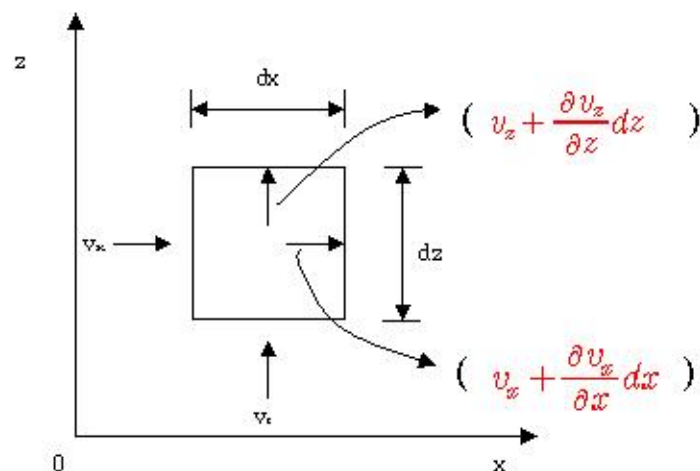


✳What to be learned :

- ① Derive governing equation
- ② Get solution ($h(x, z)$) for various B.C
- ③ Determine p.w.p / h, gradient / flow quantities

1. Seepage Equation (2-D)

- Assumptions : homogeneous, isotropic, Darcy's law valid



- The volume of water entering the element per unit time

$$= v_x dy dz + v_z dx dy$$

- The volume of water leaving the element per unit time

$$= (v_x + \frac{\partial v_x}{\partial x} dx) dy dz + (v_z + \frac{\partial v_z}{\partial z} dz) dx dy$$

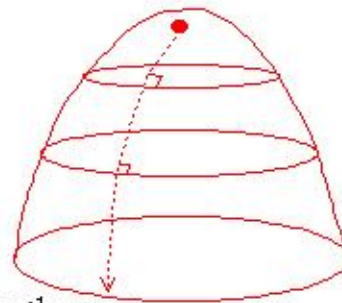
- Since no volume change assumed, i.e., (**steady - state**)

$$q_{in} = q_{out}$$

$$\rightarrow \frac{\partial v_x}{\partial x} + \frac{\partial v_z}{\partial z} = 0 \xrightarrow{(v_x = -k \frac{\partial h}{\partial x})} \left[\frac{\partial^2 h}{\partial x^2} + \frac{\partial^2 h}{\partial z^2} = 0 \right]$$

$$\rightarrow \nabla^2 h = 0 \text{ (Laplace Eq.)}$$

2. Flow nets



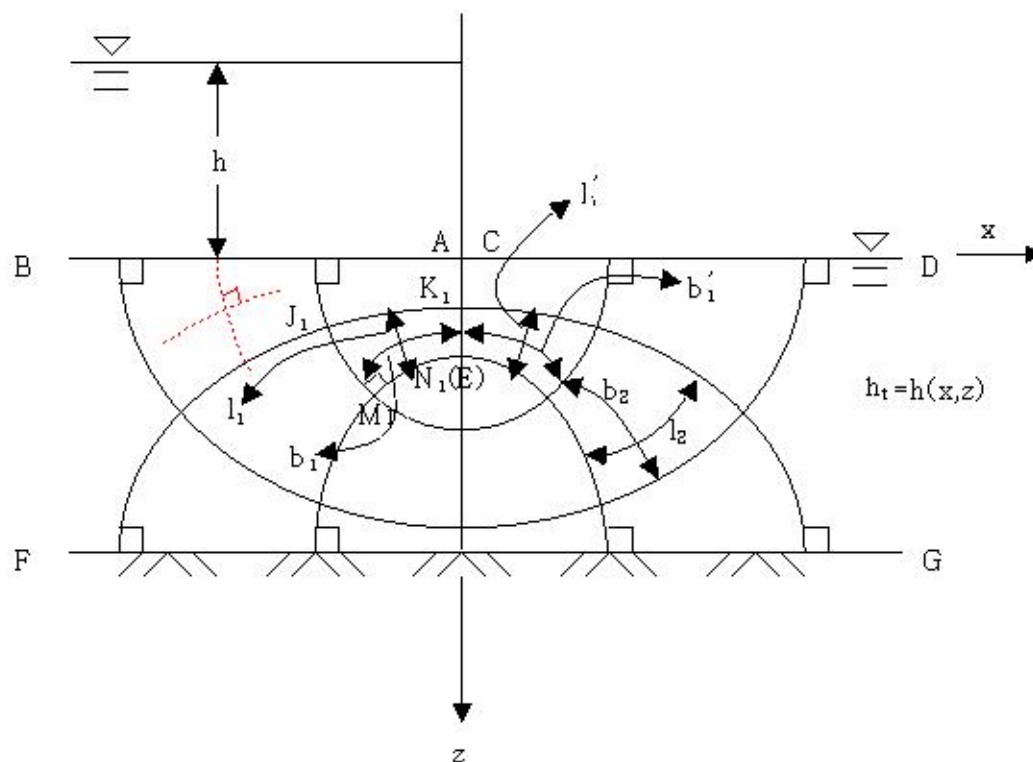
- Definition : (text p.69)

E-P line & Flow line : meet at right angle
 ↑
 Constant head

- Types of seepage flow :

- Confined flow : **Phreatic line known**
 (Top-flow)
- Unconfined flow : **not known**

3. Seepage underneath cofferdams (confined flow)



- Boundary conditions for the confined flow
 - i) Line \overline{AB} : **e-p line** ($h_t = h$)
 - ii) From pt. \textcircled{A} \rightarrow pt. \textcircled{E} \rightarrow pt. \textcircled{C} : **flow line (top)**
 - iii) Line \overline{CD} : **e-p line** ($h_t = 0$)
 - iv) Line \overline{FG} : **flow line (bottom)**

- Square figures ($\square J_1K_1M_1N_1$)
 - A : whole x-section, $A/y = B$
 - a : x-section between flow lines, $a/y = b$

- From Darcy's law,

 - $q/y = ki a/y$, y : the dimension normal to the section
 - let $\bar{q} = q/y$, $a/y = b$
 then, $\bar{q} = kib$, \bar{q} : the flow rate per running foot
 (i.e., **pet foot normal to the section**)

b : the width of a flow line

 - $\bar{q} = kib = k \frac{\Delta h}{l} b = k \Delta h \frac{b}{l}$
 Δh , l : the head loss and the length in accrossing the figure

Constant thru the section

$$\circ \Delta \bar{q}_1 = k \Delta h_1 \frac{b_1}{l_1} \quad (\text{for sub}_1 \text{ figure})$$

$$\Delta \bar{q}_1' = k \Delta h_1' \frac{b_1'}{l_1'} \quad (\text{for sub}_1' \text{ figure})$$

$$\Delta \bar{q}_2 = k \Delta h_2 \frac{b_2}{l_2} \quad (\text{for sub}_2 \text{ figure})$$

1

- If all the 3 figures are squares, i.e.,

$$\frac{b_1}{l_1} = \frac{b_1'}{l_1'} = \frac{b_2}{l_2} = 1$$

- and $\Delta \bar{q}_1 = \Delta \bar{q}_1'$ (**∵ Same flow line boundaries**)
then, $\Delta h_1 = \Delta h_1'$

- and $\Delta h_1' = \Delta h_2$ (**∵ Same e-p line boundaries**)
then, $\Delta \bar{q}_1' = \Delta \bar{q}_2$
& $\Delta h_1 = \Delta h_2$

- Thus, if all figures are squares

i) the same quantity of flow thru each figure

ii) the same head drop in crossing each figure

- In fact, these are true if $\frac{b}{l} = \text{constant} (\neq 1)$

- Graphical determination of flow nets
 - i) Trial and error
 - ii) Remember boundary conditions
 - iii) 4~5 flow channels sufficient
 - iv) All figures should resemble squares
 - v) Size of the squares change gradually
 - vi) One trial flow line (or e-p line) near a boundary line drawn first

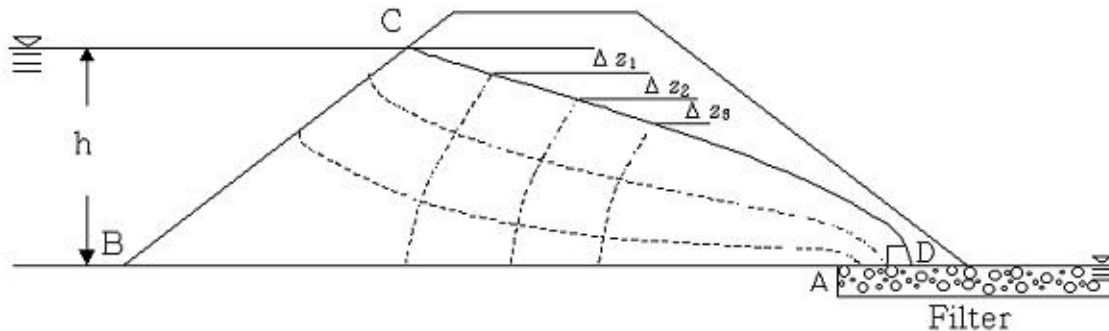
- Example (text Fig 3.7, p 72)
 - Fig (c) should be symmetric to the bottom (i.e., mirror image)

- Ref.s : "Seepage, Drainage & Flow Nets" by H. R. Cedergren (Wiley Interscience)

- Flow quantity calculation

$$\begin{aligned}
 \overline{Q_B} &= k h \frac{N_f}{N_d} & N_f &: \text{number of flow channel} \\
 &= k \frac{h}{N_d} N_f & N_d &: \text{number of e.p. drops} \\
 &= k \frac{h}{N_d} \frac{1}{l} b N_f & h &: \text{total head loss} \\
 &= k \frac{h/N_d}{l} b N_f \\
 &= k \frac{\Delta h}{l} b N_f \\
 &= k i \cdot B (= A/y) \\
 &= \overline{Q_B}
 \end{aligned}$$

4. Seepage thru earth dams (unconfined flow)



○ Boundary conditions

- i) \overline{BC} : e-p line, $h_t = h$
- ii) \overline{AD} : e-p line, $h_t = 0$
- iii) \overline{CD} : top-flow line ($h_p = 0$) : initially undetermined
- iv) \overline{BA} : bottom-flow line, $h_e = 0$

○ h_p at every pt. on the top flow line = 0

thus,

$$(h_t)_{t.f.l} = (h_e)_{t.f.l} \rightarrow \Delta z_1 = \Delta z_2 = \Delta z_3$$

∴ between each e-p line, head drops are the same, & all Δh are equal to Δh_e

○ Filter

- purpose : to keep the seepage entirely within the dam

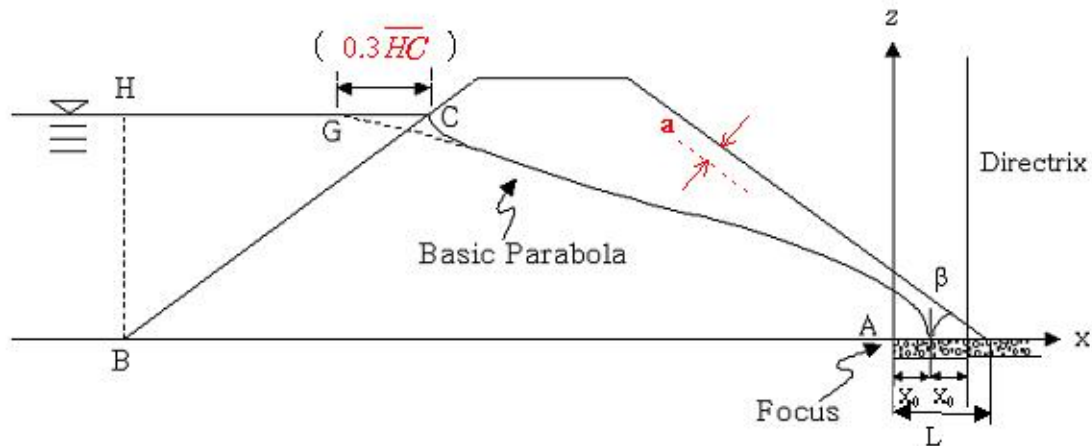
- requirements : piping/permeability

COE
 $\frac{(D_{60})_f}{(D_{60})_s} < 25$ - piping : pores be small enough to prevent particles being carried away
 $\left(\frac{(D_{15})_f}{(D_{85})_s} < 4 \sim 5 \right.$

USBR
 $(D_{\max})_f < 3''$ - permeability : high enough for rapid drain $\left(\frac{(D_{15})_f}{(D_{15})_s} > 4 \sim 5 \right.$

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- Flow net construction for earth dam



$$* L > x_0 (1 + \cot^2 \beta)$$

for capillary allowance

$$L > x_0 (1 + \cot^2 \beta) + \alpha$$

$$\uparrow$$

$$\alpha = f(\alpha)$$

- The equation of the basic parabola

$$x = x_0 - \frac{z^2}{4x_0}$$

- By Casagrande, it is recommended to take the initial pt. of the parabola at G where $\overline{GC} = [\quad 0.3\overline{HC} \quad]$

to determine the unknown constant, x_0