

INTRODUCTION TO CONDUCTION

- Thermal Transport Properties
- Heat Diffusion (Conduction) Equation
- Boundary and Initial Conditions

Thermal Properties of Matter

transport properties: physical structure of matter, atomic and molecular

- **thermal conductivity:** $k_x = -\frac{q''_x}{\partial T / \partial x}$

isotropic medium: $k_x = k_y = k_z = k$

- **thermal diffusivity:** α [m²/s]

$$\alpha = \frac{k}{\rho c_p} = \frac{\text{ability to conduct thermal energy}}{\text{ability to store thermal energy}}$$

Kinetic Theory

$$q''_x = -\frac{1}{3}Cv\lambda \frac{dT}{dx}$$

C : volumetric specific heat [J/m³K]

λ : mean free path [m]

v : characteristic velocity of particles [m/s]

Fourier law of heat conduction

$$q''_x = -k \frac{dT}{dx} \rightarrow k = \frac{Cv\lambda}{3}$$

$$k = \frac{1}{3}[(Cv\lambda)_l + (Cv\lambda)_e]$$

First term : lattice (phonon) contribution

Second term : electron contribution

Solids

$$k = k_e + k_l$$

Pure metal: $k_e \gg k_l$

Alloys: $k_e \sim k_l$

Non-metallic solids : $k_l > k_e$

Fluids

$$k = Cv\lambda/3 \rightarrow k \propto nv\lambda$$

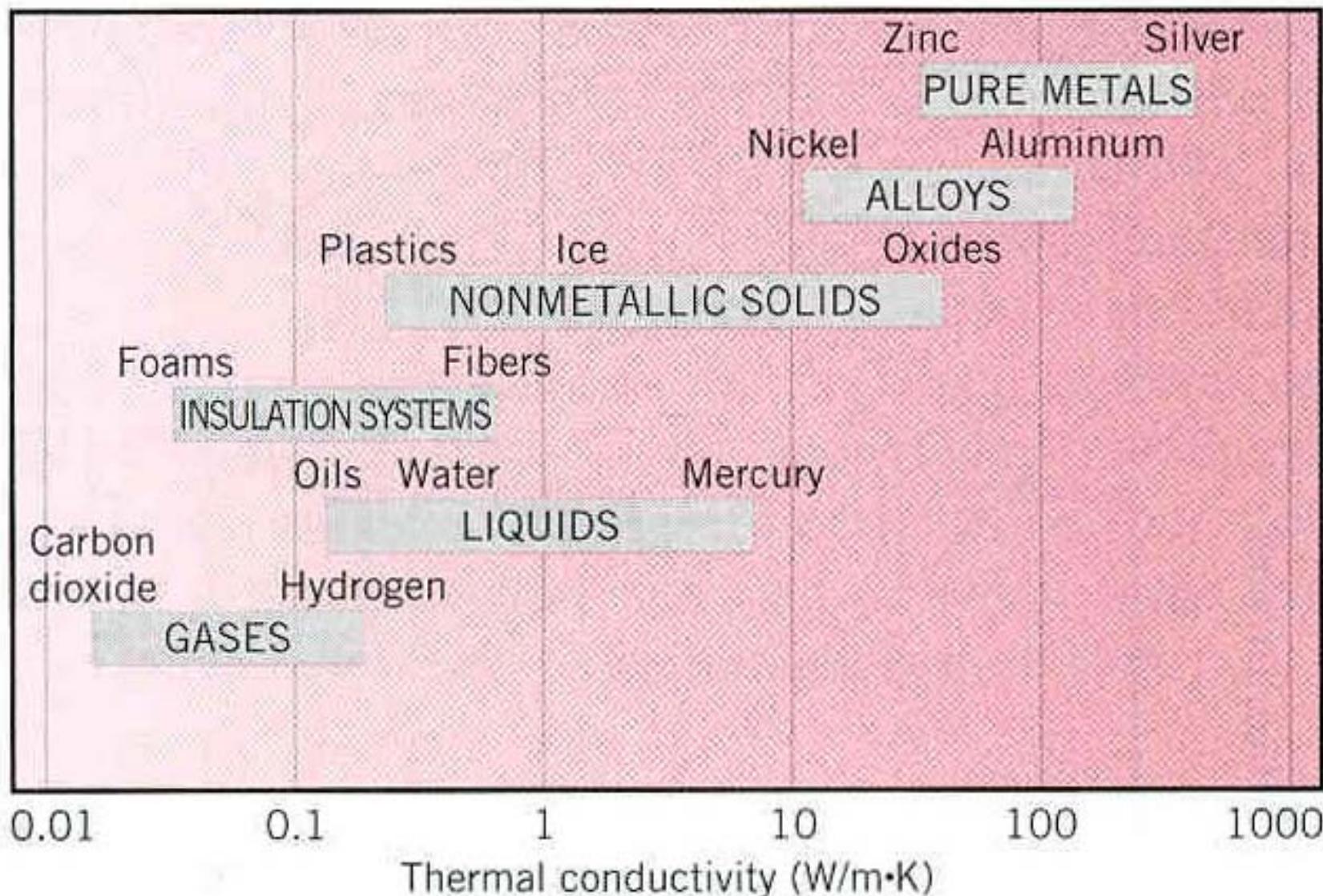
n : number of particles per unit volume

weak dependence on pressure

As p goes up, n increases

but λ becomes shorten $\rightarrow k = k(T)$

Range of thermal conductivity for various of states of matter at normal temperature and pressure



Temperature dependence of thermal conductivity of solids

Solids

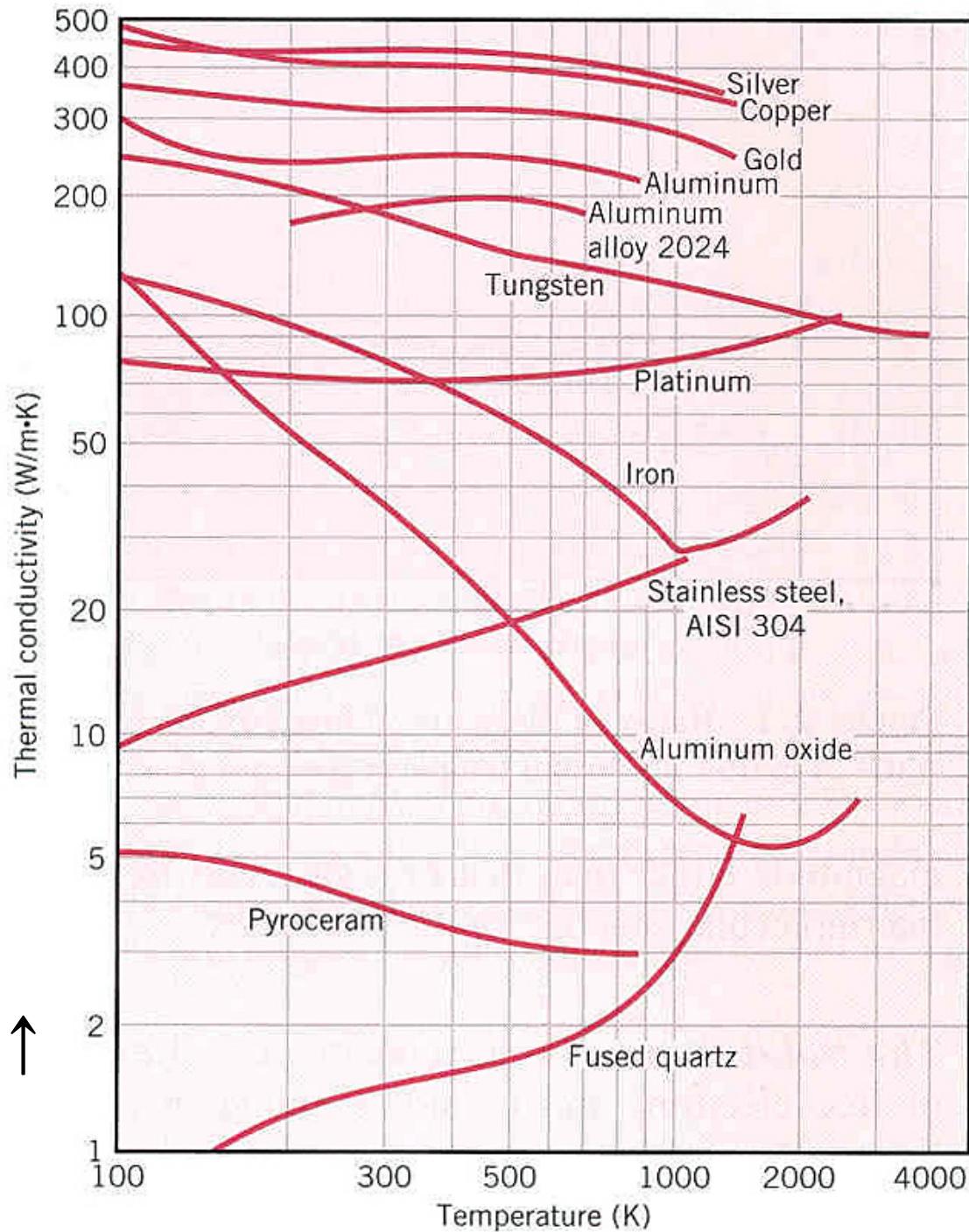
$$k = k_e + k_l$$

Pure metal: $k_e \gg k_l$

Alloys: $k_e \sim k_l$

Non-metal : $k_l > k_e$

In general, $k \downarrow$ as $T \uparrow$

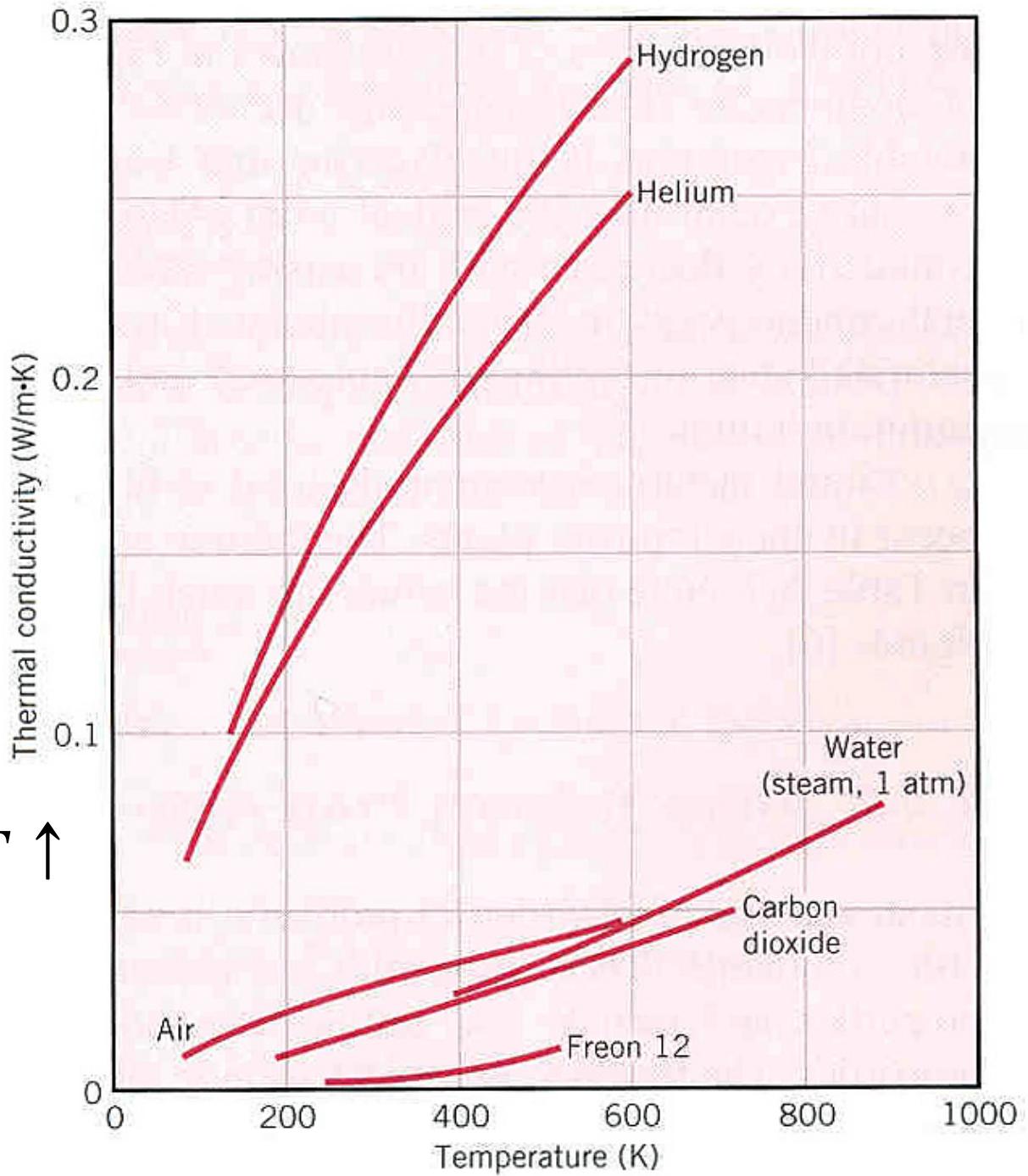


Temperature dependence of thermal conductivity of gases

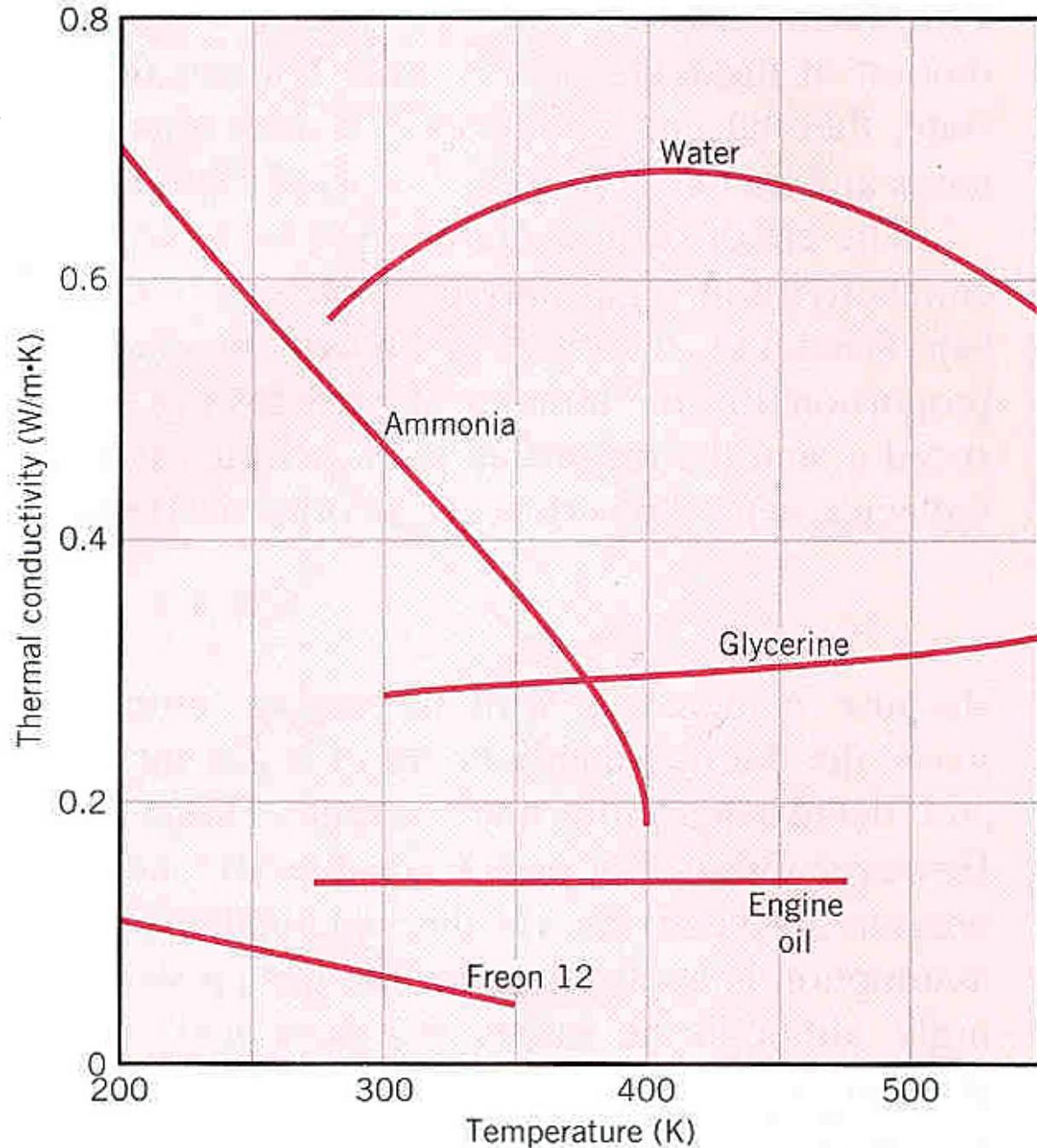
Gases

$$k = Cv\lambda/3$$

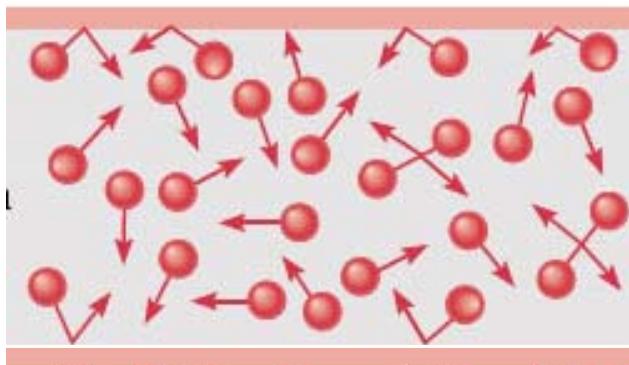
In general, $k \uparrow$ as $T \uparrow$



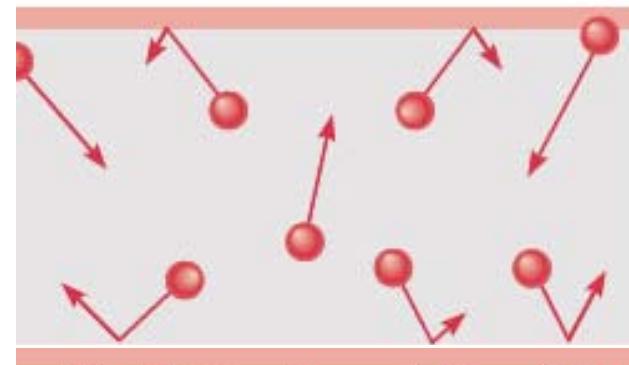
Temperature dependence of thermal conductivity of nonmetallic liquids under saturated conditions



Nanoscale Structure

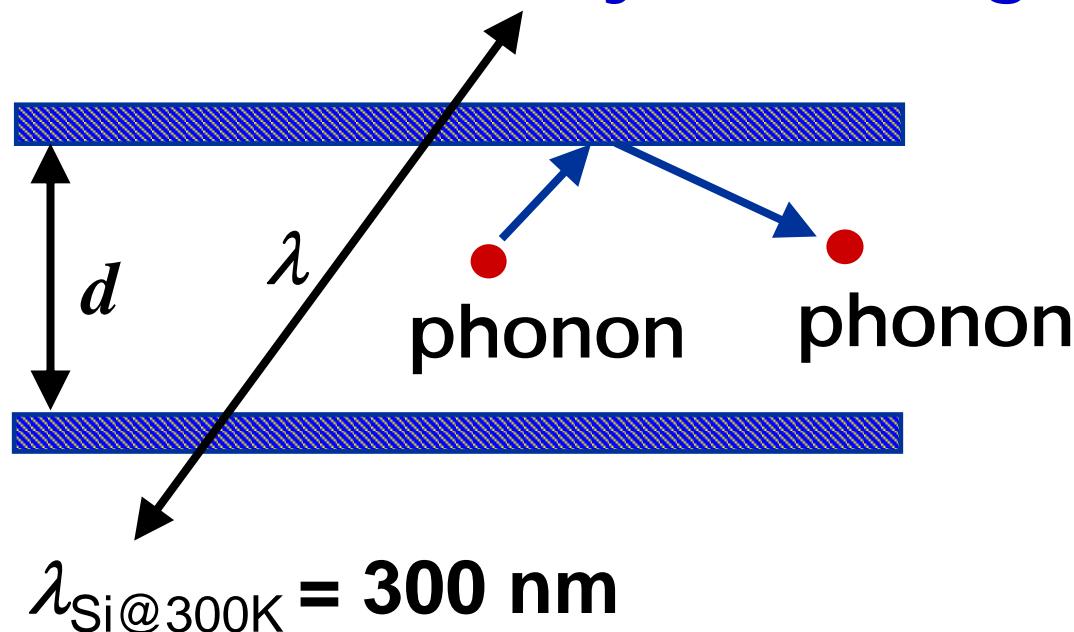


$$d \gg \lambda$$

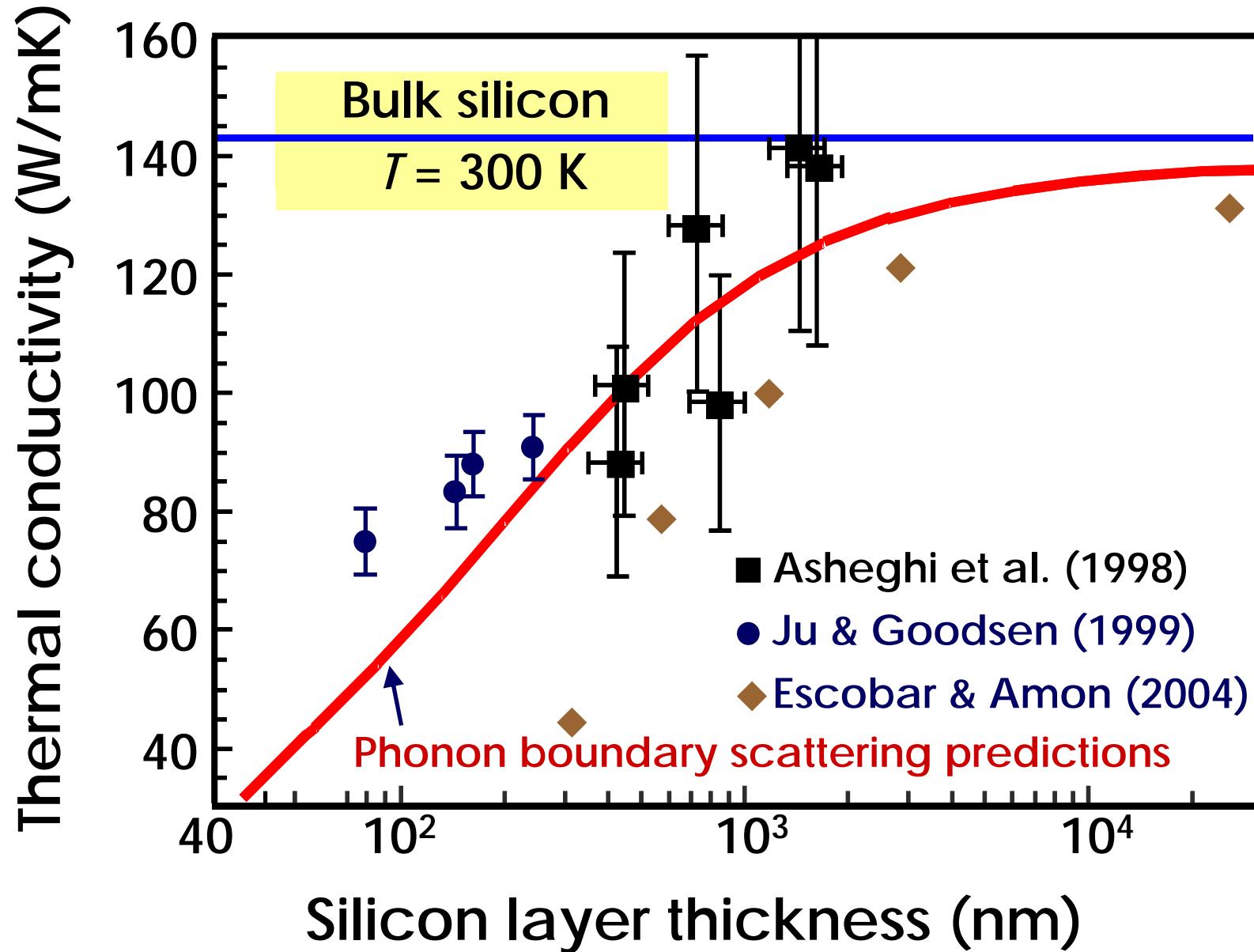


$$d \sim \lambda \text{ or less}$$

Phonon-Boundary Scattering



Thermal Conductivity of Silicon

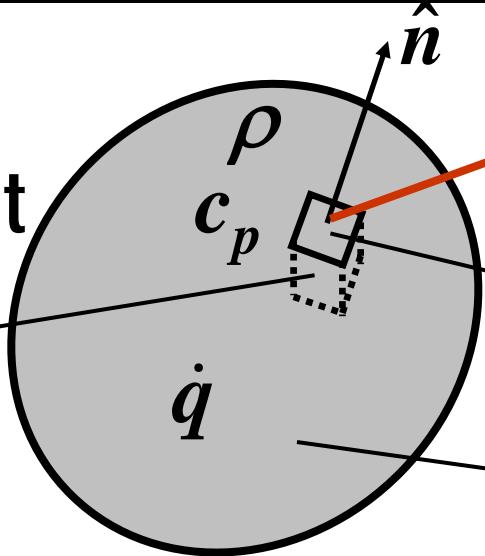


Heat Diffusion (Conduction) Equation

density ρ

specific heat

differential
volume dV



net out-going
heat flux

differential area dA

control volume V
surface area A

\dot{q} : internal heat generation rate per unit volume [W/m³]

$$\dot{E}_{\text{in}} + \dot{E}_{\text{g}} - \dot{E}_{\text{out}} = \dot{E}_{\text{st}}$$

$$\dot{E}_{\text{in}} - \dot{E}_{\text{out}} = - \int_A \vec{q}'' \cdot \hat{n} dA, \quad \dot{E}_{\text{g}} = \int_V \dot{q} dV$$

$$\dot{E}_{\text{st}} = \int_V \rho dV c_p \frac{\partial T}{\partial t} = \int_V \rho c_p \frac{\partial T}{\partial t} dV$$

$$\int_V \rho c_p \frac{\partial T}{\partial t} dV = - \int_A \vec{q}'' \cdot \hat{n} dA + \int_V \dot{q} dV$$

Divergence theorem:

$$\int_A \vec{q}'' \cdot \hat{n} dA = \int_V \nabla \cdot \vec{q}'' dV$$

Thus, $\int_V \left(\rho c_p \frac{\partial T}{\partial t} + \nabla \cdot \vec{q}'' - \dot{q} \right) dV = 0$

Since V can be chosen arbitrary, the integrand should be zero.

$$\rho c_p \frac{\partial T}{\partial t} + \nabla \cdot \vec{q}'' - \dot{q} = 0 \quad \text{or} \quad \rho c_p \frac{\partial T}{\partial t} = -\nabla \cdot \vec{q}'' + \dot{q}$$

Fourier law : $\vec{q}'' = -k\nabla T$

$$\rho c_p \frac{\partial T}{\partial t} = -\nabla \cdot \vec{q}'' + \dot{q} \rightarrow \rho c_p \frac{\partial T}{\partial t} = \nabla \cdot (k \nabla T) + \dot{q}$$

For constant k : $\frac{\partial T}{\partial t} = \alpha \nabla^2 T + \frac{\dot{q}}{\rho c_p}$

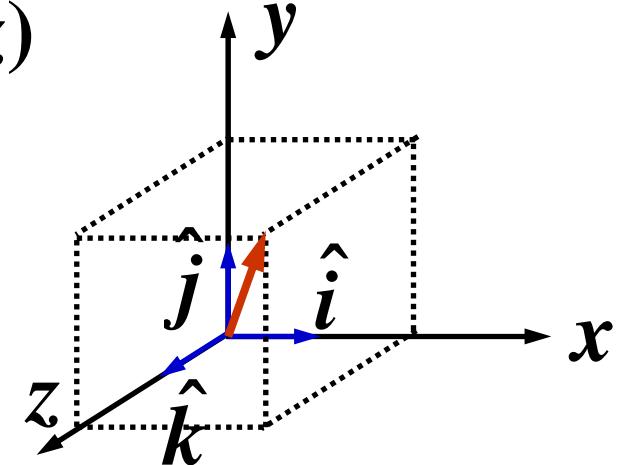
Steady-state : $\nabla \cdot (k \nabla T) + \dot{q} = 0$

Constant k : $\nabla^2 T + \frac{\dot{q}}{k} = 0$

No heat generation : $\nabla^2 T = 0$

Cartesian coordinates (x, y, z)

$$\vec{q}'' = -k \left(\frac{\partial T}{\partial x} \hat{i} + \frac{\partial T}{\partial y} \hat{j} + \frac{\partial T}{\partial z} \hat{k} \right)$$



$$\rho c_p \frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \dot{q}$$

Steady-state, constant k , no heat generation

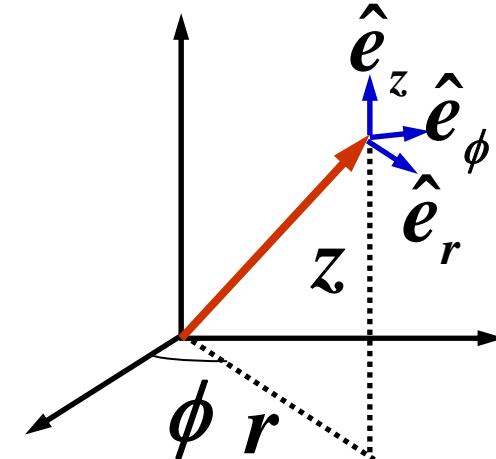
$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} = 0$$

Cylindrical coordinates (r, ϕ, z)

$$\vec{q}'' = -k \left(\frac{\partial T}{\partial r} \hat{e}_r + \frac{1}{r} \frac{\partial T}{\partial \phi} \hat{e}_\phi + \frac{\partial T}{\partial z} \hat{e}_z \right)$$

$$\rho c_p \frac{\partial T}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left(kr \frac{\partial T}{\partial r} \right)$$

$$+ \frac{1}{r^2} \frac{\partial}{\partial \phi} \left(k \frac{\partial T}{\partial \phi} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \dot{q}$$

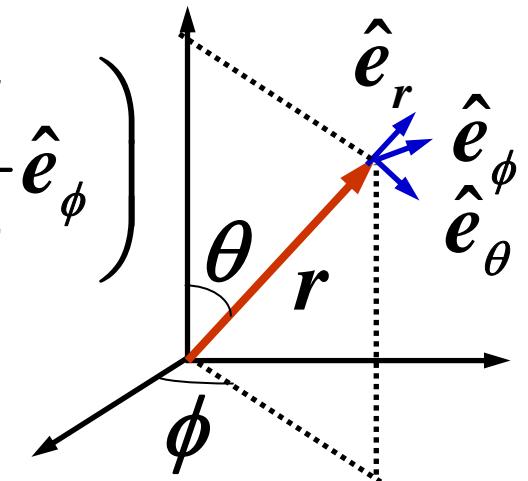


Steady-state, constant k , no heat generation

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 T}{\partial \phi^2} + \frac{\partial^2 T}{\partial z^2} = 0$$

Spherical coordinates (r, ϕ, θ)

$$\vec{q}'' = -k \left(\frac{\partial T}{\partial r} \hat{e}_r + \frac{1}{r} \frac{\partial T}{\partial \theta} \hat{e}_\theta + \frac{1}{r \sin \theta} \frac{\partial T}{\partial \phi} \hat{e}_\phi \right)$$



$$\rho c_p \frac{\partial T}{\partial t} = \frac{1}{r^2} \frac{\partial}{\partial r} \left(k r^2 \frac{\partial T}{\partial r} \right)$$

$$+ \frac{1}{r^2 \sin^2 \theta} \frac{\partial}{\partial \phi} \left(k \frac{\partial T}{\partial \phi} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(k \sin \theta \frac{\partial T}{\partial \theta} \right) + \dot{q}$$

Steady-state, constant k , no heat generation

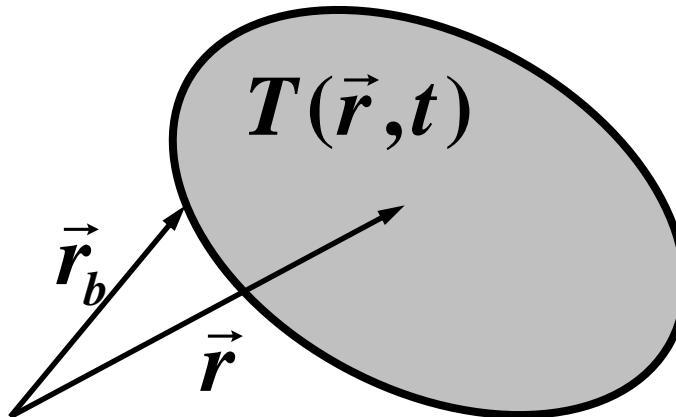
$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) = 0$$

Boundary and Initial Conditions

Equations: Elliptic, Parabolic, Hyperbolic eq.

$$\rho c_p \frac{\partial T}{\partial t} = \nabla \cdot (k \nabla T) + \dot{q}$$

elliptic in space and parabolic in time



1. Initial condition

condition in the medium at $t = 0$:

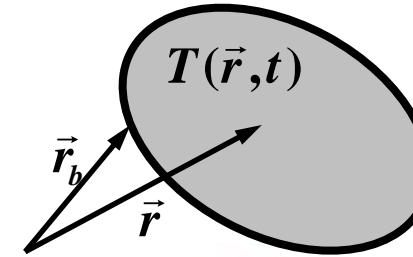
$$T(\vec{r}, 0) = f(\vec{r}) \text{ or constant}$$

2. Boundary conditions

1) Dirichlet (first kind)

variable value specified at the boundaries

$$T(\vec{r}_b, t) = \alpha(t) \text{ or constant}$$

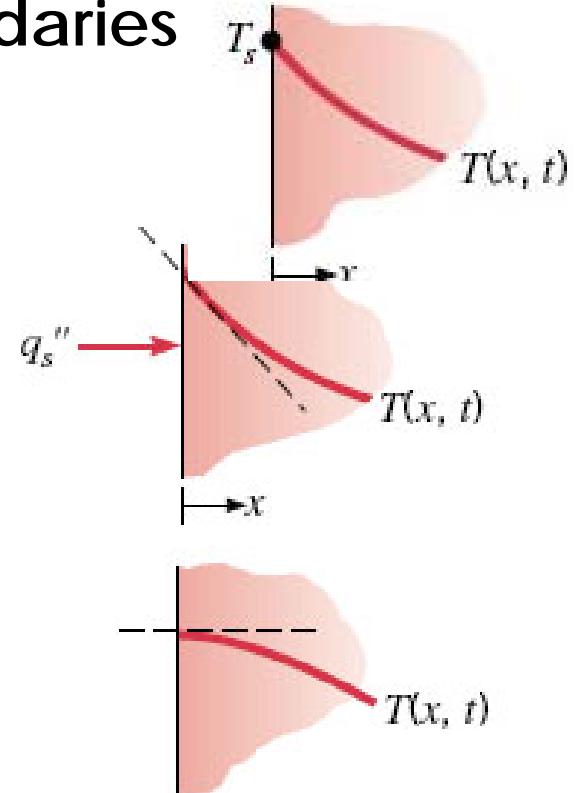


2) Neumann (second kind)

gradient specified at the boundaries

$$\frac{\partial T}{\partial n}(\vec{r}_b, t) = \beta(t) \text{ or constant}$$

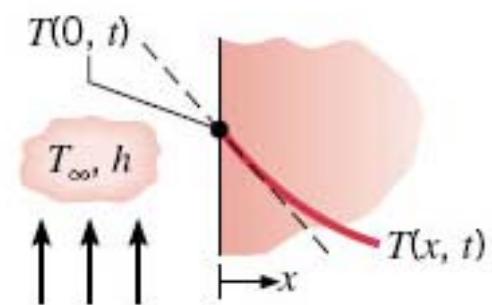
when $\beta(t) = 0$: adiabatic condition



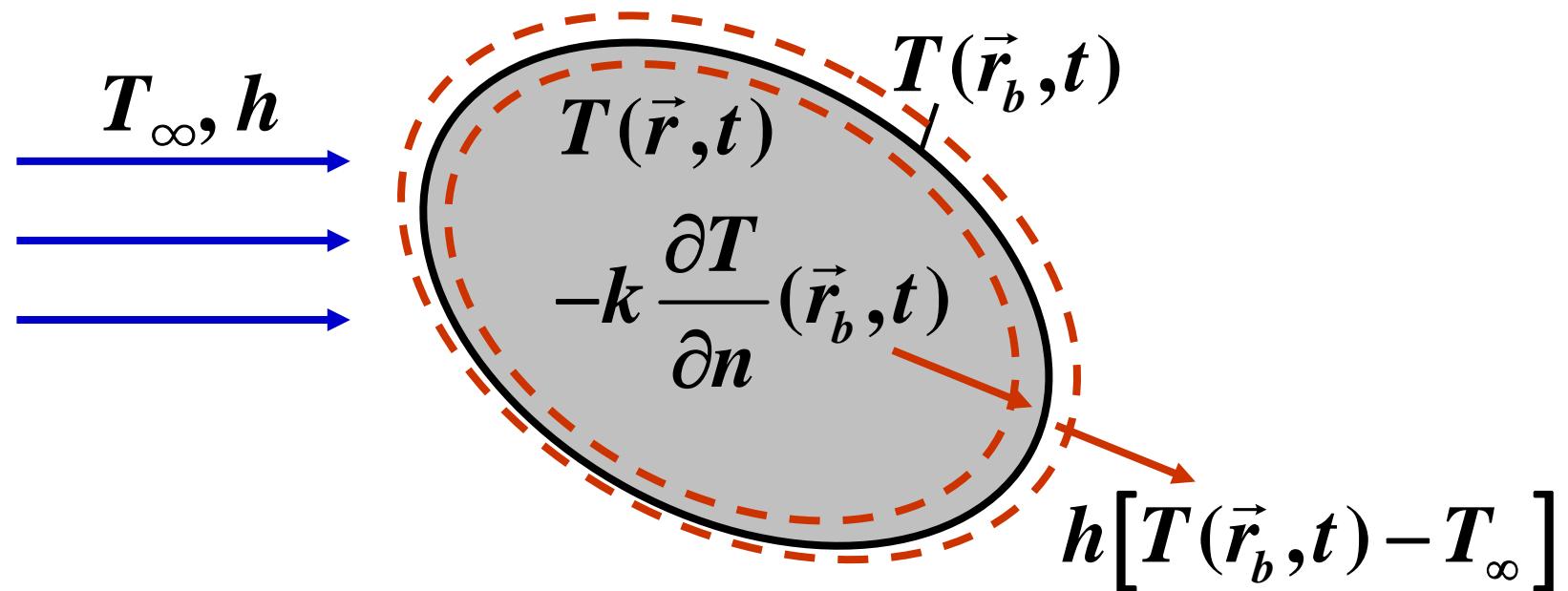
3) Cauchy (third kind)

mixed boundary condition

$$a \frac{\partial T}{\partial n}(\vec{r}_b, t) + bT(\vec{r}_b, t) = \gamma(t) \text{ or constant}$$

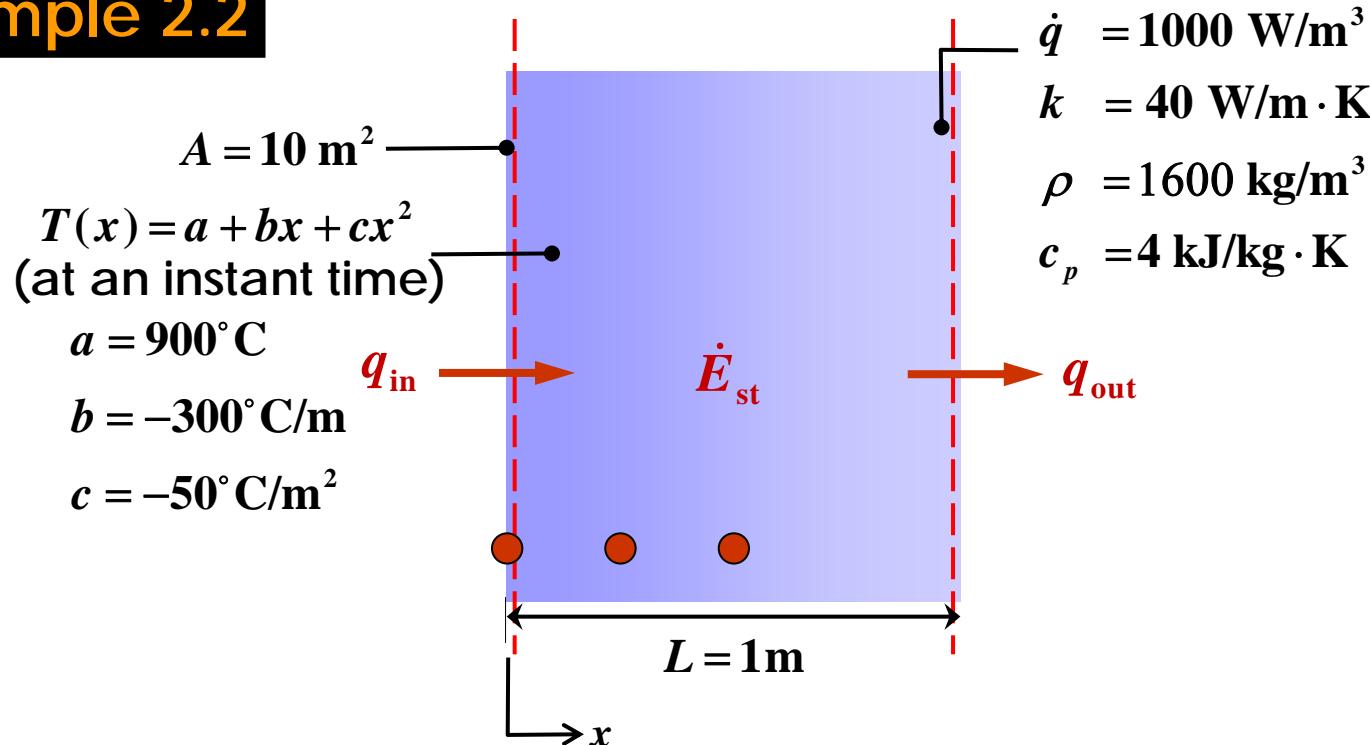


convection boundary condition



$$-k \frac{\partial T}{\partial n}(\vec{r}_b, t) = h[T(\vec{r}_b, t) - T_\infty]$$

Example 2.2

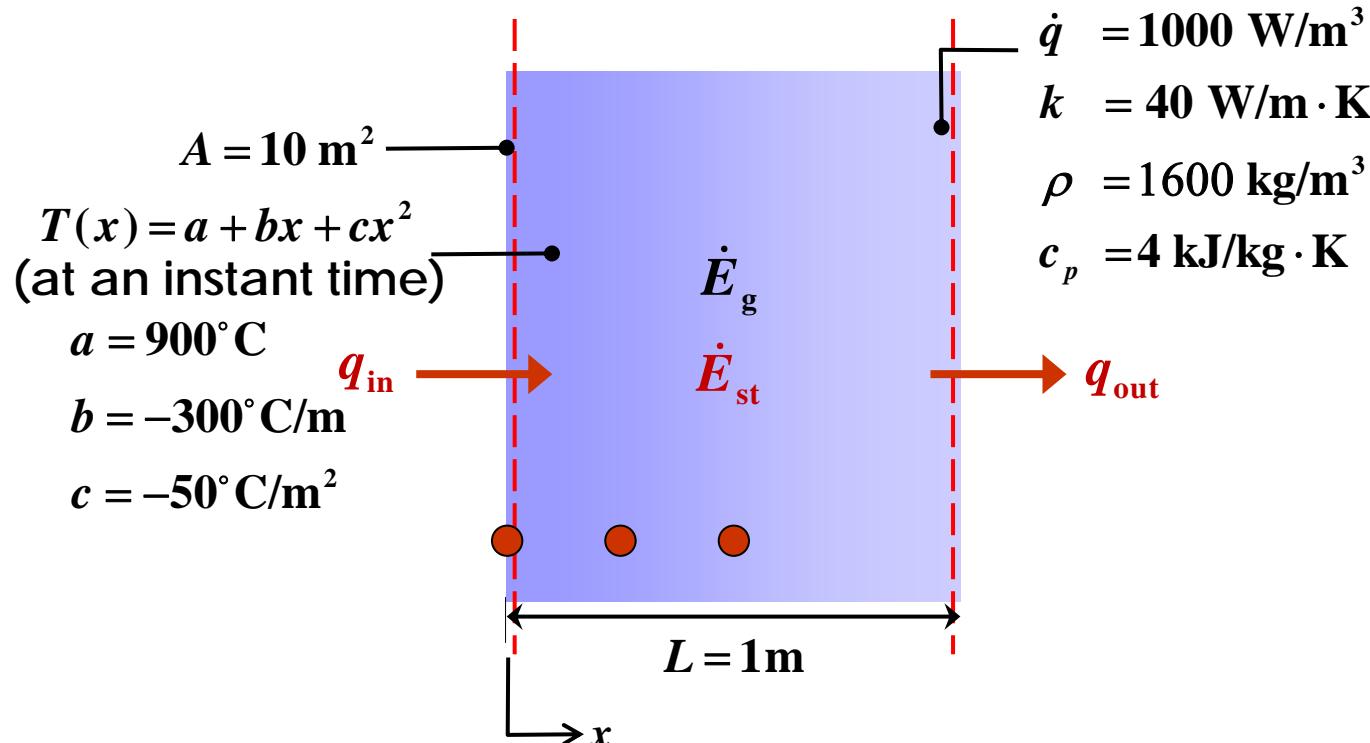


Find

- 1) Heat rates entering, $q_{\text{in}}(x = 0)$, and leaving, $q_{\text{out}}(x = 1)$, the wall
- 2) Rate of change of energy storage in the wall, \dot{E}_{st}
- 3) Time rate of temperature change $\frac{\partial T}{\partial t}$ at $x = 0, 0.25$, and 0.5 m

Assumptions :

- 1) 1-D conduction in the x -direction
- 2) Homogeneous medium with constant properties
- 3) Uniform internal heat generation

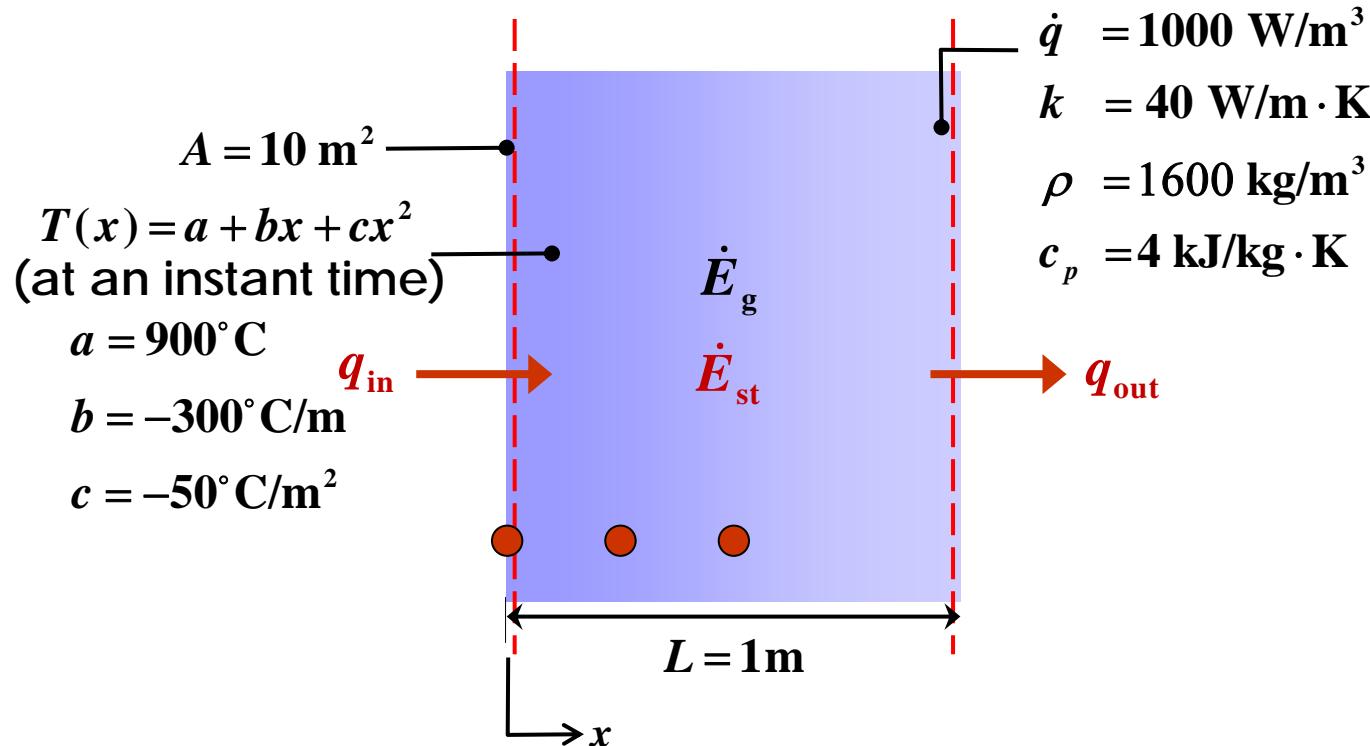


$$1) \quad q_{in} = q_x(0) = -kA \frac{\partial T}{\partial x} \Big|_{x=0}, \quad q_{out} = q_x(L) = -kA \frac{\partial T}{\partial x} \Big|_{x=L} \quad \frac{\partial T}{\partial x} = b + 2cx$$

$$q_{in} = -kAb = -(40 \text{ W/m} \cdot \text{K})(10 \text{ m}^2)(-300^\circ\text{C}/\text{m}) = 120 \text{ kW}$$

$$\begin{aligned} q_{out} &= -kA(b + 2cL) \\ &= -(40 \text{ W/m} \cdot \text{K})(10 \text{ m}^2) \left[-300^\circ\text{C}/\text{m} + 2 \times (-50^\circ\text{C}/\text{m}^2) \times (1 \text{ m}) \right] = 160 \text{ kW} \end{aligned}$$

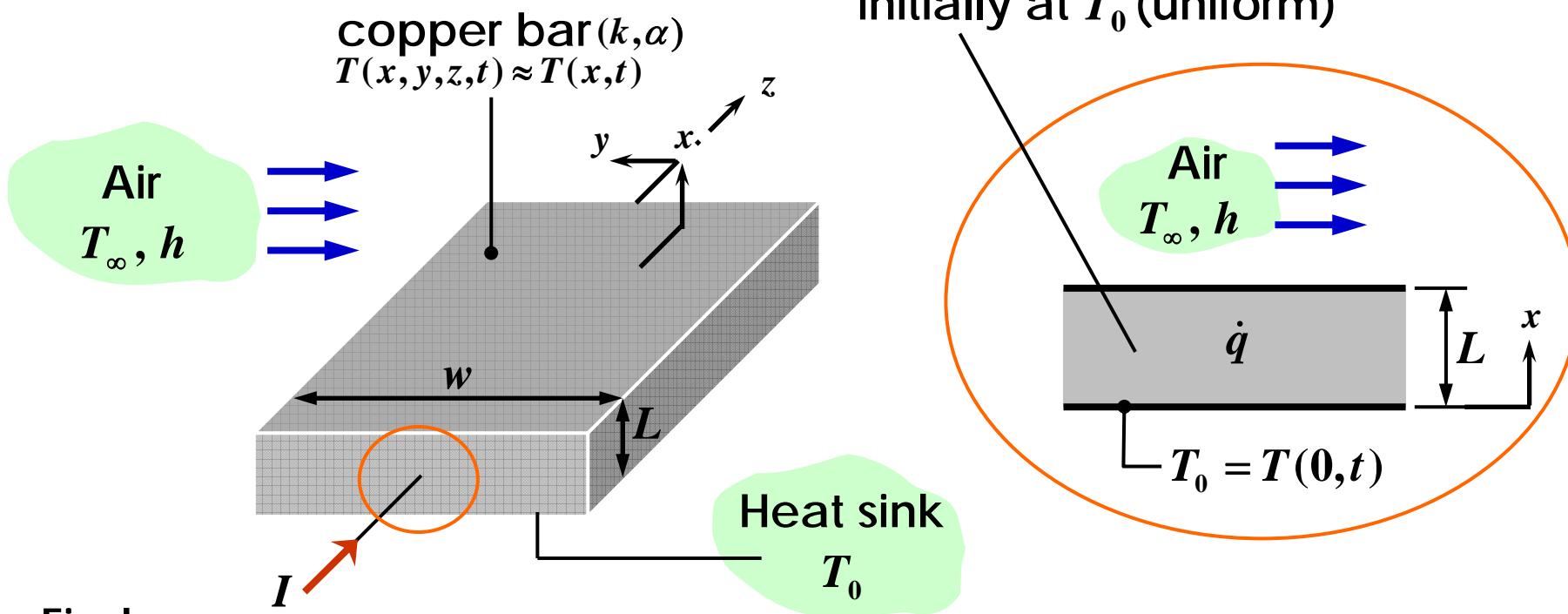
$$\begin{aligned} T(x) &= a + bx + cx^2 = 900^\circ\text{C} + (-300^\circ\text{C}/\text{m})x + (-50^\circ\text{C}/\text{m}^2)x^2 \\ &= 1173 \text{ K} + (-300 \text{ K/m})x + (-50 \text{ K/m}^2)x^2 \end{aligned}$$



$$\begin{aligned}
2) \quad \dot{E}_{\text{st}} &= \dot{E}_{\text{in}} + \dot{E}_g - \dot{E}_{\text{out}} = q_{\text{in}} + \dot{q}AL - q_{\text{out}} \\
&= 120 \text{ kW} + (1000 \text{ W/m}^3)(10 \text{ m}^2)(1 \text{ m}) - 160 \text{ kW} = -30 \text{ kW}
\end{aligned}$$

$$\begin{aligned}
3) \quad \frac{\partial T}{\partial t} &= \frac{k}{\rho C_p} \frac{\partial^2 T}{\partial x^2} + \frac{\dot{q}}{\rho C_p} \quad \frac{\partial^2 T}{\partial x^2} = 2c \\
&= -4.69 \times 10^{-4} \text{ }^\circ\text{C}
\end{aligned}$$

Example 2.3

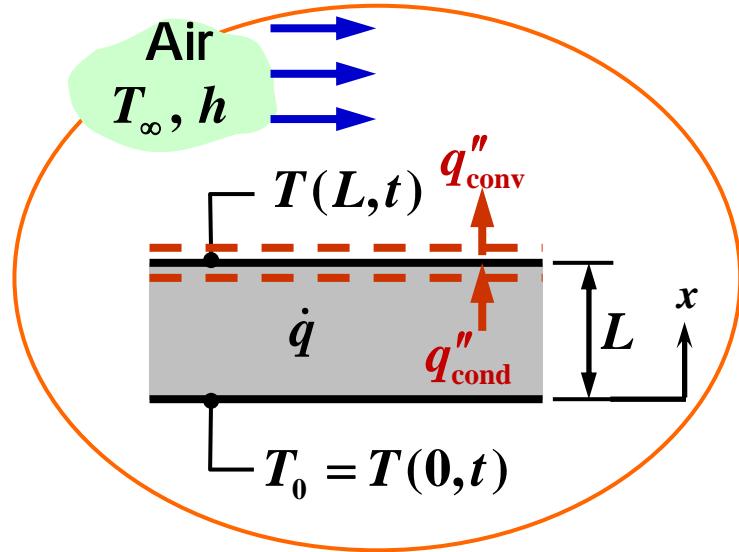


Find :

Differential equation and B.C. and I.C. needed to determine T as a function of position and time within the bar

Assumptions :

- 1) Since $w \gg L$, side effects are negligible and heat transfer within the bar is 1-D in the x -direction
- 2) Uniform volumetric heat generation
- 3) Constant properties



governing equation

1-D unsteady with heat generation

$$\rho c_p \frac{\partial T}{\partial t} = k \frac{\partial^2 T}{\partial x^2} + \dot{q}$$

B.C. at the bottom surface :

$$T(0,t) = T_0$$

B.C. at the top surface : convection boundary condition

$$q''_{\text{cond}} = q''_{\text{conv}} \rightarrow -k \frac{\partial T}{\partial x} \Big|_{x=L} = h[T(L,t) - T_\infty]$$

I.C. $T(x,0) = T_0$