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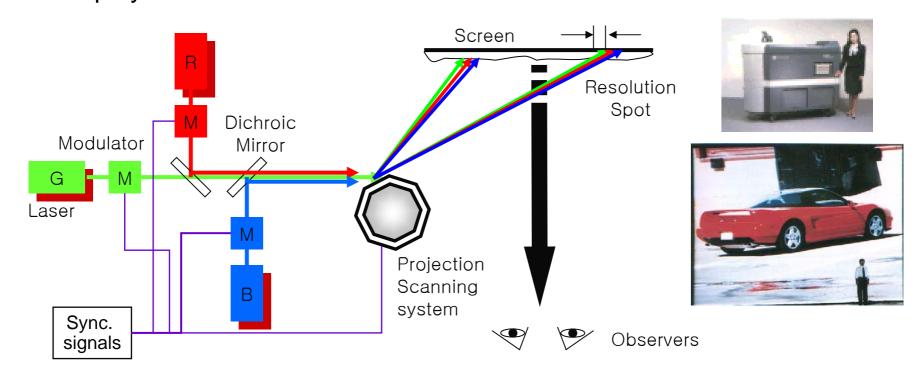
- > Introduction to laser display systems
- > Overview of speckle reduction methods
- Diffractive optical elements (DOEs)





Laser display system (scanning)

✓ RGB lasers, modulators, mirror/grating scanning devices, and display screen



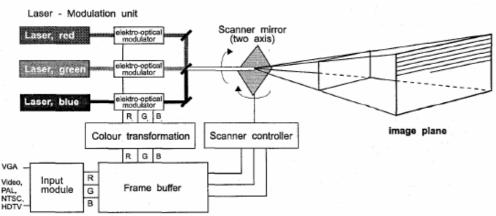
Schematic diagram of a laser display system using scanning optics





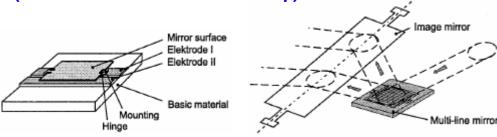
☐ Laser display system (Microscanning mirror)

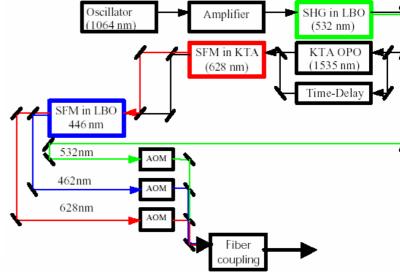
✓ Schneider Rundfunkwerke AG, LDT, Jenoptik (1998)



Horizontal deflection: 25-face polygon mirror (max. 1.3kHz rotation → 32kHz line deflection freq.)

Vertical deflection: galvanometer scanner (50/60 or 100 Hz deflection freq.)





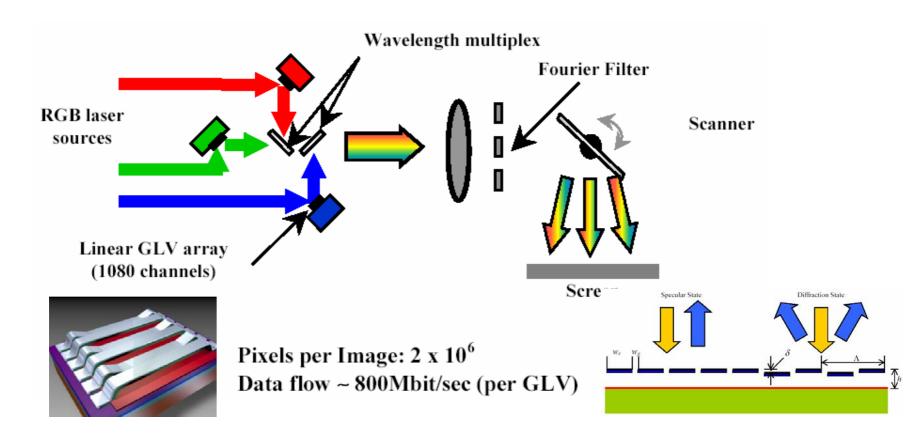


Micro-mirrors





Laser display system (Grating)



Schematic layout of a GLV-based HDTV projector





☐ GLV (Grating Light Valve) – MEMS 1-D spatial light modulator

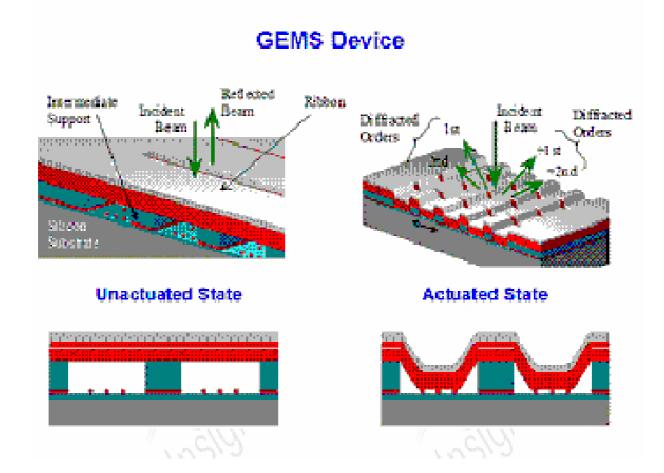
Advantages: High efficiency, large dynamic range, precise analog attenuation, fast switching speed (~1 us), high reliability, high yield, integration

Static ribbons are interlaced with the electrostatically deflectable ribbons. One or more ribbon-pairs form a pixel. The amount of diffraction can be controlled to impart an 8-bit or better gray-level intensity graduation.





Kodak's Grating Electro Mechanical System (GEMS)







☐ Mitsubishi's Laser Rear Projector Display

(When the technology is finally released to public, which Mitsubishi says will be sometime in late '07, it will be the first ever consumer laser display technology.)

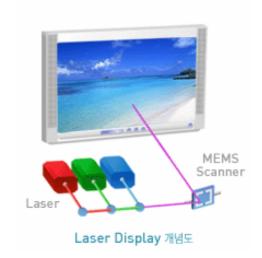


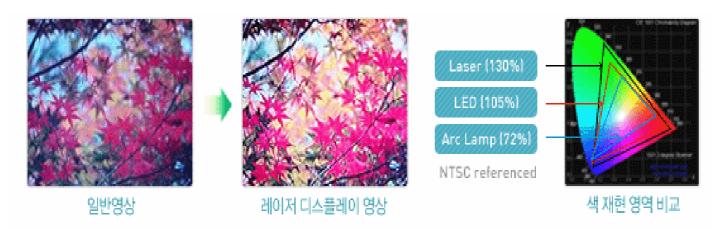
52"





삼성종합기술원











At CES (2006), Novalux demonstrated two MDTV (microdisplay-based rear-projection TV) laser-based prototypes: a 47-in. 3-LCD (liquid-crystal display) MDTV and a 52-in. MDTV using DLP (digital light processor) technology (see figure). A reference UHP-based MDTV was also shown. The baseline UHP-based MDTV offers about 400 Cd/m² of on-screen brightness. The same TV with the laser source offers about 250 Cd/m² while the DLP set produces about 300 Cd/m².

(Green: 532 nm, 1.5W, Blue: 460 nm, 1.5W, Red: 635nm)



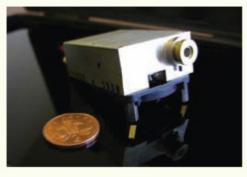


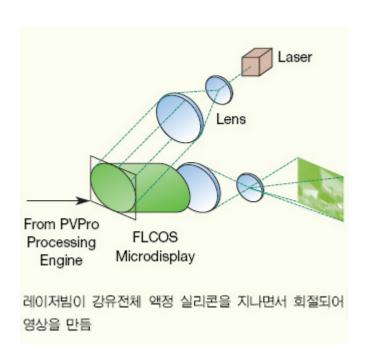
☐ Light Blue Optics

(PVPro: Ferroelectric Liquid-Crystal-On-Silicon)

손바닥보다 작은 프로젝터







☐ Univ. of Southampton – High Power Fiber Laser Display





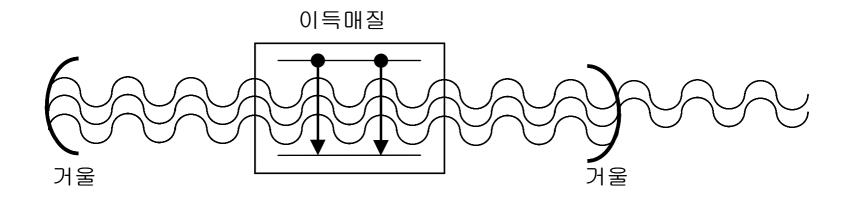
- □ Advantages of Laser Projection Display
 - Increased color gamut
 - Quasi-parallel (collinear) rays
 - No focusing is necessary.
 - Projection on non-plane surfaces is simple.
- Difficulties
 - Small, high-power, cheap lasers
 - **Speckles**





Laser

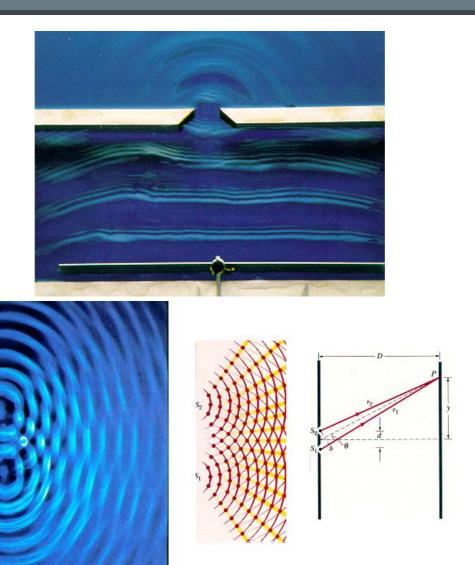
Light Amplification by Stimulated Emission of Radiation







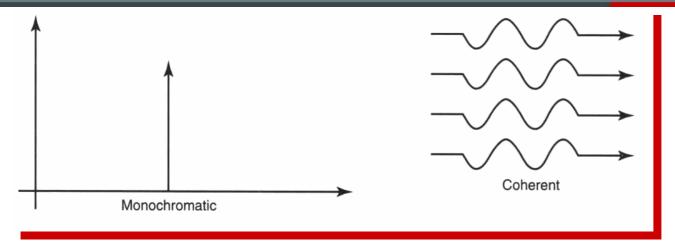
Diffraction and Interference



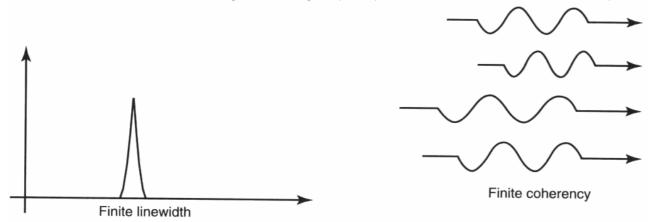




Coherency and Spectrum



An ideal monochromatic source of light has a group of photons with exactly one frequency. An ideal coherent source of light has a group of photons with the same relative phase.

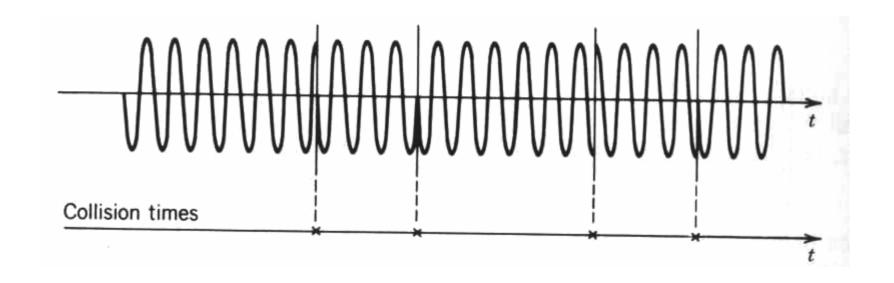


Real laser sources are neither perfectly monochromatic nor perfectly coherent. A real laser will have a finite linewidth and finite coherency.





Coherence Time and Coherence Length



$$\Delta v = \frac{1}{2\pi} \left(\frac{1}{\tau_1} + \frac{1}{\tau_2} + 2f_{\text{col}} \right)$$

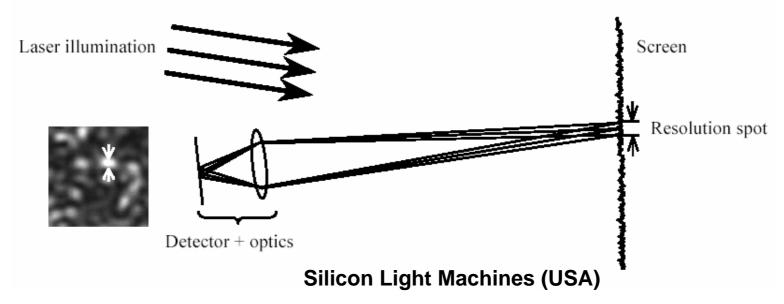




Speckles

Static speckle noise generation in laser displays

- ✓ Coherent laser beam is scattered on a spot in a rough screen surface.
- ✓ Complex interference pattern (speckle) is detected by a detector (CCD, human eye).
- ✓ Static speckle image masks the displayed image information.



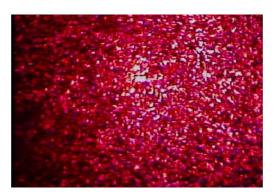
Speckle grain size is inversely proportional to beam spot radius.





Some Speckle Patterns





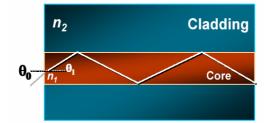
Ground Glass

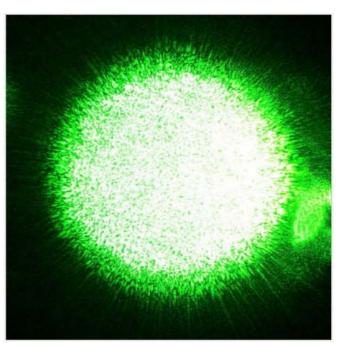


Multimode Fiber

Gray-level Film





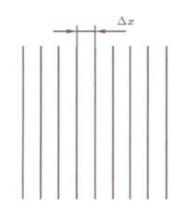


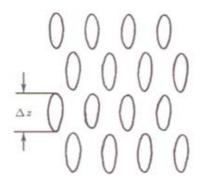
Laser pointer spot on a screen

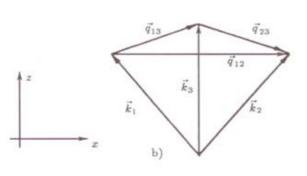




Speckle Size 1







$$\Delta x = \frac{2\pi}{K}$$

$$K = 2k \sin\left(\frac{\theta}{2}\right) \approx k\theta = \frac{2\pi}{\lambda}\theta$$
(for small θ)

$$\Delta x \approx \frac{\lambda}{\theta}$$

$$\Delta x \approx \frac{\lambda}{\theta}$$

$$\Delta z \approx \frac{\Delta x}{\theta} \approx \frac{\lambda}{\theta^2}$$





Speckle Size 2

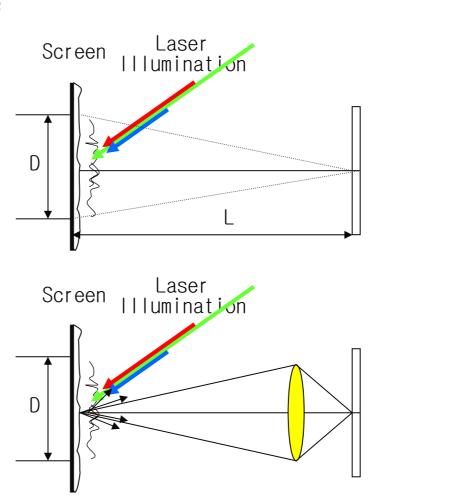
☐ Overview of the speckle

Objective speckle

$$\langle \sigma_o \rangle \cong 1.2 \lambda L / D$$

Subjective speckle

$$\langle \sigma_0 \rangle \cong 0.6 \lambda / NA$$







Speckle reduction methods

- ✓ The speckle patterns impair the image quality.
 - Strong deblurring of the color edges
 - Degradation of spatial or temporal coherence (after-image effect) of the laser
 - Degradation of spatial coherence
 - Insertion of various optical components, such as diffractive diffuser, refractive lens arrays, fiber bundle, vibrated components
 - Moving random mask or rotating circular aperture
 - Vibrational change of relative positions of a screen and an illuminating laser beam
 - Movie-like generation of collimated beams with complex phase structures using dynamic SLM
 - Laser beam is widely diffused when its spatial coherence is decreased.
 - Digital image processing (spatial averaging) of the detected image



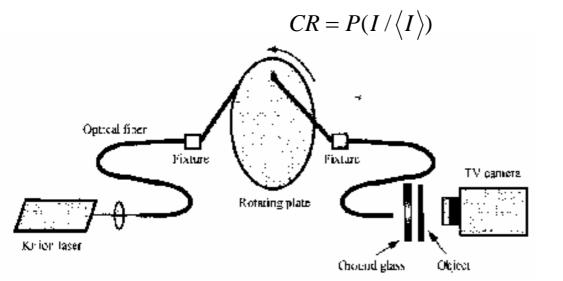


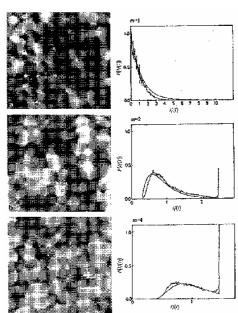
Speckle reduction using multimode fiber

✓ The laser light transmitted through a multimode optical fiber shows a speckle phenomenon due to the interference between propagation modes in the fiber.

✓ The probability density function (PDF) can be defined for

speckle contrast ratio.





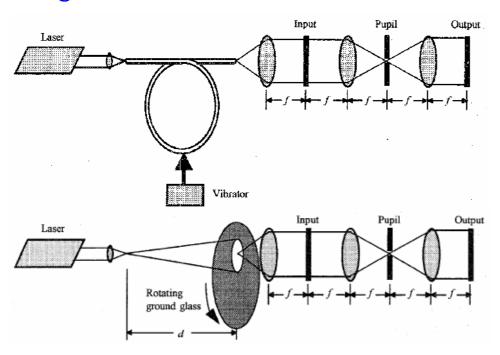
(a) Rotating multimode fiber (b) Theoretical PDF w.r.t. multiple image averaging





Speckle reduction using multimode fiber or ground glass

✓ A vibrating multimode fiber and a rotating ground glass are imaged in the telecentric two-lens imaging system.







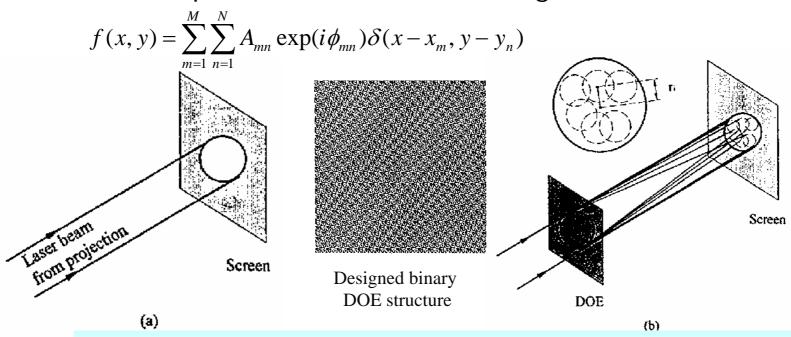
- (a) Vibrating multimode fiber and rotating ground glass
- (b) Experimental result





□ Speckle reduction using DOE

- ✓ Splits the unfocused laser beam into a number of independent beamlets with random phase distribution
- ✓ Smaller diameter than the original beam
- ✓ Multi-level phase structure DOE using IFTA





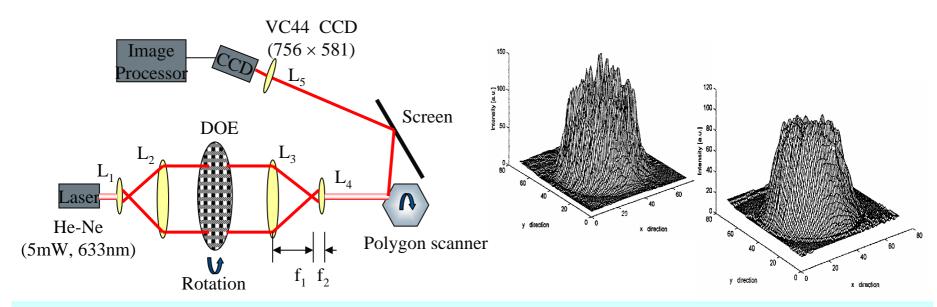
(b) Beamlets coming from the DOE





□ Speckle reducing using rotating DOE

✓ Rotating a collimated diffractive beam (after-image effect)



Experimental setup and result

(a) with a static DOE

(b) with a DOE rotating at a speed of 5 rps





Speckle reduction using moving diffuser

- ✓ Without diffuser: no speckle reduction
 - Speckle intensity of the resolution spot $S_0 = |\sum_{i=1}^{M} \sum_{j=1}^{N} E_{ij}|^2$
- ✓ Diffuser imprints N=M×M cells with relative phase $\phi_{ii}^{\ a}$
 - A different pattern is sequentially presented with equal duration during the detector integration time.

$$S = \frac{1}{A} \sum_{a=1}^{A} \left| \sum_{i=1}^{M} \sum_{j=1}^{N} H_{ij}^{a} E_{ij} \right|^{2} \qquad H_{ij}^{a} = \exp(i\phi_{ij}^{a})$$

– The summation of H_{ij}^a over all the phase patterns satisfies the decorrelation condition.

$$\sum_{a=1}^{A} H_{ij}^{a^*} H_{kl}^a = A \delta_{ik} \delta_{jl}$$
 Hadamard matrices of order M=2^{integer} satisfies this condition

$$S = \frac{1}{A} \sum_{a=1}^{A} \left| \sum_{i=1}^{M} \sum_{j=1}^{N} H_{ij}^{a} E_{ij} \right|^{2} = \frac{1}{A} \sum_{a} \sum_{i} \sum_{j} \sum_{k} \sum_{l} \left(H_{ij}^{a^{*}} E_{ij}^{*} \right) \left(H_{kl}^{a} E_{kl} \right) = \sum_{i} \sum_{j} \left| E_{ij} \right|^{2}$$

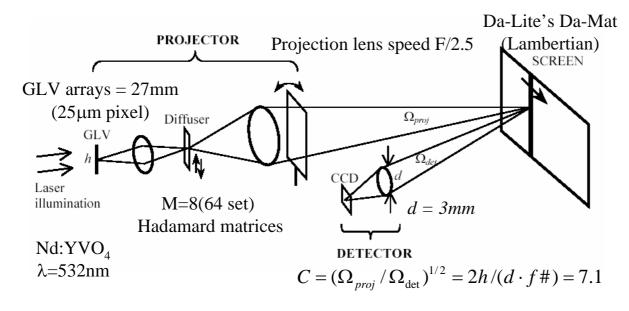
– Speckle contrast is reduced by a factor of $R_{\Omega} = M \times M$.



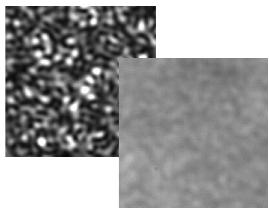


Speckle reduction using moving diffuser

- ✓ GLVTM (Grating Light Valve) array is a unique MEMS-based, 1-D SLM that modulates light by diffraction
 - High efficiency, large dynamic range, precise analog attenuation, fast switching speed(1μsec), high reliability, high yield, and high resolution.
- ✓ Hadamard diffuser suppressed speckle contrast to 8%.



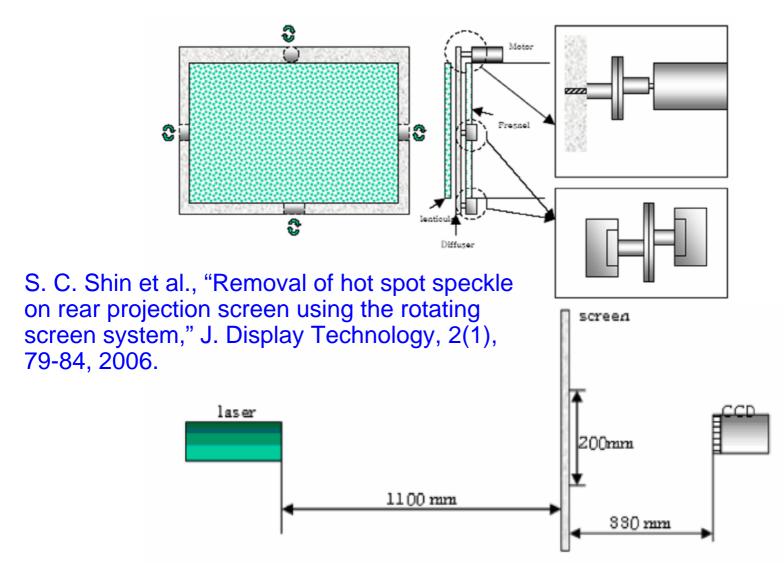
Silicon Light Machines (USA)



- (a) Original speckle (70% contrast)
- (b) Reduced speckle (8% contrast)

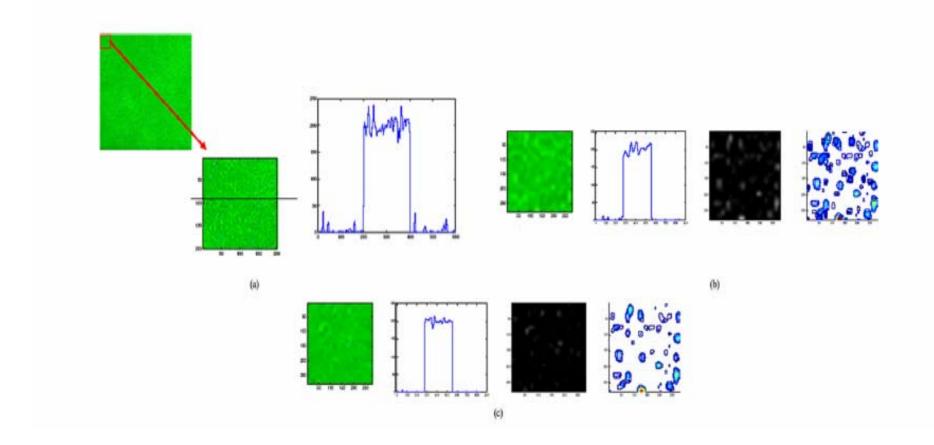






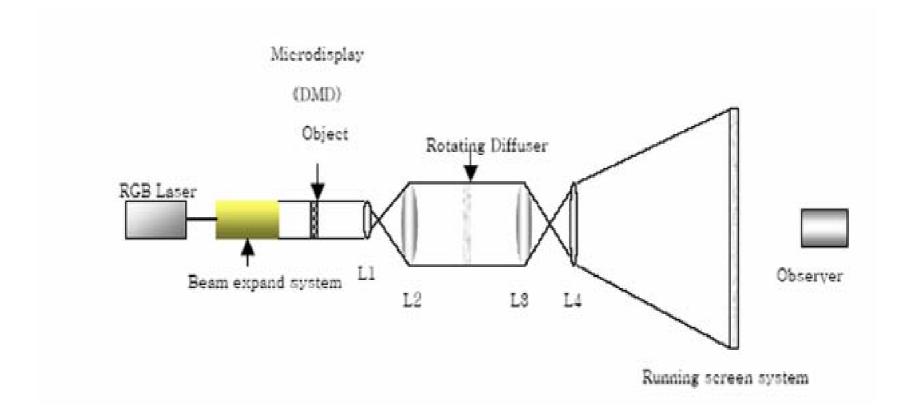






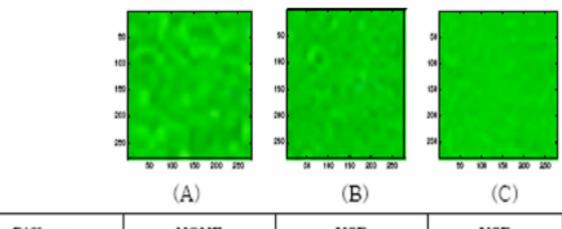












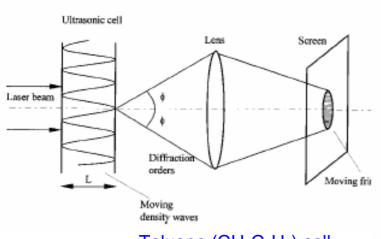
Rotating Diffuser	NONE	USE	USE
Running Screen	NONE	NONE	USE
Speckle Contrast(%)	6.5	3.1	1.6



70"

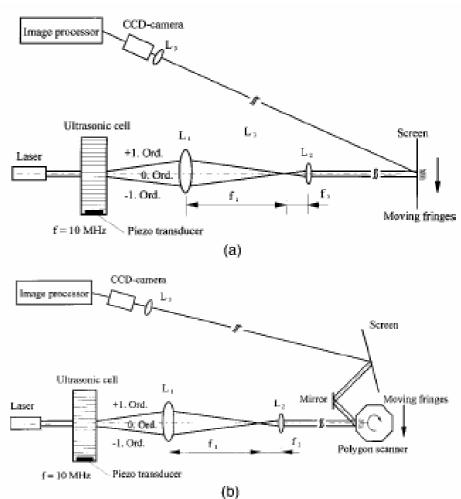






Toluene (CH₃C₆H₅) cell

L. Wang et al., "Speckle reduction in laser projections with ultrasonic waves," Opt. Eng., 39(6), 1659-1664, 2000.







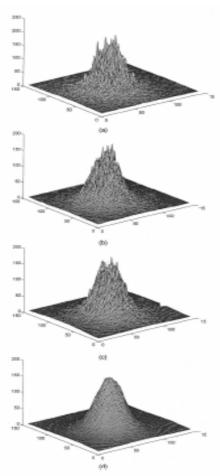


Fig. 4 Speckle contrast measured with the arrangement shown in Fig. 3(a); (a) with only the argon later (wavelength 514 nm, clamate 0.5 cm, power 1.5 W), (b) with new ultrasortic ced (2.2 MHz), (c) with two cells (2.2 and 10.0 MHz), (d) with three cells (2.2, 3.3, and 10.0 MHz).

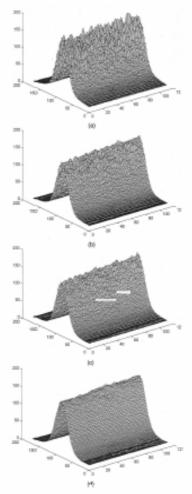
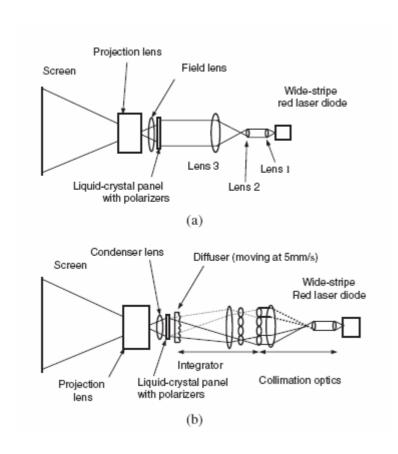


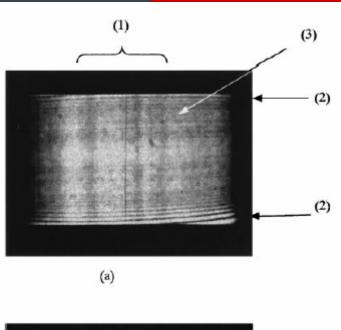
Fig. 5 Special contrast measured with the arrangement shown in Fig. 3(b): (a) with only the argan laser (asserting) 5/1 nm, date: 0.5 cm, power 1.5 W), (b) with one cell (2.2 MHz), (c) with two cells (2.2 and 10.0 MHz), (d) with three cells (2.2, 3.3, and 10.0 MHz).







K. Kasazumi et al., Jpn. J. Appl. Phys., 43(8B), 5904-5906, 2004.

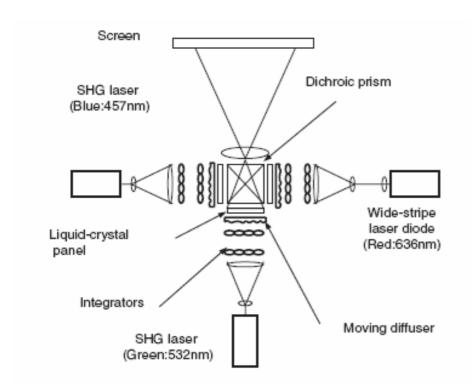


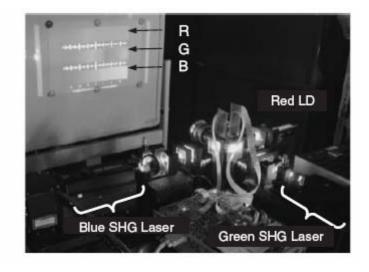


(b)



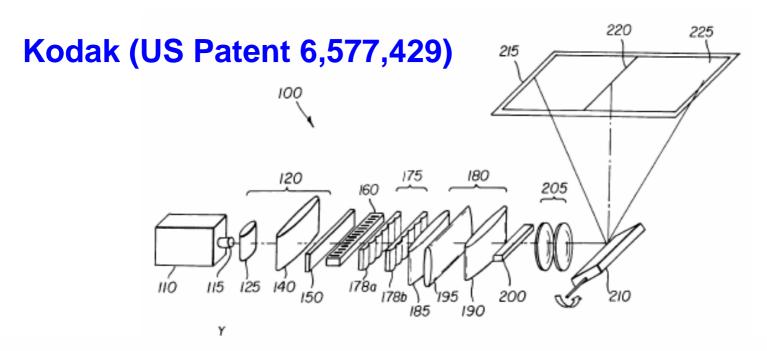


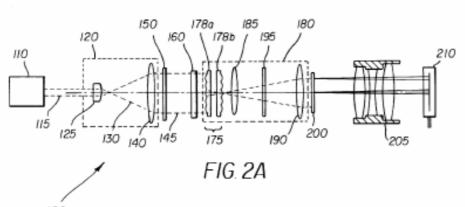


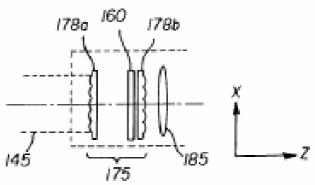








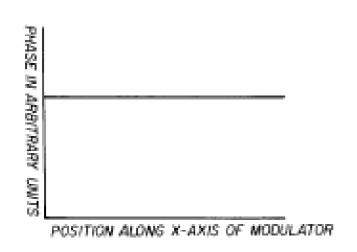


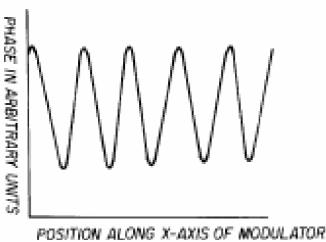


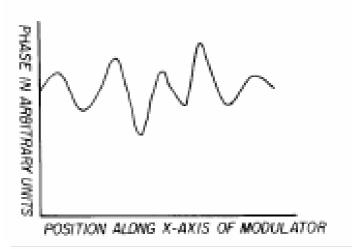


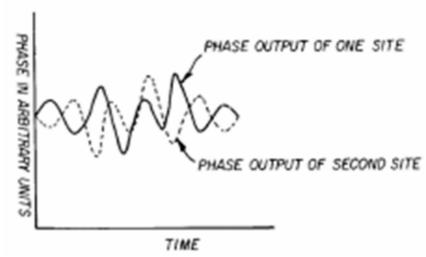


Speckle Reduction 10





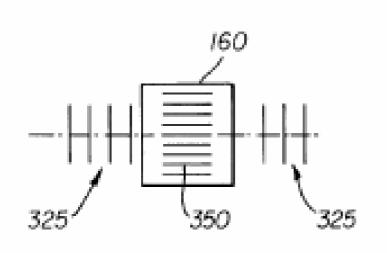


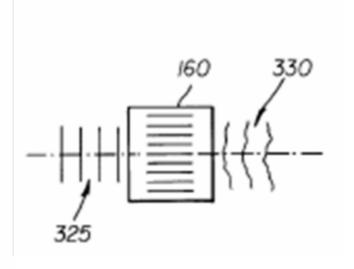


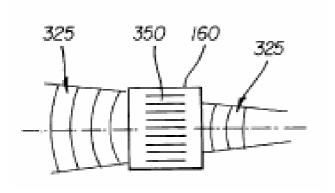


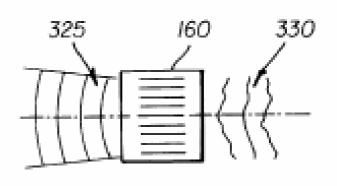


Speckle Reduction 10







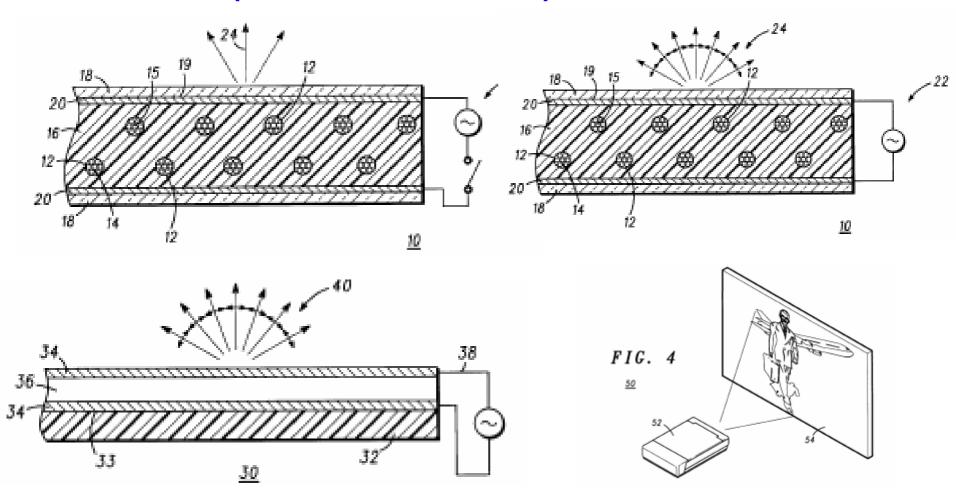






Speckle Reduction 11

Motorola (US Patent 6,122,023)







Comparison

Comparison of the speckle reducing methods

✓ Speckle contrast ratio

$$CR = \frac{\sqrt{\langle I_i^2 \rangle - \langle I_i \rangle^2}}{\langle I_i \rangle} = \frac{\sigma}{\mu}$$
 where, $\langle I_i \rangle$: intensity of the ith pixel of a CCD σ : standard deviation, μ : mean value

- "Severe" speckle is associated with contrast measurement of CR > 0.30
- Comparison of spatial coherence degradation methods

Spatial
coherence

Temporal coherence

	Component	Speckle contrast	Speckle reduction(%)	Insertion loss(%)
	Stationary diffractive diffuser	0.312	3.4	5
e	Refractive lens array(6×8)	0.309	4.3	14
C	Fiber, 2m	0.262	18.9	20
	Vibrated fiber	0.057	82.4	20
	Vibrated diffractive diffuser	0.048	85.1	5
	Vibraled projection screen	0.034	89.5	0
е	All vibrated components and lens arrays	0.009	97.2	35

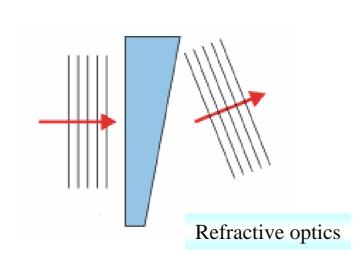
LEOS '99, IEEE, pp.354-355.

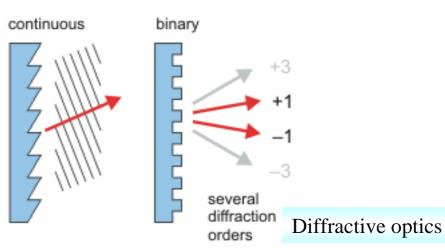




□ Diffractive optical elements (DOEs)

- Operates on the principle of diffraction and interference
- Diffractive optics control wave fronts, while traditional optic components bend light.
- DOEs can function as gratings, lenses, and any other type of optical functional elements.
- Lightweight, thin and small, low-cost, and feasible for mass-production
- Wavelength-sensitive, chromatic aberration under white light





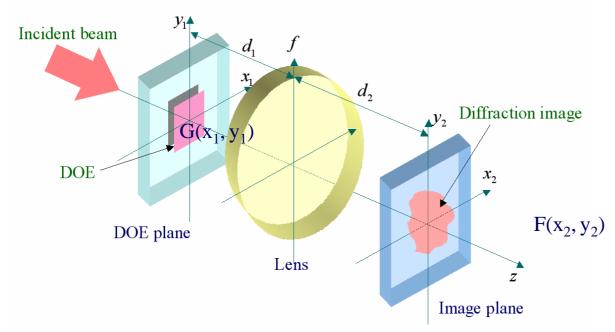


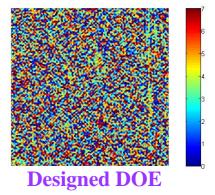


DOE Design 1

☐ Generalized paraxial optical system

$$F(x_{2}, y_{2}) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h(x_{2}, y_{2}, x_{1}, y_{1}) G(x_{1}, y_{1}) dx_{1} dy_{1} = Fr[G(x_{1}, y_{1})]$$







Reconstructed image





DOE Design 2

☐ Conventional Scalar based method

$$G(x_1, y_1) = A(x_1, y_1) \exp(i\Phi(x_1, y_1))$$

A(x, y): amplitude of incident beam \rightarrow fixed

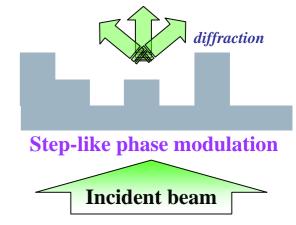
 $\Phi(x, y)$: phase distribution to be optimized

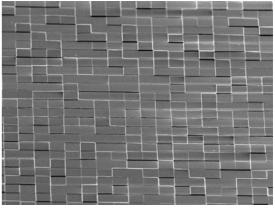
□ Optimization methods (error-reduction)

- Local optimization
 - Direct binary searching algorithm (DBS)
 - Iterative Fourier transform algorithm (IFTA)

✓ Global optimization

- Simulated annealing method (SA)
- Genetic algorithm (GA)



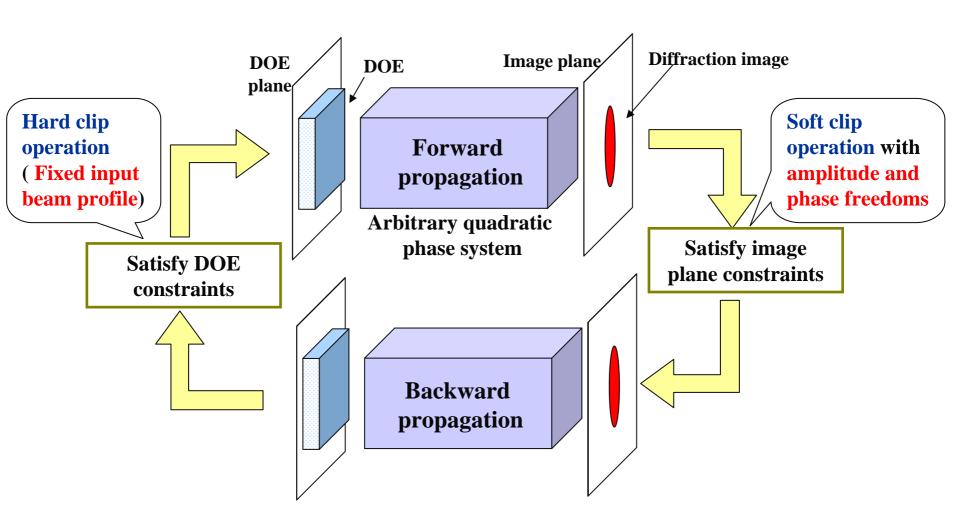


Fabricated phase profiles (SEM image)





DOE Design 3





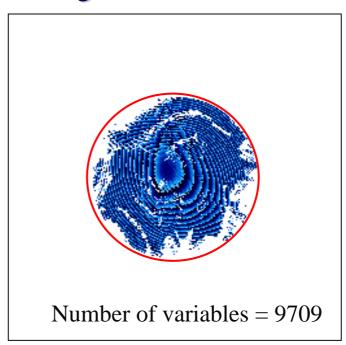


Spiral Speckle and Boundary-Modulated DOE

Proposed design



Diffraction image



DOE profile

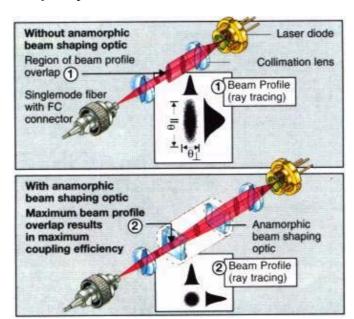
H. Kim and B. Lee, "Diffractive optical element with apodized aperture for shaping vortex-free diffraction image," Japanese Journal of Applied Physics, vol. 43, no. 12A, pp. L1530-L1533, 2004.



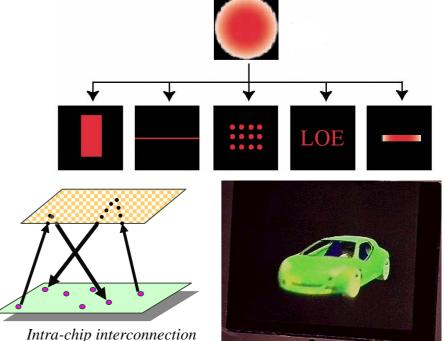


□ DOE applications

- ✓ Diffractive-refractive hybrid elements
- ✓ Beam shaping and pattern generation
- ✓ Optical interconnection
- √ 3D display





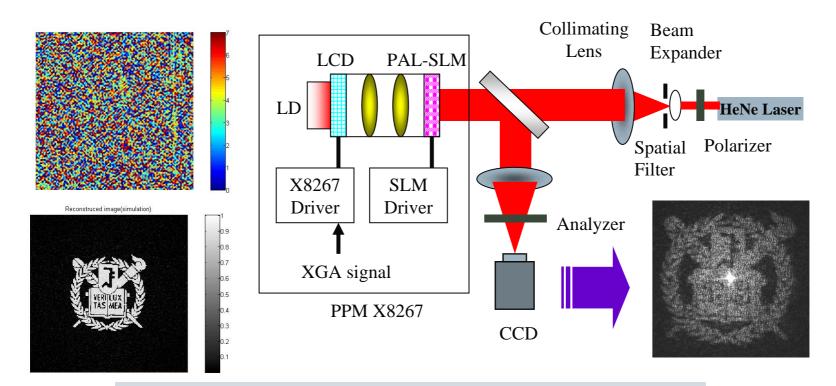






☐ Experiment of DOE

- ✓ Fourier optic system using SLM
 - Phase-type spatial light modulator + designed phase DOE

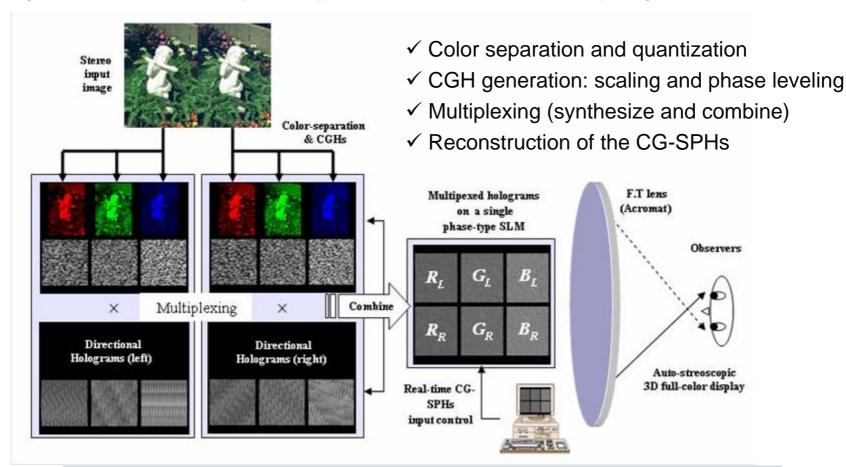


Experimental setup using phase-type SLM





☐ Synthetic DOE (CGH)s for full-color display



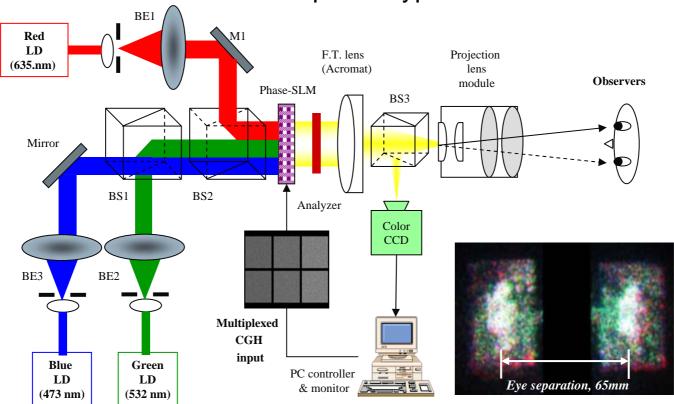
Schematic diagram for full-color 3D image generation





☐ Full-color stereoscopic image display

✓ Three color laser diodes and phase-type SLM



Experiment for full-color 3D image generation using phase-type SLM

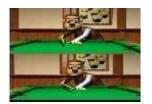




□ Full-color stereoscopic video display system



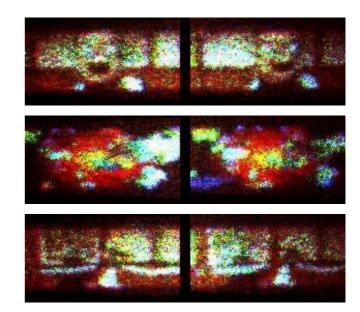
Full-color autostereoscopic 3D display demo system



Stereo input



Reconstructed stereo video (simulation)



Reconstructed stereo video (experiment)

Full-color stereoscopic video display demonstration sytem





Previous Work 1

□ Fabrication process sequence

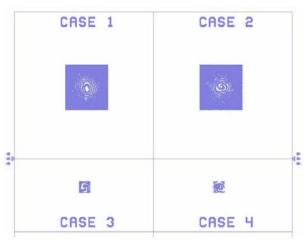
- ✓ Process sequence of DOE etching
 - Glass substrate
 - Glass cleaning
 - HMDS (hexamethyldisilane 2%) + xylene
 - PR coating
 - Soft baking
 - Photolithography exposure
 - Develop
 - Hard baking
 - Glass etching
 - PR stripe
 - Surface profile measurement

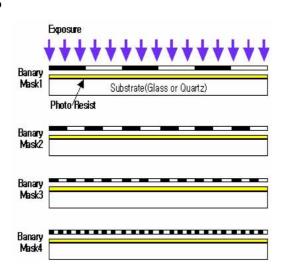


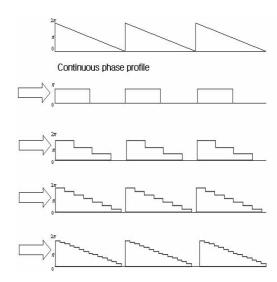


Previous Work 2

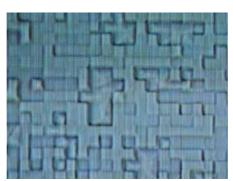
□ Fabricated DOEs

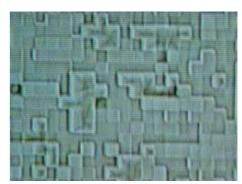












Microscope images with different focal length (height difference of the fabricated DOE)

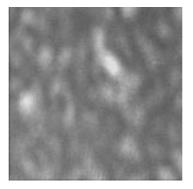




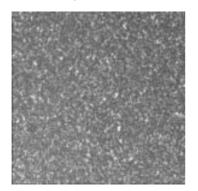
Previous Work 3

☐ Speckle intensity and histogram analysis

✓ Laser source (532nm DPSS Nd: YAG laser) + CCD



✓ DOE(16 level phase) & Rotated DOE at 5 rps









Conclusion

- □ Introduction and overview on
 - laser display systems
 - speckle reduction methods
 - DOE



