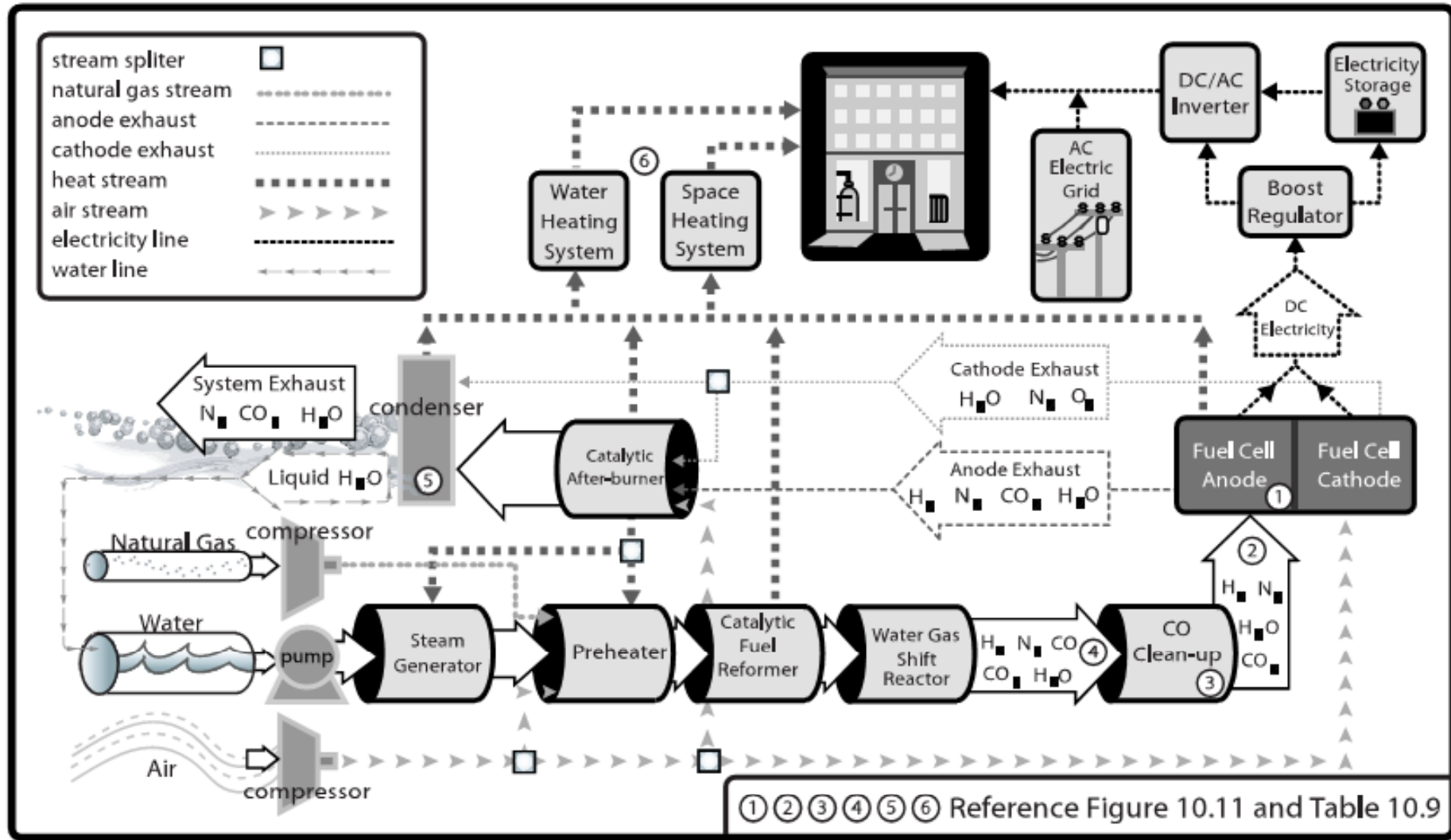


Fuel Cell System Integration & Sub-System Design

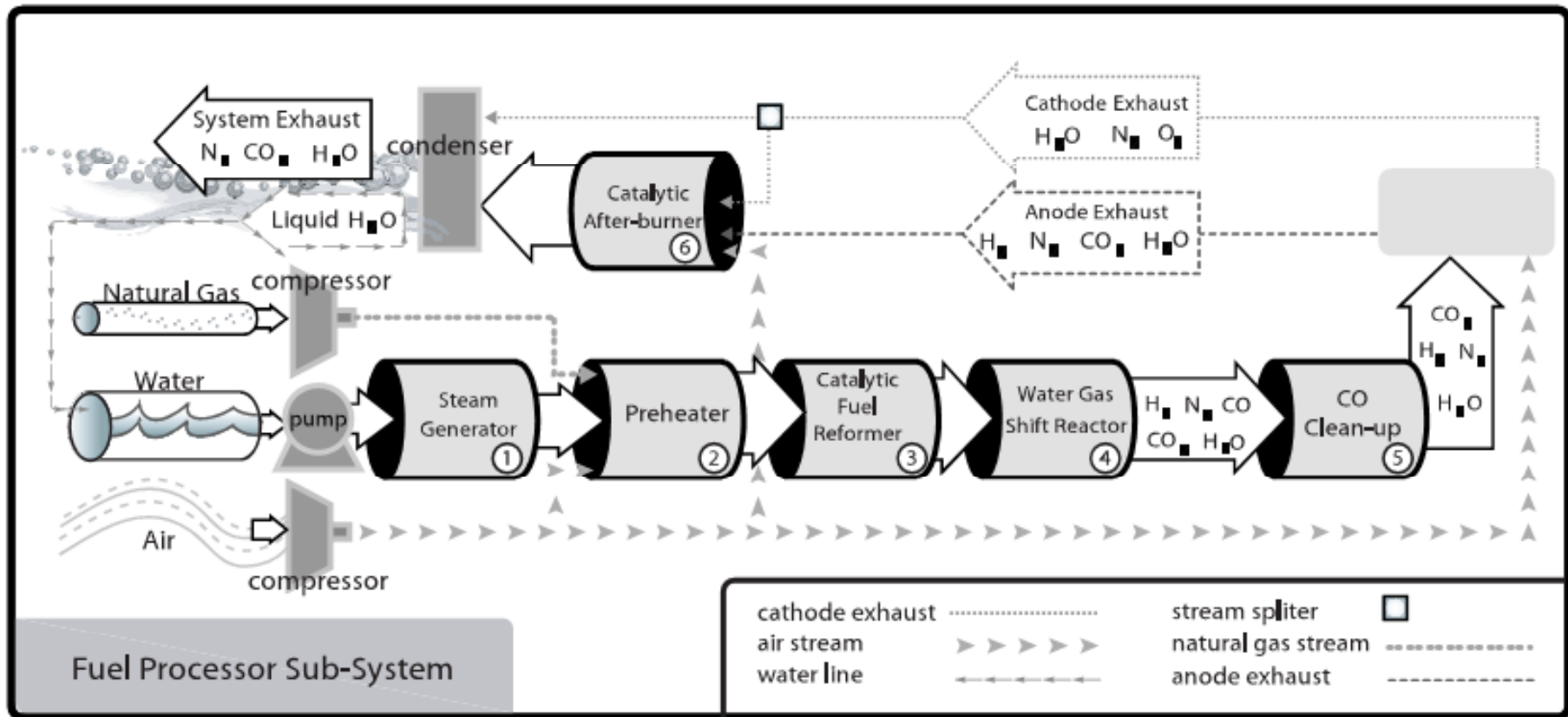
CHP Fuel Cell Systems

- Fuel processing sub-systems
- Fuel cell sub-systems
- Thermal management
- Power electronic sub-systems

CHP Fuel Cell Systems



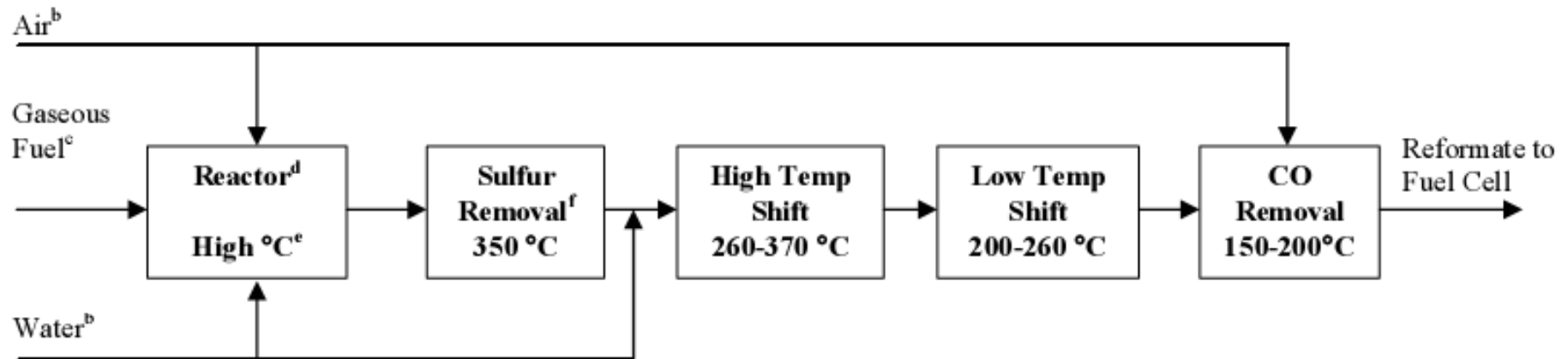
Fuel Processor Sub System



Fuel Processor Sub System

Natural Gas Fuel Composition (molar fraction)	
CH ₄	0.9674
C ₂ H ₆	0.0164
C ₃ H ₈	0.0019
C ₄ H ₁₀	0.0005
C ₅ H ₁₂	0.0002
O ₂	0
N ₂	0.0045
H ₂ O	0
CO	0
CO ₂	0.0091
H ₂	0

Fuel Processor Sub System



- a) - For MCFC & SOFC, no high temperature shift, low temperature shift, or CO removal required.
- For PAFC and circulating AFC, no CO removal required after low temperature shift.
- For PEFC, all components required except that for high temperature CO removal eliminated or reduced in complexity.
- b) Possible to use residual air, water, and heat of fuel effluent from fuel cell and other downstream components.
- c) Vaporizer required for liquid fuels.
- d) Non-catalytic POX fuel processor does not require water.
- e) Temperature dependent on fuel, sulfur content of fuel, and type of reactor.
- f) Can be located prior to, within, or after the reactor; liquid desulfurizer located prior to the vaporizer.

External Reforming

Three Primary Fuel Reforming Processes								
Type	Chemical Reaction	Temperature Range (°C)	Hydrogen Output Gas Composition (with Natural Gas Fuel)					Exothermic or Endothermic?
			H ₂	CO	CO ₂	N ₂	Other	
Steam Reforming	$C_xH_y + xH_2O_{(g)} \leftrightarrow xCO + (y/2 + x)H_2$ $\Rightarrow CO, CO_2, H_2, H_2O$	700-1000	76%	9%	15%	0%	trace NH ₃ CH ₄ SO _x	Endothermic
Partial Oxidation	$C_xH_y + x/2 O_2 \leftrightarrow xCO + y/2 H_2$	> 1000	41%	19%	1%	39%	some NH ₃ CH ₄ SO _x HC	Exothermic
Autothermal Reforming	$C_xH_y + zH_2O_{(g)} + (x - z/2)O_2 \leftrightarrow xCO_2 + (z + y/2)H_2$ $\Rightarrow CO, CO_2, H_2, H_2O$	600-900	47%	3%	15%	34%	trace NH ₃ CH ₄ SO _x HC	Neutral

External Reforming

Advantages and Disadvantages of Three Primary Fuel Reforming Types		
Type	Advantages	Disadvantages
Steam Reforming	1) highest H ₂ yield	1) requires careful thermal management to provide heat for the reaction, especially for a) start-up and b) dynamic response 2) only works on certain fuels
Partial Oxidation	1) quick to start and respond because reaction is exothermic 2) quick dynamic response 3) less careful thermal management required 4) works on many fuels	1) lowest H ₂ yield 2) highest pollutant emissions (HCs, CO)
Autothermal Reforming	1) simplification of thermal management by combining exothermic and endothermic reactions in same process 2) compact due to reduction in heat exchangers 3) quick to start	1) low H ₂ yield

Steam Reforming



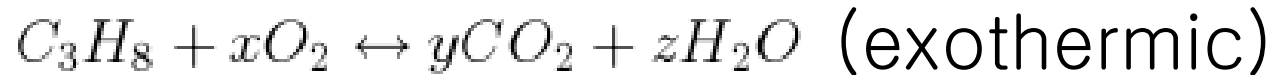
(endothermic)



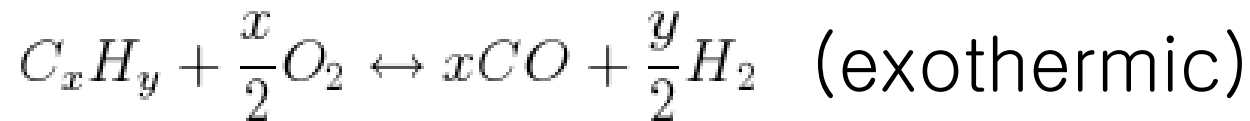
Steam Reforming Reactions			
#	Reaction Type	Stoichiometric Formula	ΔH_{rxn}° (kJ/mole)
1	Steam Reforming	$CH_4 + 2H_2O_{(g)} \rightarrow CO_2 + 4H_2$	+165.2
2	Water-Gas Shift Reaction	$CO + H_2O_{(g)} \rightarrow CO_2 + H_2$	-41.2
3	Evaporation	$H_2O_{(l)} \rightarrow H_2O_{(g)}$	+44.1

Partial Oxidation

- Complete oxidation (oxygen rich)

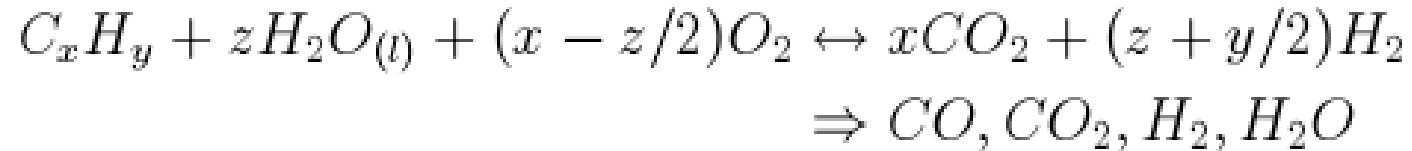


- Partial oxidation (fuel rich)



Partial Oxidation Reactions			
#	Reaction Type	Stoichiometric Formula	ΔH_{rxn}° (kJ/mole)
1	Partial Oxidation	$CH_4 + 1/2O_2 \rightarrow CO + 2H_2$	-35.7
2	Partial Oxidation	$CH_4 + O_2 \rightarrow CO_2 + 2H_2$	-319.1
3	Thermal Decomposition	$CH_4 \rightarrow C + 2H_2$	+75.0
4	Methane Combustion	$CH_4 + 2O_2 \rightarrow CO_2 + 2H_2O_{(g)}$	-803.5
5	CO Combustion	$CO + 1/2O_2 \rightarrow CO_2$	-283.4
6	Hydrogen Combustion	$H_2 + 1/2O_2 \rightarrow H_2O_{(g)}$	-242.2

Autothermal Reforming



- Neutral reaction by proper steam to carbon ratio (z/x)

Water Gas Shift Reactors



- High T

- Equilibrium shift to the reactant side

- Fast kinetics

- Low T

- Equilibrium shift to the product side

- Slow kinetics

- * 1st stage: High T => 2nd stage: Low T

Carbon Monoxide Clean-up

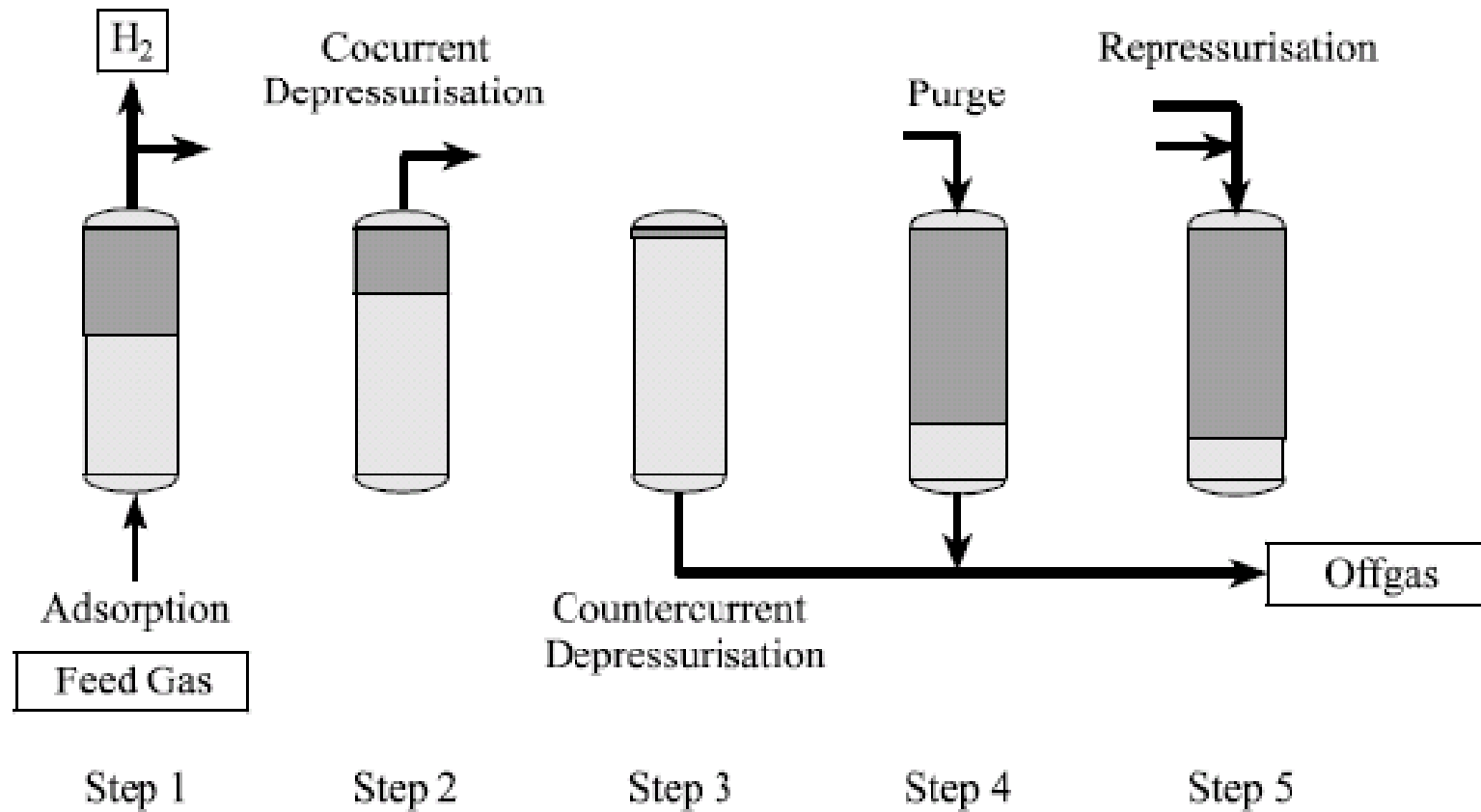
- Chemical reaction
 - Selective methanation of CO
 - Selective oxidation of CO
- Physical separation
 - Pressure-swing absorption
 - Membrane separation

Chemical Reaction

CO Clean-Up: Chemical Removal			Catalyst Promotes ✓ or Suppresses ✗ Reaction?
Type	Chemical Reaction	ΔH°_{rxn} (kJ/mole)	
1) Selective Methanation	$\text{CO} + 3\text{H}_2 \leftrightarrow \text{CH}_4 + \text{H}_2\text{O}$	-206.1	✓
	$\text{CO}_2 + 4\text{H}_2 \leftrightarrow \text{CH}_4 + 2\text{H}_2\text{O}$	-164.9	✗
2) Selective Oxidation	$\text{CO} + 0.5\text{O}_2 \leftrightarrow \text{CO}_2$	-285.0	✓
	$\text{H}_2 + 0.5\text{O}_2 \leftrightarrow \text{H}_2\text{O}$	-283.0	✗

- Low T preferred for selective
- Multi-stage catalyst bed in decreasing temperature

Pressure Swing Absorption



Membrane Separation

- Palladium

- Pressure difference

- Temperature

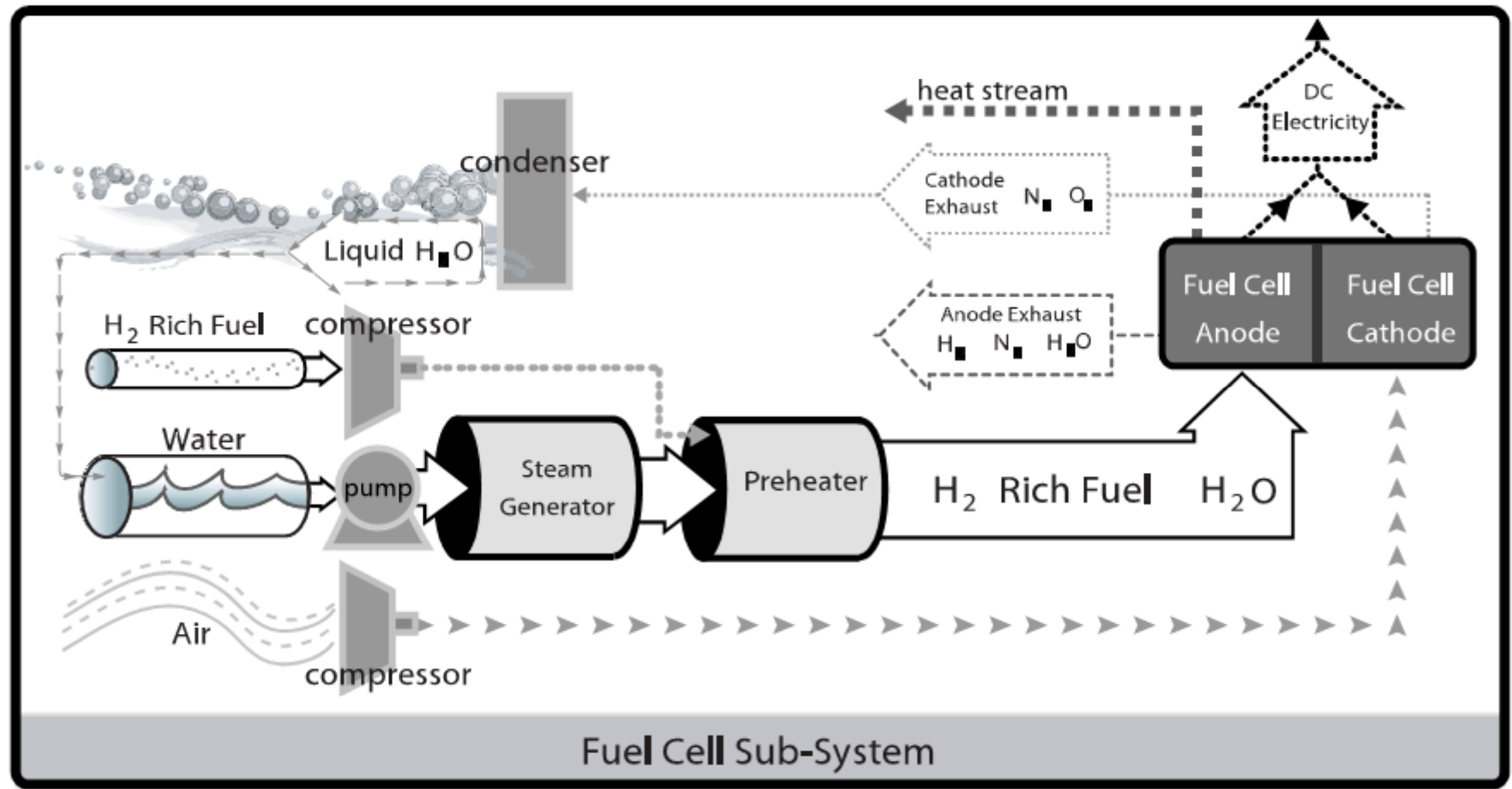
- Thickness

- Purging

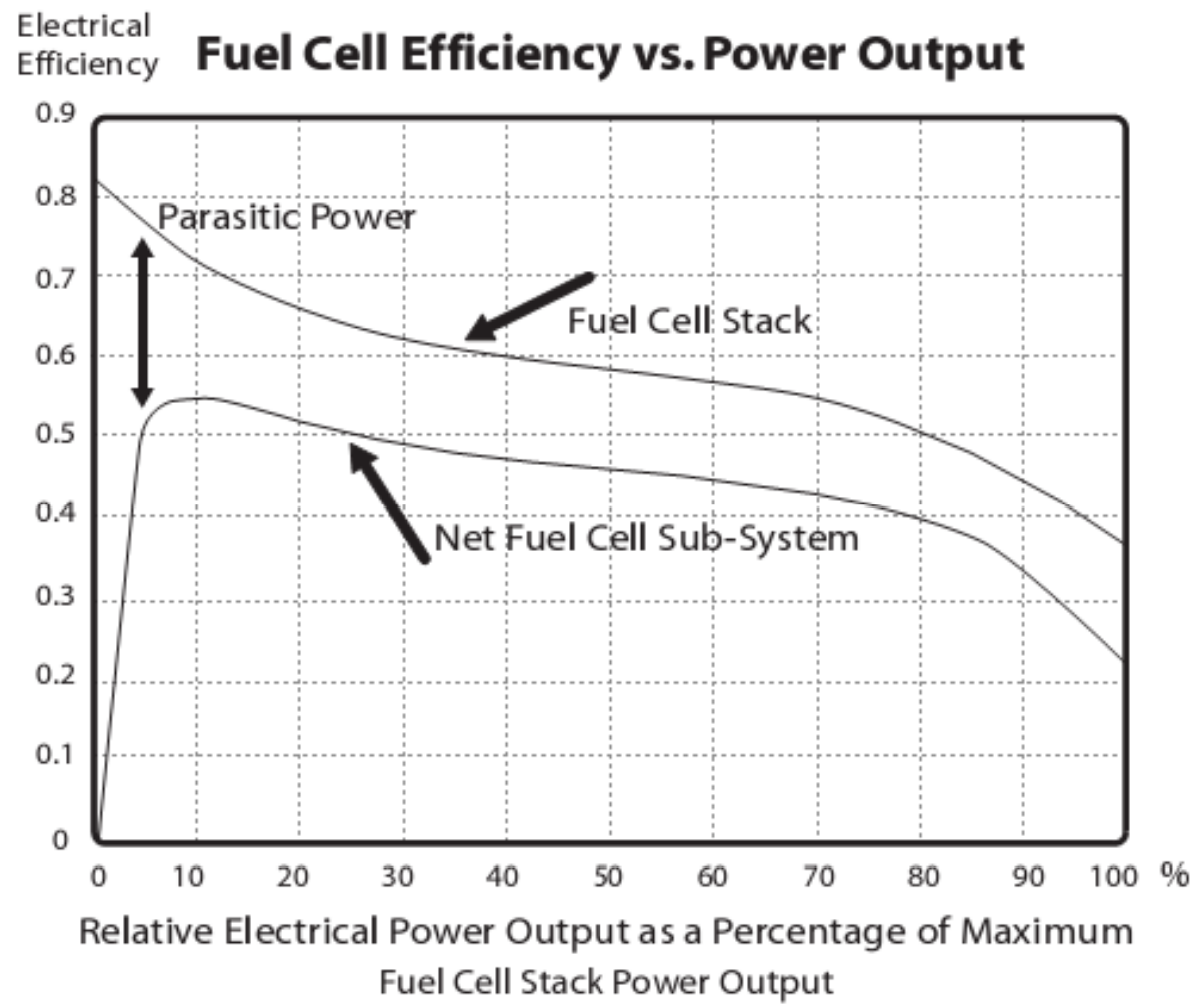
- Removes other gas near surface

- Pinhole leaks

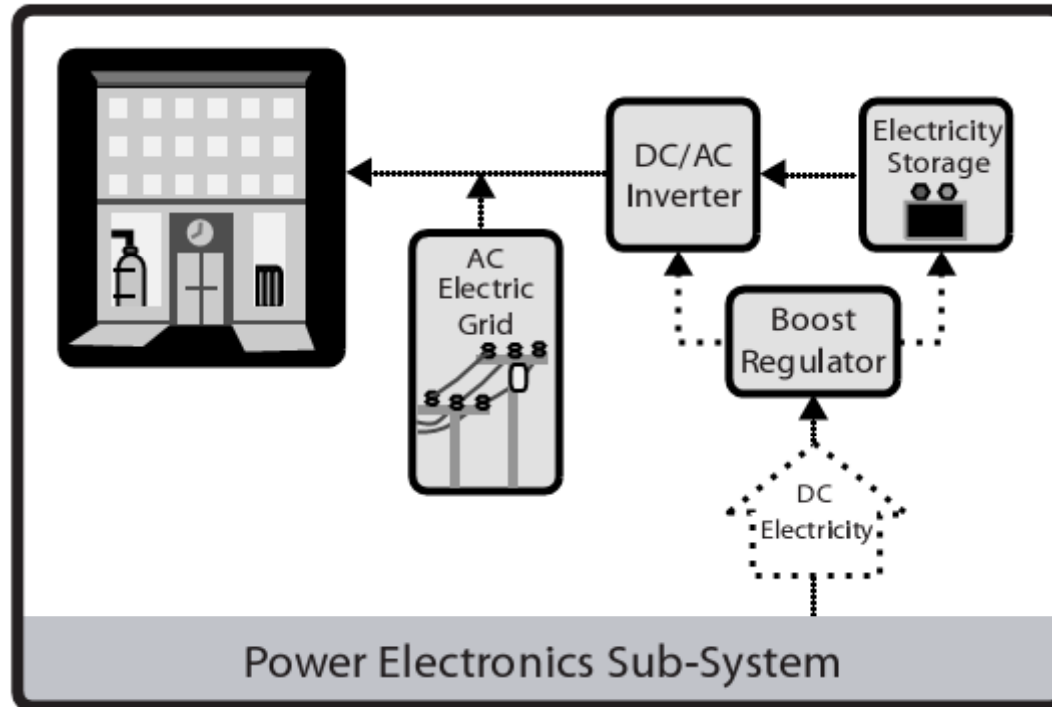
Fuel Cell Systems



Fuel Cell Systems

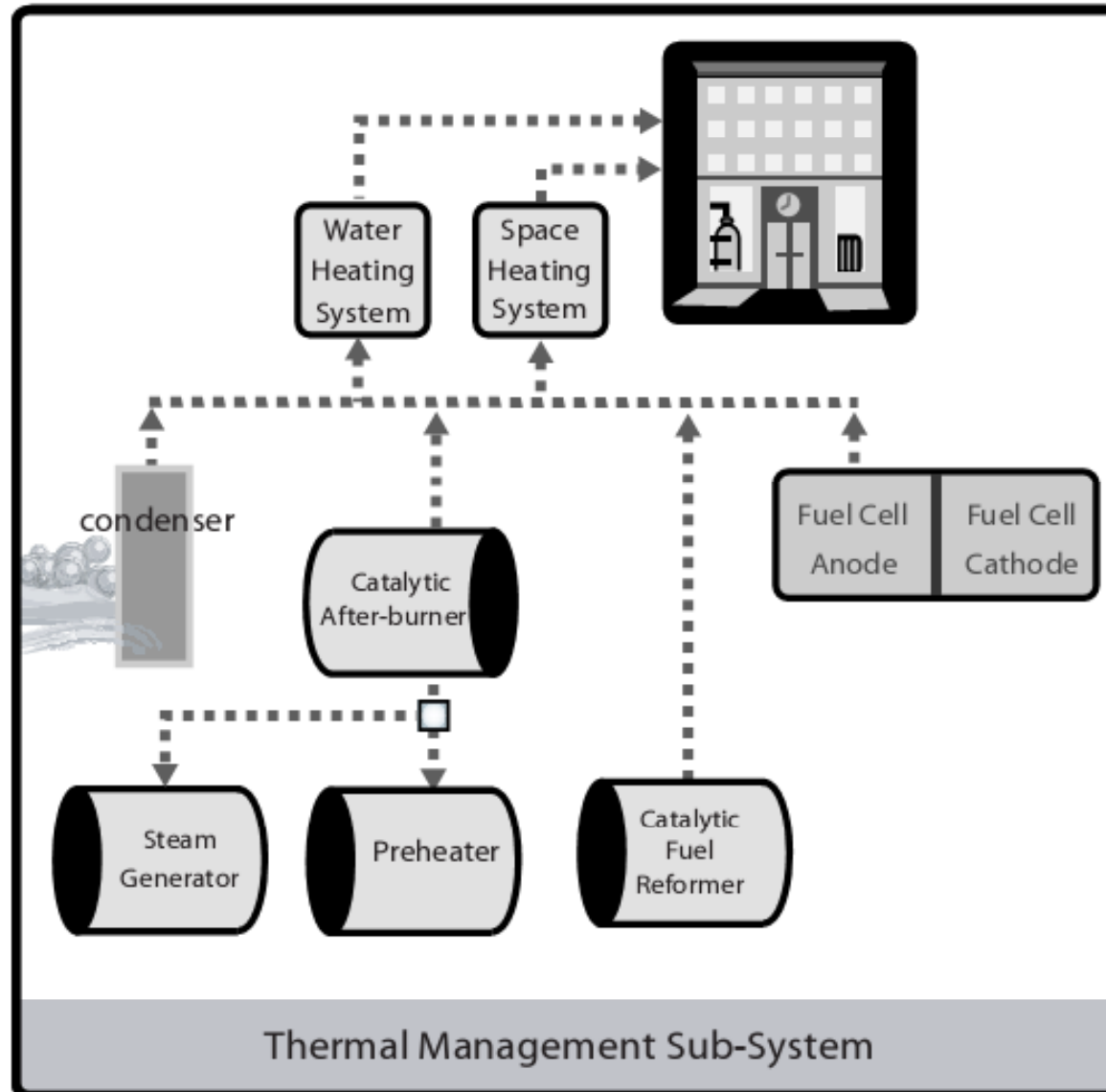


Power Electronics Sub-Systems

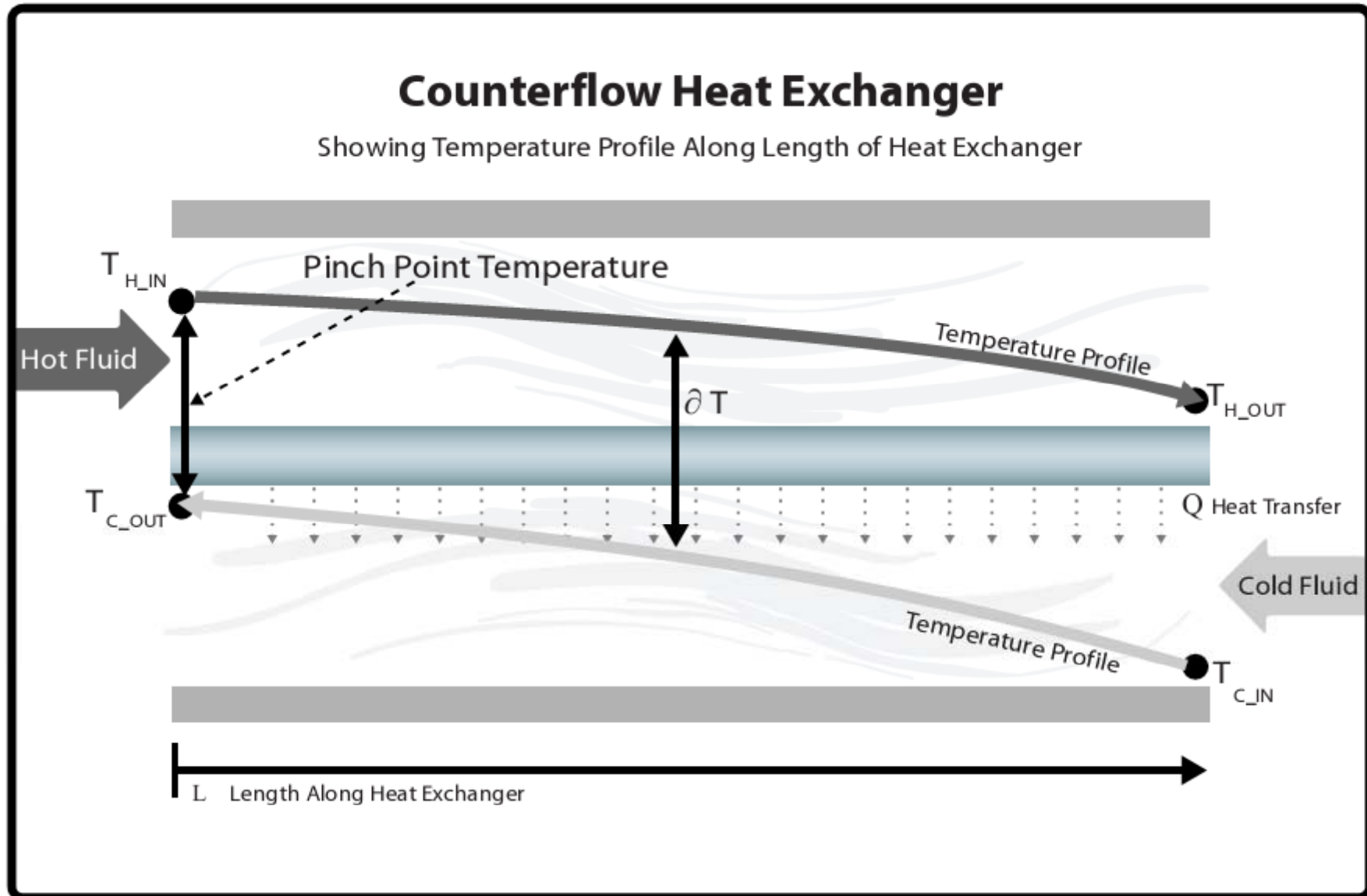


- Power conditioning
- Supply management

Thermal Management Sub-Systems



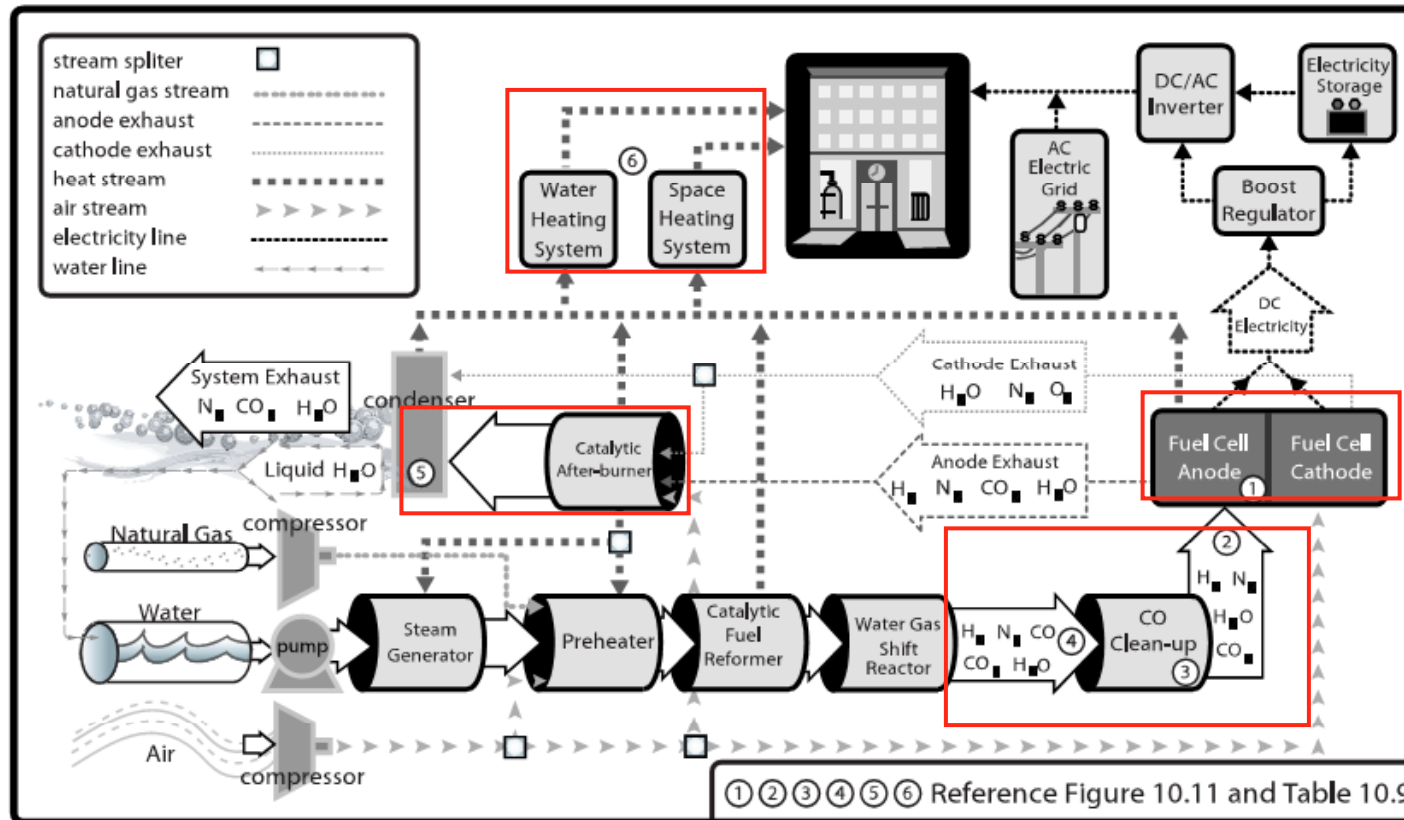
Heat Exchanger



Pinch Point Analysis

1. Identify hot and cold streams in the system
2. Determine thermal data for these streams.
3. Select a minimum acceptable temperature difference ($dT_{min,set}$) between hot and cold streams
4. Construct temperature vs. enthalpy diagrams and check $dT_{min} > dT_{min,set}$
5. If $dT_{min} < dT_{min,set}$, change heat exchanger orientation.
6. Conduct scenario analysis of heat exchanger orientation until $dT_{min} > dT_{min,set}$

Stream Identification



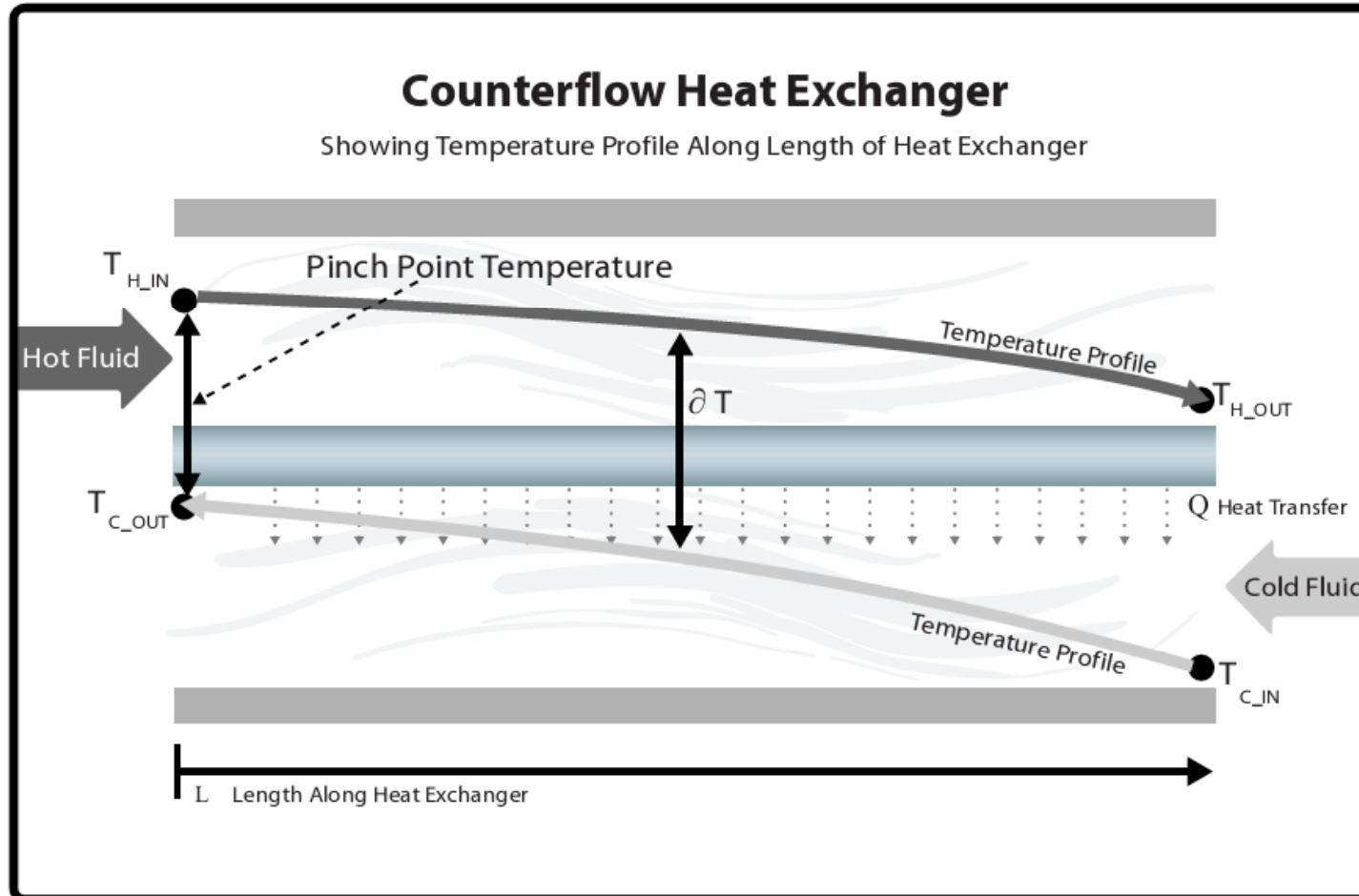
1. the hot reformat stream exiting the water gas shift reactor and eventually entering the fuel cell's anode (labeled No. 4 through to 2);
2. the cooling loop for the fuel cell stack (labeled No. 1), and
3. the hot anode and cathode exhaust stream exiting the afterburner and entering the condenser (labeled No. 5).

Thermal Data Determination

- The supply temperature (T_{in}), the initial temperature at which the stream is available before entering a heat exchanger;
- The target temperature (T_{out}), the desired outlet temperature for the stream upon exiting a heat exchanger;
- The heat capacity flow rate ($\dot{m}c_p$), the product of the stream's mass flow rate (\dot{m}) in kg/sec and the specific heat of the fluid in the stream (c_p) in $kJ/kg^\circ C$, whereby the specific heat of the stream is assumed constant over the temperature range;
- The change in enthalpy (dH) in the stream passing through the heat exchanger.

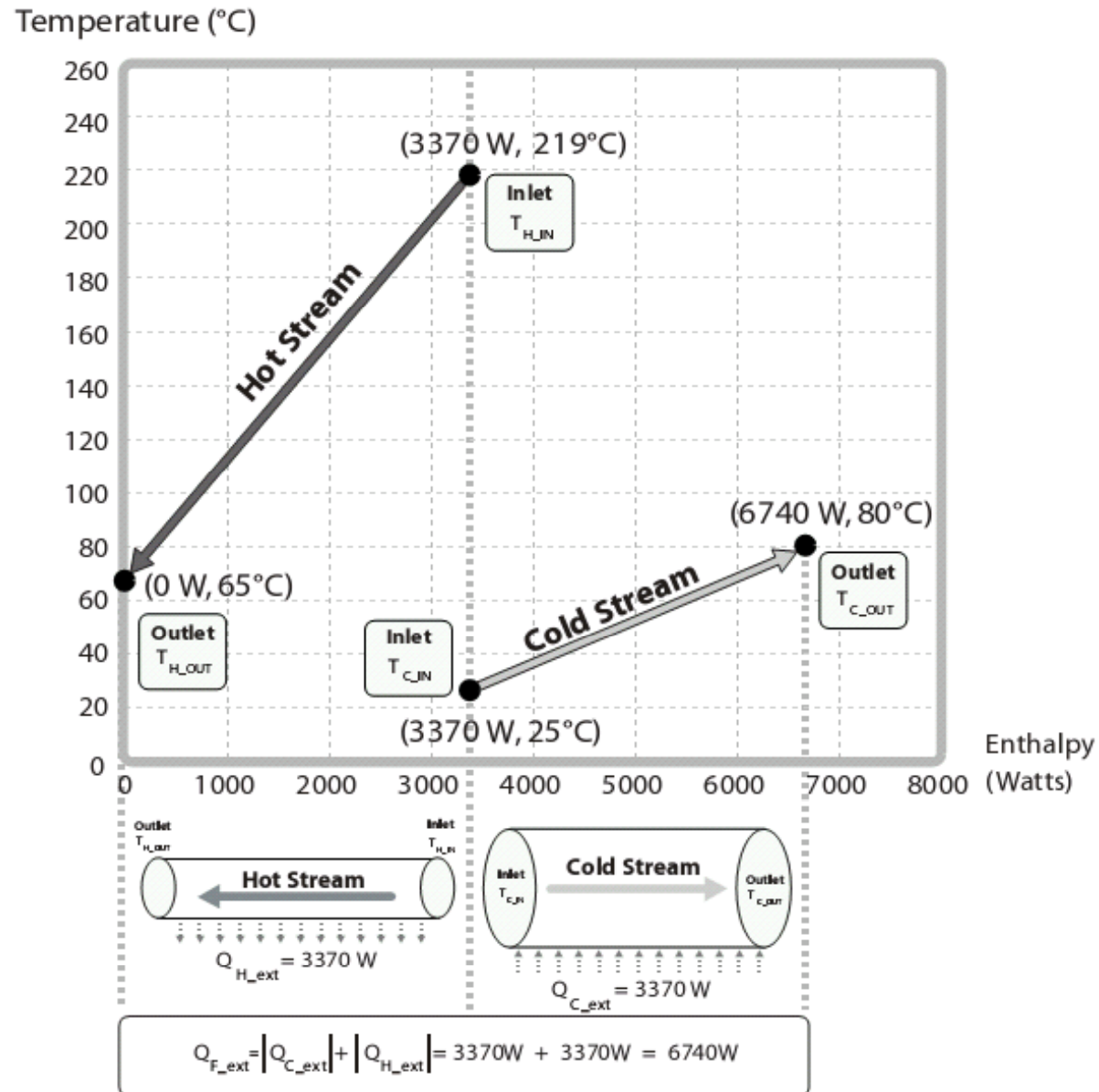
Stream Number <small>(Refers to Figure 10.1)</small>	Source of Heat or Cooling	Stream Description	Hot or Cold?	Supply Temperature, T_{in} ($^\circ C$)	Target Temperature, T_{out} ($^\circ C$)	Heat Flow Capacity, $\dot{m}c_p$ (W/K)	Heat Flow Q (watts)
①	Fuel Cell Stack	Heat extracted from fuel cell stack	Hot	70	60	276	2760
②	Aftercooler	Heat extracted from the reformat stream after the selective oxidation reactor	Hot	110	70		860
③	Selective Oxidation Reactor	Heat extracted from the reformat stream at the exothermic selective oxidation reactor	Hot	120	110	6	60
④	Post-Water Gas Shift Reactor	Heat extracted from the reformat stream after the shift reactor	Hot	260	120	6	840
⑤	Condenser	Heat extracted from condensing water from the anode and cathode exhaust	Hot	219	65		3370
⑥	Building Heat Loop	Domestic water cooling loop exchanging heat between fuel cell system and building	Cold	25	80	143	7890

Selection of $dT_{\min.set}$



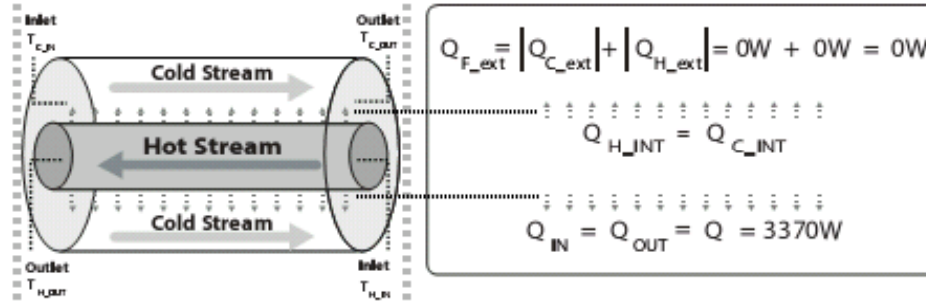
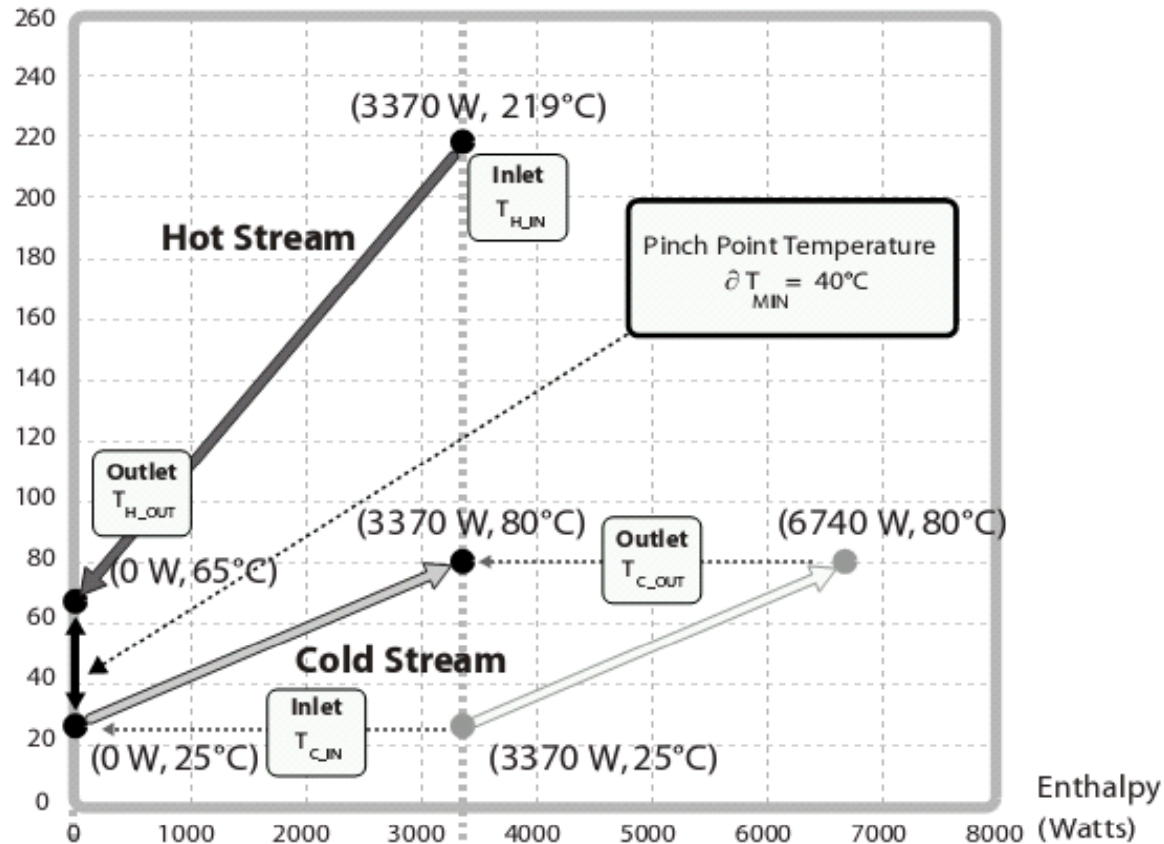
- Minimum dT at $L=0$
- $dT = 3\sim 40^\circ\text{C}$

T-H Diagram: $dT_{\min} > dT_{\min.set}$

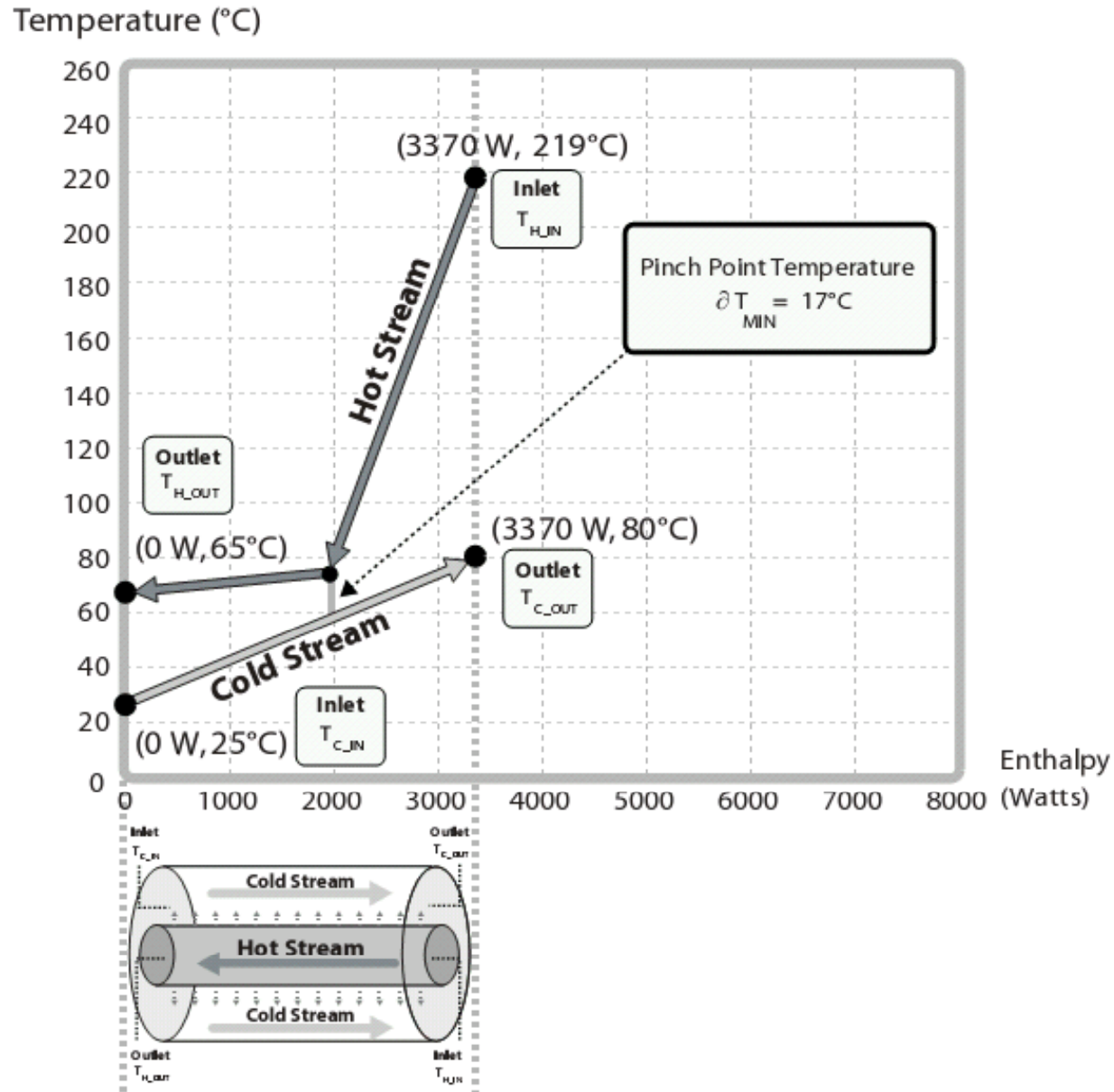


T-H Diagram: $dT_{min} > dT_{min.set}$

Temperature (°C)



T-H Diagram: Phase Change



Iteration

- Re-orientate flows until $dT_{\min} > dT_{\min, \text{set}}$
- Employ different heat exchangers
- Multiple scenario evaluation
- Cost benefit consideration
- Usually aided by computer software (e.g. ASPEN)