

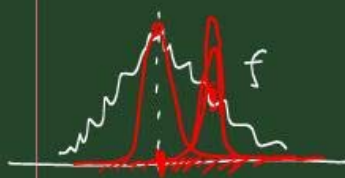
① Filtering

- is an operation which damps out all the spatial fluctuations of flow variables smaller than a prescribed length scale (filter width)

$$\bar{f}(\underline{x}) = \int f(\underline{x}') \bar{G}(\underline{x}, \underline{x}') d\underline{x}' \xrightarrow{FT} \hat{\bar{f}}(k) = \hat{f}(k) \hat{G}(k)$$

A diagram illustrating the filtering process. On the left, a jagged, noisy signal is labeled $f(x)$. An arrow labeled \bar{G} points to the right, where a smooth, bell-shaped curve is labeled $\bar{f}(x)$.


✓ Gaussian filter: $\bar{G}(x_i - x'_i) = \left(\frac{6}{\pi \Delta^2}\right)^{\frac{1}{2}} \exp\left(-\frac{6(x_i - x'_i)^2}{\Delta^2}\right)$



$$\hat{G}(k) = e^{-\frac{k^2 \Delta^2}{24}}$$

Δ : filter width (\approx grid size)

\vee (Sharp) cut-off filter : $\bar{G}(x_i - x'_i) = \frac{\text{sim}[\pi(x_i - x'_i)/\Delta]}{\pi(x_i - x'_i)}$

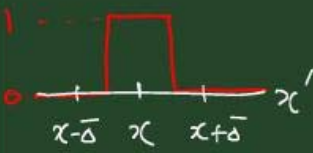


$\hat{G}(k) = \begin{cases} 1 & \text{for } k \leq k_c = \pi/\Delta \\ 0 & \text{for } k > k_c \end{cases}$

$f(x) \xrightarrow{\text{FT}} \hat{f}(k) \rightarrow \hat{f}(k) \hat{G}(k) \xrightarrow{\text{IFT}} \bar{f}(x)$


cut-off filter is used for spectral method.

\vee Box filter : $\bar{G}(x_i - x'_i) = \begin{cases} 1 & \text{for } x_i - \frac{\Delta}{2} \leq x'_i \leq x_i + \frac{\Delta}{2} \\ 0 & \text{otherwise} \end{cases}$



$\hat{G}(k) = \frac{\text{sim}(\frac{1}{2}k\Delta)}{\frac{1}{2}k\Delta}$

appropriate for FDM or FVM or FEM



- Filtering the Navier-Stokes equation

$$\frac{\partial u_i}{\partial x_i} = 0 \Rightarrow \int \cdot \bar{G} d\mathbf{x}' \quad \int \frac{\partial u_i}{\partial x_i} \cdot \bar{G} d\mathbf{x}' = \frac{\partial}{\partial x_i} \int u_i \bar{G} d\mathbf{x}' = \frac{\partial}{\partial x_i} \bar{u}_i$$

$\rightarrow \frac{\partial \bar{u}_i}{\partial x_i} = 0$

$$\int \left(\frac{\partial u_i}{\partial t} + \frac{\partial}{\partial x_j} u_i u_j - \frac{\partial p}{\partial x_i} + \frac{1}{\text{Re}} \frac{\partial}{\partial x_j} \frac{\partial u_i}{\partial x_j} \right) \cdot \bar{G} d\mathbf{x}'$$

$\rightarrow \frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j} \overline{u_i u_j} = -\frac{\partial \bar{p}}{\partial x_i} + \frac{1}{\text{Re}} \frac{\partial}{\partial x_j} \frac{\partial \bar{u}_i}{\partial x_j}$

$$\overline{u_i u_j} = \overline{u_i} \overline{u_j} + \underbrace{(\overline{u_i u_j} - \overline{u_i} \overline{u_j})}_{\tau_{ij}}$$

$\overline{u_i}$
 $\overline{u_j}$

$$\rightarrow \frac{\partial \overline{u_i}}{\partial t} + \frac{\partial \overline{u_i u_j}}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{1}{Re} \nabla^2 \overline{u_i} - \frac{\partial \tau_{ij}}{\partial x_j}$$

$\overline{u_i u_j}$
 $\overline{u_i} \overline{u_j}$

$\tau_{ij} = \overline{u_i u_j} - \overline{u_i} \overline{u_j} \Leftarrow$ must be modelled.

- Smagorinsky eddy viscosity model (1963)
 - isotropic turbulence

$$\tau_{ij} - \frac{1}{3} \delta_{ij} \tau_{kk} = -2 (C_s \overline{\Delta})^2 |\overline{s}| \overline{s}_{ij}$$

$\overline{\Delta}$: filter width

where $\overline{s}_{ij} = \frac{1}{2} \left(\frac{\partial \overline{u_i}}{\partial x_j} + \frac{\partial \overline{u_j}}{\partial x_i} \right)$ and $|\overline{s}| = \sqrt{2 \overline{s}_{ij} \overline{s}_{ij}}$

$$\tau_{ij} - \frac{1}{3} \delta_{ij} \tau_{kk} = -2 \nu_T \overline{s}_{ij}, \quad \nu_T = (C_s \overline{\Delta})^2 |\overline{s}|$$

eddy viscosity

- ✓ $C_s = 0.17$: Smagorinsky constant
- 0.1 ~ 0.3 depending on the flow type
- ✓ Damping function is required near the wall

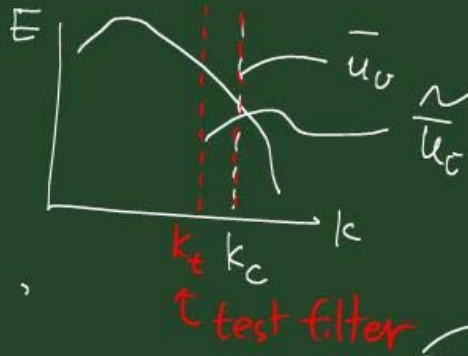
$$C_s \overline{\Delta} \rightarrow C_s \overline{\Delta} [1 - \exp(-y^+ / A^+)]$$

Kim & Moin (1982) : turb. channel flow

prob: C_s ?

• Dynamic subgrid-scale model (Germano et al. 1991)

use two filters



Apply two filters
to the N-S eqs,

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0$$

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j} (\bar{u}_i \bar{u}_j) = -\frac{\partial \bar{p}}{\partial x_i} + \frac{1}{Re} \nabla^2 \bar{u}_i - \frac{\partial \tau_{ij}}{\partial x_j}$$

where $\tau_{ij} = \overline{u_i u_j} - \bar{u}_i \bar{u}_j$.

Let $L_{ij} = \overline{u_i u_j} - \bar{u}_i \bar{u}_j$: computable

$$\tau_{ij} = \overline{u_i u_j} - \bar{u}_i \bar{u}_j$$

$$\tilde{\tau}_{ij} = \overline{\tilde{u}_i \tilde{u}_j} - \tilde{u}_i \tilde{u}_j$$

① $L_{ij} = \tau_{ij} - \tilde{\tau}_{ij}$: Germano identity

Modelling : $\tau_{ij} - \frac{1}{3} \delta_{ij} \tau_{kk} = -2c \frac{\Delta^2}{\Delta} |\bar{s}| \bar{s}_{ij}$ ②

$$\tilde{\tau}_{ij} - \frac{1}{3} \delta_{ij} \tilde{\tau}_{kk} = -2c \frac{\tilde{\Delta}^2}{\tilde{\Delta}} |\tilde{s}| \tilde{s}_{ij}$$
 ③

②, ③ → ①

$$L_{ij} - \frac{1}{3} \delta_{ij} L_{kk} = -2c \frac{\tilde{\Delta}^2}{\tilde{\Delta}} |\tilde{s}| \tilde{s}_{ij} + 2c \frac{\Delta^2}{\Delta} |\bar{s}| \bar{s}_{ij}$$

Lilly (1992)

$$\tau_{ij} \approx -2C \left[\frac{\tilde{u}^2 \tilde{u}}{\Delta |S|} \tilde{S}_{ij} - \overline{\frac{\tilde{u}^2 |S| S_{ij}}{\Delta |S|}} \right]$$

Least square error

$$Q = \left(L_{ij} - \frac{1}{3} \delta_{ij} L_{kk} + 2C M_{ij} \right)^2$$



$$\frac{\partial Q}{\partial C} = 0 \rightarrow$$

$$C = -\frac{1}{2} \frac{L_{ij} M_{ij}}{M_{ij} M_{ij}} \quad (x, y, z, t)$$

probs: C can be negative \rightarrow computation blows up
 \rightarrow requires averaging over homogeneous direction(s) and/or ad hoc clipping.

$$C = -\frac{1}{2} \frac{\langle L_{ij} M_{ij} \rangle_n}{\langle M_{ij} M_{ij} \rangle_n}$$

\rightarrow hinders application of dynamic model to complex geometries.

Alternative SGS models for flows in complex geometry

Ghosal et al. (1995) JFM

Meneveau et al. (1996) JFM/PoF

\rightarrow Park et al. (2006) PoF

Vreman model (2004; PoF) — Smagorinsky model

$\tau_{ij} = 0$ for simple laminar shear flow.

$\tau_{ij} \neq 0$ even for laminar shear flow.

