

458.308 Process Control & Design

Lecture 2: Dynamic Modeling

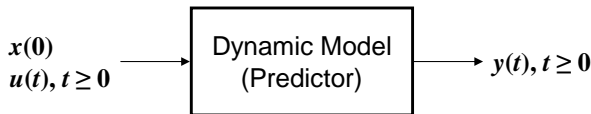
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Dynamic Modeling

Express the process's **time behaviour**

- Non steady-state initial condition, parameter changes, disturbances, etc.
- Often in the form of mathematical equation (time differential equation).



$x(0)$: initial "state"
 $u(t)$: time behaviour of some
parameter (independent
variable)

$y(t)$: time behaviour of (depen-
dent) variables of interest

Why Dynamic Modeling?

Process dynamics must be understood well (often at a quantitative level) in order to design and operate the process effectively (e.g., design an effective control system).

Usage:

- Design (esp. batch processes, cyclic continuous processes that are inherently dynamic)
- Operability assessment (stability of intended operating condition, sensitivity to disturbances)
- Operator training
- Process optimization
- Design of startup / shutdown / transition procedure
- Design of control system

Modeling Approaches

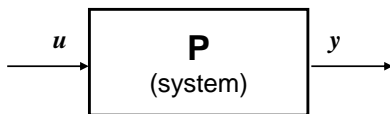
Fundamental Modeling

- Theoretical/Mechanistic modeling
- **Physico-chemical** understanding + Conservation principle
- Difficult to develop: need detailed process knowledge
- Usually complex: a large set of ODEs or PDEs
- Fundamentally correct - can be used for exploratory purposes
- Used for simulation (operator training), optimization, and transition control

Empirical Modeling

- Explain the **observed** response, cause-effect, pattern, etc.
- Easier to develop: need experimental data
- Usually kept simple: a small set of **linear** ODEs
- Lacks fundamental correctness: may not be useful in applications that require extrapolation beyond the conditions under which data were collected
- Used for controller design

Linear System



System can be seen as a mapping between input u and output y .

Linear System

Should satisfy...

- Principle of **superposition**

This also implies...

- $P(0) = 0$

Principle of superposition

$$y = P(u), u \in \mathcal{D}, y \in \mathcal{R}$$

Consider $u_1, u_2 \in \mathcal{D}$

$$y_1 = P(u_1), y_2 = P(u_2)$$

for any scalar values of a, b

$$P(au_1 + bu_2) = aP(u_1) + bP(u_2) = ay_1 + by_2$$

Affine System

- Q. $y = 3u$?
- A.
- Q. $y = 3u + 2$?
- A.
- Q. Deviation variable?
- A.

Note: People often call affine system linear system.

Linear? Nonlinear?: Examples We Worked on

- Surge Tank

$$\frac{dh}{dt} = \frac{F_1 - F_2}{A} \Leftrightarrow \frac{dy}{dt} = \frac{u_1 - u_2}{A}$$

- CSTR (constant hold-up)

$$\frac{dC_A}{dt} = \frac{q}{V}(C_{Ai} - C_A) - kC_A$$

$$\Leftrightarrow \frac{dy}{dt} = \frac{u_1}{V}(u_2 - y) - ky$$

Degree of Freedom Analysis

- DoF: Number of variables that can be specified **independently**

$$\mathbf{N}_F = \mathbf{N}_V - \mathbf{N}_E$$

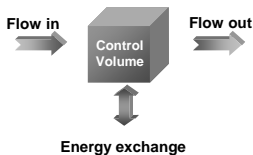
- \mathbf{N}_F : Degree of freedom (# of independent variables)
 - \mathbf{N}_V : Total number of variables
 - \mathbf{N}_E : Number of equations (# of independent variables)
- Another perspective: # of equations needed?

$$\mathbf{N}_E = \mathbf{N}_V - \mathbf{N}_F$$

Stirred-Tank Heating Process

- $\mathbf{N}_V = 6$: T_i , w_i , T , w , V , Q
- $\mathbf{N}_E = 2$: mass and energy balances
- $\mathbf{N}_F = N_V - N_E = 4$
- If we have constant holdup and $w = w_i$
 - $\mathbf{N}_V = 4$
 - $\mathbf{N}_E = 1$: Only energy balance
 - $\mathbf{N}_F = 3$: Three independent variables would be T_i , w , Q

General Modeling Principle



- **Total mass** balance

- Rate of mass accumulation within CV = Rate of mass in from surroundings - Rate of mass out to surroundings

- **Component mass** (molar) balance

- Rate of mass accumulation within CV = Rate of mass in from surroundings - Rate of mass out to surroundings + Rate of mass creation within CV

- **Total energy** (enthalpy) balance

- Rate of energy accumulation within CV = Rate of energy in from surroundings - Rate of energy out to surroundings
- For flow systems,

Rate of enthalpy accumulation within CV = Rate of enthalpy in by material flow - Rate of enthalpy out by material flow + Rate of total heat addition from surroundings

Illustrative Example: Stirred-Tank Heating Process

Total mass inside CV = $V\rho$

Rate of mass accumulation inside CV = $\frac{d(V\rho)}{dt}$

Rate of mass into CV by flow = w_i

Rate of mass out of CV by flow = w

Total energy inside CV = $H = \rho V\hat{H}$

Rate of energy into CV by flow = $w_i\hat{H}_i = w_i C(T_i - T_{ref})$

Rate of energy out of CV by flow = $w\hat{H} = w C(T - T_{ref})$

Rate of energy addition = Q

$$\frac{dV}{dt} = \frac{1}{\rho}(w_i - w)$$

$$\frac{dT}{dt} = \frac{w_i}{V\rho}(T_i - T) + \frac{Q}{\rho VC}$$

Note: Several additional examples are available in the textbook. To become good at modeling, you must try many different problems **on your own**.

Lumped Parameter System

- Spatial dependence of variables is ignored
 - Well-mixed system
 - Systems with insignificant temperature or concentration gradient
 - Variables are functions of time only, not spatial position
 - Ordinary differential equation model
- Examples
 - Mixer, CSTR
 - Tray of distillation column
 - Steel ball for which heat conduction within is much faster than heat transfer to the surrounding

Distributed Parameter System

- Variables have spatial dependence
 - Instead of $y(t)$, you have $y(t, z)$, $y(t, r, z)$, or $y(t, r, z, \theta)$.
- Type of equation
 - Lumped parameter system \Rightarrow ODEs
 - Distributed parameter system \Rightarrow PDEs
- Example
 - Counter-current heat exchanger
 - Plug-flow reactor or packed-tube reactor
 - Heat conduction through a plate
 - Almost all systems show some spatial variations (e.g., due to imperfect mixing) but many systems can be treated as lumped parameter system.