

2010-3-30

노트 제목

2010-03-27

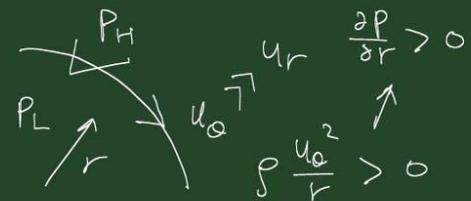
① Euler-n eq.

In a cylindrical coordinate,

$$\rho \left( \frac{\partial u_r}{\partial t} + u_r \frac{\partial u_r}{\partial r} + \frac{u_\theta}{r} \frac{\partial u_r}{\partial \theta} - \frac{u_\theta^2}{r} + u_z \frac{\partial u_r}{\partial z} \right) = -\frac{\partial p}{\partial r} + \rho \left( \nabla^2 u_r - \frac{u_r}{r^2} - \frac{2}{r^2} \frac{\partial u_\theta}{\partial \theta} \right) + \rho f_r$$

In many cases, the press. grad. term is balanced with  $\rho u_\theta^2/r$ ; i.e.,

$$\rho \frac{u_\theta^2}{r} = \frac{\partial p}{\partial r}$$



A detailed diagram illustrating the Euler-n equation balance. It shows a streamline curving to the right. A pressure gradient  $\frac{\partial p}{\partial r}$  points towards the center of curvature. The centrifugal force term  $\rho \frac{u_\theta^2}{r}$  is shown pointing towards the center, balancing the pressure gradient. The diagram includes labels for  $\rho_f < \rho_p$ ,  $r$ ,  $u_\theta$ , and  $\frac{\partial p}{\partial r}$ . The text "Euler-n eq." is written twice, and the equation  $\rho \frac{u_\theta^2}{r} = \frac{\partial p}{\partial r}$  is written at the bottom.

# PART II : Ideal Fluid Flow

neglecting viscous effects  $\rightarrow$  mathematical simplification  
 compressible

$$\nabla \cdot \underline{u} = 0$$

$$\frac{\partial \underline{u}}{\partial t} + (\underline{u} \cdot \nabla) \underline{u} = -\frac{1}{\rho} \nabla p + \underline{f} \quad \text{Euler equation}$$

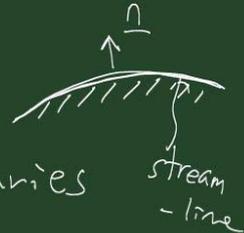
1st order PDE in space

$\rightarrow$  only one b.c. per boundary

$$\Rightarrow \underline{u} \cdot \underline{n} = \underline{U} \cdot \underline{n} \quad \text{on solid boundaries}$$

$\hookrightarrow$  velocity of the body

Surface of the body must be a streamline.



If the flow of an ideal fluid ( $\nu=0$ ) about a body originates in an irrotational flow ( $\underline{\omega}=0$ ) such as a uniform flow, then the flow will remain irrotational even near the body (Kelvin Th.).

$$\rightarrow \underline{\omega} \equiv 0 \quad \rightarrow \quad \nabla \times \underline{u} = 0$$

irrotational  $\rightarrow$   $\underline{u} = \nabla \phi$   $\phi$ : velocity potential  
 "potential flow"

$$\nabla \cdot \underline{u} = 0 \quad \rightarrow \quad \nabla^2 \phi = 0 \quad \leftarrow \text{linear eq. !}$$

superposition principle  
 solve this eq. to get  $\phi \rightarrow$  get  $\underline{u} = \nabla \phi \rightarrow p$ ?

Use Bernoulli eq.

$$\frac{\partial \phi}{\partial t} + \frac{p}{\rho} + \frac{1}{2} \nabla \phi \cdot \nabla \phi - G = F(t)$$

→ simple algebraic eq. for  $p$ .

ch. 4 Two-dimensional potential flows  
stream function, vel. potential

↳ "complex potential"

① stream function: a ft. which automatically satisfies the continuity eq.

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \Rightarrow u = \frac{\partial \psi}{\partial y}$$

$$v = -\frac{\partial \psi}{\partial x}$$

$\psi$ : stream function

valid for all 2D flows.

$$\omega_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = -\nabla^2 \psi \quad \mu=0 \rightarrow \omega=0$$

For potential flow (inviscid irrotational flow),

$$\nabla^2 \psi = 0 \rightarrow \frac{\partial^2 \psi}{\partial x^2} + \frac{\partial^2 \psi}{\partial y^2} = 0$$

Solve this eq. to get  $\psi$  → get  $u$  &  $v$  → get  $p$  from Bernoulli eq.

• The flow lines which correspond to  $\psi = \text{const}$  are the streamlines of the flow field.

pf.  $d\psi = \frac{\partial \psi}{\partial x} dx + \frac{\partial \psi}{\partial y} dy$

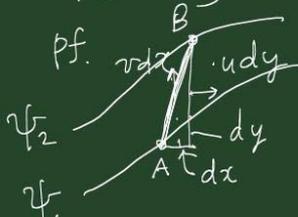
$$= -v dx + u dy = 0 \text{ for const } \psi$$

$$\rightarrow \left. \frac{dy}{dx} \right|_{\psi} = \frac{v}{u} : \text{streamline for const } \psi$$



( streamline :  $\frac{dx}{u} = \frac{dy}{v} = ds$  )

- The difference of the stream fn's values between two streamlines gives the volume of fluid which is flowing between these two streamlines.

pf.  total vol. of fluid flowing bet.  $\psi_1$  and  $\psi_2$  per unit time

$$Q = \int_A^B u dy - \int_A^B v dx$$

$$\int_A^B (d\psi = -v dx + u dy)$$

$$\rightarrow \psi_2 - \psi_1 = \int_A^B -v dx + \int_A^B u dy = Q$$

- The streamlines ( $\psi = \text{const}$ ) and the (equi)potential lines ( $\phi = \text{const}$ ) are orthogonal to each other.

pf.  $d\phi = \frac{\partial\phi}{\partial x} dx + \frac{\partial\phi}{\partial y} dy = u dx + v dy = 0$  for  $\phi = \text{const}$ .

$$\rightarrow \left. \frac{dy}{dx} \right|_{\phi} = -\frac{u}{v}$$

$$d\psi = \frac{\partial\psi}{\partial x} dx + \frac{\partial\psi}{\partial y} dy = -v dx + u dy = 0$$
 for  $\psi = \text{const}$ .

$$\rightarrow \left. \frac{dy}{dx} \right|_{\psi} = \frac{v}{u}$$

$$\Rightarrow \left. \frac{dy}{dx} \right|_{\phi} \cdot \left. \frac{dy}{dx} \right|_{\psi} = \left(-\frac{u}{v}\right) \left(\frac{v}{u}\right) = -1$$

$$\Rightarrow (\psi = \text{const}) \perp (\phi = \text{const}).$$

① Complex potential and complex velocity

$$\left. \begin{aligned} u &= \frac{\partial \phi}{\partial x} = \frac{\partial \psi}{\partial y} \\ v &= \frac{\partial \phi}{\partial y} = -\frac{\partial \psi}{\partial x} \end{aligned} \right) \text{Cauchy-Riemann eq}$$

$F(z) \equiv \phi(x, y) + i\psi(x, y)$  : complex potential

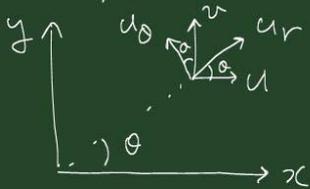
$z = x + iy$

$$\boxed{W(z) = \frac{dF}{dz}} = \frac{\partial F}{\partial z} = \frac{\partial \phi}{\partial x} + i \frac{\partial \psi}{\partial x} = u - iv \quad \text{: Complex velocity}$$

$$= \frac{\partial F}{\partial (iy)} = \frac{1}{i} \frac{\partial \phi}{\partial y} + \frac{\partial \psi}{\partial y} = u - iv$$

$$W\bar{W} = (u - iv)(u + iv) = u^2 + v^2$$

In cylindrical coord.



$$u = u_r \cos \theta - u_\theta \sin \theta$$

$$v = u_r \sin \theta + u_\theta \cos \theta$$

$$W = u - iv$$

$$= (u_r \cos \theta - u_\theta \sin \theta) - i(u_r \sin \theta + u_\theta \cos \theta)$$

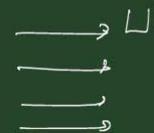
$$= u_r e^{-i\theta} - i u_\theta e^{-i\theta}$$

$$\therefore \underline{W = (u_r - i u_\theta) e^{-i\theta}} \quad \text{in cyl. coord.}$$

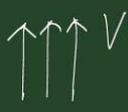
① uniform flow :  $F(z) = cz$

$$W(z) = \frac{dF}{dz} = c = u - iv \Rightarrow \begin{aligned} u &= c = U \\ v &= 0 \end{aligned}$$

$$\therefore \boxed{F(z) = Uz}$$



$$F(z) = -iVz \rightarrow W(z) = \frac{dF}{dz} = -iV = u - iv$$

$$\rightarrow u=0, v=V$$


$$F(z) = Ve^{-i\alpha}z \rightarrow W(z) = \frac{dF}{dz} = Ve^{-i\alpha}$$

$$= V\cos\alpha - iV\sin\alpha$$

$$= u - iv$$

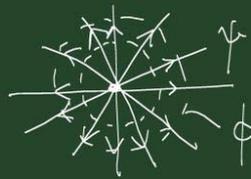
$$u = V\cos\alpha, v = V\sin\alpha$$


② Source/sink:  $F(z) = c \ln z$  ( $z = re^{i\theta}$ )

$$= c \ln re^{i\theta}$$

$$= c \ln r + ic\theta = \phi + i\psi$$

$$\phi = c \ln r, \psi = c\theta$$



direction?

$$W(z) = \frac{dF}{dz} = \frac{c}{z} = \frac{c}{r} e^{-i\theta}$$

$$= (u_r - iu_\theta) e^{-i\theta}$$

$$\rightarrow u_r = \frac{c}{r}, u_\theta = 0$$

$c > 0$  source  
 $c < 0$  sink

$r=0$ ; singular pt.

Strength  $m \equiv \int u_r dl = \int_0^{2\pi} u_r r d\theta = 2\pi c$

$$\rightarrow F(z) = \frac{m}{2\pi} \ln z$$

$$F(z) = \frac{m}{2\pi} \ln(z - z_0)$$

source located at  $z = z_0$