# **Chapter 9**

# **Rubber Elasticity**

### Rubber

業 rubber (지우개?) = elastomer (탄성체, better term) 業 A rubber

stretches to 100's of %
← flexible chain (T<sub>g</sub> < room temp)</li>
snaps back to its original length instantly
← crosslinked (chemically)
✓ vulcanization (가황) □p432
✓ physically crosslinked in TPE
➤ TPE ~ thermoplastic elastomer □p483



## Rubber is an entropy spring.

metal spring ~ energy-driven elasticity

internal energy, U

$$\partial U/\partial r = f$$
, force

F = U - TSFor ideal gas,  $\partial U/\partial V = 0$  $P = T \partial S / \partial V$ 

rubber ~ entropy-driven elasticity

S

$$r_i = \langle r_i^2 \rangle^{\frac{1}{2}}$$

 $\int f = \partial (-T\Delta S)/\partial r$   $\checkmark$  ideal rubber

Fig 9.7 p439

### **Rubber elasticity equations**

#### Statistical Thermodynamics

- Helmoltz free energy, F = U T S (9.5)
- (retractive) force, f

 $f = \partial F / \partial r = \partial U / \partial r - T \partial S / \partial r = -kT \partial In\Omega / \partial r \quad \squareeqn (9.6), (9.20)$ 

- For one chain;
  - $\Omega \sim \#$  of conformations  $\rightarrow$  probability of a conformation
  - W(r) ~ probability finding the other end at betw r & r+dr  $\square$  Fig 9.9 W(r)dr = [ $\Omega$ dr /  $\int \Omega$ dr]  $4\pi$ r<sup>2</sup>  $\square$  eqn (9.22)
  - $\Omega$  for Gaussian W(r)  $\square$  Fig 9.10

 $\partial \ln \Omega / \partial r = -2 \beta^2 r$  where  $\beta = 3/(2 < r_0^2 >)$  log eqn (9.26)

f from eqn (9.20) & (9.26)

 $f = 3 kTr/\langle r_0^2 \rangle$  @eqn (9.27)  $f \propto r \sim a spring$ 

### Stat thermo 2

- For n chains;
  - deformation from r<sub>i</sub> to r
    - r<sub>0</sub> → r for 1 chain, r<sub>i</sub> → r for many chains practically, r<sub>0</sub> = r<sub>i</sub>



$$<\mathbf{r}^{2}>/<\mathbf{r}_{i}^{2}> = (1/3)(\alpha_{x}^{2} + \alpha_{y}^{2} + \alpha_{z}^{2})$$
 @eqn (9.28)

work done, using eqn (9.27)

 $-W = \Delta F = [3nRT/\langle r_0^2 \rangle] \int r \, dr \, (\int \text{from } r_i \text{ to } r) \quad \square eqn (9.30)$ 

Integrating and using eqn (9.28)

 $\Delta F = (nRT/2) (\alpha_x^2 + \alpha_y^2 + \alpha_z^2 - 3)$  and eqn (9.31)

• When incompressible (v = 0.5),  $\alpha_x \alpha_y \alpha_z = 1$ ,  $\alpha_y = \alpha_z = 1/\alpha_x^{\nu_2} = 1/\alpha^{\nu_2}$  $\Delta F = (nRT/2) (\alpha^2 + 2/\alpha - 3)$  and eqn (9.33)

stress, σ

 $\sigma = \partial F / \partial \alpha = nRT (\alpha - 1/\alpha^2)$   $\square eqn (9.34)$ 

Equation of state (EOS) for rubber elasticity



extension ratio,  $\alpha = 1 + \varepsilon$ 

### Stat thermo 3

- constitutive eqn (구성방정식, relation betw σ and ε)
  - extension ratio, α

•  $\alpha = 1 + \varepsilon$ 

- $\alpha^{-2} = (1 + \varepsilon)^{-2} = 1 2\varepsilon + \cdots \approx 1 2\varepsilon$  for small  $\varepsilon$
- modulus, E from eqn (9.34)
  - $E = \sigma/\epsilon = [nRT (1 + \epsilon (1 2\epsilon)) / \epsilon = 3nRT$
- For rubber, v = 0.5
  - $G = E / 2(1 + v) = E/3 = nRT = (\rho RT/M_c)$
  - n ~ # of chains → # of chain fragments
  - M<sub>c</sub> ~ mol wt betw Xlinks



 $G_N^0 = \rho RT/M_e$  for linear polymers  $M_e \sim entanglement mol wt$  $\square$  Fig 9.21 p464

## **Continuum mechanics eqn**

Continuum Mechanics approach

Mooney-Rivlin eqn

 $\sigma = (2C_1 + 2C_2/\alpha) (\alpha - 1/\alpha^2) = G (\alpha - 1/\alpha^2)$  Compared eqn (9.49)

#### Comparison with experiments

f (σ)



Rubber becomes compressible, anisotropic, and strain-induced crystallizes.

Fig 9.5 p436