

**Lecture Note 2**

**Group Constants in Resonance Region**

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# Introduction

- Group Constants

a. average xsec (spectrum-weighted),  $\sigma_{xg}$

$$\sigma_{xg} = \frac{\int_{E_g}^{E_{g-1}} \sigma(E)\phi(E)dE}{\int_{E_g}^{E_{g-1}} \phi(E)dE}$$

b. diffusion constant,  $D_g$

c. resonance integral,  $RI_g$

d. fission spectrum,  $\chi_g$

→ Mostly averaged xsec is meant.

- Smooth cross sections

Non-resonance cross sections in **fine** group (~50G) can be obtained by **ultra-fine** group slowing down calculations for typical composition as a function of temperature

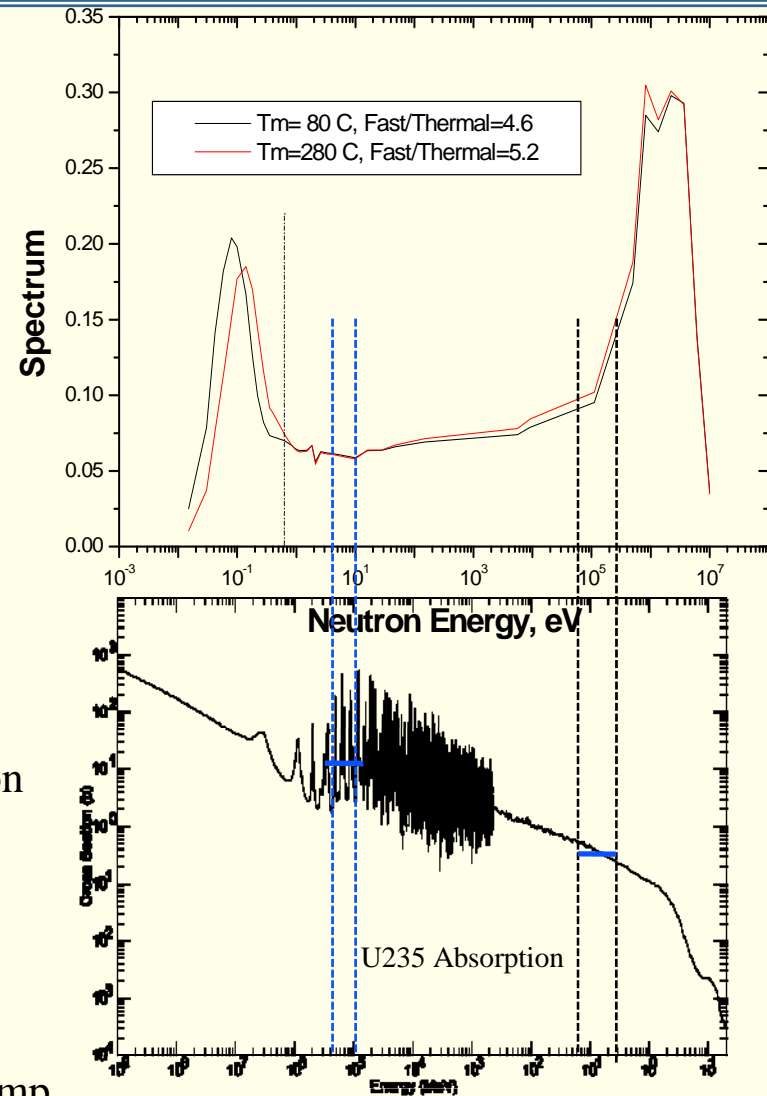
- Cross section change due to deviation from ref. condition

– for fine group, the change in within group spectrum is not large

– for **coarse** group (e.g. 2G), the spectrum change is considerable → need a reevaluation of spectrum and consequently coarse group xsec by lattice calc.

- Resonance cross sections

– need to be reevaluated for given composition and temp



∴ numerous resonances within a fine group and self-shielding changes depending on composition

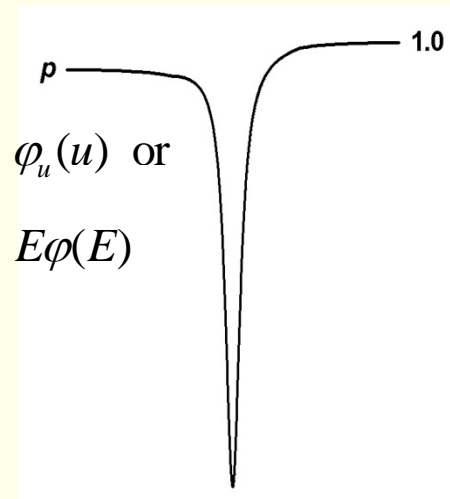
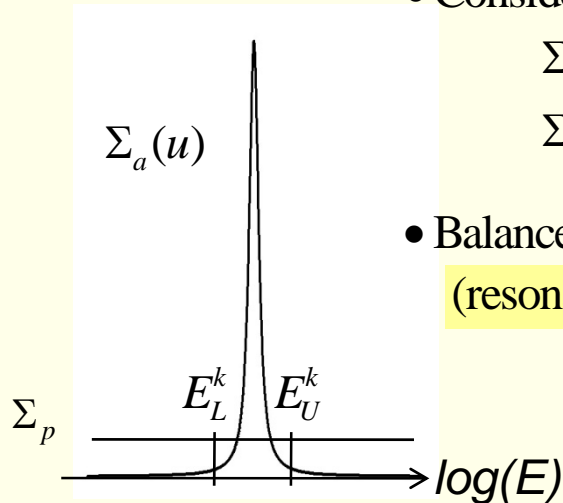
# Resonance Self-Shielding and Effective Xsec

- Consider a **homogeneous** mixture of a resonance absorber and moderator

$$\Sigma_p = N_R \sigma_p^R + N_M \sigma_p^M$$

$$\Sigma_t(E) = \Sigma_a^R(E) + \Sigma_s^R(E) + \Sigma_p$$

- Balance during slowing down under **Narrow Resonance approximation**  
(resonance so narrow that scattering source inside the resonance is negligible)



$$\Sigma_t(E)\phi(E) = \int_E^{\frac{E}{\alpha}} \Sigma_s(E' \rightarrow E)\phi(E')dE'$$

$$= \int_E^{\frac{E}{\alpha}} \frac{\Sigma_s}{(1-\alpha)E'}\phi(E')dE'$$

$$= \int_E^{\frac{E}{\alpha}} \frac{s_0}{\xi(1-\alpha)E'^2}dE' = -\frac{s_0}{\xi(1-\alpha)E'} \Big|_E^{\frac{E}{\alpha}} = \frac{s_0}{\xi(1-\alpha)E}(1-\alpha)$$

$$= \frac{s_0}{\xi E}$$

in case of no absorption

$$\phi(E') = \frac{s_0}{\xi \Sigma_s E'}, E' > E_U^k$$

$$\rightarrow \phi(E) = \frac{s_0}{\xi \Sigma_t(E)E} \text{ or } E\phi(E) = \frac{s_0}{\xi \Sigma_t(E)} \propto \frac{1}{\Sigma_t(E)}$$

# Resonance Self-Shielding and Effective Xsec

- Source Normalization for  $E\varphi(E) = 1$  above Resonance

$$E\varphi(E) = 1 \text{ for } E > E_U^k$$

$$E\varphi(E) = \frac{s_0}{\xi \Sigma_s} = \frac{s_0}{\xi \Sigma_p} = 1 \quad \rightarrow \quad \frac{s_0}{\xi} = \Sigma_p$$

$$\Sigma_t(E) = \underbrace{\Sigma_a^R(E) + \Sigma_s^R(E)}_{\Sigma_t^R(E)} + \Sigma_p = \Sigma_t^R(E) + \Sigma_p$$

- Self-Shielded Flux

$$E\varphi(E) = \frac{s_0}{\xi \Sigma_t(E)} = \frac{\Sigma_p}{\Sigma_t(E)} = \frac{\Sigma_p}{\Sigma_t^R(E) + \Sigma_p} = \frac{N_R \sigma_p^R + N_M \sigma_p^M}{N_R \sigma_t^R(E) + N_R \sigma_p^R + N_M \sigma_p^M}$$

$$= \frac{\sigma_b}{\sigma_t^R(E) + \sigma_b}$$

$$\sigma_b = \frac{\Sigma_p}{N_R} = \sigma_p^R + \frac{N_M}{N_R} \sigma_p^M = f(\sigma_p^R, \sigma_p^M, \frac{N_M}{N_R})$$

dilution parameter

– Unshielded Flux with infinite dilution, with  $N_R \rightarrow 0$ ,  $\frac{N_M}{N_R} \rightarrow \infty$ ,  $\sigma_b \rightarrow \infty \rightarrow E\varphi(E) = 1$

- Effective Xsec

$$\bar{\sigma}_a^R = \frac{\int \sigma_a^R(E) \varphi(E) dE}{\int \varphi(E) dE} = \frac{\int \sigma_a^R(E) \frac{\sigma_b}{\sigma_t^R(E) + \sigma_b} \frac{dE}{E}}{\int \frac{\sigma_b}{\sigma_t^R(E) + \sigma_b} \frac{dE}{E}} = \frac{\int \sigma_a^R(u) \frac{\sigma_b}{\sigma_t^R(u) + \sigma_b} du}{\int \frac{\sigma_b}{\sigma_t^R(u) + \sigma_b} du} = f(\sigma_b)$$

$$du = -\frac{dE}{E}$$

# Resonance Integral

- Reaction Rate per Atom with Normalized Flux  $E\phi(E) = 1$  above Resonance

$$I_k = \int_{E_L^k}^{E_U^k} \frac{\sigma_a^R(E)\sigma_b}{\sigma_t^R(E) + \sigma_b} \frac{dE}{E} = \int_{u_L^k}^{u_U^k} \frac{\sigma_a^R(u)\sigma_b}{\sigma_t^R(u) + \sigma_b} du = f(\sigma_b, T)$$

given in a form of 2-D table in a Xsec Lib

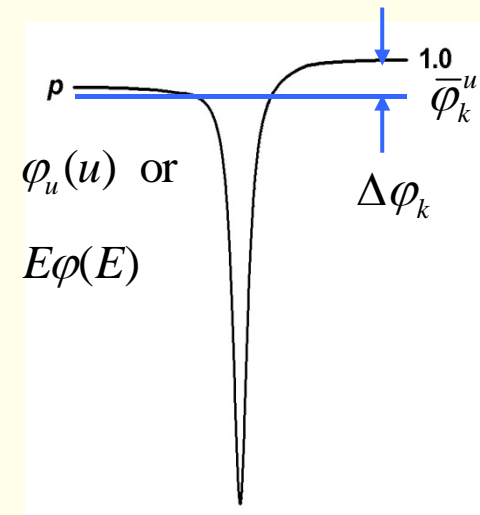
- Effective Xsec in terms of RI

$$\bar{\sigma}_a^R = \frac{I_k}{\phi_k} = \frac{I_k / \Delta u}{\phi_k / \Delta u} = \frac{\bar{I}_k}{\bar{\phi}_k^u} = \frac{\bar{I}_k}{1 - \Delta\phi_k}$$

$$\begin{aligned} \bar{\phi}_k^u &= \frac{1}{\Delta u} \int_{u_L^k}^{u_U^k} \frac{\sigma_b}{\sigma_t^R(u) + \sigma_b} du = \frac{1}{\Delta u} \int_{u_L^k}^{u_U^k} \left( 1 - \frac{\sigma_t^R(u)}{\sigma_t^R(u) + \sigma_b} \right) du \\ &= 1 - \frac{1}{\Delta u \sigma_b} \int_{u_L^k}^{u_U^k} \frac{(\sigma_a^R(u) + \sigma_s^R(u)) \sigma_t^R(u)}{\sigma_t^R(u) + \sigma_b} du = 1 - \frac{\bar{I}_k}{\sigma_b} \rightarrow \Delta\phi_k = \frac{\bar{I}_k}{\sigma_b} \end{aligned}$$

$$\bar{\sigma}_a^R = \frac{\bar{I}_k}{1 - \frac{\bar{I}_k}{\sigma_b}}$$

If  $\sigma_s^R(u)$  is negligible..., really?



# Resonance Integral

- Reaction Rate per Atom with Normalized Flux  $E\phi(E) = 1$  above Resonance

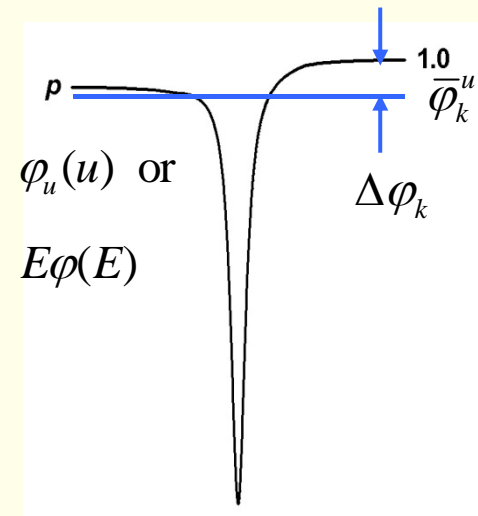
$$I_k = \int_{E_L^k}^{E_U^k} \frac{\sigma_a^R(E)\sigma_b}{\sigma_t^R(E) + \sigma_b} \frac{dE}{E} = \int_{u_L^k}^{u_U^k} \frac{\sigma_a^R(u)\sigma_b}{\sigma_t^R(u) + \sigma_b} du = f(\sigma_b, T)$$

given in a form of 2-D table in a Xsec Lib

- Effective Xsec in terms of RI

$$\bar{\sigma}_a^R = \frac{I_k}{\phi_k} = \frac{I_k / \Delta u}{\phi_k / \Delta u} = \frac{\bar{I}_k}{\bar{\phi}_k^u} = \frac{\bar{I}_k}{1 - \Delta\phi_k}$$

$$\begin{aligned} \bar{\phi}_k^u &= \frac{1}{\Delta u} \int_{u_L^k}^{u_U^k} \frac{\sigma_b}{\sigma_t^R(u) + \sigma_b} du = \frac{1}{\Delta u} \int_{u_L^k}^{u_U^k} \left( 1 - \frac{\sigma_t^R(u)}{\sigma_t^R(u) + \sigma_b} \right) du \\ &= 1 - \frac{1}{\sigma_b \Delta u} \int_{u_L^k}^{u_U^k} \frac{(\sigma_a^R(u) + \sigma_s^R(u))\sigma_b}{\sigma_t^R(u) + \sigma_b} du = 1 - \frac{\bar{I}_k}{\sigma_b} \rightarrow \Delta\phi_k = \frac{\bar{I}_k}{\sigma_b} \end{aligned}$$



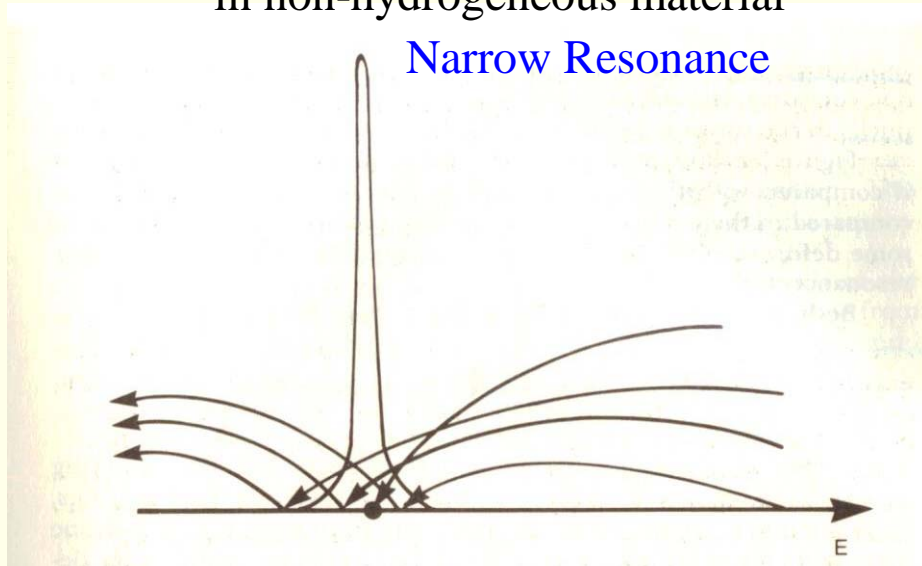
$$\bar{\sigma}_a^R(\sigma_b) = \frac{\bar{I}_k(\sigma_b)}{1 - \frac{\bar{I}_k(\sigma_b)}{\sigma_b}} \dots (*)$$

If  $\sigma_s^R(u)$  is negligible..., really?

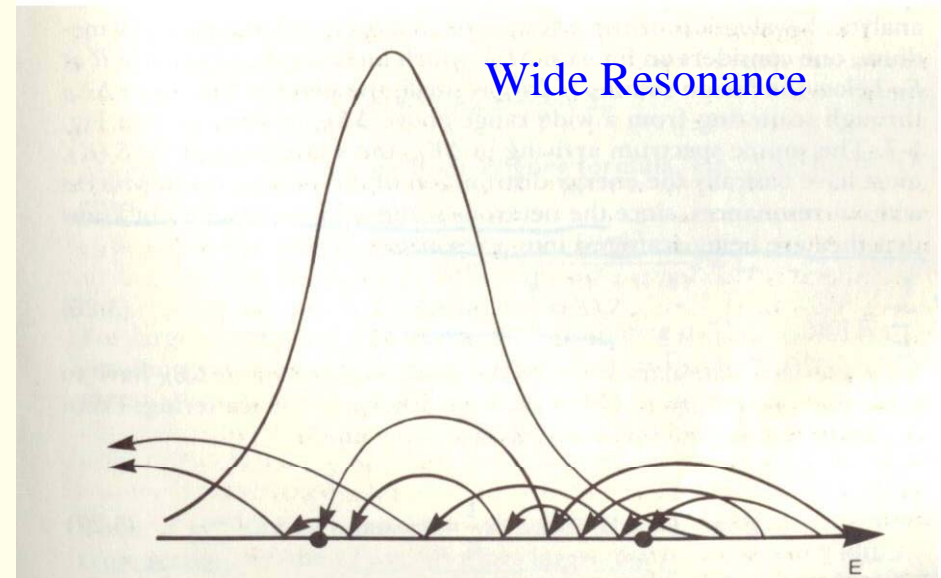
$I_k^a(\sigma_b)$  is adjusted so that (\*) gives the correct avg. xsec!

# Basic Approximations for Resonance Treatment

- Need : analytical solution for resonance absorption not possible for slowing down in non-hydrogeneous material



- Resonance width considered narrow compared with scattering energy loss
- regard all scattering source initiated above the resonance
- scattering inside the resonance bring neutron out of the resonance
- valid more for resonance at high energy



- Resonance considered much wider or scattering loss much smaller than the resonance width
- neutron resides inside the resonance after scattering
- regard in-scattering same as out-scattering
- most likely for scattering with heavy nuclides at low energy

# Intermediate Resonance Approximation in Homo. Mixture

by Goldstein and Cohen (1962)

- Scattering by Narrow Resonance

$$R_{SS}^{NR}(E) = \sum_i \int_E^E \frac{\sum_{si} \varphi(E')}{(1-\alpha_i)E'} dE' \approx \sum_i \sum_{pi} \int_E^E \frac{C}{(1-\alpha_i)E'^2} dE' \approx \sum_i \sum_{pi} \frac{C}{E}$$

$$\varphi(E') = \frac{C}{E'}$$

- Scattering by Wide Resonance

$\alpha_i \ll 1$ , Narrow integration range

$$\begin{aligned} R_{SS}^{WR}(E) &= \sum_i \int_E^E \frac{\sum_{si} \varphi(E')}{(1-\alpha_i)E'} dE' = \sum_i \int_E^E \frac{\sum_{si}(E')E' \varphi(E')}{(1-\alpha_i)E'^2} dE' \approx \sum_i \sum_{si}(E) E \varphi(E) \int_E^E \frac{dE'}{(1-\alpha_i)E'^2} \\ &= \sum_i \sum_{si}(E) E \varphi(E) \frac{1}{E} = \sum_i \sum_{si}(E) \varphi(E) \end{aligned}$$

- Intermediate Resonance (IR) with Normalization,  $C = 1$

$$R_{SS}(E) = \sum_i \left( \lambda_i \frac{\sum_{pi}}{E} + (1-\lambda_i) \sum_{si}(E) \varphi(E) \right) \quad R_{SS}(u) = \sum_i \left( \lambda_i \sum_{pi} + (1-\lambda_i) \sum_{si}(u) \varphi(u) \right)$$

$$R_{SS}(E) dE = \sum_i \left( \lambda_i \sum_{pi} \frac{dE}{E} + (1-\lambda_i) \sum_{si}(E) \varphi(E) dE \right) \quad R_{SS}(u) du = \sum_i \left( \lambda_i \sum_{pi} du + (1-\lambda_i) \sum_{si}(u) \varphi(u) du \right)$$



# Slowing-Down Equation with IR Source

- Balance Equation for Fuel and Moderator Mixture

$$\Sigma_t(E)\phi(E) = \sum_i \left( \lambda_i \frac{\Sigma_{pi}}{E} + (1 - \lambda_i) \Sigma_{si}(E)\phi(E) \right) = \lambda \frac{\Sigma_p}{E} + (1 - \lambda_F) \Sigma_s^F(E)\phi(E)$$

where  $\Sigma_t(E) = \Sigma_a^F(E) + \Sigma_s^F(E) + \Sigma_p^M$

\*  $\Sigma_s^F(E) = \Sigma_s^{F,res}(E) + \Sigma_p^F$

$\lambda_i = 1$  for moderator

$$\sum_i \lambda_i \Sigma_{pi} = \Sigma_p^M + \lambda_F \Sigma_p^F = \lambda \Sigma_p \text{ where } \Sigma_p = \Sigma_p^M + \Sigma_p^F \text{ (}\lambda \text{ properly defined)}$$

– Move flux dependent term of RHS to LHS

$$\left( \Sigma_a^F(E) + \lambda_F \Sigma_s^F(E) + \Sigma_p^M \right) \phi(E) = \left( \Sigma_a^F(E) + \lambda_F \Sigma_s^{F,res}(E) + \lambda \Sigma_p \right) \phi(E) = \frac{\lambda \Sigma_p}{E}$$

- Flux with IR Approximation

$$\therefore E\phi(E) = \frac{\lambda \Sigma_p}{\Sigma_a^F(E) + \lambda_F \Sigma_s^{F,res}(E) + \lambda \Sigma_p}$$

$$\text{or } \phi(u) = \frac{\sigma_b}{\sigma_a^F(u) + \sigma_b}$$

$$\text{or } E\phi(E) = \frac{\sigma_b}{\sigma_a^F(E) + \lambda_F \sigma_s^{F,res}(E) + \sigma_b} \text{ where } \sigma_b = \frac{\lambda \Sigma_p}{N}$$

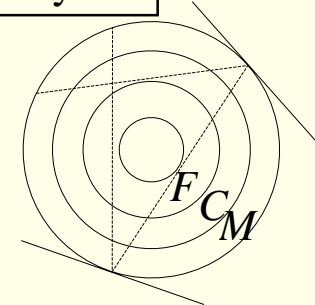
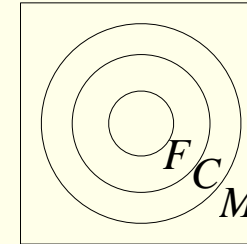
with neglect of  $\lambda_F \sigma_s^{F,res}(u)$  for  $\lambda_F \ll 1$ .

# Slowing Down Equation in a Single Pin Cell

- Balance Equation for Fuel in terms of Collision Probabilities

$$V_F \Sigma_F(u) \phi_F(u) = \sum_{J \neq F} V_J \Sigma_J \cdot 1 \cdot \tilde{P}_{JF} + V_F \left( \lambda_F \Sigma_{pF} + (1 - \lambda_F) \Sigma_{sF}(E) \phi_F(u) \right) \tilde{P}_{FF}$$

$\phi_M(u) = 1, u < u_L^k$   
in moderator by NR



-Reciprocity in CP

$$V_J \Sigma_J \tilde{P}_{JF} = V_F \Sigma_F(u) \tilde{P}_{FJ}$$

$$\tilde{P}_{ji} = \frac{1}{V_j} \int_{V_i} \int_{V_j} \Sigma_i n(\vec{r}_j \rightarrow \vec{r}_i) dV_j dV_i$$

$$\Sigma_J = \Sigma_{sJ} = \text{const.}$$

$$\Sigma_F = \Sigma_{tF}(u)$$

$$\sum_{J \neq F} V_J \Sigma_J \tilde{P}_{JF} = V_F \Sigma_F(u) \sum_{J \neq F} \tilde{P}_{FJ} = V_F \Sigma_F(u) \underbrace{(1 - \tilde{P}_{FF})}_{P_{esc}^F}$$

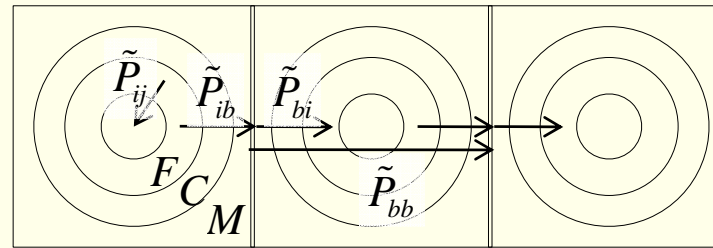
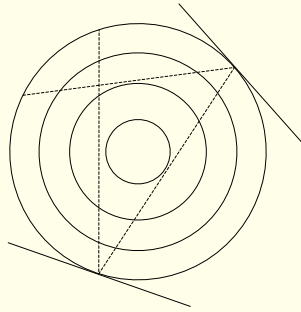
$$\nabla_F \left( \Sigma_F(u) - (1 - \lambda_F) \Sigma_{sF}(u) \tilde{P}_{FF} \right) \phi_F(u) = \nabla_F \Sigma_F(u) P_{esc}^F + \nabla_F \lambda \Sigma_{pF} \tilde{P}_{FF}$$

- IR Flux

$$\phi_F(u) = \frac{\lambda_F \Sigma_{pF} \tilde{P}_{FF} + \Sigma_F(u) P_{esc}^F}{\Sigma_F(u) - (1 - \lambda_F) \Sigma_{sF}(u) \tilde{P}_{FF}}$$

→ Need to find  $\tilde{P}_{FF}(u)$  to determine resonance flux

# Fuel to Fuel Collision Probability in a Cell and in a Lattice



- Cell first-flight probabilities

$\tilde{P}_{ij}$  : First Flight (FF) collision probability for source  $i$  and destination  $j$

$\tilde{P}_{ib}$  : Probability for a neutron in  $i$  to reach boundary

$\tilde{P}_{bi}$  : Probability for a neutron isotropically entering boundary (cosine current) to have first collision in  $i$

$\tilde{P}_{bb}$  : Probability for a neutron isotropically entering boundary (cosine current) to pass through the cell **without collision**

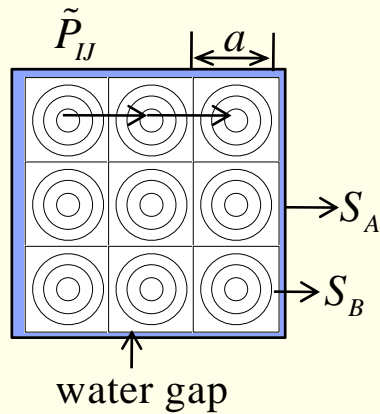
- Reflection (**reentrance**) Ratio,  $R(= \alpha)$  : Return ratio of neutrons escaping from the cell  
-1.0 for infinite lattice

- Lattice CP (Upper case suffixes)

$$\tilde{P}_{IJ} = \tilde{P}_{ij} + \tilde{P}_{ib} R \tilde{P}_{bi} + \underbrace{\tilde{P}_{ib} R \tilde{P}_{bb} R \tilde{P}_{bi}}_{\text{Coll. in 3rd cell}} + \tilde{P}_{ib} R (\tilde{P}_{bb} R)^2 \tilde{P}_{bi} + \dots = \tilde{P}_{ij} + \frac{\tilde{P}_{ib} R \tilde{P}_{bi}}{\underbrace{1 - R \tilde{P}_{bb}}_X}$$

← Lattice FF CP increased by this much

# Reflection Probability for an Assembly

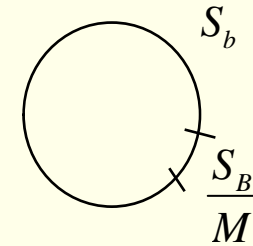


- Assembly area ( $S_B$ ) fraction to total cell surface area

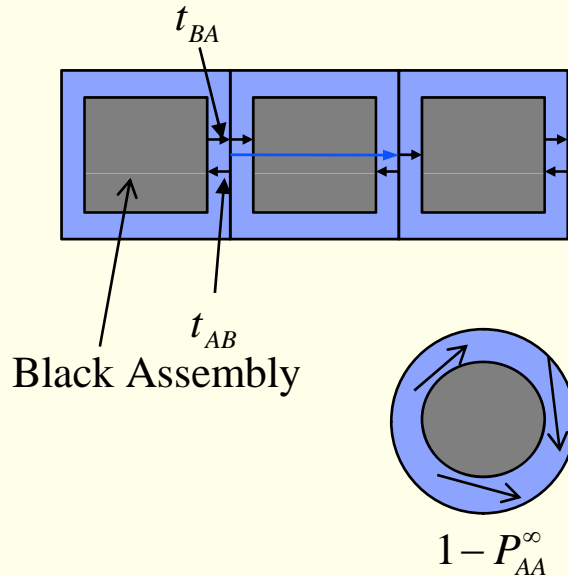
$$f = \frac{4 \cdot n a}{n^2 a} = \frac{1}{n} = \frac{1}{\sqrt{M}} \quad \leftarrow M = n^2$$

→ fraction of neutrons exiting through assembly surface per unit neutron exiting a cell

→ these neutrons can encounter the assembly gap



- Return fraction of a neutron leaving FA avoiding loss in the FA gap



$$g = t_{BA} t_{AB} + t_{BA} \underbrace{(1 - P_{AA}^{\infty})}_{\text{assembly bypass fraction}} t_{AB} + t_{BA} \underbrace{(1 - P_{AA}^{\infty})^2}_{\text{absorbed in the 4th FA}} t_{AB} + \dots = \frac{t_{BA} t_{AB}}{1 - P_{AA}^{\infty}}$$

- Reflection probability for a neutron leaving a cell to return in a lattice

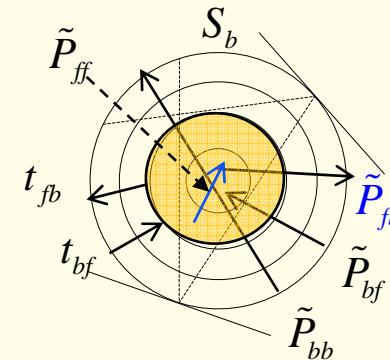
$$R = (1 - f) + f \cdot g$$

with no gap,  $g = 1 \rightarrow R = 1$ .

# First Flight Probabilities for a Pin Cell

- Lattice Enhanced Fuel-to-Fuel Collision Prob.

$$X_{FF} = \frac{\tilde{P}_{fb} R \tilde{P}_{bf}}{1 - R \tilde{P}_{bb}} = \frac{\tilde{P}_{fb} \tilde{P}_{bf}}{\frac{1}{R} - \tilde{P}_{bb}} = \frac{(1 - \tilde{P}_{ff}) t_{fb} \cdot t_{bf} \gamma_f}{\frac{1}{R} - \tilde{P}_{bb}}$$



vol. to surface prob. which can't be found from v-v prob.

- First-flight probabilities for a cell

$\tilde{P}_{ff}$  : first collision in fuel  $\rightarrow P_{esc}^f = 1 - \tilde{P}_{ff}$

$\tilde{P}_{fb}$  : fuel vol. to boundary

$\tilde{P}_{bf}$  : boundary surface to fuel vol. with cosine incoming current (isotropic)

$\tilde{P}_{bb}$  : boundary-to-boundary transmission

$t_{fb}$  : fuel surface to boundary for neutrons exiting fuel with cosine current

$t_{bf}$  : cell surface to fuel surface for neutrons incoming with cosine current

$\gamma_f$  : F.F. blackness of fuel

$\Sigma_f$  : total Xsec of fuel

isotropic exiting current at fuel surface?

- Reciprocity Relations

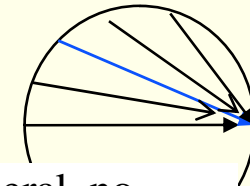
$$\gamma_f = \frac{4V_f}{S_f} \Sigma_f P_{esc}^f = \underbrace{\bar{l}_f \Sigma_f}_{x} P_{esc}^f = x(1 - \tilde{P}_{ff})$$

$$\tilde{P}_{bf} = \frac{4V_f}{S_b} \Sigma_f \tilde{P}_{fb}$$

$$S_f t_{fb} = S_b t_{bf}$$

$$\tilde{P}_{fb} \square \tilde{P}_{esc}^f t_{fb}$$

$$\tilde{P}_{bf} \square t_{bf} \gamma_f$$



in general, no.  
But practically OK for large  $\Sigma_f$

# Determination of FF Probabilities for a Cell

- How to determine  $t_{bf}$  or  $t_{fb}$  ?

– Assume black fuel ( $\Sigma_f > 5\text{cm}^{-1}$ )  $\rightarrow \gamma_f^\infty = 1$

– Perform CP calculation to obtain volume CP kernel and then  $\gamma_f^b$  (fuel blackness for boundary)

$$-t_{bf} = \gamma_f^b$$

$$-t_{fb} = \frac{S_b}{S_f} t_{bf}$$

$$\gamma_f^b = \frac{4V_f}{S_b} \Sigma_f P_{esc}^f = \frac{4}{S_b} \Sigma_f V_f (1 - \sum_{j=1}^n \tilde{P}_{ffj}) = \frac{4}{S_b} (\Sigma_f V_f - \sum_{j=1}^n P_{ffj}) \dots (1)$$

- $\tilde{P}_{bb}$  ? FF cell blackness  $\rightarrow \tilde{P}_{bb} = 1 - \gamma_b$

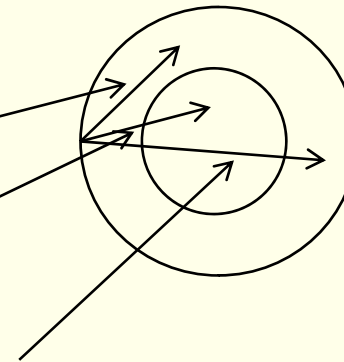
$$\gamma_b = 1 - \tilde{P}_{bb}$$

$$= \sum_{j \neq f} \tilde{P}_{bj}^\infty$$

← for neutrons never reached fuel

+  $t_{bf} \gamma_f$  ← for neutrons entering fuel surface then reacting within fuel

+  $t_{bf} (1 - \gamma_f)(1 - t_{fb})$  ← for neutrons passing fuel then reacting within non fuel



$$= t_{bf} t_{fb} \gamma_f + \sum_{j \neq f} \tilde{P}_{bj}^\infty + t_{bf} (1 - t_{fb}) = \frac{S_f}{S_b} t_{fb}^2 \underbrace{\bar{l}_f \Sigma_f}_{x} \tilde{P}_{esc}^f + \gamma_b^0 = \frac{S_f}{S_b} t_{fb}^2 x (1 - \tilde{P}_{ff}) + \gamma_b^0$$

- Cell Transmission Prob.  $\gamma_b^0 \rightarrow$  cell blackness with  $\Sigma_f = 0$  can be calculated in a way similar to (1)

$$\tilde{P}_{bb} = 1 - \frac{S_f}{S_b} t_{fb}^2 x (1 - \tilde{P}_{ff}) - \gamma_b^0$$

# Fuel Collision Probability for Assembly

- Lattice Enhanced Fuel-to-Fuel Collision Prob.

$$\begin{aligned}
 X_{FF} &= \frac{\tilde{P}_{fb} R \tilde{P}_{bf}}{1 - R \tilde{P}_{bb}} = \frac{(1 - \tilde{P}_{ff}) t_{fb} \cdot t_{bf} \gamma_f}{\frac{1}{R} - \tilde{P}_{bb}} = \frac{(1 - \tilde{P}_{ff}) t_{fb} \cdot \frac{S_f}{S_b} t_{fb} x (1 - \tilde{P}_{ff})}{\frac{1}{R} - \left(1 - \frac{S_f}{S_b} t_{fb}^2 x (1 - \tilde{P}_{ff}) - \gamma_b^0\right)} = \frac{x (1 - \tilde{P}_{ff})^2 \frac{S_f}{S_b} t_{fb}^2}{\frac{1 - R}{R} + \frac{S_f}{S_b} t_{fb}^2 x (1 - \tilde{P}_{ff}) + \gamma_b^0} \\
 &= \frac{x (1 - \tilde{P}_{ff})^2}{x (1 - \tilde{P}_{ff}) + \underbrace{\frac{S_b}{S_f t_{fb}^2} \gamma_b^0}_A + \underbrace{\frac{S_b}{S_f t_{fb}^2} \frac{f(1-g)}{1-f+f \cdot g}}_B} = \frac{x (1 - \tilde{P}_{ff})^2}{x (1 - \tilde{P}_{ff}) + A + B} = \frac{\gamma_f (P_{esc}^f)^2}{\gamma_f + A + B}
 \end{aligned}$$

If no gap,  $g=1 \rightarrow B=0$ .

$$\tilde{P}_{FF} > \tilde{P}_{ff} \rightarrow 1 - \tilde{P}_{FF} < 1 - \tilde{P}_{ff}$$

- Ratio of assembly fuel escape prob. to cell fuel escape prob. in the limit of black fuel

$$\begin{aligned}
 D &= \frac{1 - \tilde{P}_{FF}}{1 - \tilde{P}_{ff}} = \frac{1 - \tilde{P}_{ff} - X_{FF}}{1 - \tilde{P}_{ff}} = 1 - \frac{x (1 - \tilde{P}_{ff})}{x (1 - \tilde{P}_{ff}) + A + B} \quad \lim_{\Sigma_f \rightarrow \infty} D = ? \\
 \lim_{\Sigma_f \rightarrow \infty} x (1 - \tilde{P}_{ff}) &= \lim_{\Sigma_f \rightarrow \infty} \gamma_f = 1 \quad \lim_{\Sigma_f \rightarrow \infty} D = 1 - \frac{1}{1 + \underbrace{A+B}_C} = 1 - \frac{1}{1+C} = \frac{C}{1+C}
 \end{aligned}$$

# Dancoff Factor and Wigner Approximation

- Various Definitions of Dancoff Factors

- Ratio of fuel escape probability of FA to that of cell for black fuel
- FF Blackness of all other materials other than fuel
- Probability of a neutron leaving a fuel pin (black fuel pin) to have first collision in other materials than fuel

$$D_{\infty} = 1 - \frac{1}{1 + A + \beta} = \frac{A}{1 + A} \text{ for infinite medium}$$

- Single Term Rational Approximation of  $P_{ff}$

$$P_{ff} = \frac{x}{x+a} \text{ with } a = \begin{cases} 1.00 & \text{for Wigner Approx.} \\ 1.16 & \text{for Bell Factor} \end{cases}$$

$$= \frac{\bar{l}\Sigma_f}{\bar{l}\Sigma_f + a} = \frac{\Sigma_f}{\Sigma_f + a} = \frac{\Sigma_f}{\Sigma_f + a\Sigma_l}$$

$$\Sigma_l = \frac{1}{l} = \frac{S}{4V} : \text{leakage cross section or surface area density}$$

Assembly fuel to fuel CP is also given as a rational form!

$$\tilde{P}_{FF} = \tilde{P}_{ff} + \frac{x(1-\tilde{P}_{ff})^2}{x(1-\tilde{P}_{ff})+C} = \frac{x}{x+a} + \frac{x\left(\frac{a}{x+a}\right)^2}{x\frac{a}{x+a}+C} = \frac{x}{x+\frac{aC}{a+C}} = \frac{x}{x+\alpha}$$



# Escape Cross Section

- Dancoff Factor with Rational Approximation

$$D = \lim_{\Sigma_f \rightarrow \infty} \frac{1 - \tilde{P}_{FF}}{1 - \tilde{P}_{ff}} = \lim_{\Sigma_f \rightarrow \infty} \frac{\frac{\alpha}{x + \alpha}}{\frac{a}{x + a}} = \lim_{\Sigma_f \rightarrow \infty} \frac{\frac{\alpha}{x}}{\frac{a}{x}} = \frac{\alpha}{a} = \frac{C}{a + C} \equiv \frac{C}{1 + C}$$

$\therefore \lim_{\Sigma_f \rightarrow \infty} a = 1 \rightarrow$  Winger approximation is valid for black fuel or  $\alpha = D$ , otherwise  $\alpha = aD$ .

- Fuel Flux for Assembly with Rational Approximation

$$\tilde{P}_{FF} = \frac{x}{x + \alpha} = \frac{\bar{l} \Sigma_f}{\bar{l} \Sigma_f + \alpha} = \frac{\Sigma_f}{\Sigma_f + \underbrace{\alpha \Sigma_l}_{\Sigma_e}} = \frac{\Sigma_f}{\Sigma_f + \Sigma_e}$$

Equivalent to homogeneous system with additional escape cross section!

$$P_{esc}^F = 1 - \tilde{P}_{FF} = \frac{\Sigma_e}{\Sigma_f + \Sigma_e}$$

escape cross section

$$\sigma_b = \frac{1}{N_F} (\lambda_F \Sigma_{pF} + \Sigma_e)$$

$$\begin{aligned} \varphi_F(u) &= \frac{\lambda_F \Sigma_{pF} \tilde{P}_{FF} + \Sigma_F(u) P_{esc}^F}{\Sigma_F(u) - (1 - \lambda_F) \Sigma_{sF}(u) \tilde{P}_{FF}} = \frac{\lambda_F \Sigma_{pF} \frac{\Sigma_f}{\Sigma_f + \Sigma_e} + \Sigma_F(u) \frac{\Sigma_e}{\Sigma_f + \Sigma_e}}{\Sigma_F(u) - (1 - \lambda_F) \Sigma_{sF}(E) \frac{\Sigma_f}{\Sigma_f + \Sigma_e}} = \frac{\lambda_F \Sigma_{pF} + \Sigma_e}{\Sigma_F(u) + \Sigma_e - (1 - \lambda_F) \Sigma_{sF}(E)} \\ &= \frac{\lambda_F \Sigma_{pF} + \Sigma_e}{\Sigma_{aF}(u) + \lambda_F \Sigma_{sF}(u) + \Sigma_e} = \frac{\lambda_F \Sigma_{pF} + \Sigma_e}{\Sigma_{aF}(u) + \lambda_F \Sigma_{sF}^{Res}(u) + \lambda_F \Sigma_{pF} + \Sigma_e} = \frac{\sigma_b}{\sigma_{aF}(u) + \lambda_F \sigma_{sF}^{Res}(u) + \sigma_b} \end{aligned}$$

# Two-Term Rational Approximation by Calvik (1962)

- General Form

$$\tilde{P}_{ff} = \sum_{n=1}^N \frac{b_n x}{x + a_n} \quad \text{where } \sum_{n=1}^N b_n = 1, \quad \because \tilde{p}_{ff} = 1 \text{ as } x \rightarrow \infty$$

- Two-Term Form

$$\tilde{P}_{ff} = x \left( \frac{b_1}{x + a_1} + \frac{b_2}{x + a_2} \right) \quad = x \left( \frac{2}{x + 2} - \frac{1}{x + 3} \right)$$

where  $b_1 + b_2 = 1$

$$\lim_{x \rightarrow \infty} x(1 - \tilde{P}_{ff}) = \sum_f \lim_{x \rightarrow \infty} \gamma_f = 1$$

$$1 - \tilde{P}_{ff} = \frac{1}{x} \rightarrow \tilde{P}_{ff} = 1 - \frac{1}{x} \rightarrow \lim_{x \rightarrow \infty} \tilde{P}'_{ff} = \frac{1}{x^2}$$

$$\lim_{x \rightarrow 0} \tilde{P}'_{ff} = \frac{b_1}{a_1} + \frac{b_2}{a_2} = \frac{2}{3} \leftarrow \text{white boundary condition for weak absorption}$$

$$\tilde{P}'_{ff} = \left( \frac{b_1 x}{x + a_1} + \frac{b_2 x}{x + a_2} \right)' = \frac{a_1 b_1}{(x + a_1)^2} + \frac{a_2 b_2}{(x + a_2)^2}$$

$$b_1 = 2, b_2 = -1, a_1 = 2, a_2 = 3$$

$$\lim_{x \rightarrow \infty} \tilde{P}'_{ff} = \frac{1}{x^2} (a_1 b_1 + a_2 b_2) \equiv \frac{1}{x^2} \rightarrow a_1 b_1 + a_2 b_2 = 1$$

# N-term Rational Approximation

- For assembly

$$\tilde{P}_{FF} = \tilde{P}_{ff} + \frac{x(1 - \tilde{P}_{ff})^2}{x(1 - \tilde{P}_{ff}) + C} = \frac{x(1 - \tilde{P}_{ff})\tilde{P}_{ff} + x(1 - \tilde{P}_{ff})^2 + C\tilde{P}_{ff}}{x(1 - \tilde{P}_{ff}) + C} = \frac{x(1 - \tilde{P}_{ff}) + C\tilde{P}_{ff}}{x(1 - \tilde{P}_{ff}) + C}$$

$$1 - \tilde{P}_{ff} = \underbrace{\sum_{n=1}^N b_n}_{=1} - x \sum_{n=1}^N \frac{b_n}{x + a_n} = \sum_{n=1}^N \frac{a_n b_n}{x + a_n}$$

$$= \frac{x \left( \sum_{n=1}^N \frac{a_n b_n}{x + a_n} + C \sum_{n=1}^N \frac{b_n}{x + a_n} \right)}{x \sum_{n=1}^N \frac{a_n b_n}{x + a_n} + C} = \frac{x \left( \sum_{n=1}^N a_n b_n \prod_{\substack{j=1 \\ j \neq n}}^N (x + a_j) + C \sum_{n=1}^N b_n \prod_{\substack{j=1 \\ j \neq n}}^N (x + a_j) \right)}{x \sum_{n=1}^N a_n b_n \prod_{\substack{j=1 \\ j \neq n}}^N (x + a_j) + C \prod_{n=1}^N (x + a_n)} \begin{matrix} \sum_{n=1}^N \beta_n = 1 \\ \therefore \text{unity coeff. of } x^{n-1} \end{matrix}$$

$$= x \frac{\left( \sum_{n=1}^N a_n b_n + C \sum_{n=1}^N b_n \right) x^{n-1} + \dots}{\left( \sum_{n=1}^N a_n b_n + C \right) x^n + \dots} = x \frac{x^{N-1} + d_{N-2} x^{N-2} + \dots}{x^N + c_{N-1} x^{N-1} + \dots} = x \frac{P_{N-1}(x)}{\prod_{n=1}^N (x + \alpha_n)} = x \sum_{n=1}^N \frac{\beta_n}{x + \alpha_n}$$

$$= \sum_{n=1}^N \frac{\beta_n \Sigma_f}{\Sigma_f + \alpha_n \Sigma_l}$$

by method of partial fraction

## Flux with Rational Approximation

$$\tilde{P}_{FF} = \sum_{n=1}^N \frac{\beta_n \Sigma_f}{\Sigma_f + \alpha_n \Sigma_l} \quad \tilde{P}_{ESC} = 1 - \tilde{P}_{FF} = \sum_{n=1}^N \left( \beta_n - \frac{\beta_n \Sigma_f}{\Sigma_f + \alpha_n \Sigma_l} \right) = \sum_{n=1}^N \frac{\alpha_n \beta_n \Sigma_l}{\Sigma_f + \alpha_n \Sigma_l}$$

$$\begin{aligned} \varphi_F(u) &= \frac{\lambda_F \Sigma_{pF} \tilde{P}_{FF} + \Sigma_F(u) P_{esc}^F}{\Sigma_F(u) - (1 - \lambda_F) \Sigma_{sF}(u) \tilde{P}_{FF}} \\ &= \frac{\lambda_F \Sigma_{pF} \sum_{n=1}^N \frac{\beta_n \Sigma_f}{\Sigma_f + \alpha_n \Sigma_l} + \Sigma_F(u) \sum_{n=1}^N \frac{\alpha_n \beta_n \Sigma_l}{\Sigma_f + \alpha_n \Sigma_l}}{\Sigma_F(u) - (1 - \lambda_F) \Sigma_{sF}(u) \sum_{n=1}^N \frac{\beta_n \Sigma_f}{\Sigma_f + \alpha_n \Sigma_l}} = \frac{\sum_{n=1}^N (\lambda_F \Sigma_{pF} + \alpha_n \Sigma_l) \frac{\beta_n}{\Sigma_f + \alpha_n \Sigma_l}}{1 - (1 - \lambda_F) \Sigma_{sF}(u) \sum_{n=1}^N \frac{\beta_n}{\Sigma_f + \alpha_n \Sigma_l}} \end{aligned}$$

If  $\lambda_F = 1$

$$\varphi_F(u) = \sum_{n=1}^N \beta_n \frac{\Sigma_{pF} + \alpha_n \Sigma_l}{\Sigma_f + \alpha_n \Sigma_l} \approx \sum_{n=1}^N \beta_n \frac{\lambda_F \Sigma_{pF} + \alpha_n \Sigma_l}{\Sigma_a(u) + \lambda_F \Sigma_{sF}(u) + \alpha_n \Sigma_l} \quad \text{approximated separate equivalence with IR}$$

$$= \beta \frac{\Sigma_p + \alpha_1 \Sigma_l}{\Sigma_f + \alpha_1 \Sigma_l} + (1 - \beta) \frac{\Sigma_{pF} + \alpha_2 \Sigma_l}{\Sigma_f + \alpha_2 \Sigma_l} \quad \text{for two term}$$

# Effective Cross Section with Calvik's Rational Approx.

$$\begin{aligned}\varphi_F(u) &= \beta \frac{\Sigma_p + \alpha_1 \Sigma_l}{\Sigma_t(u) + \alpha_1 \Sigma_l} + (1 - \beta) \frac{\Sigma_p + \alpha_2 \Sigma_l}{\Sigma_t(u) + \alpha_2 \Sigma_l} \\ &= \beta \frac{\sigma_p + \alpha_1 \sigma_l}{\sigma_t(u) + \alpha_1 \sigma_l} + (1 - \beta) \frac{\sigma_p + \alpha_2 \sigma_l}{\sigma_t(u) + \alpha_2 \sigma_l} \text{ where } \sigma_l = \frac{\Sigma_l}{N_F} = \frac{S}{4VN_F} \\ &= \beta \frac{\sigma_p + \alpha_1 \sigma_l}{\underbrace{\sigma_a(u) + \sigma_s^{res}(u) + \sigma_p + \alpha_1 \sigma_l}_{\sigma_{b1}}} + (1 - \beta) \frac{\sigma_p + \alpha_2 \sigma_l}{\underbrace{\sigma_a(u) + \sigma_s^{res}(u) + \sigma_p + \alpha_2 \sigma_l}_{\sigma_{b2}}} \\ &= \beta \frac{\sigma_{b1}}{\sigma_a(u) + \sigma_{b1}} + (1 - \beta) \frac{\sigma_{b2}}{\sigma_a(u) + \sigma_{b2}} \text{ with neglect of } \sigma_s^{res} \text{ with adjusted RI's}\end{aligned}$$

$$\bar{\sigma}_g = \frac{\int_g \left( \beta \frac{\sigma_a(u) \sigma_{b1}}{\sigma_a(u) + \sigma_{b1}} + (1 - \beta) \frac{\sigma_a(u) \sigma_{b2}}{\sigma_a(u) + \sigma_{b2}} \right) du}{\int_g \left( \beta \frac{\sigma_{b1}}{\sigma_a(u) + \sigma_{b1}} + (1 - \beta) \frac{\sigma_{b2}}{\sigma_a(u) + \sigma_{b2}} \right) du}$$

$$= \frac{\beta \bar{I}_g(\sigma_{b1}) + (1 - \beta) \bar{I}_g(\sigma_{b2})}{1 - \left( \beta \frac{\bar{I}_g(\sigma_{b1})}{\sigma_{b1}} + (1 - \beta) \frac{\bar{I}_g(\sigma_{b2})}{\sigma_{b2}} \right)}$$

← Equivalence Theorem used in CASMO

$$\bar{\sigma}_{i,g} = \bar{\sigma}_g \frac{\bar{I}_g(\sigma_p + D_i \sigma_l)}{\bar{I}_g(\sigma_p + D_\infty \sigma_l)}$$

with position-dependent Dancoff