



**457.562 Special Issue on
River Mechanics
(Sediment Transport)
.08 Mechanics of Bedload Transport**



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1. Equations of particle motion

- We already learned the appropriate equations governing particle motion in the previous class
- For simplicity, the z-coordinate is taken to be approximately upward vertical. Variation in the n-coordinate is taken to be negligible. The mean near-bed flow field is

$$\bar{u}(s, n, z, t) = 2.5u_* \ln\left(30 \frac{z}{k_s}\right)$$

$$\bar{v}(s, n, z, t) = \bar{w}(s, n, z, t) = 0$$



1. Equations of particle motion

- Getting back to the old equations of particle

$$(\rho_s + c_m \rho) V_p \frac{du_p}{dt} = -\frac{1}{2} \rho c_D A_p |u_r| (u_p - u_f) + \rho (1 + c_m) V_p \frac{du_f}{dt}$$

$$(\rho_s + c_m \rho) V_p \frac{dw_p}{dt} = -\frac{1}{2} \rho c_D A_p |u_r| w_p - (\rho_s - \rho) g V_p + \frac{1}{2} \rho c_L A_p (u_{rT}^2 - u_{rB}^2)$$

- In the previous relations

$$u_f(t) = \bar{u}(s_p(t), n_p(t), z_p(t), t) = 2.5 u_* \ln \left(30 \frac{z}{k_s} \right)$$

- denotes the fluid velocity extrapolated to the particle centroid, and $|u_r|$ denotes the magnitude of the particle velocity relative to the fluid
- $$|u_r|^2 = (u_p - u_f)^2 + w_p^2$$



1. Equations of particle motion

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$$(\rho_s + c_m \rho) V_p \frac{dw_p}{dt} = -\frac{1}{2} \rho c_D A_p |u_r| w_p - (\rho_s - \rho) g V_p + \frac{1}{2} \rho c_L A_p (u_{rT}^2 - u_{rB}^2)$$

u_{rT} and u_{rB} represent the magnitude of the relative particle velocity at the top and bottom

$$u_{rT}^2 = (u_p - u_{fT})^2 + w_p^2 \quad u_{rB}^2 = (u_p - u_{fB})^2 + w_p^2$$

- Where

$$u_{fT} = 2.5 u_* \ln \left(30 \frac{z_p + 1/2D}{k_s} \right); \quad u_{fB} = 2.5 u_* \ln \left(30 \frac{z_p - 1/2D}{k_s} \right)$$



1. Equations of particle motion

- Remember, in the previous relations

$$u_f(t) = \bar{u}(s_p(t), n_p(t), z_p(t), t) = 2.5u_* \ln\left(30 \frac{z}{k_s}\right)$$

- In streamwise directional equation, there is the fluid acceleration term and this must be evaluated following particle (Lagrangian),

$$\frac{du_f}{dt} = \frac{\partial u_f}{\partial t} + u_p \frac{du_f}{ds_p} + w_p \frac{du_f}{dz_p} = 2.5w_p \frac{u_*}{z_p}$$

$$\left(\text{differentiate } \ln\left(30 \frac{z_p(t)}{k_s}\right) = w_p \frac{1}{z_p} \right)$$

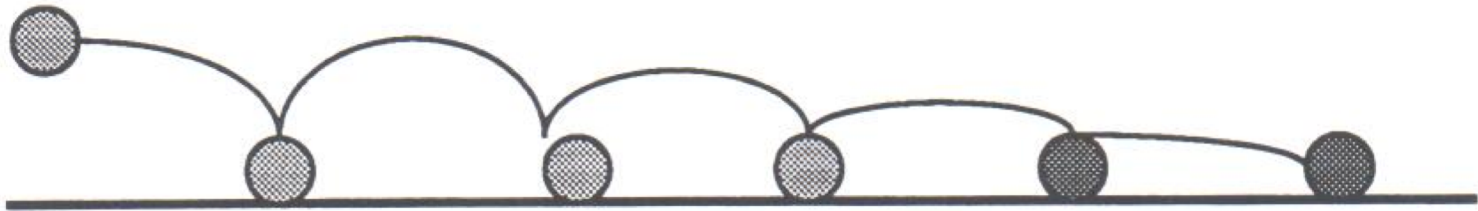


2. Collision at the bed: Splash function

- As will be found in the homework assignment, the effect of lift and fluid acceleration in momentum equations can often be neglected in a consideration of the motion of saltating bedload particles.
- If this is taken to be the case, it is clear that there is no upward force in vertical direction momentum equation acting on the particle during its entire saltation trajectory.
- Since collisions with the bed can be expected to be only partially elastic ($e < 1$), the particle will rebound from the bed with less energy and thus momentum, than it collided.
- A particle would saltate with progressively lower height, until the trajectory devolved into a rolling or sliding motions.



2. Collision at the bed: Splash function

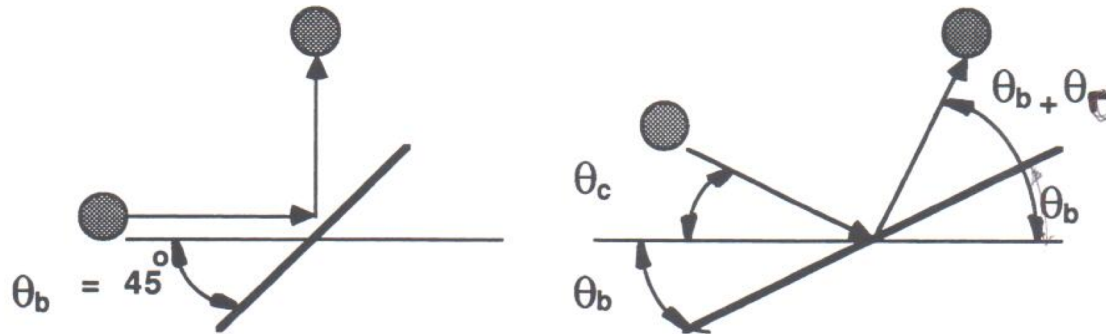


- This devolution does indeed occur when particles saltate over a ***smooth bed***. The key to maintenance of a stable saltation path is ***bed roughness***.
- In order to see this, it is useful to start with a simple model, in which a particle collides at angle θ_c to the horizontal against a surface that is always facing an angle θ_b in the upstream direction to the horizontal



2. Collision at the bed: Splash function

- For example $\theta_c = 0$ and $\theta_b = 45^\circ$. In this case, the incoming forward momentum of the particle is converted solely into upward normal momentum,



- It is seen that collision against an upward-facing surface can provide a mechanism to convert forward momentum to upward vertical momentum.
- The forward momentum lost in the collision is replaced as the particle rebounds upward into the flow; fluid drag again accelerates the particle downstream.



2. Collision at the bed: Splash function

- This model can be generalized.

$$u_{pT}|_{in} = \left(u_p^2 + w_p^2 \right)_{in}^{1/2} \cos(\theta_c + \theta_b)$$

$$u_{pN}|_{in} = - \left(u_p^2 + w_p^2 \right)_{in}^{1/2} \sin(\theta_c + \theta_b)$$

- As in the previous class,

$$u_{pT}|_{out} = u_{pT}|_{in}; \quad u_{pN}|_{out} = -e \cdot u_{pN}|_{in}$$

- It follows from the above relations that the angle of rebound between the particle path and the bed surface is given by θ_r , where

$$\tan(\theta_r) = \frac{u_{pN}|_{out}}{u_{pT}|_{out}} = \frac{e \cdot u_{pN}|_{in}}{u_{pT}|_{in}} = e \cdot \tan(\theta_b + \theta_c)$$



2. Collision at the bed: Splash function

- The values of out bound velocities are

$$u_p \Big|_{out} = \left(u_{pT}^2 + u_{pN}^2 \right)_{out}^{1/2} \cos(\theta_b + \theta_r)$$

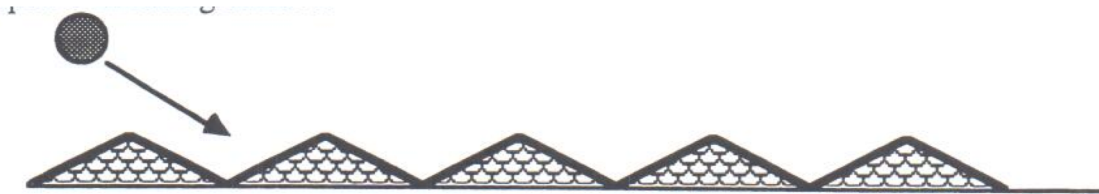
$$w_p \Big|_{out} = \left(u_{pT}^2 + u_{pN}^2 \right)_{out}^{1/2} \sin(\theta_b + \theta_r)$$

- Basic picture of the mechanics of saltation
 - The streamwise fluid drag force provides the source of particle momentum.
 - Gravity pulls the particle toward the bed, causing collision.
 - Particle energy is lost due to the collision
 - Forward momentum is partially converted to upward normal momentum
 - The energy lost in the collision is then replaced by the work of the fluid drag force as the particle rebounds in to the high-velocity

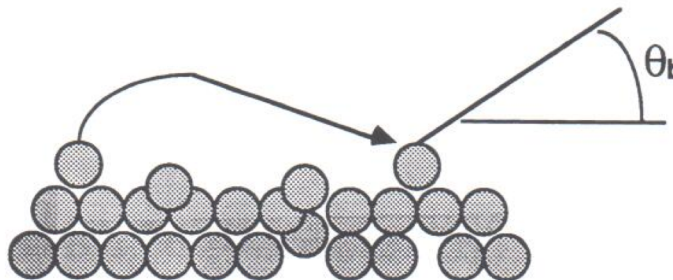


2. Collision at the bed: Splash function

- The limitation of the simplified model
 - Not true that a particle collides with an upstream-facing surface, even if upstream- and downstream-facing surfaces are equally distributed in space, a particle striking the bed obliquely is far more likely to strike an upstream-facing surface



- Angle probability distribution of upstream-facing surfaces. Since the bed is distributed randomly.





2. Collision at the bed: Splash function

- In a full model of saltation, the probability distribution of bed angle (the ***splash function***) must be specified.
- The previous many researches showed that particle preferentially strike upward-facing surfaces.
- In any actual computation of saltation, then it is necessary to include both a deterministic element (particle trajectory) and a stochastic element (collision and splash). Even at “equilibrium” conditions, each saltation differs from every other due to this random element; the equilibrium is defined in terms of an average over many saltations.



3. Results of Sample Numerical Solution

- This may be helpful for your mini-project.
- In an actual calculation of saltation, the parameters c_m and e are normally set to constant values of each 0.5 and 0.6. The parameters c_D and c_L are specified as functions of particle Reynolds number

$$\frac{|u_r|D}{\nu} \quad \text{and} \quad k_s = a_k D \quad (a_k \text{ is one order number})$$

- Appropriate initial conditions are specified, the details are not too important since the asymptotic equilibrium state is not dependent of them.
- As shown in the project assignment, the final results can be expressed in dimensionless forms.



3. Results of Sample Numerical Solution

$$\bar{u}_p = \frac{1}{T_s} \int_0^{T_s} u_p(t) dt; \quad \bar{u}_f = \frac{1}{T_s} \int_0^{T_s} u_f(t) dt$$

(mean streamwise particle and fluid velocities, where T_s time duration)

- Ensemble averaging over many realization at equilibrium yields the following relationships;

$$\frac{\lambda_s}{D} = f_\lambda(\tau^*, R_{ep}, R); \quad \frac{u_* T_s}{D} = f_T(\tau^*, R_{ep}, R); \quad \frac{h_s}{D} = f_h(\tau^*, R_{ep}, R);$$

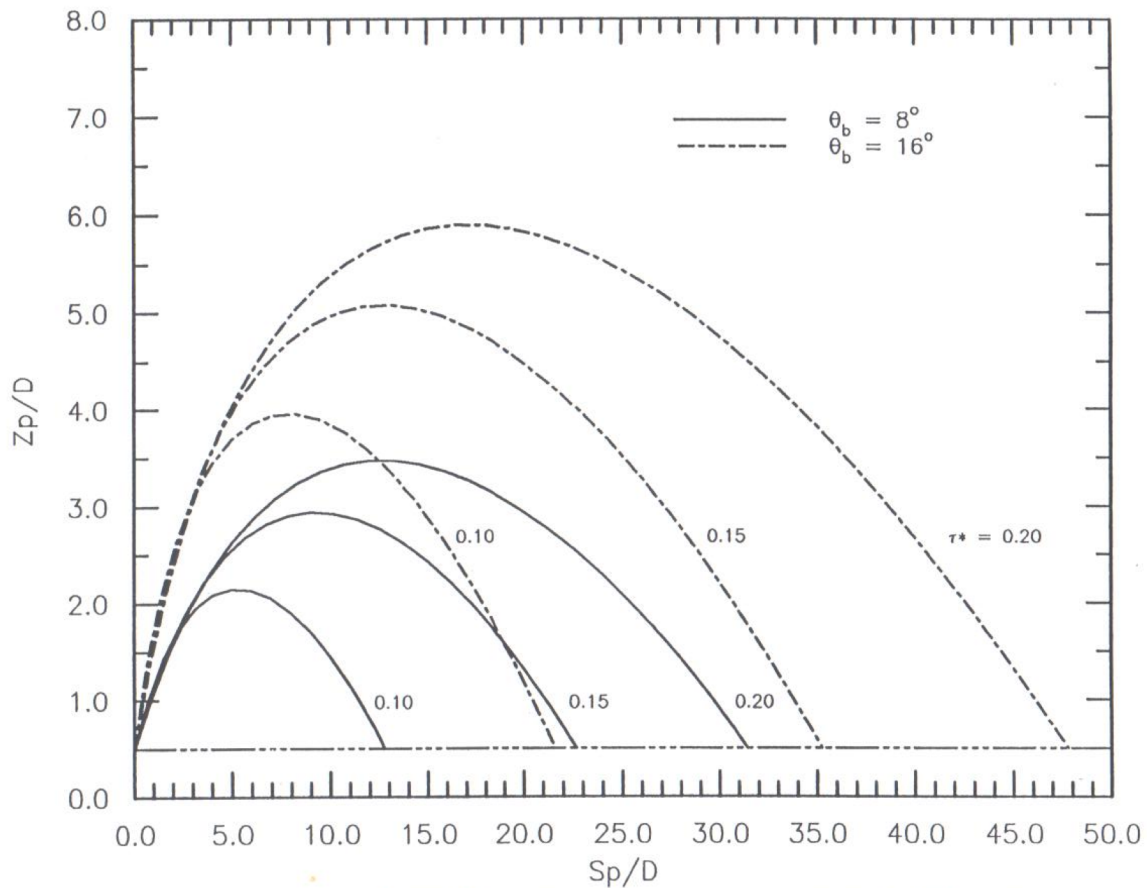
$$\frac{\bar{u}_p}{D} = f_p(\tau^*, R_{ep}, R); \quad \frac{\bar{u}_f}{D} = f_f(\tau^*, R_{ep}, R)$$

- Here $\tau^* = \frac{u_*^2}{RgD}$ (Shields stress), $R_{ep} = \frac{\sqrt{RgDD}}{\nu}$, $R = \left(\frac{\rho_s}{\rho} - 1 \right)$



Example

- The results show the following figure.





Example

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