

458.308 Process Control & Design

Lecture 5: Feedback Control System

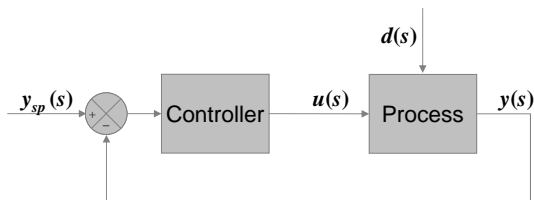
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Feedback Control Scheme: The Continuous Blending Process

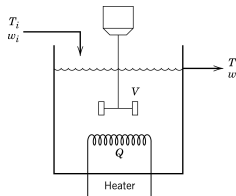
- 1 Sensor (AT) measures the controlled variable: x .
- 2 Controller (AC) calculates the **manipulated input**: w_2 in terms of an electronic signal.
- 3 Current-to-pressure (I/P) converts it to an equivalent pneumatic signal.

Simplified Control Block Diagram



- Negative feedback: self-stabilizing property with positive process gain
 - $e = y_{sp} - y$
- Positive feedback: makes a process unstable with positive process gain in general
 - $e = y_{sp} + y$
 - Used for describing complex systems (i.e., biological system)

Block Diagram



- See lecture 2 for mass, energy balance eqns.
- $w_i = w$: No need for mass balance

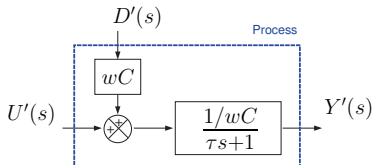
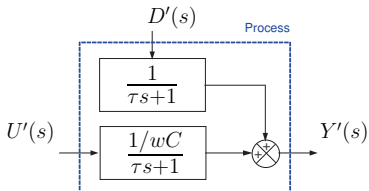
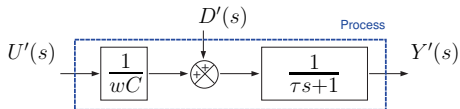
$$\frac{dT}{dt} = \frac{w_i}{V\rho} (T_i - T) + \frac{Q}{\rho V C}$$

$$\Rightarrow \tau \frac{dT}{dt} = (T_i - T) + \frac{Q}{Cw}$$

$$y' = T - \bar{T}, \quad u' = Q - \bar{Q}, \quad d' = T_i - \bar{T}_i$$

$$Y'(s) = \frac{1}{\tau s + 1} \left(\frac{U'(s)}{Cw} + D'(s) \right)$$

Equivalent Representations



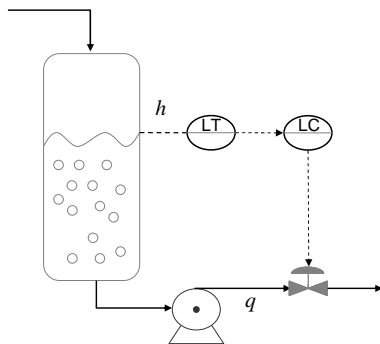
Proportional Control

Adjustment proportional to the current error

$$p(t) = \bar{p} + K_c(y_{sp}(t) - y_m(t)) \quad \Rightarrow \quad p'(t) = K_c e(t)$$

- Static control, memory-less control
- Proportional Band (PB) = $\frac{100}{K_c} \%$ (Foxboro, etc.)
- Reverse acting vs. Direct acting (Read section 8.3.2 in the textbook.)
 - Reverse acting: sensor output $(y_m) \uparrow \Rightarrow$ Controller output $\downarrow \Rightarrow K_c > 0$
 - Direct acting: sensor output $(y_m) \uparrow \Rightarrow$ Controller output $\uparrow \Rightarrow K_c < 0$

Level Controller (LC): Reverse-Acting or Direct-Acting?



- Level transmitter (LT): designed to be direct-acting (most transmitters are direct-acting)
 - Its output signal increases as the level increases.
- Air-to-Open Valve: direct-acting
- Air-to-Close Valve: reverse-acting

P-Controller: Advantages and Disadvantages

- Advantage: simplicity
- Disadvantage
 - Leaves **offset** with a set-point change or a sustained disturbance.

Note: \bar{p} is a equilibrium point (input) for the ``previous" set point or disturbance.

Proportional Integral (PI) Control

Adjustment proportional to the current error + accumulated error

$$p(t) = \bar{p} + K_c \left(e(t) + \frac{1}{\tau_I} \int_0^t e(t^*) dt^* \right)$$

- τ_I : Integral time or Reset time ($\rightarrow \infty$ =P-control)

- Integral control action: reset control, floating control
- Some variations
 - Honeywell: $p(t) = \bar{p} + K_c \left(e(t) + \tau_R \int_0^t e(t^*) dt^* \right)$
 - Foxboro: $p(t) = \bar{p} + \frac{100}{PB} \left(e(t) + \tau_R \int_0^t e(t^*) dt^* \right)$
 - τ_R : reset rate

PI-Controller: Advantages and Disadvantages

- Advantage: eliminates offset (regardless of size of K_c)
- Disadvantage
 - One more parameter to tune
 - Easier to induce oscillation or instability

Proportional Integral Derivative (PID) Control

Adjustment proportional to the current error + accumulated error + current rate of change in the error

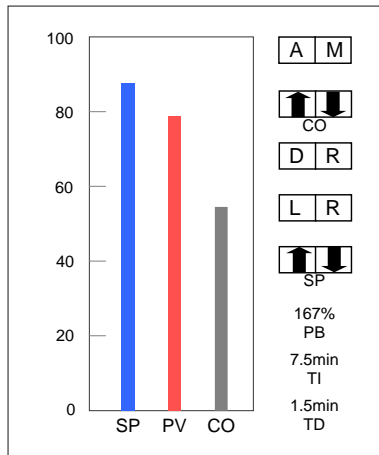
$$p(t) = \bar{p} + K_c \left(e(t) + \frac{1}{\tau_I} \int_0^t e(t^*) dt^* + \tau_D \frac{de}{dt} \right)$$

- τ_D : Derivative time constant
- Pure differentiation in real-time is not possible since evaluation of de/dt at time t requires error information beyond time t . But it can be approximated very closely.

PID-Controller: Advantages and Disadvantages

- Advantages
 - Quick action to a change in the error -- effective prevention of runaway (e.g., in an auto-catalytic reactor)
 - Decrease settling time for processes with slow dynamics and fast disturbances
 - Decrease oscillation (stabilizing factor for integral mode, etc.)
- Disadvantage
 - Yet one more parameter to tune
 - Amplifies measurement noise effect (not suitable in flow control)

Typical PID Controller Display



- PV, SP, CO: Process variable, Set point, Control output (normalized 0--100%)
- Local/Remote Switch: source of set point signal
- Auto/Manual Switch: Auto ↔ Manual (Bumpless transfer)
- Direct/Reverse Switch

Digital PID Controller

Analog:

$$p(t) = \bar{p} + K_c \left(e(t) + \frac{1}{\tau_I} \int_0^t e(t^*) dt^* + \tau_D \frac{de}{dt} \right)$$

Digital:

$$p(t_k) = \bar{p} + K_c \left(e(t_k) + \frac{\Delta t}{\tau_I} \sum_{i=0}^k e(t_i) + \tau_D \frac{e(t_k) - e(t_{k-1})}{\Delta t} \right)$$

- Δt : sampling period (interval)
- $e(t_k)$: error at the k^{th} sample time
- $p(t_k)$: controller output at the k^{th} sample time

Removing "Kicks"

- Sudden set point change (a step change)
 - de/dt will be very large, giving a sudden jump in the valve position (undesirable in most cases)
 - Apply the derivative action only on the output signal, not set point signal

$$\frac{de}{dt} = \frac{d}{dt} (y_{sp}(t) - y_m(t)) \Rightarrow -\frac{dy_m}{dt}$$

- Similar phenomenon can show up for the P-mode, though not as severe as the D-mode

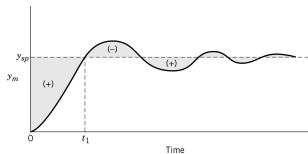
Windup and Anti-Windup

- Windup

- When a constant error persists for a long time (such as when the valve "saturates"), the integral term can be **wound up** to a very large term

- Consequence

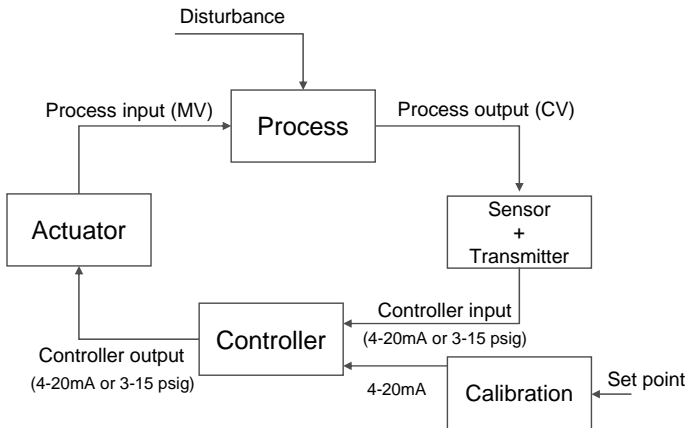
- When the reason for the constant error (e.g., un-realizable set point change or too large a disturbance to reject completely) goes away, the integral term must **unwind** before the valve position returns to the normal value and control resumes.
- **Large error in the opposite direction** will result.



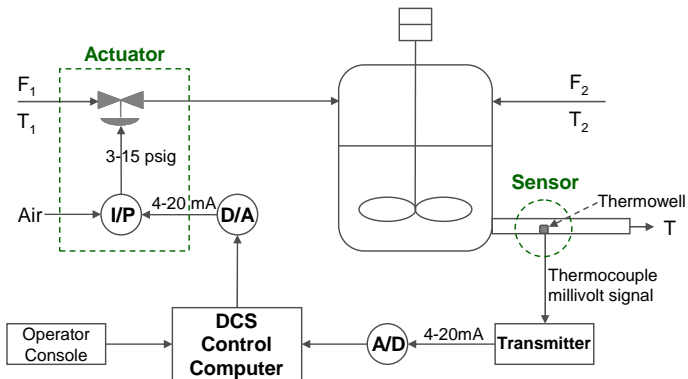
What do we need?

- Sensor (e.g., thermocouple)
- Transmitter (e.g., signal converter/amplifier/conditioner)
- Transmission Line (e.g., electrical line, air tube, data line)
- Controller (e.g., computer)
- Actuator (e.g., control valve)

Typical Setup



Exemplary Control Loop: Temperature Control



Implementation Modes

- Digital
 - Transmission: either analog signal (which gets converted to digital signal just before entering the controller) or digital signal (sequence of 0-1 binary pulses)
 - A/D: converts analog signal to digital signal
 - D/A: converts digital signal to analog signal
 - Controller: digital computer
 - High flexibility and easy reconfiguration
 - Easy access of remote data and past data

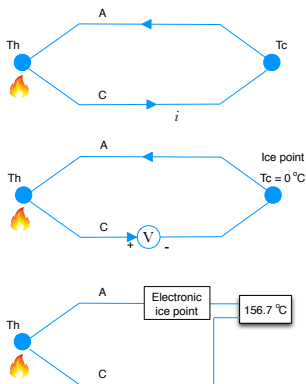
Sensors

- Physical properties \Rightarrow signals appropriate for electric and mechanical processing
- Common sensors
 - Temperature: thermocouple, resistance temperature detector (RTD)
 - Pressure: bellows, bourdon tube, diaphragm
 - Differential pressure: same as above
 - Flow rate: orifice, venturi, vane, magnetic flow meter
 - Liquid level: free float, fixed float, differential pressure
 - pH: pH meter (electrode)
 - Viscosity: differential pressure under constant flowrate
 - Chemical composition: gas chromatography

See Table 8.1 (p. 143) in the textbook.

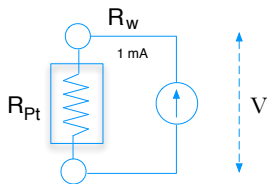
Thermocouple

- Two metal junctions at different temperatures generating a voltage that is proportional to the temperature.
 - Chromel-alumel (K-type): most popularly used
 - Iron-constantan (J-type): higher emf
 - Copper-constantan (T-type): cryogenic temperature
 - 13% Rh.Pt-Pt (R-type): high temperature ($>900^{\circ}\text{C}$)



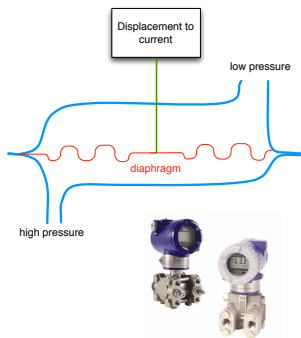
Resistance Thermometer Detector (RTD)

- Resistance of certain metals depends strongly upon their temperature
- Platinum and nickel are typical choices
- More accurate and repeatable but more expensive and less rugged than TCs
- Used for important temperature control points (reactors, distillation columns)



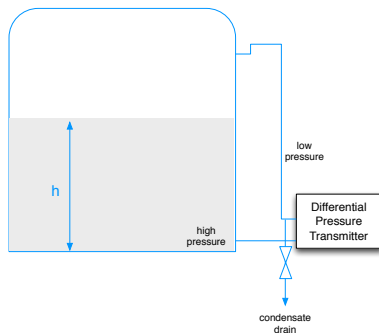
Pressure Measurement

DP Cells



- Strain gauges
 - High pressure measurements
 - Stretched wire (elastic) → Increased resistance

Level Measurement: Closed Tank



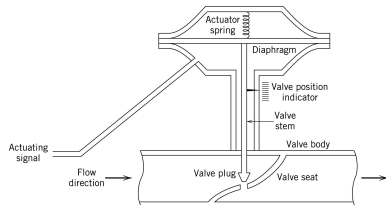
$$\Delta P = \rho gh$$

Transmitter

- Sensor signal (typically in mV) \Rightarrow signal that can be transmitted and accepted by the controller (e.g., 4--20mA)
- Example
 - $50^{\circ}C - 150^{\circ}C \Rightarrow 4mA - 20mA$
 - **Gain** of the transmitter = $16mA/100^{\circ}C = 0.16 mA/^{\circ}C$
 - **Zero** of the transmitter = value when the output is at the minimum (4mA) = $50^{\circ}C$
- Why make the minimum output 4mA instead of 0mA?

Actuators

- Convert controller output signal (4--20 mA or 3--15 psig) to physical adjustment in the process input variables (MVs).
- For process control, the most common type of actuator is the **control valve**.
- Others include
 - Variable speed pumps
 - Hydraulic actuators



Air-to-Open vs. Air-to-Close

- Air-to-Open (A-O) or Fail-Close (FC)
 - More air \rightarrow larger opening \Rightarrow No air \rightarrow valve closes
- Air-to-Close (A-C) or Fail-Open (FO)
 - More air \rightarrow smaller opening \Rightarrow No air \rightarrow valve opens completely
- Proper type to use is determined from safety considerations
 - Air-to-Close: Coolant valve in an exothermic reactor or in a condenser of a distillation column
 - Air-to-Open: Steam valve in a reactor, inlet flow valve to a tank
- Control Valve Dynamics

$$\frac{U(s)}{P(s)} = G_v(s) = \frac{K_v}{\tau_v s + 1}$$

Specifying and Sizing Control Valves

- Basic valve equation

$$q(\ell) = C_v f(\ell) \sqrt{\frac{\Delta P_v}{g_s}} \quad 0 \leq \ell \leq 1$$

ℓ : valve lift, g_s : specific gravity of the fluid (water = 1)

- Valve size: determines C_v (valve coefficient)
- Valve trim type (valve characteristic)
 - Linear: $f(\ell) = \ell$
 - Square-root (Quick opening): $f(\ell) = \sqrt{\ell}$
 - Equal percentage: $f(\ell) = R^{\ell-1}$, $R \approx 20 - 50$