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## Thermodynamics

Ch. 1 Overview

Ch. 2 Thermodynamics

## Kinetics

Ch. 3 & 4

Charge-transfer limiting

Mass-transfer limiting

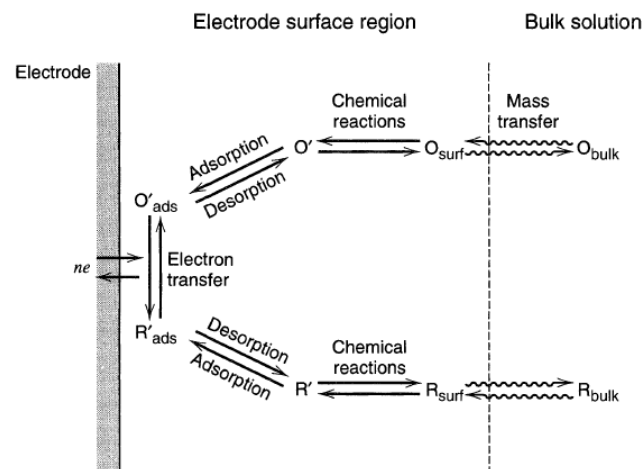
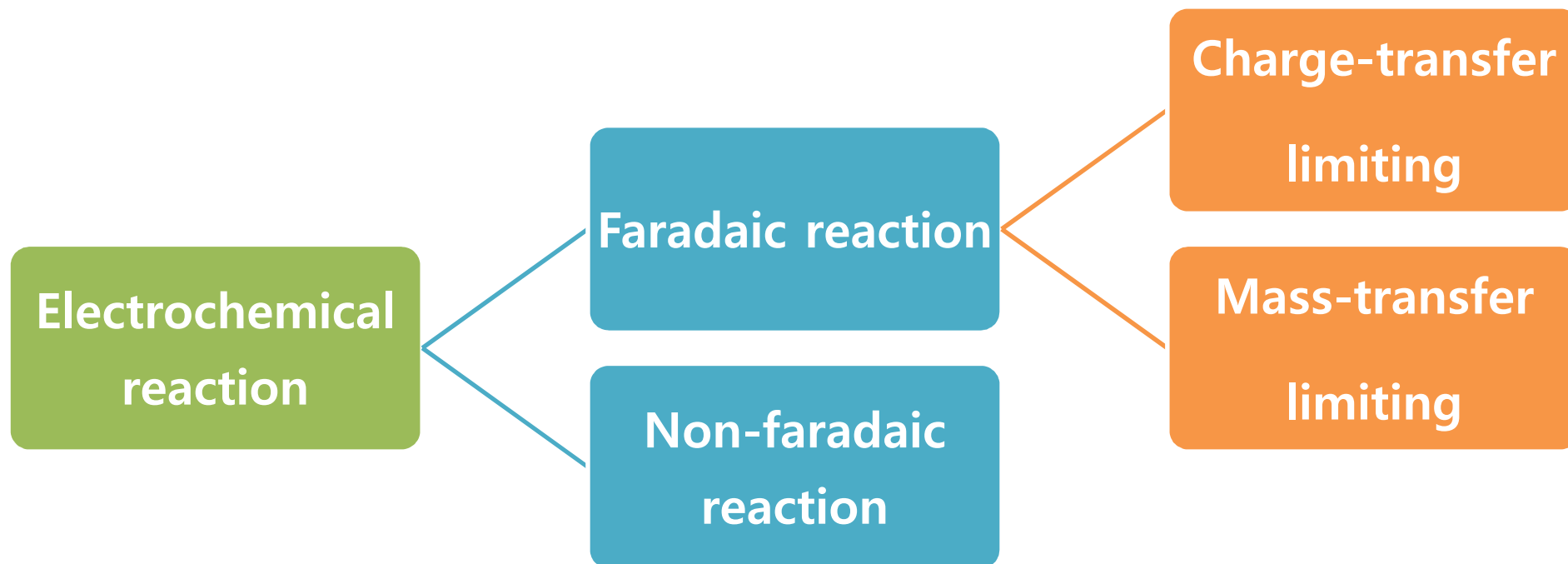
## Methods

Ch. 5 Potential step

Ch. 6 Potential sweep

Ch. 8 Controlled current

Ch. 10 Impedance



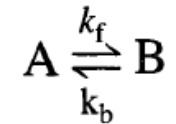
**Figure 1.3.6** Pathway of a general electrode reaction.

# **KINETICS OF ELECTRODE REACTIONS**

## 3.1 REVIEW OF HOMOGENEOUS KINETICS

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- Consider a simple unimolecular elementary [chemical reaction](#) between A and B



→ The rate of the [forward](#) process,  $v_f$  (M/s),

$$v_f = k_f C_A$$

$k_f$  and  $k_b$ : rate constants

→ The rate of the [backward](#) process,  $v_b$  (M/s),

$$v_b = k_b C_B$$

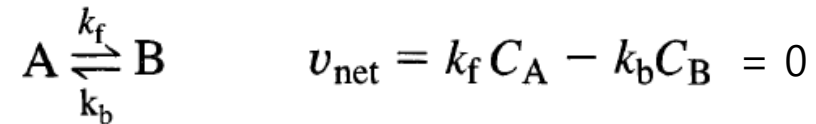
→ The [net conversion rate](#) of A to B

$$v_{\text{net}} = k_f C_A - k_b C_B$$

## 3.1 REVIEW OF HOMOGENEOUS KINETICS

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- At equilibrium, the net conversion rate is zero



→ But, the rate of the forward or backward processes is not zero

→ The rate of the forward process = The rate of the backward process

$$v_0 = k_f(C_A)_{\text{eq}} = k_b(C_B)_{\text{eq}}$$

→  $v_0$ : the exchange velocity of the reaction

## 3.1 REVIEW OF HOMOGENEOUS KINETICS

- The **rate constants** are expressed in the **Arrhenius form**:

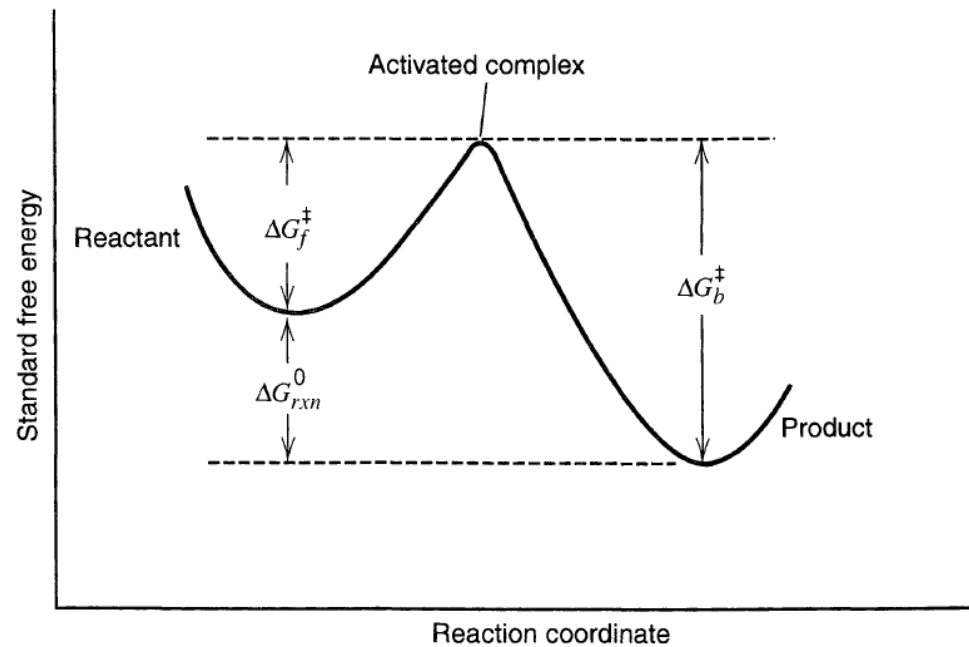
$$k = Ae^{-E_A/RT}$$

$E_A$ : activation energy

A: frequency factor

- In terms of free energy based on the **activated complex theory**:

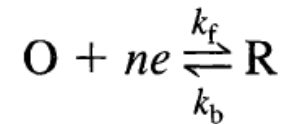
$$k = A' e^{-\Delta G^\ddagger/RT}$$



## 3.2 ESSENTIALS OF ELECTRODE REACTIONS

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- Consider a general electrode reaction ([electrochemical reaction](#)) of



→ The rate of the [forward \(cathodic\)](#) reaction,  $v_f$  (M/s),

$$v_f = k_f C_{\text{O}}(0, t) = \frac{i_c}{nFA}$$

-  $k_f$  and  $k_b$  : rate constants

-  $C(x,t)$ : concentration at distance  $x$  and time  $t$ )

→ The rate of the [backward \(anodic\)](#) reaction,  $v_b$  (M/s),

$$v_b = k_b C_{\text{R}}(0, t) = \frac{i_a}{nFA}$$

-  $C(0,t)$ : surface concentration

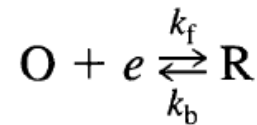
→ The [net reaction rate](#)

$$v_{\text{net}} = v_f - v_b = k_f C_{\text{O}}(0, t) - k_b C_{\text{R}}(0, t) = \frac{i}{nFA}$$

$$i = i_c - i_a = nFA[k_f C_{\text{O}}(0, t) - k_b C_{\text{R}}(0, t)]$$

## 3.2 ESSENTIALS OF ELECTRODE REACTIONS

- Consider the simplest possible electrode process, wherein species O and R engage in a **one-electron transfer** at the interface **without being involved in any other chemical step**

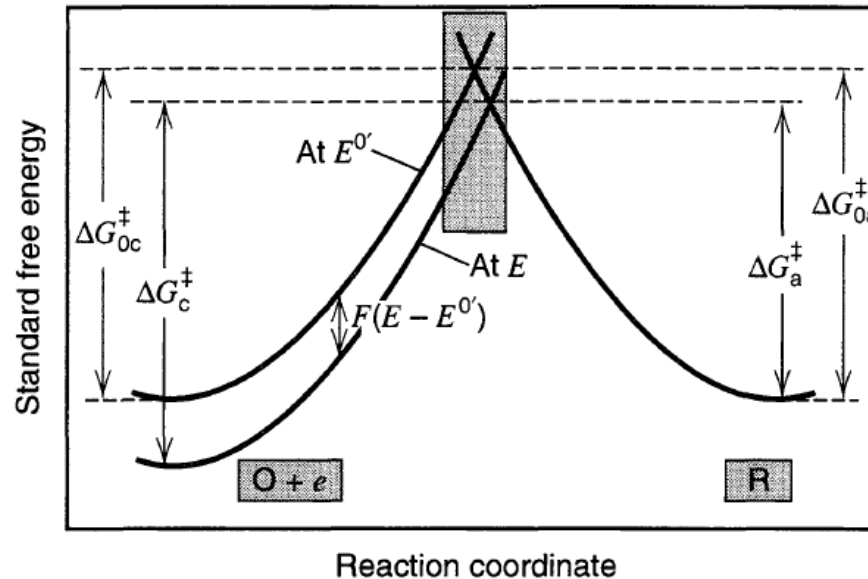


$$E = E^{0'} + \frac{RT}{nF} \ln \frac{C_{\text{O}}^*}{C_{\text{R}}^*}$$

at equilibrium

cathodic activation energy at  $E^{0'}$

$$\Delta G_{0c}^{\ddagger}$$

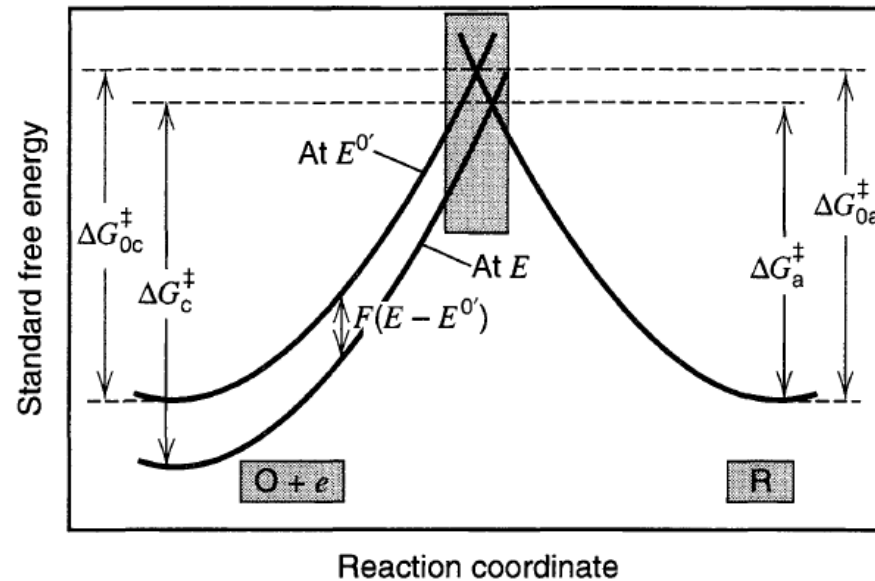


anodic activation energy  
at  $E^{0'}$

$$\Delta G_{0a}^{\ddagger}$$

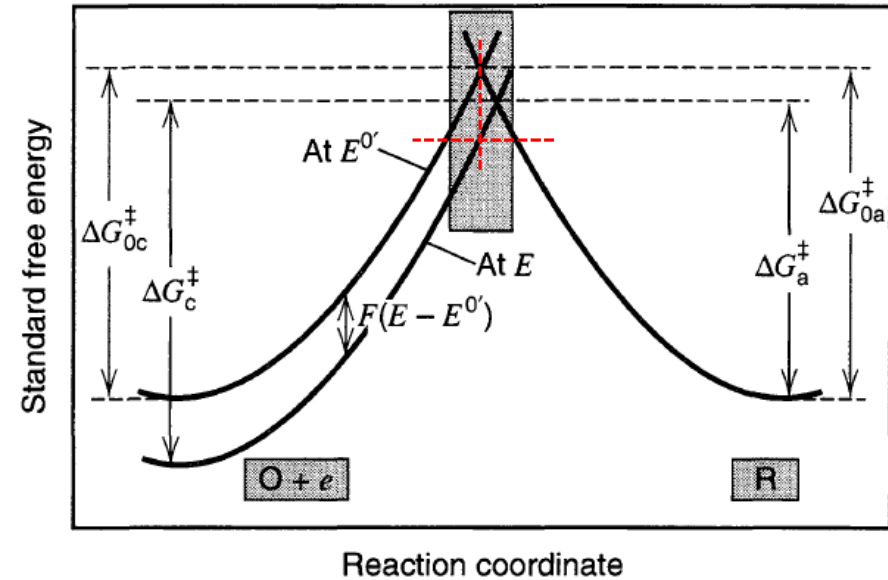
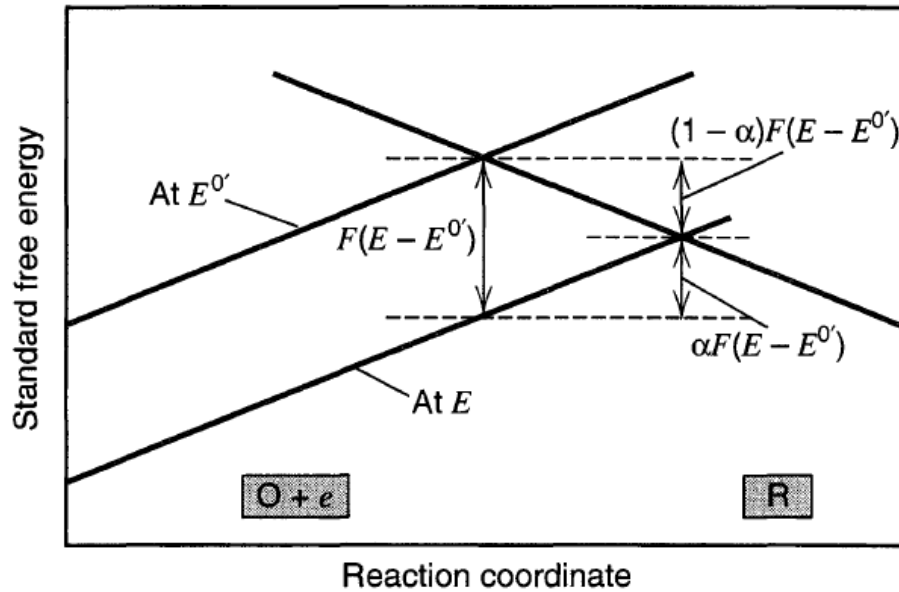


## 3.2 ESSENTIALS OF ELECTRODE REACTIONS



- If the potential is changed by  $\Delta E$  to a new value,  $E$ ,
  - the relative energy of the electron resident on the electrode changes by  $-F\Delta E = -F(E - E^0) = \Delta G$
  - hence the  $O + e$  curve shifts up or down by that amount
  - At a positive potential difference ( $E > E^0$ )
    - : the energy of electron is lowered, and the  $O + e$  curve shifts down
    - : the anodic activation energy is lowered

## 3.2 ESSENTIALS OF ELECTRODE REACTIONS



$\alpha$  : the [transfer coefficient](#)

→ can range from zero to unity → dependent on the shape of the intersection region

- At potential  $E$

$$\Delta G_a^{\ddagger} = \Delta G_{0a}^{\ddagger} - (1 - \alpha)F(E - E^0)$$

$$\Delta G_a^{\ddagger} < \Delta G_{0a}^{\ddagger}$$

$$\Delta G_c^{\ddagger} = \Delta G_{0c}^{\ddagger} + \alpha F(E - E^0)$$

$$\Delta G_c^{\ddagger} > \Delta G_{0c}^{\ddagger}$$

## 3.2 ESSENTIALS OF ELECTRODE REACTIONS

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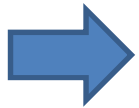
- Now let us assume that the rate constants  $k_f$  and  $k_b$  have an Arrhenius form that can be expressed as

$$k_f = A_f \exp(-\Delta G_c^\ddagger/RT)$$

$$k_b = A_b \exp(-\Delta G_a^\ddagger/RT)$$

$$\Delta G_a^\ddagger = \Delta G_{0a}^\ddagger - (1 - \alpha)F(E - E^{0'})$$

$$\Delta G_c^\ddagger = \Delta G_{0c}^\ddagger + \alpha F(E - E^{0'})$$



$$k_f = A_f \exp(-\Delta G_{0c}^\ddagger/RT) \exp[-\alpha f(E - E^{0'})]$$

$$k_b = A_b \exp(-\Delta G_{0a}^\ddagger/RT) \exp[(1 - \alpha)f(E - E^{0'})]$$

: where  $f = F/RT$

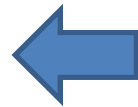
- The first two factors in each of these expressions
  - : independent of potential
  - : equal to the rate constant at  $E = E^{0'}$ .

## 3.2 ESSENTIALS OF ELECTRODE REACTIONS

- Consider the special case in which the interface is **at equilibrium** with a solution in which  $C_O^* = C_R^*$ .

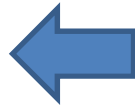
→ In this situation,

$$E = E^{0'}$$



$$E = E^{0'} + \frac{RT}{nF} \ln \frac{C_O^*}{C_R^*} \quad \text{at equilibrium}$$

$$k_f C_O^* = k_b C_R^*$$



$$\begin{aligned} v_{\text{net}} = v_f - v_b &= k_f C_O(0, t) - k_b C_R(0, t) \\ &= k_f C_O^* - k_b C_R^* \\ &= 0 \end{aligned}$$

$$k_f = k_b$$

$$E = E^{0'}$$

→ The potential where the **forward and reverse rate constants** have the same value

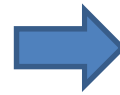
→ That value of rate constant: **standard rate constant,  $k^0$**

## 3.2 ESSENTIALS OF ELECTRODE REACTIONS

- The rate constants at other potentials can then be expressed simply in terms of  $k^0$

$$k_f = A_f \exp(-\Delta G_{0c}^\ddagger/RT) \exp[-\alpha f(E - E^{0'})]$$

$$k_b = A_b \exp(-\Delta G_{0a}^\ddagger/RT) \exp[(1 - \alpha)f(E - E^{0'})]$$



$$k_f = k^0 \exp[-\alpha f(E - E^{0'})]$$

$$k_b = k^0 \exp[(1 - \alpha)f(E - E^{0'})]$$

- The net reaction rate for  $O + e \xrightleftharpoons[k_b]{k_f} R$

$$v_{\text{net}} = v_f - v_b = k_f C_O(0, t) - k_b C_R(0, t) = \frac{i}{nFA}$$

$$i = i_c - i_a = nFA[k_f C_O(0, t) - k_b C_R(0, t)]$$

$$i = F A k^0 \left[ C_O(0, t) e^{-\alpha f(E - E^{0'})} - C_R(0, t) e^{(1-\alpha)f(E - E^{0'})} \right]$$

→ the relationship between **current and potential**

## 3.4 THE BUTLER-VOLMER MODEL

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- At equilibrium ( $E = E_{\text{eq}}$ ), the net current is zero

$$i = F A k^0 \left[ C_{\text{O}}(0, t) e^{-\alpha f (E - E^{0'})} - C_{\text{R}}(0, t) e^{(1-\alpha) f (E - E^{0'})} \right] = 0$$

$$\Rightarrow F A k^0 C_{\text{O}}(0, t) e^{-\alpha f (E_{\text{eq}} - E^{0'})} = F A k^0 C_{\text{R}}(0, t) e^{(1-\alpha) f (E_{\text{eq}} - E^{0'})}$$

- Also, at equilibrium,  $C(0, t) = C^*$

$$e^{f (E_{\text{eq}} - E^{0'})} = \frac{C_{\text{O}}^*}{C_{\text{R}}^*} \quad : \text{ simply an exponential form of the [Nernst relation](#) }$$

$$\Rightarrow E_{\text{eq}} = E^{0'} + \frac{RT}{F} \ln \frac{C_{\text{O}}^*}{C_{\text{R}}^*} \quad : \text{ reasonable to use the activated complex theory for electrochemical reactions}$$

## 3.4 THE BUTLER-VOLMER MODEL

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- Even though the net current is zero at equilibrium, the cathodic and anodic reaction rates (currents) are not zero

$$\rightarrow i = i_c - i_a = 0$$

$$\rightarrow i_c = i_a$$

- At equilibrium, the magnitude to either component current,  $i_c$  or  $i_a$  is called [the exchange current  \$i\_0\$](#)

→ Similar to [exchange velocity](#) for chemical reactions

$$i = FAk^0 \left[ C_{\text{O}}(0, t)e^{-\alpha f(E - E^{0'})} - C_{\text{R}}(0, t)e^{(1-\alpha)f(E - E^{0'})} \right] = 0$$

$$FAk^0 C_{\text{O}}(0, t)e^{-\alpha f(E_{\text{eq}} - E^{0'})} = FAk^0 C_{\text{R}}(0, t)e^{(1-\alpha)f(E_{\text{eq}} - E^{0'})}$$

$$\Rightarrow i_0 = FAk^0 C_{\text{O}}^* e^{-\alpha f(E_{\text{eq}} - E^{0'})}$$

### 3.4 THE BUTLER-VOLMER MODEL

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$$e^{f(E_{\text{eq}} - E^{0'})} = \frac{C_{\text{O}}^*}{C_{\text{R}}^*}$$

If both sides of the above equation are raised to the  $-\alpha$  power, we obtain

$$e^{-\alpha f(E_{\text{eq}} - E^{0'})} = \left( \frac{C_{\text{O}}^*}{C_{\text{R}}^*} \right)^{-\alpha}$$

$$i_0 = F A k^0 C_{\text{O}}^* e^{-\alpha f(E_{\text{eq}} - E^{0'})}$$



$$i_0 = F A k^0 C_{\text{O}}^{*(1-\alpha)} C_{\text{R}}^{*\alpha}$$

$$i = F A k^0 \left[ C_{\text{O}}(0, t) e^{-\alpha f(E - E^{0'})} - C_{\text{R}}(0, t) e^{(1-\alpha)f(E - E^{0'})} \right]$$



### 3.4 THE BUTLER-VOLMER MODEL

$$\frac{i}{i_0} = \frac{C_O(0, t)e^{-\alpha f(E-E^{0'})}}{C_O^{*(1-\alpha)}C_R^{*\alpha}} - \frac{C_R(0, t)e^{(1-\alpha)f(E-E^{0'})}}{C_O^{*(1-\alpha)}C_R^{*\alpha}}$$

➔ 
$$\frac{i}{i_0} = \frac{C_O(0, t)}{C_O^*} e^{-\alpha f(E-E^{0'})} \left(\frac{C_O^*}{C_R^*}\right)^\alpha - \frac{C_R(0, t)}{C_R^*} e^{(1-\alpha)f(E-E^{0'})} \left(\frac{C_O^*}{C_R^*}\right)^{-(1-\alpha)}$$

$$E_{\text{eq}} = E^{0'} + \frac{RT}{F} \ln \frac{C_O^*}{C_R^*} \quad \left[ e^{f(E_{\text{eq}}-E^{0'})} = \frac{C_O^*}{C_R^*} \right]$$

➔ 
$$i = i_0 \left[ \frac{C_O(0, t)}{C_O^*} e^{-\alpha f\eta} - \frac{C_R(0, t)}{C_R^*} e^{(1-\alpha)f\eta} \right] \quad \eta = E - E_{\text{eq}}$$

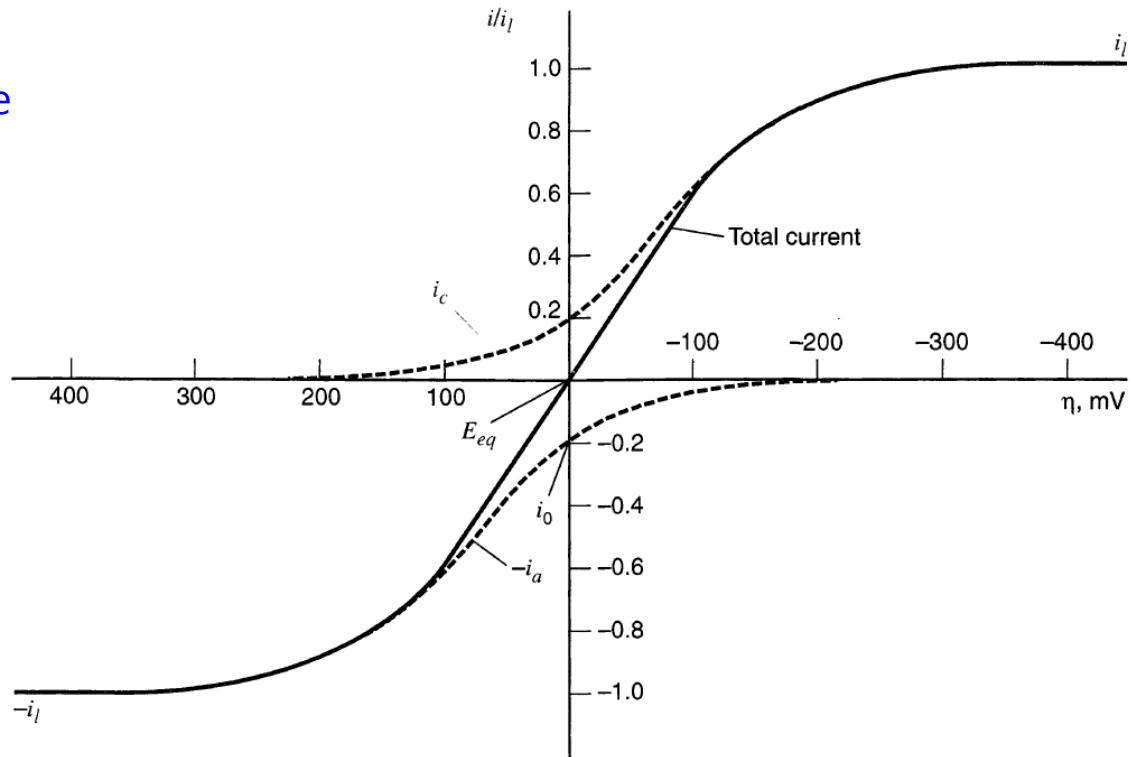
: the **current-overpotential equation**

→ the first term describes the **cathodic** component current at any potential, and the second gives the **anodic** contribution

### 3.4 THE BUTLER-VOLMER MODEL

$$i = i_0 \left[ \frac{C_O(0, t)}{C_O^*} e^{-\alpha f \eta} - \frac{C_R(0, t)}{C_R^*} e^{(1-\alpha) f \eta} \right]$$

For large positive overpotentials,  
 → the cathodic component is negligible  
 → the total current is the same as  $i_a$



**Figure 3.4.1** Current-overpotential curves for the system  $O + e \rightleftharpoons R$  with  $\alpha = 0.5$ ,  $T = 298$  K,  $i_{l,c} = -i_{l,a} = i_l$  and  $i_0/i_l = 0.2$ . The dashed lines show the component currents  $i_c$  and  $i_a$ .

For large negative overpotentials,  
 → the anodic component is negligible  
 → the total current is the same as  $i_c$

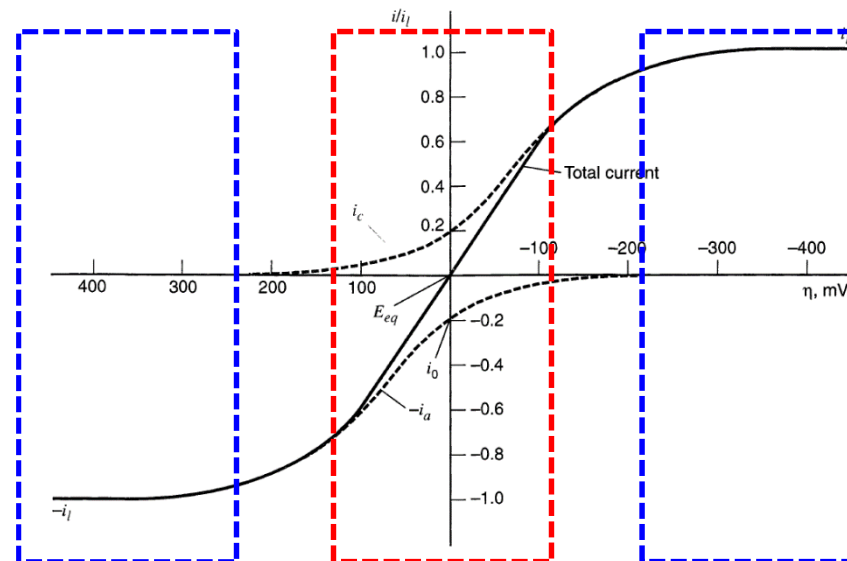
: The solid curve shows the actual total current, which is the sum of the components  $i_c$  and  $i_a$ , shown as dashed traces.

## 3.4 THE BUTLER-VOLMER MODEL

- In going either direction from  $E_{eq}$  (red box),
  - the magnitude of the current rises rapidly
  - the exponential factors dominate behavior

$$i = i_0 \left[ \frac{C_O(0, t)}{C_O^*} e^{-\alpha f \eta} - \frac{C_R(0, t)}{C_R^*} e^{(1-\alpha) f \eta} \right]$$

- At extreme  $\eta$  (blue box),
  - the current approaches the limiting current
  - the current is limited by mass transfer



**Figure 3.4.1** Current-overpotential curves for the system  $O + e \rightleftharpoons R$  with  $\alpha = 0.5$ ,  $T = 298$  K,  $i_{l,c} = -i_{l,a} = i_l$  and  $i_0/i_l = 0.2$ . The dashed lines show the component currents  $i_c$  and  $i_a$ .

## 3.4 THE BUTLER-VOLMER MODEL

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### (a) No Mass-Transfer Effects

- If the solution is well stirred, or currents are kept so low that the surface concentrations do not differ appreciably from the bulk values

$$i = i_0 \left[ \frac{C_O(0, t)}{C_O^*} e^{-\alpha f \eta} - \frac{C_R(0, t)}{C_R^*} e^{(1-\alpha) f \eta} \right]$$



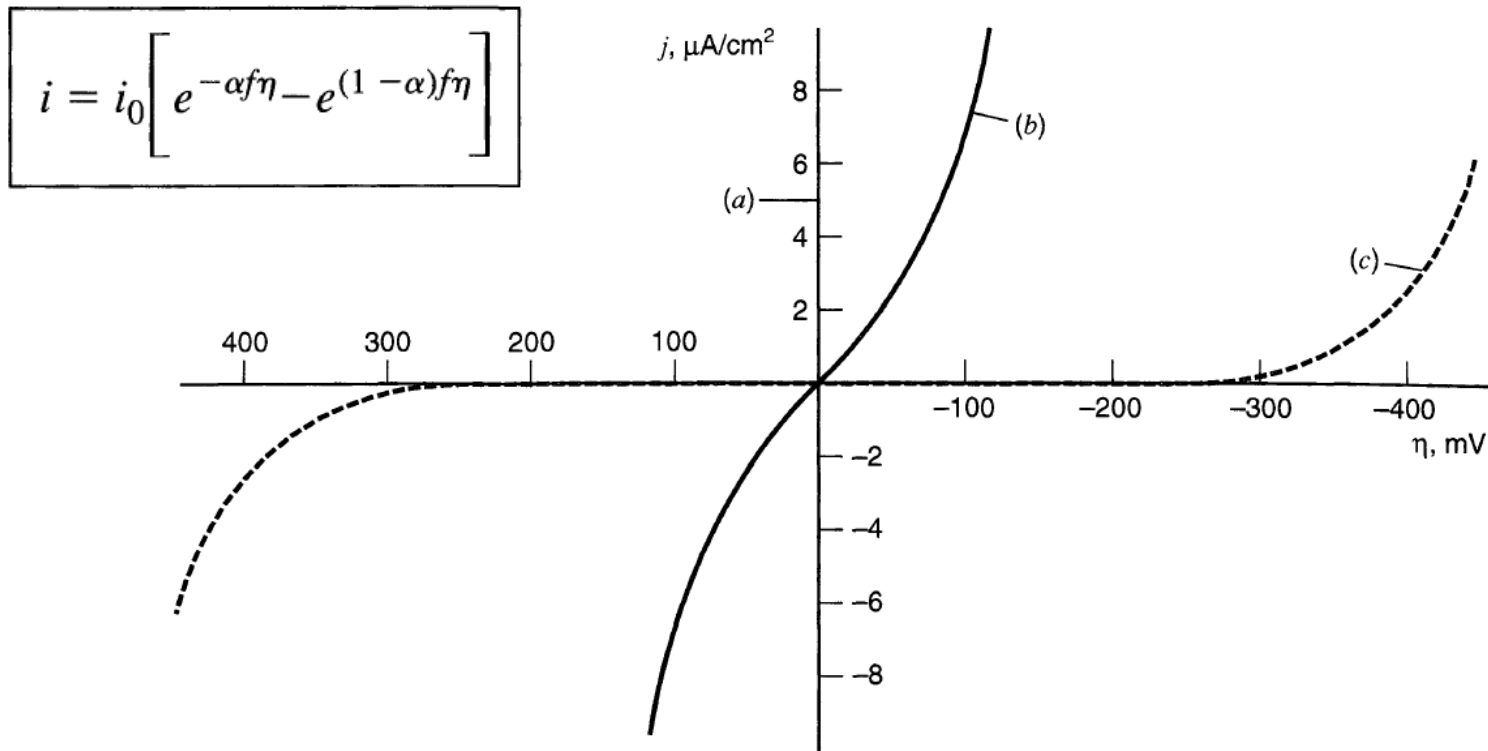
$$i = i_0 \left[ e^{-\alpha f \eta} - e^{(1-\alpha) f \eta} \right]$$

: the [Butler-Volmer equation](#)

→ It is a good approximation when  $i$  is less than about 10% of the smaller limiting current,  $i_{l,c}$  or  $i_{l,a}$ .

## 3.4 THE BUTLER-VOLMER MODEL

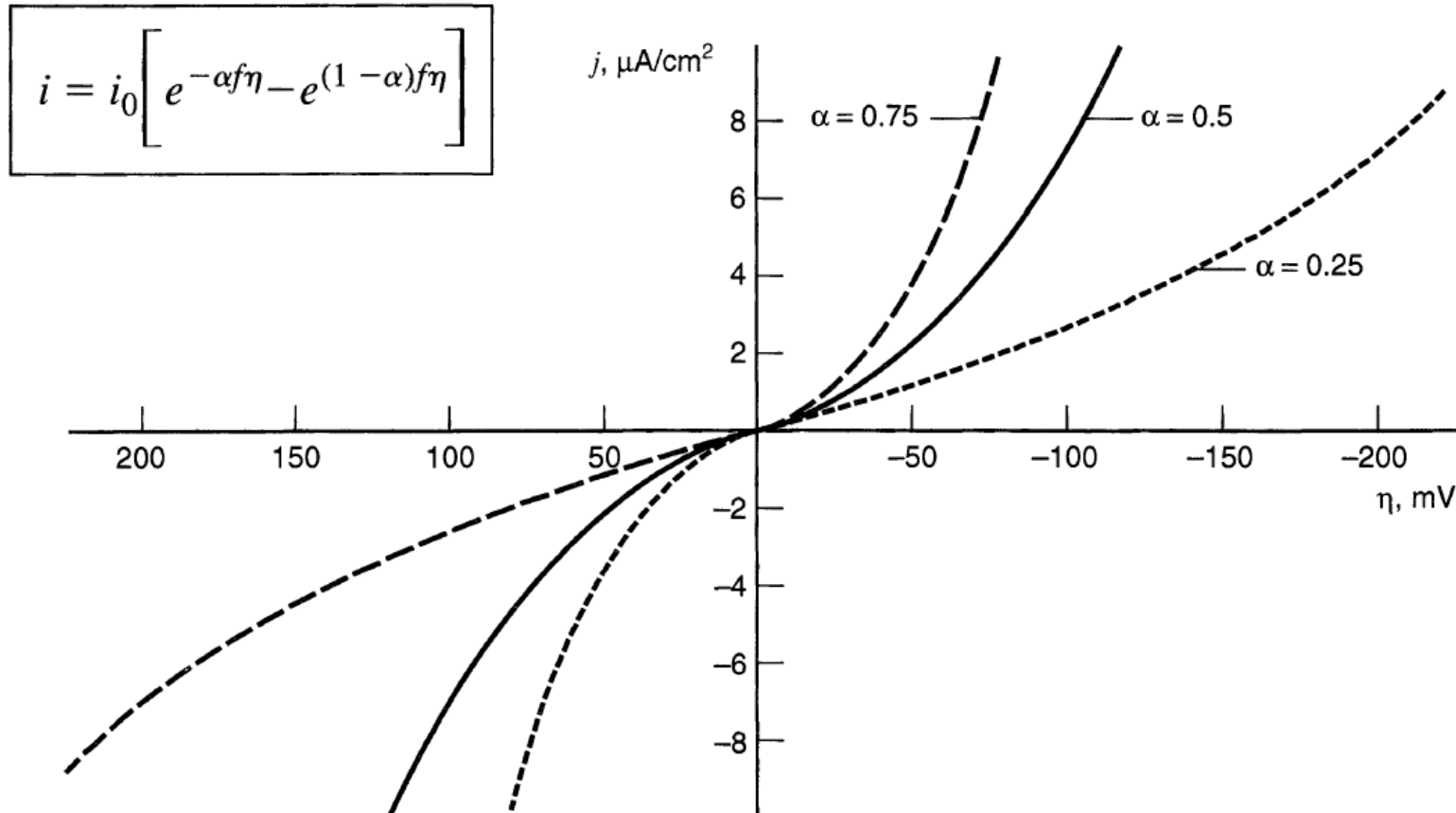
- Effect of exchange current density on the current-overpotential profile



**Figure 3.4.2** Effect of exchange current density on the activation overpotential required to deliver net current densities. (a)  $j_0 = 10^{-3} \text{ A}/\text{cm}^2$  (curve is indistinguishable from the current axis), (b)  $j_0 = 10^{-6} \text{ A}/\text{cm}^2$ , (c)  $j_0 = 10^{-9} \text{ A}/\text{cm}^2$ . For all cases the reaction is  $\text{O} + e \rightleftharpoons \text{R}$  with  $\alpha = 0.5$  and  $T = 298 \text{ K}$ .

## 3.4 THE BUTLER-VOLMER MODEL

- Effect of the transfer coefficient on the current-overpotential profile



**Figure 3.4.3** Effect of the transfer coefficient on the symmetry of the current-overpotential curves for  $\text{O} + e \rightleftharpoons \text{R}$  with  $T = 298 \text{ K}$  and  $j_0 = 10^{-6} \text{ A}/\text{cm}^2$ .

## 3.4 THE BUTLER-VOLMER MODEL

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### (b) Linear Characteristic at Small $\eta$

- For small values of  $x$ ,  
→ the exponential  $e^x$  can be approximated as  $1 + x$   
→ For sufficiently small  $\eta$

$$i = i_0 \left[ e^{-\alpha f \eta} - e^{(1-\alpha) f \eta} \right]$$



$$i = i_0 [1 - \alpha f \eta - \{1 + (1 - \alpha) f \eta\}]$$



$$i = -i_0 f \eta$$

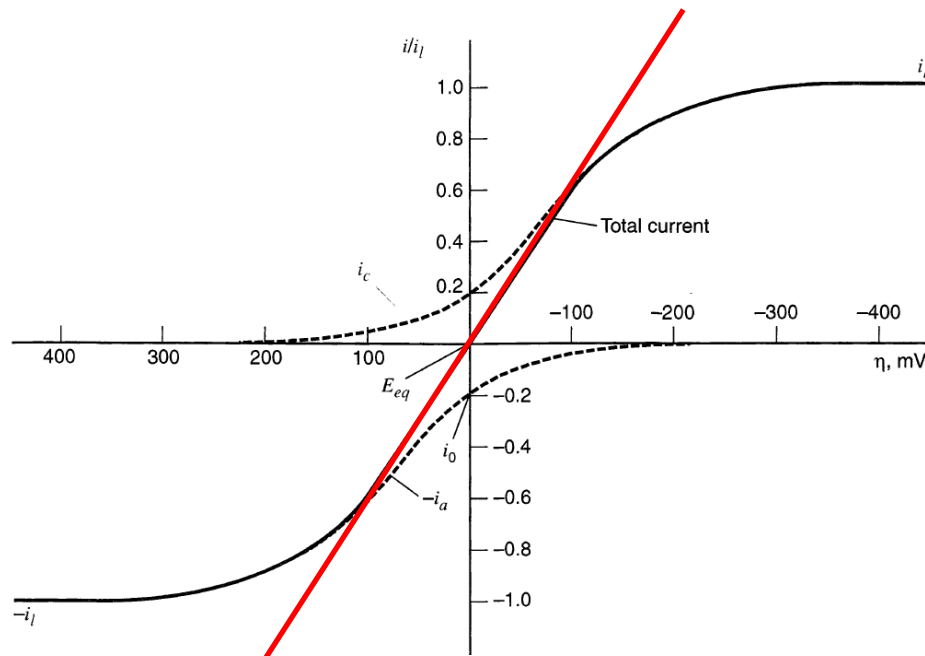
→ The net current is **linearly related** to overpotential in a narrow potential range near  $E_{eq}$ .

### 3.4 THE BUTLER-VOLMER MODEL

$$i = -i_0 f \eta$$

→ The ratio  $-\eta/i$  has units of resistance  
 : called the **charge-transfer resistance**,  $R_{ct}$

$$R_{ct} = \frac{RT}{Fi_0}$$



**Figure 3.4.1** Current-overpotential curves for the system  $O + e \rightleftharpoons R$  with  $\alpha = 0.5$ ,  $T = 298$  K,  $i_{l,c} = -i_{l,a} = i_l$  and  $i_0/i_l = 0.2$ . The dashed lines show the component currents  $i_c$  and  $i_a$ .

→ the **negative reciprocal slope** of the  $i$ - $\eta$  curve where that curve passes through the origin ( $i = 0$ ,  $\eta = 0$ )



## 3.4 THE BUTLER-VOLMER MODEL

### (c) Tafel Behavior at Large $\eta$

- For large values of  $\eta$  (either negative or positive), one of the bracketed terms in the  $i - \eta$  equation becomes negligible.

$$i = i_0 \left[ e^{-\alpha f \eta} - e^{(1-\alpha) f \eta} \right]$$

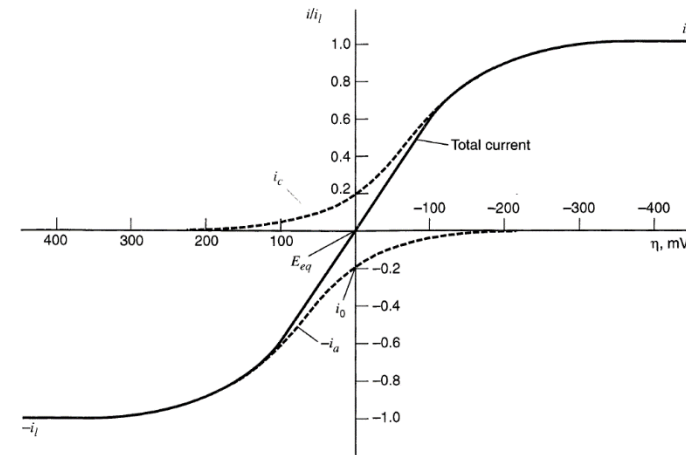
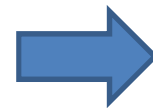


Figure 3.4.1 Current-overpotential curves for the system  $O + e \rightleftharpoons R$  with  $\alpha = 0.5$ ,  $T = 298$  K,  $i_{l,c} = -i_{l,a} = i_l$  and  $i_0/i_l = 0.2$ . The dashed lines show the component currents  $i_c$  and  $i_a$ .

- At large negative overpotentials,  $\exp(-\alpha f \eta) \gg \exp[(1 - \alpha) f \eta]$

$$i = i_0 \left[ e^{-\alpha f \eta} - e^{(1-\alpha) f \eta} \right]$$



$$i = i_0 e^{-\alpha f \eta}$$

$$\eta = \frac{RT}{\alpha F} \ln i_0 - \frac{RT}{\alpha F} \ln i$$

: the Tafel equation

## 3.4 THE BUTLER-VOLMER MODEL

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- The Tafel equation can be expected to hold whenever the backward reaction contributes **less than 1%** of the forward current (or vice versa)

→

$$\frac{e^{(1-\alpha)f\eta}}{e^{-\alpha f\eta}} = e^{f\eta} \leq 0.01$$

: implies that  $|\eta| > 118 \text{ mV}$  at 25°C