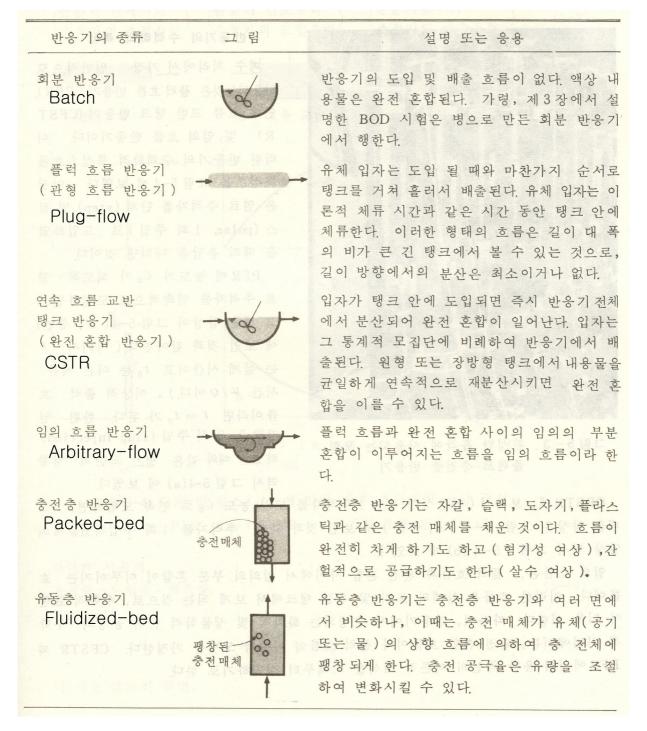
1. Reactors

- Reactors : Batch reactors vs. Continuous-flow reactors
- Completely stirred tank reactor (CSTR or CMF, Completely mixed flow reactor, CFSTR, Continuous flow stirred tank reactor) and Plug-flow reactor





1.1 Introduction on Reactor Models

Batch reactor

- no flow in or out (no transport across the boundary of the reactor)
- Contents are mixed.
- may contain a single or multiple fluids (e.g., air and water)
- -

Completely stirred tank reactor

- Generally constant flow in and out
- Contents are thoroughly mixed (Perfect mixing assumption).
- Concentration of a species in the effluent is equal to its concentration throughout the reactor.

-

Plug-flow reactor

- A tube through which fluid flows
- Assumptions: (1) The tube has constant cross-section at all axial positions, (2) the fluid velocity is uniform over the cross-section of the tube, and (3) no mixing in the axial direction of the tube (mass transport occurs only by advection).

(1) and (2) most important key concepts for the reactor modeling.

are the

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1.2 Reactor Material Balances

Material balance equation follows this general form

Accumulation rate = Inflow rate – Outflow rate \pm Net transformation rate

Net transformation rate : gain "+" and loss "-"

Inflow rate = Outflow rate = Accumulation rate =

where $Q_{in} = flow rates of fluid in [L³/T];$ $Q_{out} = flow rate of fluid out [L³/T];$ $C_{in} = concentration of species in the inflow [M/L³] or [moles/L³];$ $C_{out} = concentration of the species in the outflow [M/L³] or [moles/L³];$ C = concentration of the species [M/L³] or [moles/L³]; V = fluid volume [L³]; andt = elapsed time [T].

For general chemical reactions,

Net transformation rate =

where r = net rate of degradation of species concentration due to the reaction $[M/T,L^3]$ or $[moles/T,L^3]$.

For examples,

For flux across fluid interface,

Net transformation rate =

where J_{gl} = the species flux across the interface area [M/L²] or [moles/L²]; and A = interface area [L²].



Residence time, θ

Mean residence time of fluid molecule (hydraulic retention time in the water-based system)

Sometimes, more than one material balance equation is needed to describe a system.

1.3 Reactor Models

Batch Reactor

dt

$$\frac{d(C \cdot V)}{dt} = \text{net transformation rate} = r \cdot V$$
$$\frac{dC}{dt} = r \text{ or } \frac{d(C \cdot V)}{dt} = J \cdot A$$

dt

EXAMPLE 5.A.2 Species Decay in a Batch Reactor as a Function of Reaction Order

A species is placed in a batch reactor, where it decays by either a zeroth-, first-, or second-order reaction. Derive equations to describe the change in species concentration and characteristic times in each case. Plot the results.



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<u>CSTR</u>

$$\frac{d(C \cdot V)}{dt} = Q \cdot C_{in} - Q \cdot C + r \cdot V$$

Since V = constant

$$\frac{\mathrm{dC}}{\mathrm{dt}} = \frac{1}{\theta} \cdot \left(\mathbf{C}_{\mathrm{in}} - \mathbf{C} \right) + \mathbf{r}$$

where $\theta = V/Q$

If there is no reaction occurred in the reactor (just

Under steady state conditions (dC/ct = 0), a time dependent solution, C(t) is not required. For example, a zero order reaction



<u> PFR</u>

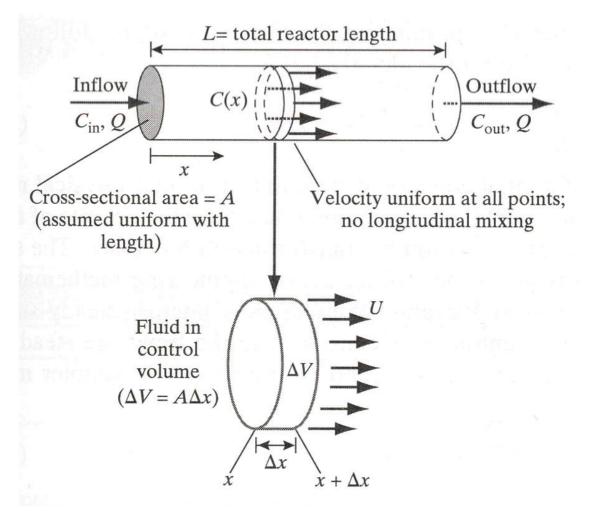
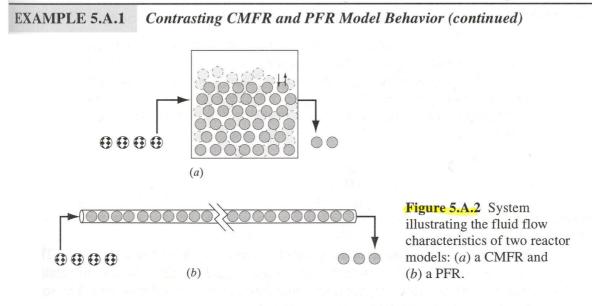


Figure 5.A.12 Schematic of an idealized plug-flow reactor and the control volume used for writing a material balance



Comparison between CSTR and PFR



How will the total number of gray and spotted marbles in the two reactors change over time?



EXAMPLE 5.A.10 Comparing CMFR and PFR Performance

Reactor performance is often characterized by calculating the ratio of the outlet concentration to the inlet concentration under steady-state conditions. Given fixed mean residence times, Θ , compare reactor performance for a CMFR and a PFR for contaminants that undergo zeroth-order, first-order, and second-order decay reactions.

SOLUTION Each of the required results has been calculated in Examples 5.A.5 and 5.A.9. The results are summarized in Table 5.A.1 and Figure 5.A.16.

For the case of a zeroth-order reaction, the reactor configuration does not affect performance: The CMFR and the PFR yield the same results. For all positive reaction orders, though, greater conversion is obtained in a PFR than in a CMFR. The difference in performance is negligible if the overall conversion is small $(C_{out}/C_{in} \sim 1)$, but the difference becomes progressively greater as conversion increases $(C_{out}/C_{in} \rightarrow 0)$.

Table 5.A.1Comparison of the Steady-State Performanceof CMFRs and PFRs

Reaction order	$C_{\rm out} / C_{\rm in}$		
	r	CMFR	PFR
Zeroth ^a	$-k_0$	$1-rac{k_0\Theta}{C_{ ext{in}}}$	$1-rac{k_0\Theta}{C_{ m in}}$
First	$-k_1C$	$\frac{1}{1+k_1\Theta}$	$\exp(-k_1\Theta)$
Second	$-2k_2C^2$	$\frac{(8k_2\Theta C_{\rm in}+1)^{1/2}-1}{4k_2\Theta C_{\rm in}}$	$\frac{1}{1+2k_2\Theta C_{\rm in}}$

^aExpressions are valid provided that $k_0 \Theta \leq C_{in}$; otherwise, $C_{out} = 0$.

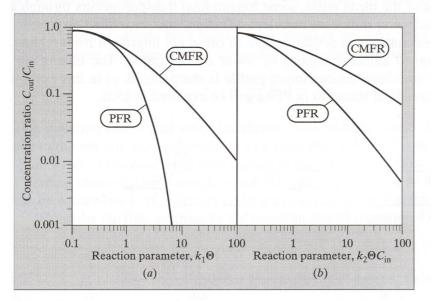


Figure 5.A.16 Steady-state reactor performance, comparing the outlet to inlet concentration ratio for a CMFR and a PFR for a species decaying by a homogeneous reaction of (a) first order or (b) second order.



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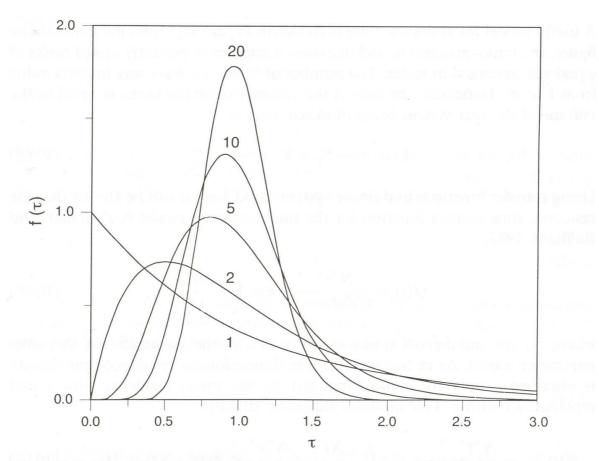


Figure 10.12. Dimensionless residence-time density for tanks-in-series model. The numbers next to the curves are the number of tanks in the series.



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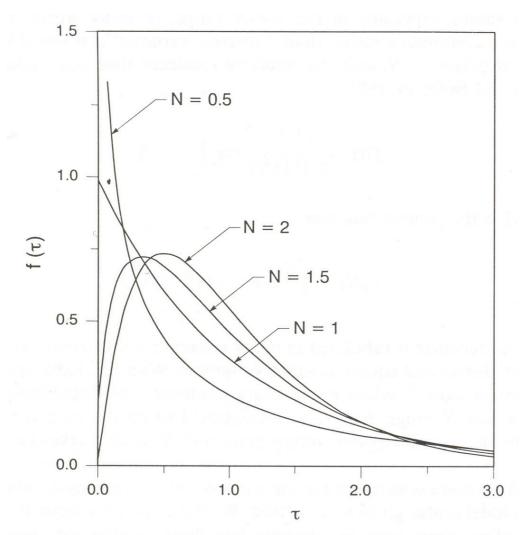


Figure 10.13. Gamma-function extension to the tanks-in-series model.

