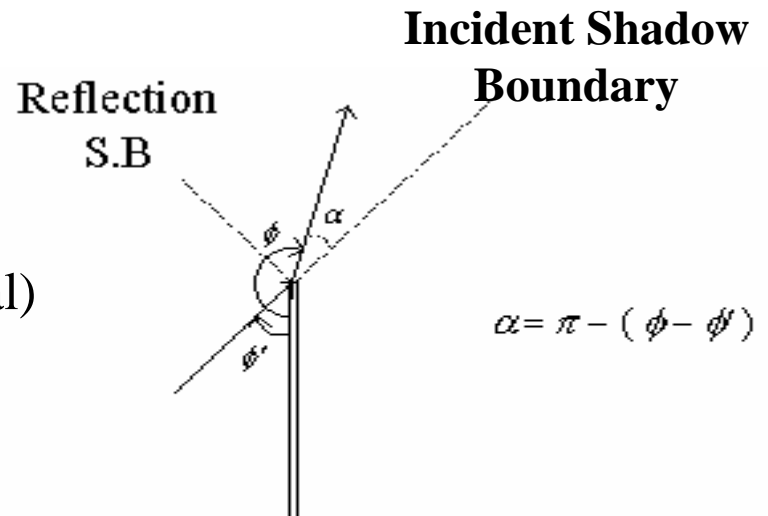
$$D(\alpha) = \frac{-1}{\sqrt{2\pi k}} \left[\frac{1}{\pi - |\Phi - \Phi'|} + \frac{1}{\pi + |\Phi - \Phi'|} \right]$$

Diffraction coefficient

- For a conducting screen, there is a reflected wave that has its own shadow boundary. The diffraction coefficient in this case is different for two vertical and horizontal polarizations and is given by

$$D(\alpha) = \frac{-1}{\sqrt{2\pi k}} \frac{1}{2} \left[\frac{1}{\cos \frac{\Phi - \Phi'}{2}} \pm \frac{1}{\cos \frac{\Phi + \Phi'}{2}} \right]$$

where + is for E // edge axis (horizontal)
 - is for H // edge axis (vertical)



- In this case the second term blows up along the reflection shadow boundary $\Phi + \Phi' = \pi$. To cancel this infinity, two more terms are required.

Reference



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- R.F. Luebbers, “Finite Conductivity Uniform GTD versus knife Edge Diffraction in Prediction of propagation path loss”IEEE, Tras. AP., vol Ap-32,no.1 pp70~76. Jan.1984