

Chapter 2. Stresses, Strains & Effective Stresses

Key words : Stress, Strain, Stress-strain relationship, Subsurface stress distribution, Effective stress

1. Stresses ?

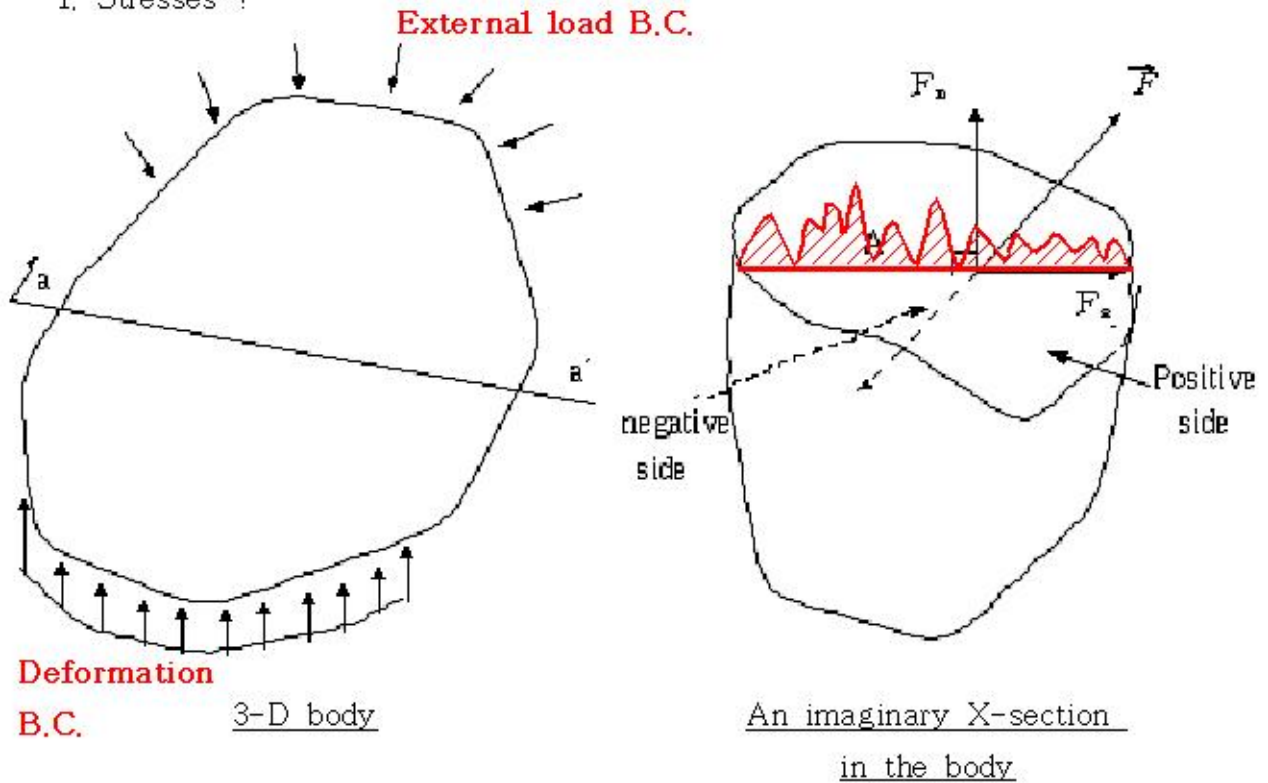


Fig.1

- F : the force transmitted thru the area A ← **Internal force**
 ∴ **reaction exerted within the body**

○ The magnitude of the average forces per unit area are :

F_n / A : **the average normal stress**

F_s / A : **the average shear stress**

○ Stress at a point,

$$\lim_{A \rightarrow 0} \frac{F_n}{A} = \sigma \quad , \quad \lim_{A \rightarrow 0} \frac{F_s}{A} = \tau$$

○ Pressure (in fluid) = **Positive normal stress, or Compressive stress**

↓

no	tensile	}	→ stresses accepted (i.e., no such strength)
no	shear		

2. Body forces vs. Stresses

○ Stresses : act on surface elements inside or on the boundary of the body

ex) contact force between solid bodies

hydrostatic pressure between a solid body and a fluid

○ Body forces : act on the elements of volume (or mass) of the body

ex) **gravitational, magnetic, inertia forces**

3. Stresses after Transformed

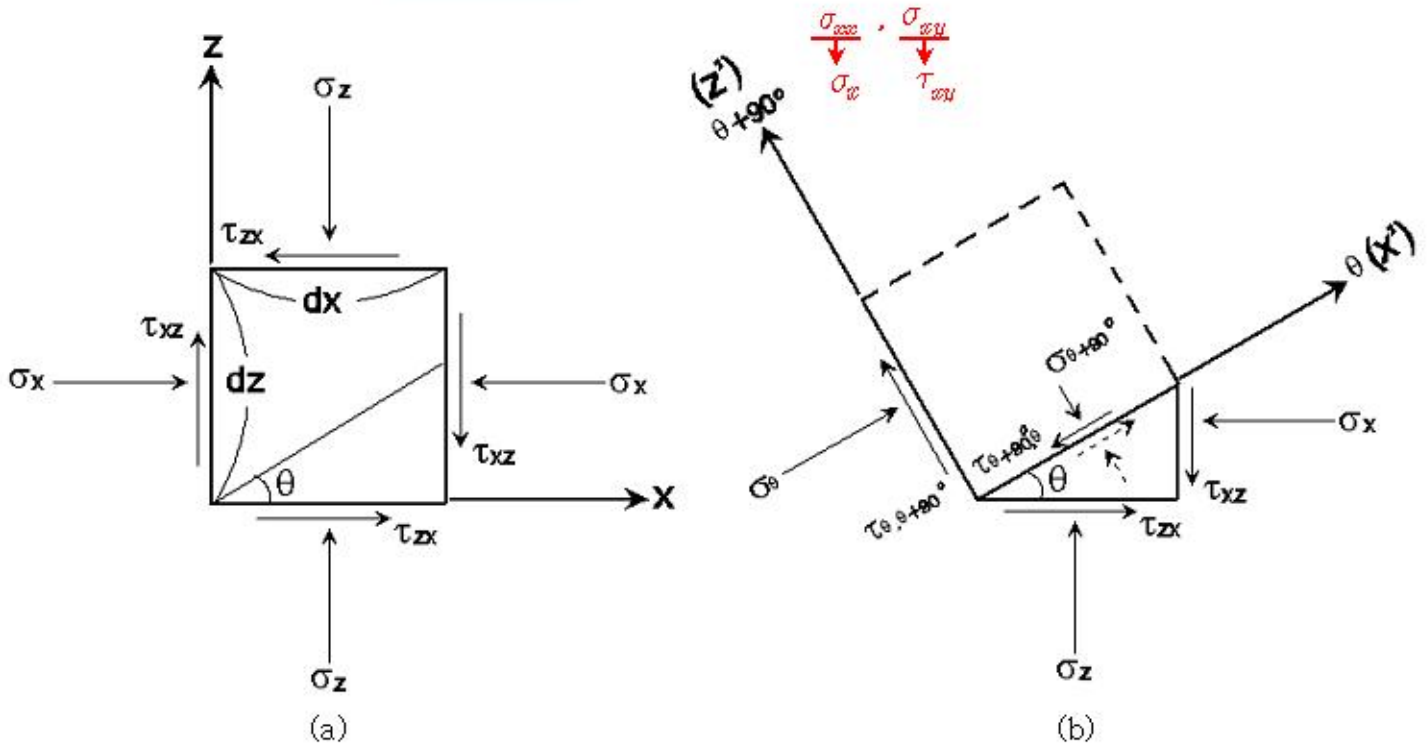


Fig. 2

○ $\Sigma F_{\theta+90^\circ} = 0,$ $\sigma_{\theta+90^\circ}(dx/\cos\theta) - \sigma_x(dx \tan\theta)\sin\theta$
 $+ \tau_{xz}(dx \tan\theta)\cos\theta - \sigma_z(dx)\cos\theta$
 $+ \tau_{xz}(dx)\sin\theta = 0$

→ $\sigma_{\theta+90^\circ} = \sigma_x \sin^2\theta + \sigma_z \cos^2\theta - \tau_{xz} \sin\theta \cos\theta$ -- ①

f(2θ) → $= \frac{\sigma_x + \sigma_z}{2} + \frac{\sigma_z - \sigma_x}{2} \cos 2\theta - \tau_{xz} \sin 2\theta$

○ $\Sigma F_\theta = 0,$ $\tau_{\theta+90^\circ, \theta} = (\sigma_z - \sigma_x)\sin\theta \cos\theta - \tau_{xz}(\sin^2\theta - \cos^2\theta)$ -- ②

f(2θ) → $= \frac{\sigma_z - \sigma_x}{2} \sin 2\theta + \tau_{xz} \cos 2\theta$

$$\sigma_{\theta} \leftarrow \sigma_{\theta+90^\circ} \quad (\theta \rightarrow \theta - 90^\circ)$$

$$\tau_{\theta, \theta+90^\circ} = \tau_{\theta+90^\circ, \theta} \quad \text{always}$$

----- ③

○ If $\tan 2\theta = \frac{2\tau_{xz}}{\sigma_x - \sigma_z}$, $\tau_{\theta+90^\circ, \theta} \neq 0$

($\theta = \theta_{cr}$, $\sigma_{\theta_{cr}} = \sigma_1$ or σ_3 : principal stresses
 if $\sigma_{\theta_{cr}} = \sigma_1$, $\sigma_3 = \sigma_{\theta_{cr}+90^\circ}$)

4. Stress transformation matrix

$$\begin{bmatrix} \sigma_{x'} (= \sigma_{\theta}) \\ \sigma_{z'} (= \sigma_{\theta+90^\circ}) \\ \tau_{x'z'} (= \tau_{\theta, \theta+90^\circ}) \end{bmatrix} = \begin{bmatrix} \cos^2\theta & \sin^2\theta & \sin 2\theta \\ \sin^2\theta & \cos^2\theta & -\sin 2\theta \\ -\frac{1}{2}\sin 2\theta & \frac{1}{2}\sin 2\theta & \cos 2\theta \end{bmatrix} \begin{bmatrix} \sigma_x \\ \sigma_z \\ \tau_{xz} \end{bmatrix}$$

$$\tau_{z'y'} \parallel \tau_{\theta+90^\circ, \theta}$$

5. Mohr circle

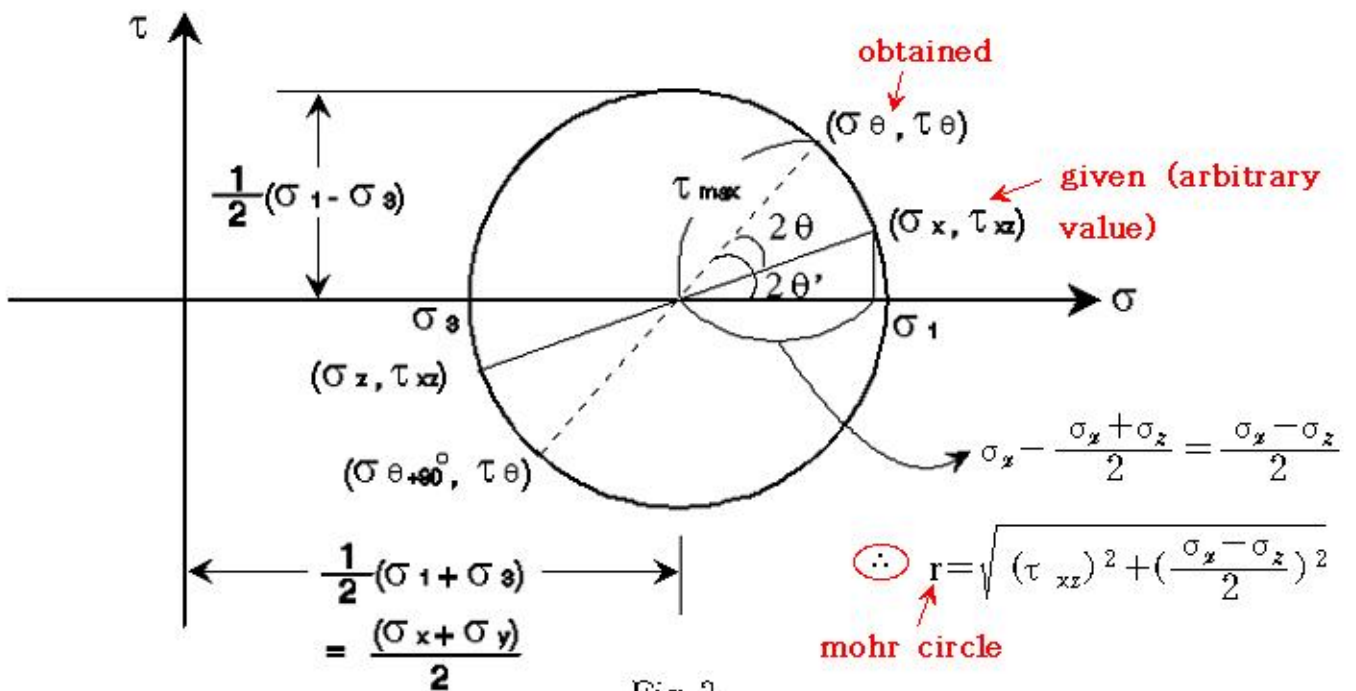


Fig.3

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○ $\sigma_\theta, \tau_\theta$ in terms of σ_1 & σ_3

(From Eqs. ① & ② : $\sigma_x = \sigma_1, \sigma_z = \sigma_3, \tau_{xz} = 0$)

$$\sigma_\theta = \frac{\sigma_1 + \sigma_3}{2} + \frac{\sigma_1 - \sigma_3}{2} \cos 2\theta' \quad \text{-----} \quad \text{④}$$

$$\tau_\theta = \frac{\sigma_1 - \sigma_3}{2} \sin 2\theta'$$

$$\text{Let } \frac{1}{2} (\sigma_1 + \sigma_3) = \sigma_{av}, \quad \frac{1}{2} (\sigma_1 - \sigma_3) = \tau_{max} \quad \text{-----} \quad \text{⑤}$$

Sub. into Eq.④

$$\sigma_\theta = \sigma_{av} + \tau_{max} \cos 2\theta' ,$$

$$\tau_\theta = \tau_{max} \sin 2\theta' \quad \text{-----} \quad \text{⑥}$$

To eliminate θ , manipulate the following.

$$\cos 2\theta' = \sqrt{1 - \sin^2 2\theta'} = \sqrt{1 - \frac{\tau_\theta^2}{\tau_{max}^2}} \quad \text{-----} \quad \text{⑦}$$

Sub. into Eq.⑥.

$$\sigma_\theta - \sigma_{av} = \tau_{max} \sqrt{1 - \frac{\tau_\theta^2}{\tau_{max}^2}}$$

$$\text{or } (\sigma_\theta - \sigma_{av})^2 + \tau_\theta^2 = \tau_{max}^2 \quad \text{-----} \quad \text{⑧}$$

,which is the equation of a circle. (center at σ_{av} & $r = \tau_{max}$)

$$\frac{1}{2} (\sigma_1 + \sigma_3) \quad \frac{1}{2} (\sigma_1 - \sigma_3)$$

○ σ_1 & σ_3 in terms of σ_x , σ_z & τ_{xz}

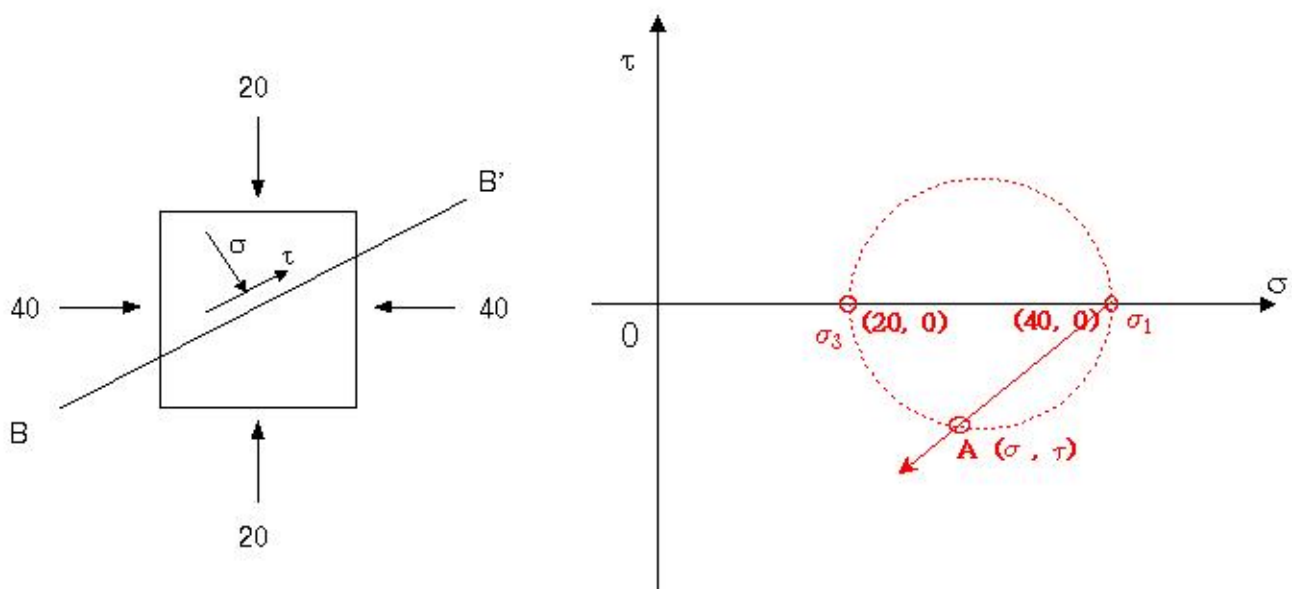
$$\sigma_1 = \frac{1}{2}(\sigma_x + \sigma_z) + \sqrt{\tau_{xz}^2 + \left(\frac{\sigma_x - \sigma_z}{2}\right)^2}$$

$$\sigma_3 = \frac{1}{2}(\sigma_x + \sigma_z) - \sqrt{\tau_{xz}^2 + \left(\frac{\sigma_x - \sigma_z}{2}\right)^2}$$

○ In fact,

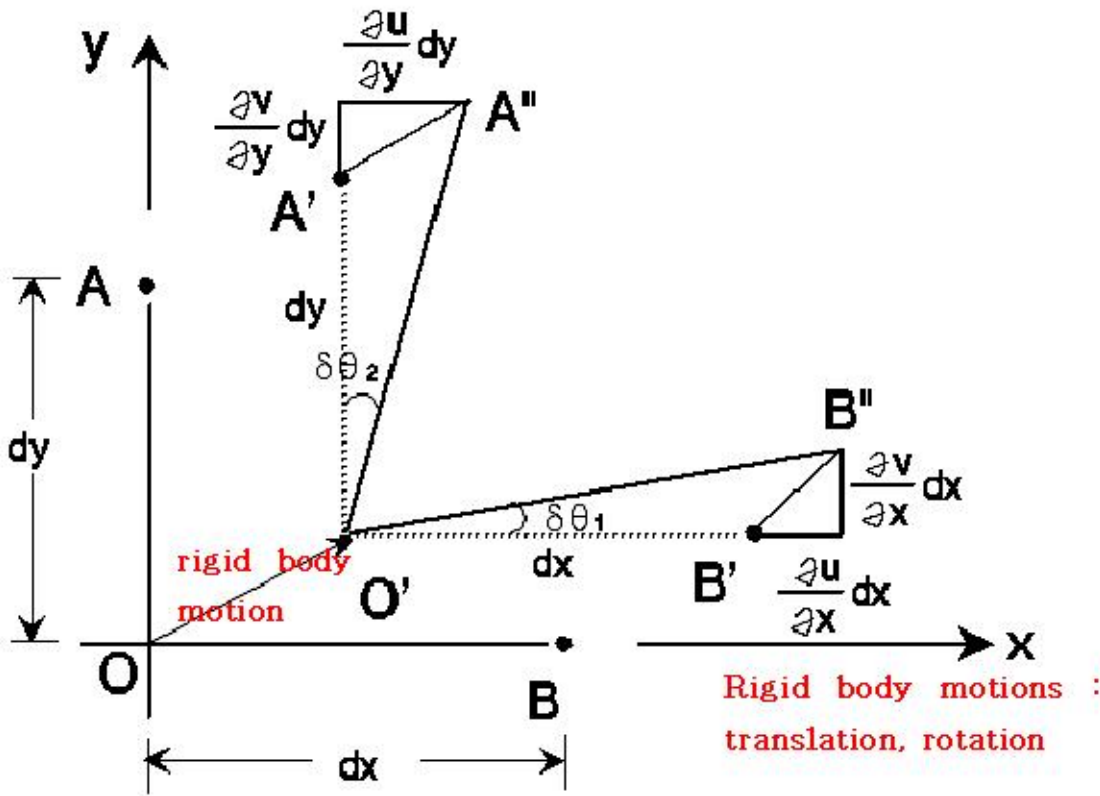
$$\sigma_1 + \sigma_3 = \sigma_x + \sigma_z = \sigma_\theta + \sigma_{\theta+90^\circ} = \text{constant (1st Invariant)}$$

6. Origin of Planes(Pole, O_p)



A line through O_p and any point A of the Mohr circle will be parallel to the plane on which the stresses given by point A act.

7. Strains (Infinitesimal \rightarrow 2nd order terms neglected \rightarrow e.g. $(\frac{\partial u}{\partial x})^2 = 0$)



where $OB = O'B'$, $OA = O'A'$

u : displacement function in x direction

v : displacement function in y direction

$$O'B'' = \left[\left(dx + \frac{\partial u}{\partial x} dx \right)^2 + \left(\frac{\partial v}{\partial x} dx \right)^2 \right]^{\frac{1}{2}}$$

$$\epsilon_x = \frac{\Delta L}{L} = \frac{\left[\left(dx + \frac{\partial u}{\partial x} dx \right)^2 + \left(\frac{\partial v}{\partial x} dx \right)^2 \right]^{\frac{1}{2}} - dx}{dx}$$

$$= \left[\left(1 + \frac{\partial u}{\partial x} \right)^2 + \left(\frac{\partial v}{\partial x} \right)^2 \right]^{\frac{1}{2}} - 1$$

$$\approx 1 + \frac{\partial u}{\partial x} - 1 = \frac{\partial u}{\partial x}$$



Similarly,

$$\epsilon_y = \frac{\partial v}{\partial y}, \quad \left(\epsilon_z = \frac{\partial w}{\partial z} \right)$$

○ Change in angle (radian)

$$\gamma_{xy} = \frac{\frac{\partial v}{\partial x} dx}{dx} + \frac{\frac{\partial u}{\partial y} dy}{dy}$$

$$= \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \quad (= \quad \delta\theta_1 + \delta\theta_2 \quad)$$

$$\gamma_{yz} = \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y}$$

$$\gamma_{xz} = \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x}$$

