

재료상변태

Phase Transformation of Materials

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Contents for previous class

- **Tracer Diffusion in Binary Alloys**
- **Diffusion in Ternary Alloy**
- **High-Diffusivity Paths**
 - 1) **Diffusion along Grain Boundaries and Free Surface**
 - 2) **Diffusion Along Dislocation**
- **Diffusion in Multiphase Binary Systems**

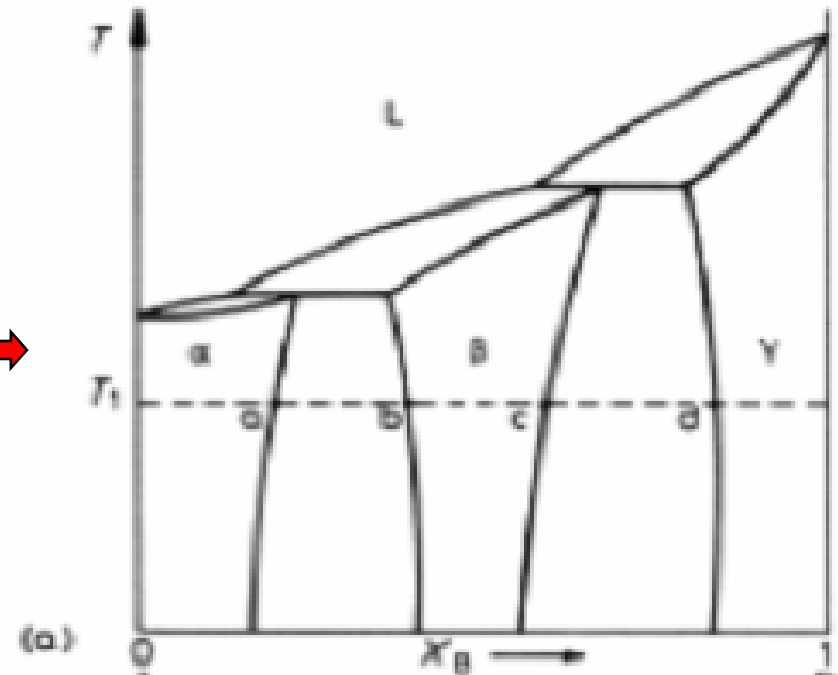
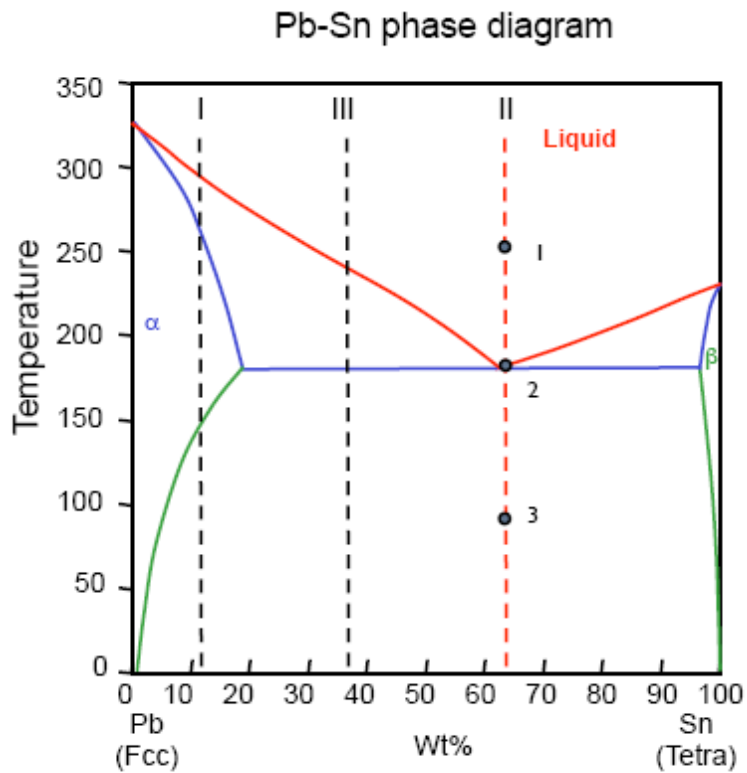
Contents for today's class

- Diffusion in multiphase binary system

Chapter 3 Crystal Interfaces and Microstructure

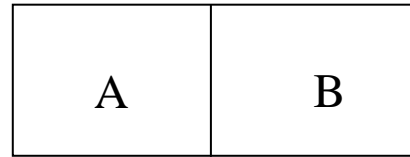
- Interfacial Free Energy
- Solid/Vapor Interfaces

2.8 Diffusion in multiple binary system



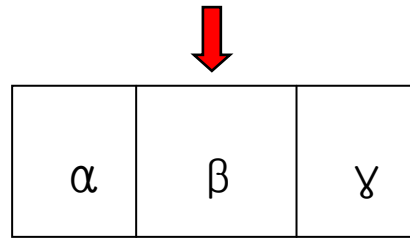
2.8 Diffusion in multiple binary system

A diffusion couple made by welding together pure A and pure B

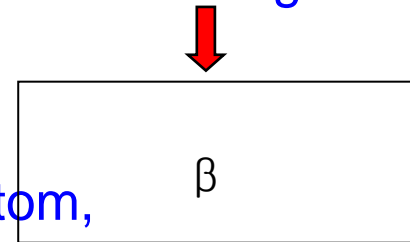


What would be the microstructure evolved after annealing at T_1 ?

→ a layered structure containing α , β & γ .



Draw a phase distribution and composition profile in the plot of distance vs. X_B after annealing at T_1 .

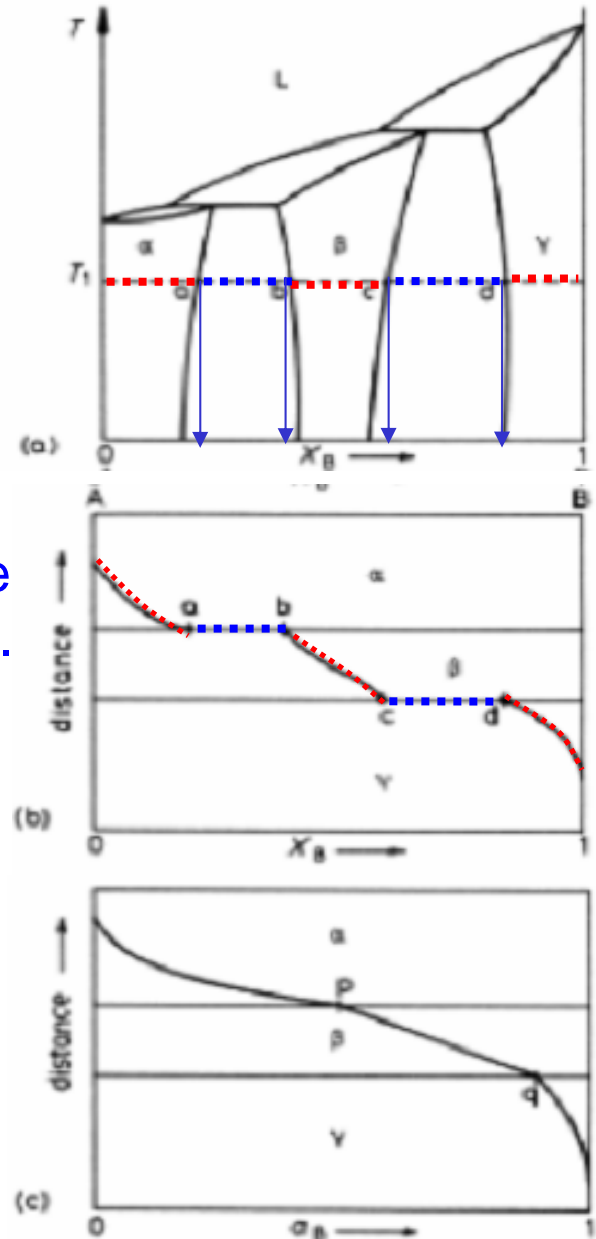


Draw a profile of activity of B atom, in the plot of distance vs. a_B after annealing at T_1 .

A or B atom → easy to jump interface (local equil.)

$$\rightarrow \mu_A^\alpha = \mu_A^\beta, \mu_A^\beta = \mu_A^\gamma \text{ at interface}$$

$$(a_A^\alpha = a_A^\beta, a_A^\beta = a_A^\gamma)$$



How can we formulate the interface (α/β , β/γ) velocity?

If unit area of the interface moves a distance dx ,
 a volume ($dx \cdot 1$) will be converted
 from α containing C_B^α atoms/ m^3
 to β containing C_B^β atoms/ m^3 .

$$(C_B^\beta - C_B^\alpha) dx \rightarrow \text{shaded area}$$

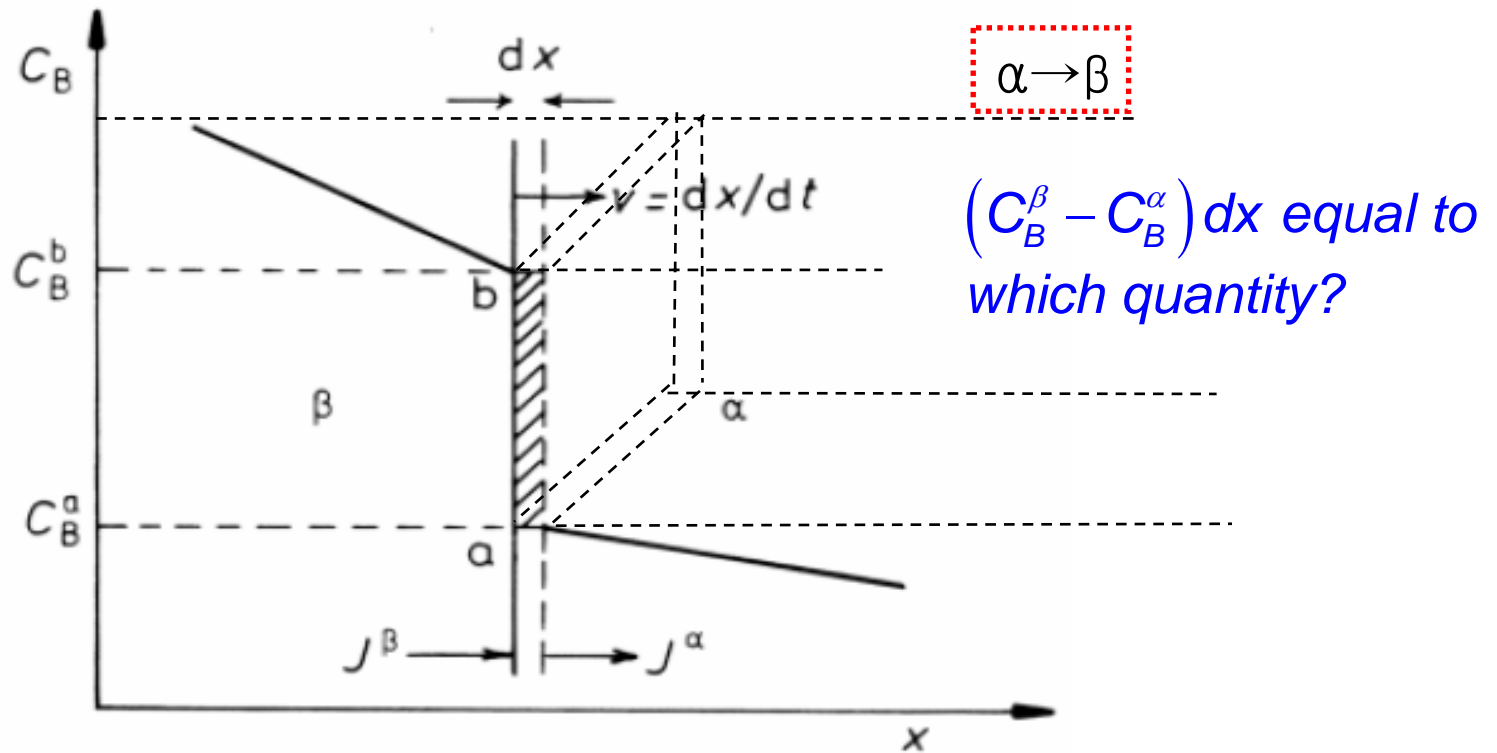


Fig. 2.30. Concentration profile across the α/β interface and its associated movement assuming diffusion control.

Local equilibrium is assumed.

A flux of B towards the interface from the β phase

$$J_B^\beta = -\tilde{D}(\beta) \frac{\partial C_B^b}{\partial x}$$

A flux of B away from the interface into the α phase

$$J_B^\alpha = -\tilde{D}(\alpha) \frac{\partial C_B^a}{\partial x}$$

In a time dt , there will be an accumulation of B atoms given by

$$\frac{\partial C}{\partial t} = -D \frac{\partial^2 C}{\partial x^2}$$



$$\frac{\partial C}{\partial t} = -\frac{\partial J}{\partial x}$$

$$- [J_B^\beta - J_B^\alpha] dt$$

$$dC dx$$

$$\left\{ -\left(\tilde{D}(\beta) \frac{\partial C_B^b}{\partial x} \right) - \left(-\tilde{D}(\alpha) \frac{\partial C_B^a}{\partial x} \right) \right\} dt = (C_B^b - C_B^a) dx$$

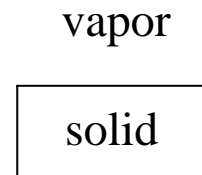
$$v = \frac{dx}{dt} = \frac{1}{(C_B^b - C_B^a)} \left\{ \tilde{D}(\alpha) \frac{\partial C_B^a}{\partial x} - \tilde{D}(\beta) \frac{\partial C_B^b}{\partial x} \right\}$$

(velocity of the α/β interface)

3. Crystal interfaces and microstructure

- Types of Interface

1. Free surface (solid/vapor interface)



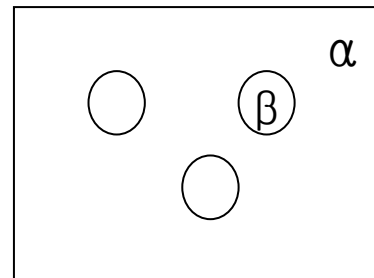
2. Grain boundary (α/α interfaces)

> same composition, same crystal structure

> different orientation

3. inter-phase boundary (α/β interfaces)

> different composition & crystal structure



⇒ defect

⇒ energy ↑

3.1 Interfacial Free Energy

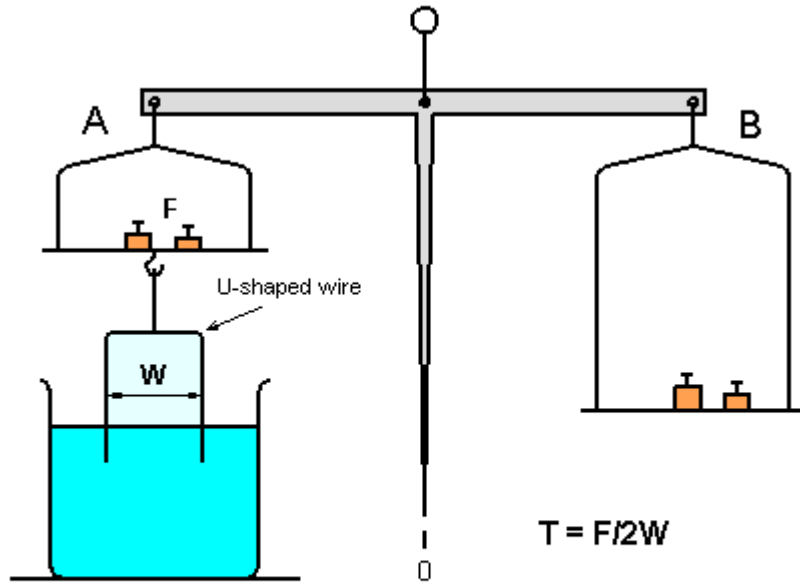


Figure 5 - Experimental device to measure the surface tension of a liquid.

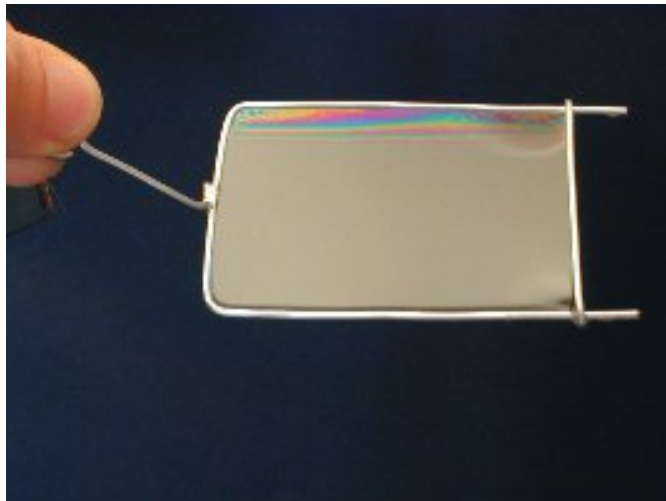


Figure 6 - "U" frame in the liquid under examination.

3.1. Interfacial free energy

Interfacial energy (γ : J/m²)

→ The Gibbs free energy of a system containing an interface of area A

$$\rightarrow G_{\text{bulk}} + G_{\text{interface}} \begin{array}{|c|} \hline \text{vapor} \\ \hline \text{solid} \\ \hline \end{array} \rightarrow G = G_0 + \gamma A$$

Interfacial energy (γ) vs. surface tension (F: a force per unit length)

1) work done : $F dA = dG$

2) $dG = \gamma dA + A d\gamma$

→ $F = \gamma + A d\gamma/dA$

In case of a liq. film, $d\gamma/dA = 0$, $F = \gamma$ (N/m = J/m²)

Ex) liq. : $d\gamma/dA = 0$ Why? **Rearrangement**

sol. : $d\gamma/dA \neq 0$, but, very small value

At near melting temperature $d\gamma/dA = 0$

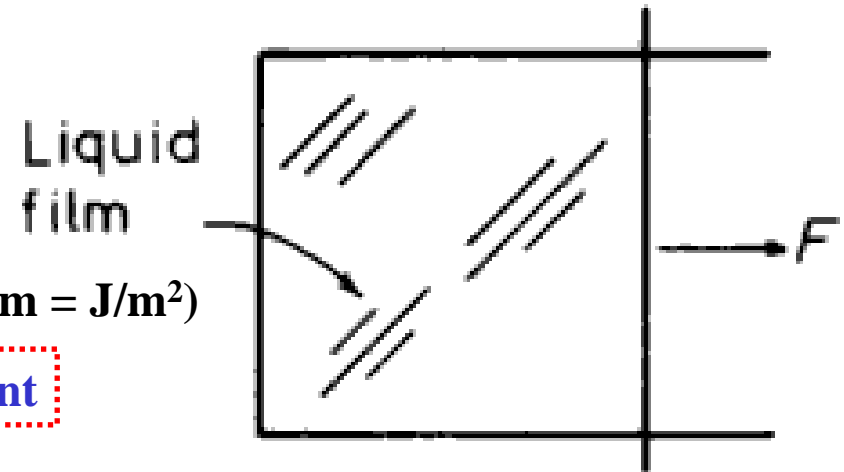


Fig. 3.1 A liquid film on a wire frame.

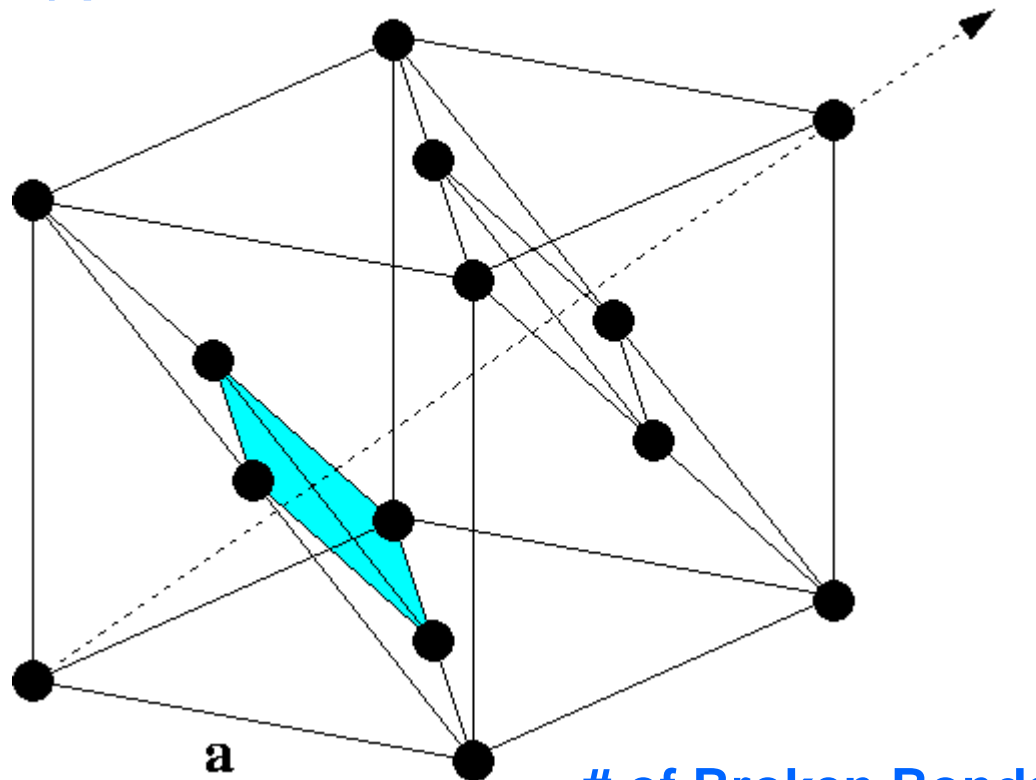
3.2 Solid / Vapor Interfaces

* Hard sphere model

- Fcc : density of atoms in these planes decreases as $(h^2+k^2+l^2)$ increases

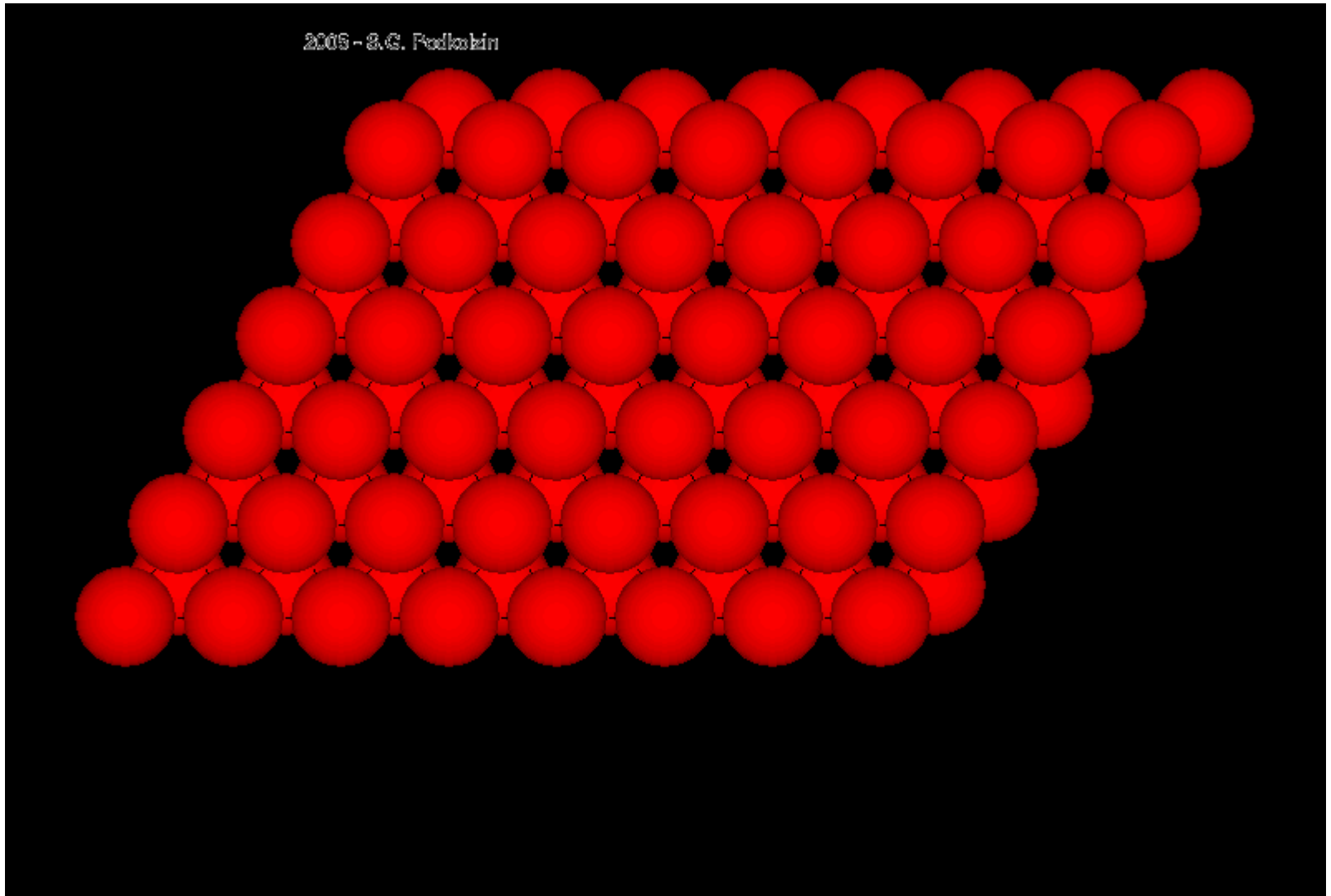
Origin of the surface free energy? → Broken Bonds

For (111) plane CN=12



of Broken Bonds per atom at surface?

of Broken Bonds per atom at surface? → 3 per atom



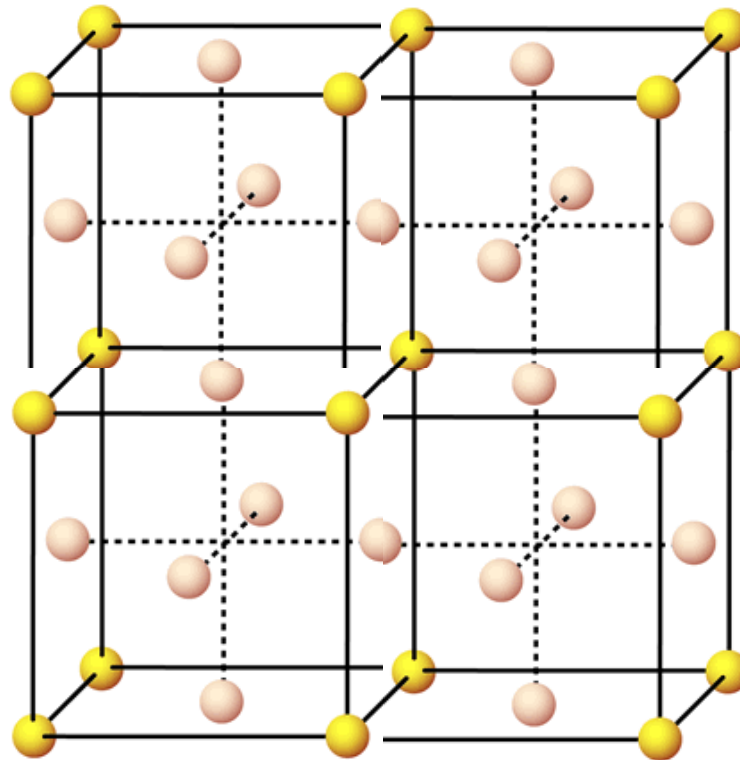
For (111) plane

of broken bond at surface : 3 broken bonds

Bond Strength: ϵ >> for each atom : $\epsilon/2$

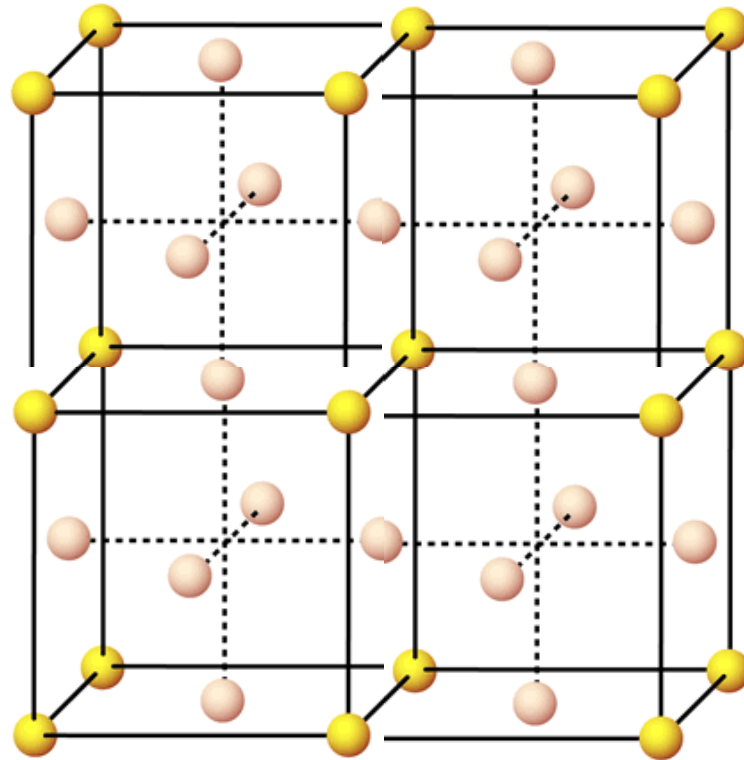
Lowering of Internal Energy per Bond: $3\epsilon/2$ ↓

For (200) plane CN=12



of Broken Bonds per atom at surface?

For (200) plane CN=12



of Broken Bonds per atom at surface?

of broken bond at surface : 4 broken bonds

Bond Strength: ϵ \gg for each atom : $\epsilon/2$

Lowering of Internal Energy per Bond: $4\epsilon/2$ ↓

For (100) plane

of broken bond at surface : **3 broken bonds**

Bond Strength: ϵ >> for each atom : $\epsilon/2$

Lowering of Internal Energy per Bond: $3\epsilon/2$

Heat of Sublimation in terms of ϵ ? $\rightarrow L_S = 12 N_a \epsilon/2$

Energy per atom of a {111} Surface?

$$E_{SV} = 3 \epsilon/2 = 0.25 L_S / N_a \quad E_{SV} \text{ vs } \gamma ?$$

γ interfacial energy = free energy (J/m²)

$$\rightarrow \gamma = G = H - TS$$

$$= E + PV - TS \quad (: PV \text{ is ignored})$$

$$\rightarrow \gamma = E_{sv} - TS_{sv} \quad (S_{sv} \text{ thermal entropy, configurational entropy})$$

$$\rightarrow \frac{\partial \gamma}{\partial T} = -S \quad : \text{ surface energy decreases with increasing } T$$

due to increased contribution of entropy

- Average Surface Free Energies of Selected Metals

Crystal	$T_m/^\circ\text{C}$	$\gamma_{sv}/\text{mJ m}^{-2}$
Sn	232	680
Al	660	1080
Ag	961	1120
Au	1063	1390
Cu	1084	1720
δ -Fe	1536	2080
Pt	1769	2280
W	3407	2650

γ of Sn : 680 mJ/m² (T_m : 232°C)

γ of Cu : 1720 mJ/m² (T_m : 1083°C)

C.F. G.B. energy γ_{gb} is about one third of γ_{sv}

Higher T_m ,

>> stronger bond (large negative bond energy)

>> larger surface energy

- The measured γ values for pure metals near the melting temperature

$$\gamma_{sv} = 0.15 L_s / N_a \quad \text{J / surface atom}$$

high $T_m \rightarrow high L_s \rightarrow high \gamma_{sv}$

Surface energy for high or irrational {hkl} index

Closer surface packing, \gg smaller number of broken bond
 \gg lower surface energy

A crystal plane at an angle θ to the close-packed plane will contain broken bonds in excess of the close-packed plane due to the atoms at the steps.

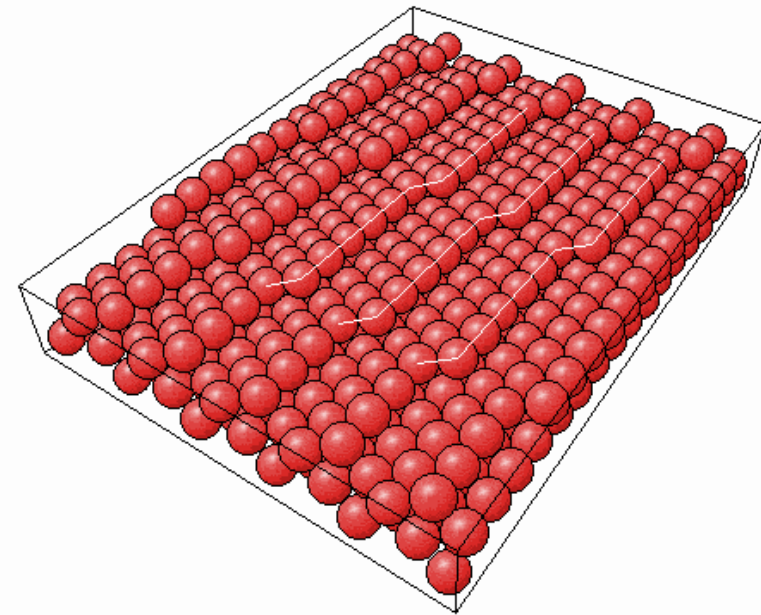
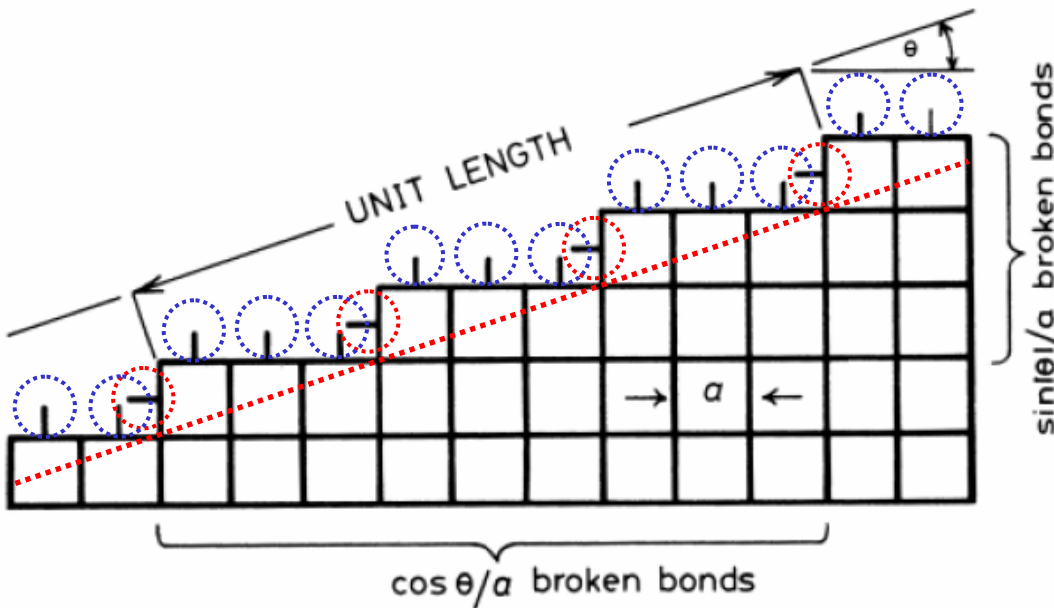


Fig. 3.3 The 'broken-bond' model for surface energy.

$(\cos\theta/a)(1/a)$: **broken bonds**
from the atoms on the steps

$(\sin|\theta|/a)(1/a)$: **additional broken bonds**
from the atoms on the steps

Surface energy for high or irrational {hkl} index

$(\cos\theta/a)(1/a)$: broken bonds from the atoms on the steps

$(\sin|\theta|/a)(1/a)$: additional broken bonds from the atoms on the steps

Attributing $\varepsilon/2$ energy to each broken bond,

$$E_{sv} = \frac{1}{1 \times a} \frac{\varepsilon}{2} \left(\frac{\cos\theta}{a} + \frac{\sin|\theta|}{a} \right)$$
$$= \frac{\varepsilon(\cos\theta + \sin(|\theta|))}{2a^2}$$

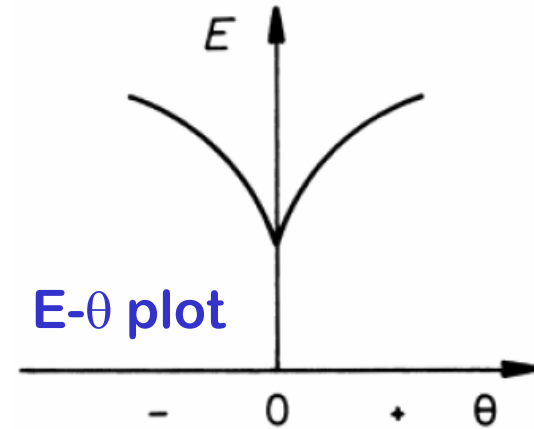
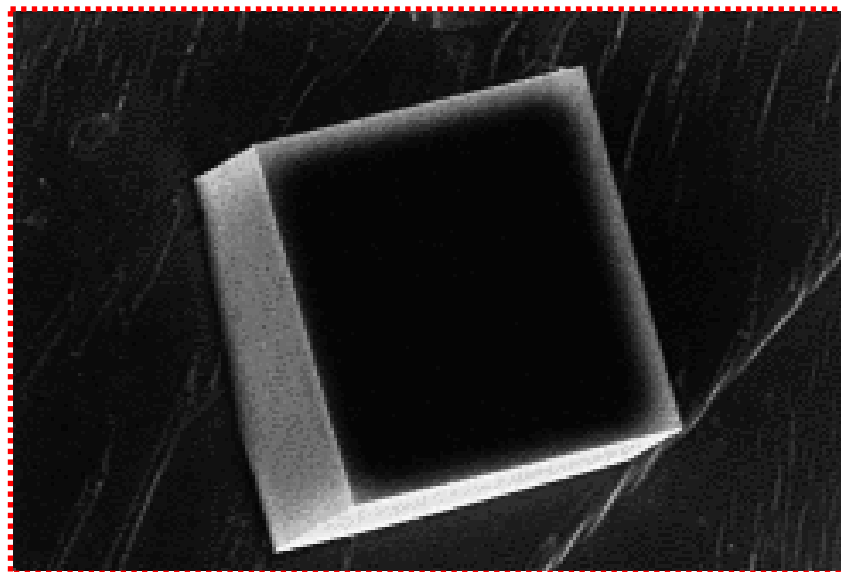
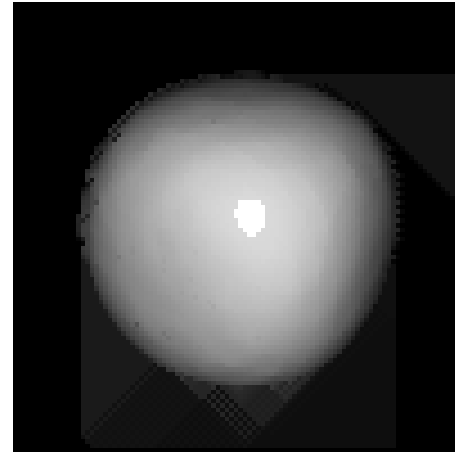
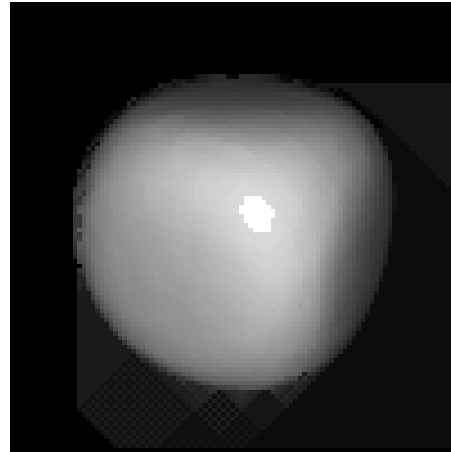
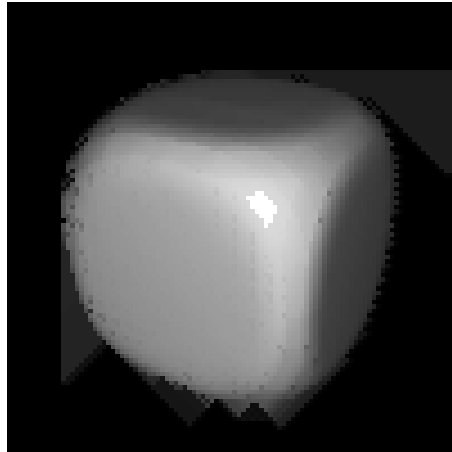
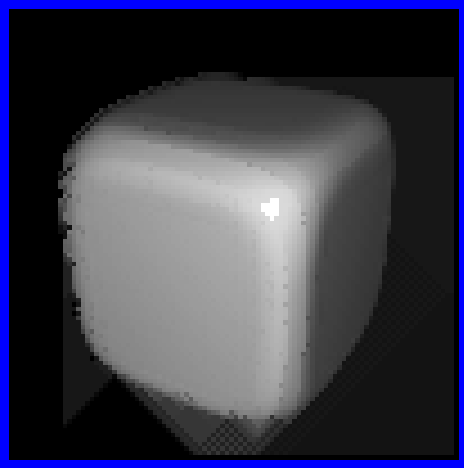


Fig. 3.4 Variation of surface energy as a function of θ

- The close-packed orientation ($\theta = 0$) lies at a cusped minimum in the E plot.
- Similar arguments can be applied to any crystal structure for rotations about any axis from any reasonably close-packed plane.
- All low-index planes should therefore be located at low-energy cusps.

Equilibrium shape of a crystal?

- 기지와 β 입자와의 평형을 고려함에 있어서,
 - 자유에너지는 입자 모양이 고정된 경우는 입자의 크기에 대해 최소화된다.
 - 그러나 입자의 크기가 고정화 된다면 자유에너지는 모양에 대해 최소값을 가질 것이다.



Equilibrium shape: Wulff surface

Distance from center : r_{sv}

Several plane A_1, A_2 etc. with energy γ_1, γ_2

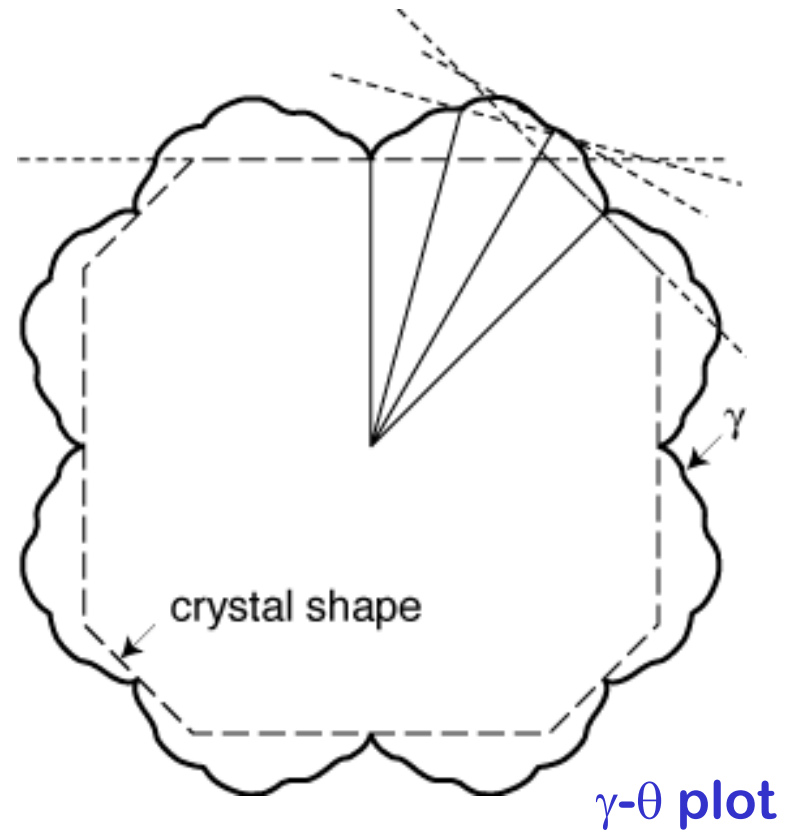
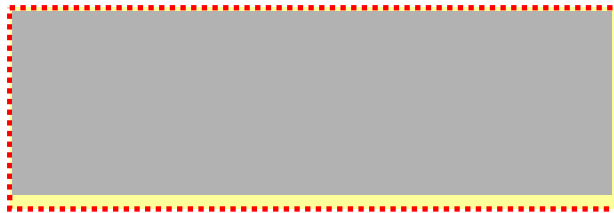
Total surface energy : $A_1\gamma_1 + A_2\gamma_2 \dots$

$= \sum A_i \gamma_i \rightarrow$ minimum

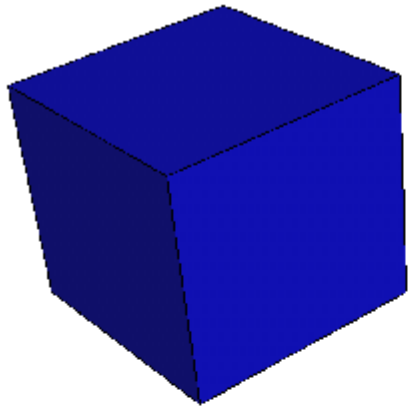
\rightarrow equilibrium morphology

Analytical solution in 2D is reported

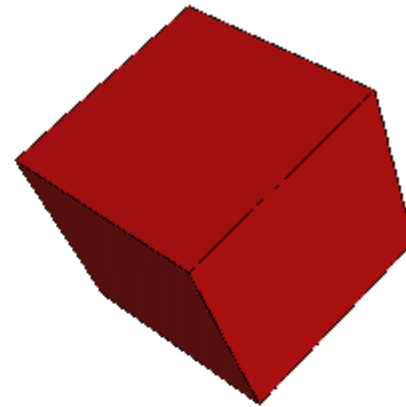
How is the equilibrium shape determined?



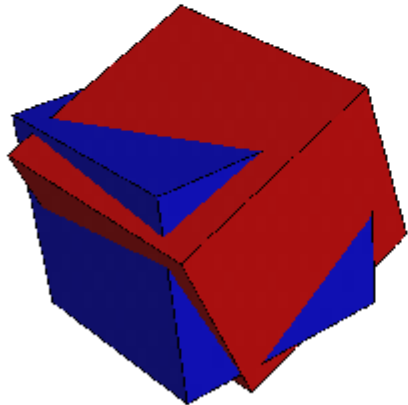
Equilibrium shape: Wulff surface



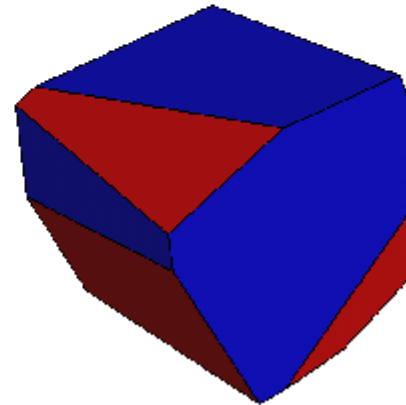
(a) Wulff Shape I



(b) Wulff Shape II



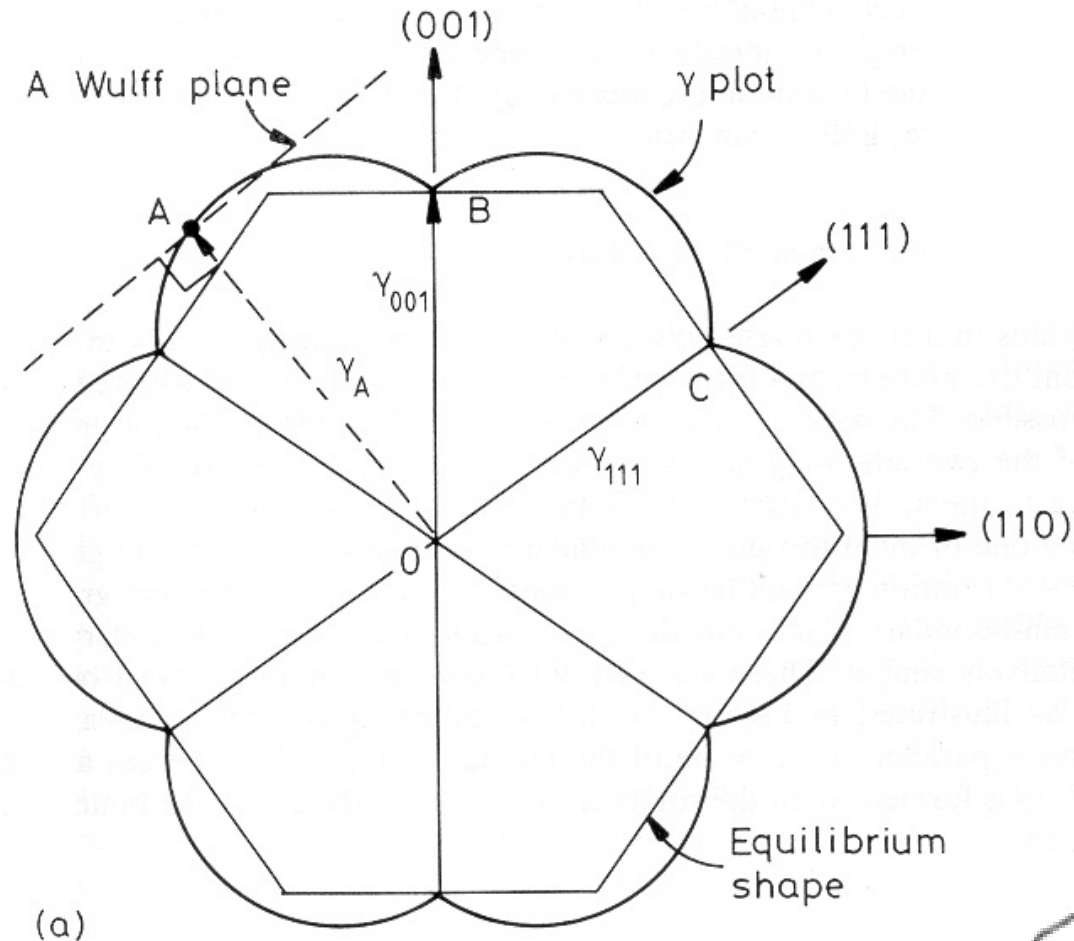
(c) Union of I and II



(d) Intersection of I and II

Figure 1: The process of Wulff shape intersection for two cubic Wulff shapes with displaced origins and rotated coordinate systems. Each individual shape has cubic symmetry $m\bar{3}m$ and $[100]$ facets.

Equilibrium shape: Wulff surface



Equilibrium shape can be determined experimentally by annealing small single crystals (high T, inert atmosphere)

