

2.7 Consolidation Test

2.7.1 General

- Consolidation can be defined as a dissipation process of excess pore pressure induced by applied load or change of boundary conditions.

- It is a time dependent behavior of soil deformation.
 - ⇒ Significant in **saturated clayey soils**.
 - ⇒ Factors on consolidation time
 - 1) Degree of saturation
 - 2) Coefficient of permeability of soil**
 - 3) Viscosity and compressibility of the pore fluid
 - 4) Length of path the expelled pore fluid must take to find equilibrium.**
 - 5) Compressibility of soils

- Consolidation test determines parameters for the time dependent behavior of soils.
 - 1) The amount of deformation ⇒ (Primary) Consolidation settlement (+ Secondary compression settlement)
 - 2) Rate of consolidation (i.e. Consolidation time)

- Idealized stages in primary consolidation

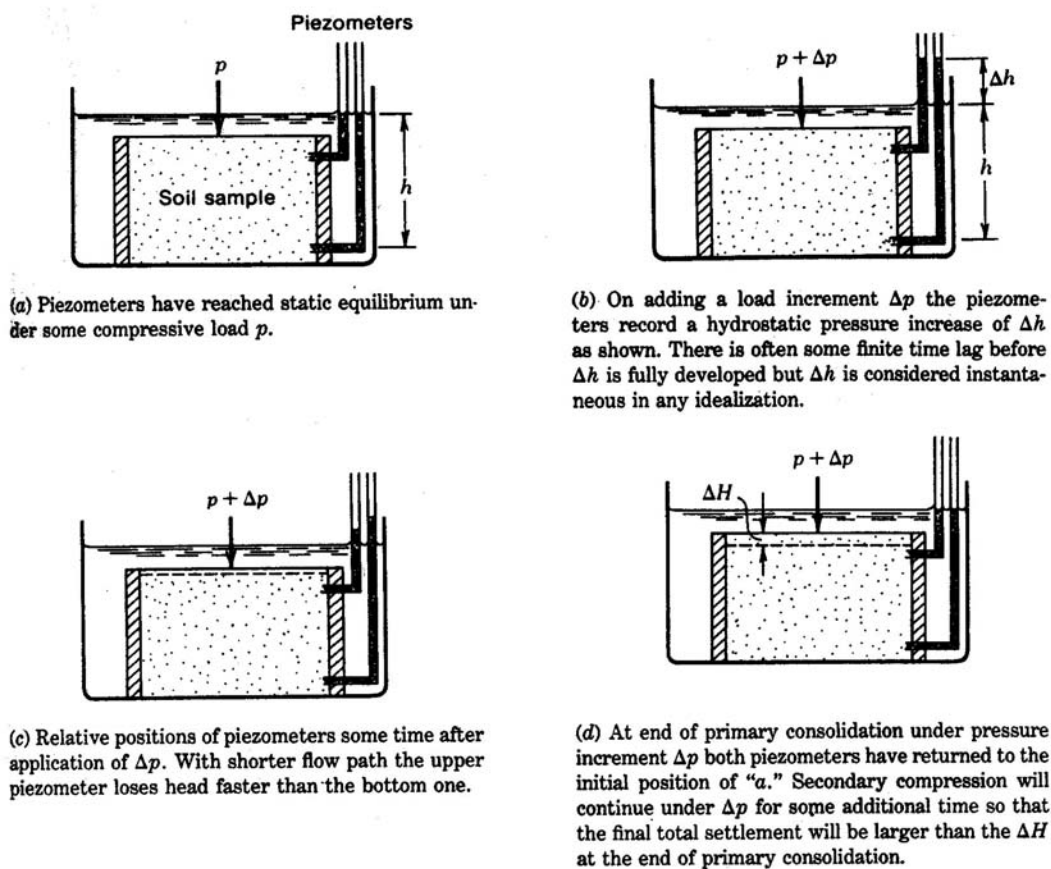


Figure 13-2 Stages in primary consolidation (idealized).

- Consolidation theory follows Darcy's law.

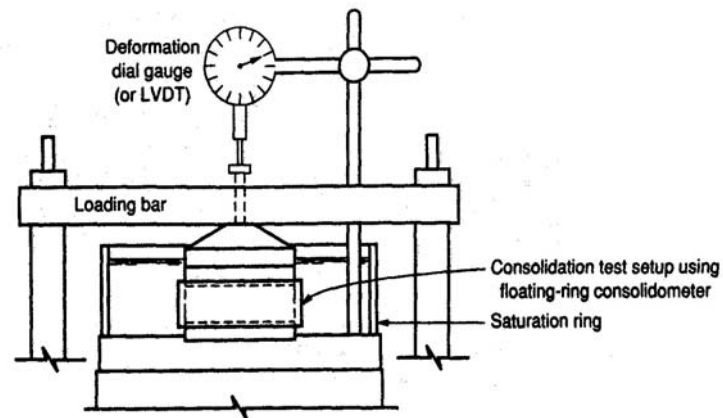
$$v = ki = k(\Delta h/L) \Rightarrow \Delta t = L/v = L/\{k(\Delta h/L)\} = L^2/(k\Delta h)$$

⇒ Doubling L requires 4 times for consolidation.

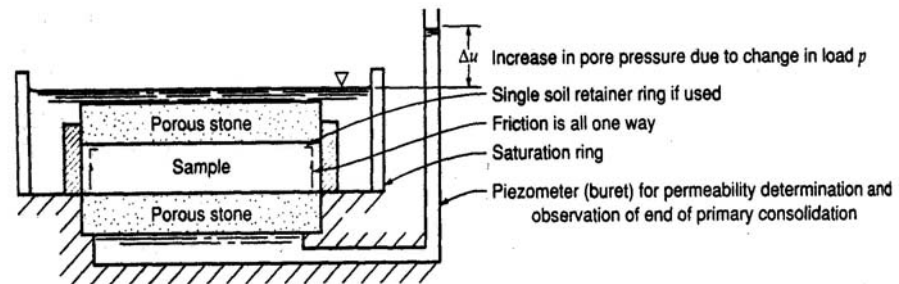
⇒ Consolidation rate is getting slower with decreasing Δh as time passes.

2.7.2 Consolidation Test

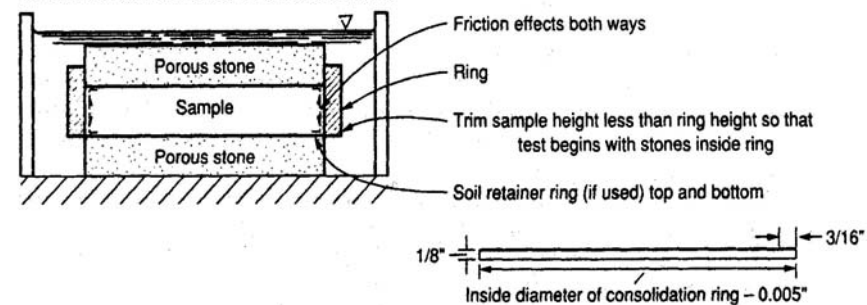
- Simulates 1-dimensional state (flow and deformation)
 - ⇒ Using a circular metal ring (the fixed-ring type or floating-ring type) confining the sample.
 - ⇒ Possible to measure the pore pressure during consolidation and to perform the permeability tests in the oedometer.



(a) Consolidometer.



(b) Fixed-ring consolidometer. May be used to perform a falling-head permeability test by attaching a buret to the piezometer outlet at base. Fill buret with water to level h_1 and at some time interval measure h_2 as in Test 12. Remove and drain buret for next load increment.



(c) Floating-ring consolidometer.

Figure 13-3
Select line details of a consolidation test.

- Sample size : 20 – 40 mm thickness(H) and 45 – 113 mm diameter(D).
 $D/H > 2.5$ and $D < (\text{Tube sample}) - 6\text{mm}$.
 (Commonly used sample size : $D = 63.5\text{mm}$, $H = 25.4\text{mm}$)
- Ring-to-soil friction problems:
 \Rightarrow Should be reduced by limiting sample thickness, spraying the inner ring wall with tefron powder or using a tefron-lined ring.
- Equipment calibration
 \Rightarrow Check the compressibility of load block and porous stones, if necessary.
- A loading sequence and measurements
 - 1) A loading sequence
 - * Applying loads with a load ratio $\Delta p/p = 1$ in general, such as (5, 10), 20, 40, 80, 160, 320, 640 ... etc., kPa with at least 1 unload-reload cycle (after reaching maximum past pressure, p_{max})
 - * Each load is sustained for one day (24 hrs)
 - * The specimen is kept under water throughout the test.
 - 2) Measurements
 - * Measuring vertical deformation from dial gage or LVDT with time. (Vertical strain, volumetric strain, change of void ratio)
 Dial gage reading \times Calibration factor = Vertical deformation (ΔH)
 \Rightarrow Vertical strain $\epsilon_{vertical}$ (= volumetric strain, ϵ_{volume}) = $\Delta H/H_o$
 \Rightarrow Change of void ratio, $\Delta e = (1+e_o) \epsilon_{vertical}$
 - * Take a dial gage reading at time sequence for each load as below (example)
 8sec, 15sec, 30sec, 1min, 2min, 4min, 8min, 15min, 30min, 1hr, 2hr...

2.7.3 Evaluating consolidation parameters from consolidation test

Typical plot of the test results

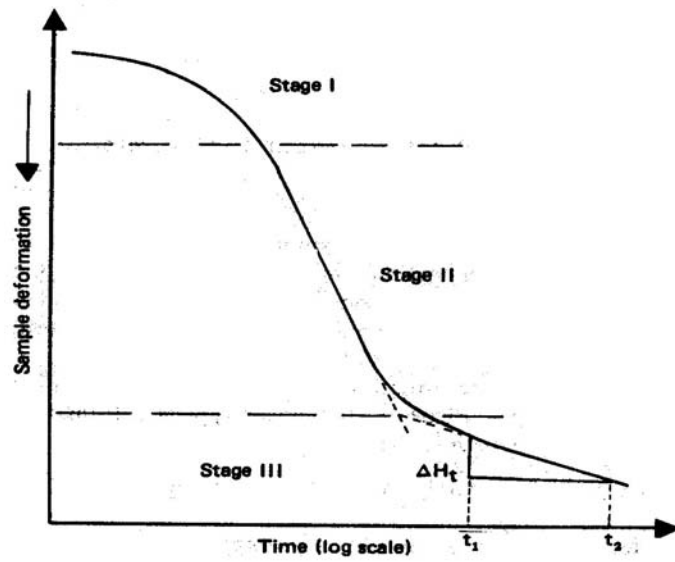


Fig. ΔH vs. t (log scale) for each load increment

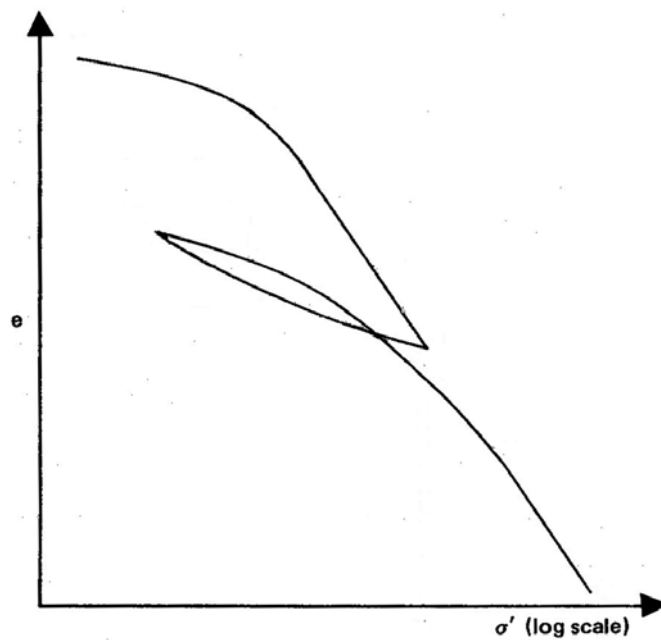


Fig. e vs. σ' (log scale)

1) Parameters for time dependent behavior.

- The coefficient of consolidation (c_v) and the secondary compression coefficient (c_a)
- From Terzaghi's 1-dimensional consolidation theory

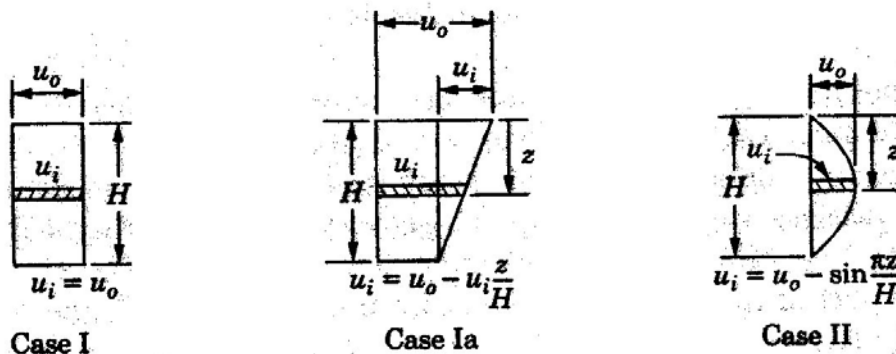
$$T_i = \frac{c_v t_i}{H_d^2} \quad \text{and} \quad c_v = \frac{T_i H_d^2}{t_i}$$

where T_i = time factor given in Table 13.1

t_i = corresponding time for T_i

H_d = the longest drainage path

Table 13-1 Time factors for indicated pressured distribution



Pore-pressure distribution for case I usually assumed for case Ia.

$U, \%$	Case I	Case II
0	0.000	0.000
10	0.008	0.048
20	0.031	0.090
30	0.071	0.115
40	0.126	0.207
50	0.197	0.281
60	0.287	0.371
70	0.403	0.488
80	0.567	0.652
90	0.848	0.933
100	∞	∞

i) Logarithm-of-time method

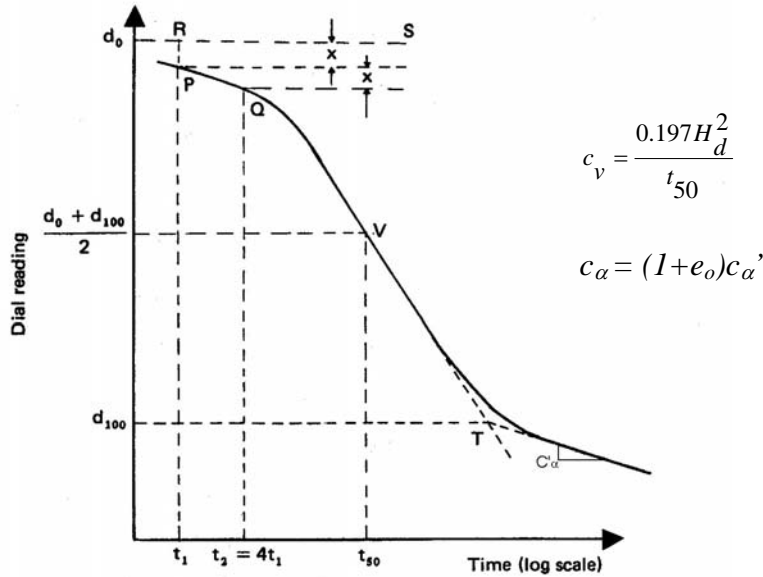


Fig. 5.37 Logarithm-of-time method for determination of C_v .

ii) Square-root-time method

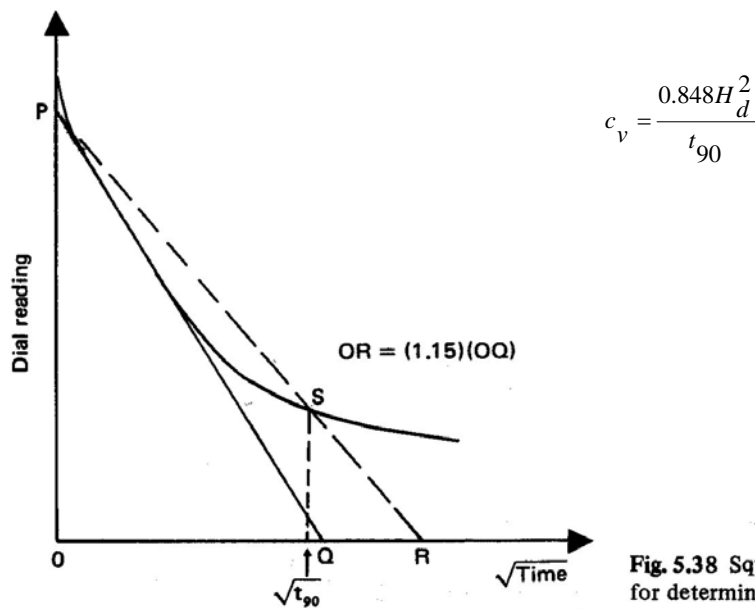


Fig. 5.38 Square-root-of-time method for determination of C_v .

2) Deformation parameters.

- The compressive index (C_c), the recompression (or swelling) index (C_r), and the preconsolidation pressure (or maximum past pressure) (p_{max})

i) The preconsolidation pressure (p_{max})

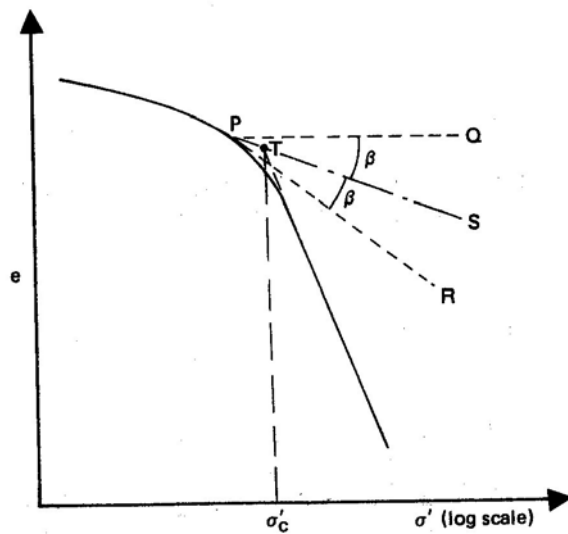


Fig. 5.32 Graphical procedure for determination of preconsolidation pressure.

ii) The compressive index (C_c), and the recompression (or swelling) index (C_r)

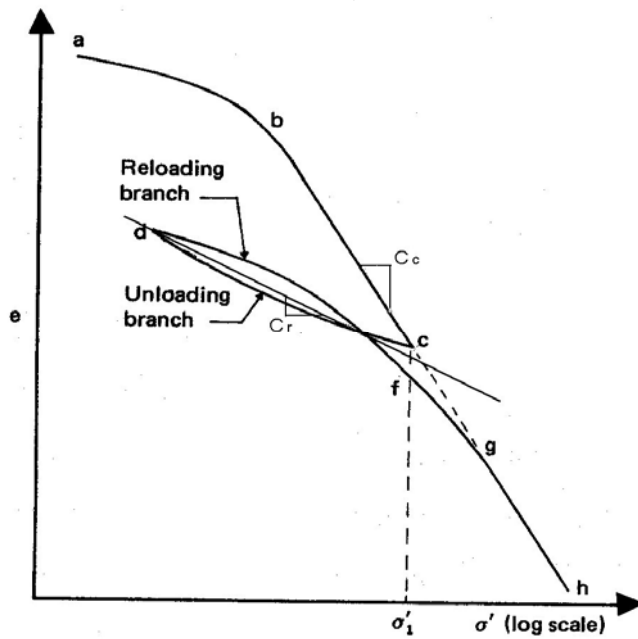


Fig. 5.31 Plot of void ratio vs. effective pressure showing unloading and reloading branches.

- $C_c = (1+e_0)C'_c$ and $C_r = (1+e_0)C'_r$
 - Note : C'_c , C'_r and c'_α is related to dial reading or volumetric(vertical) strain.
- C_c , C_r and c_α is related to void ratio e .