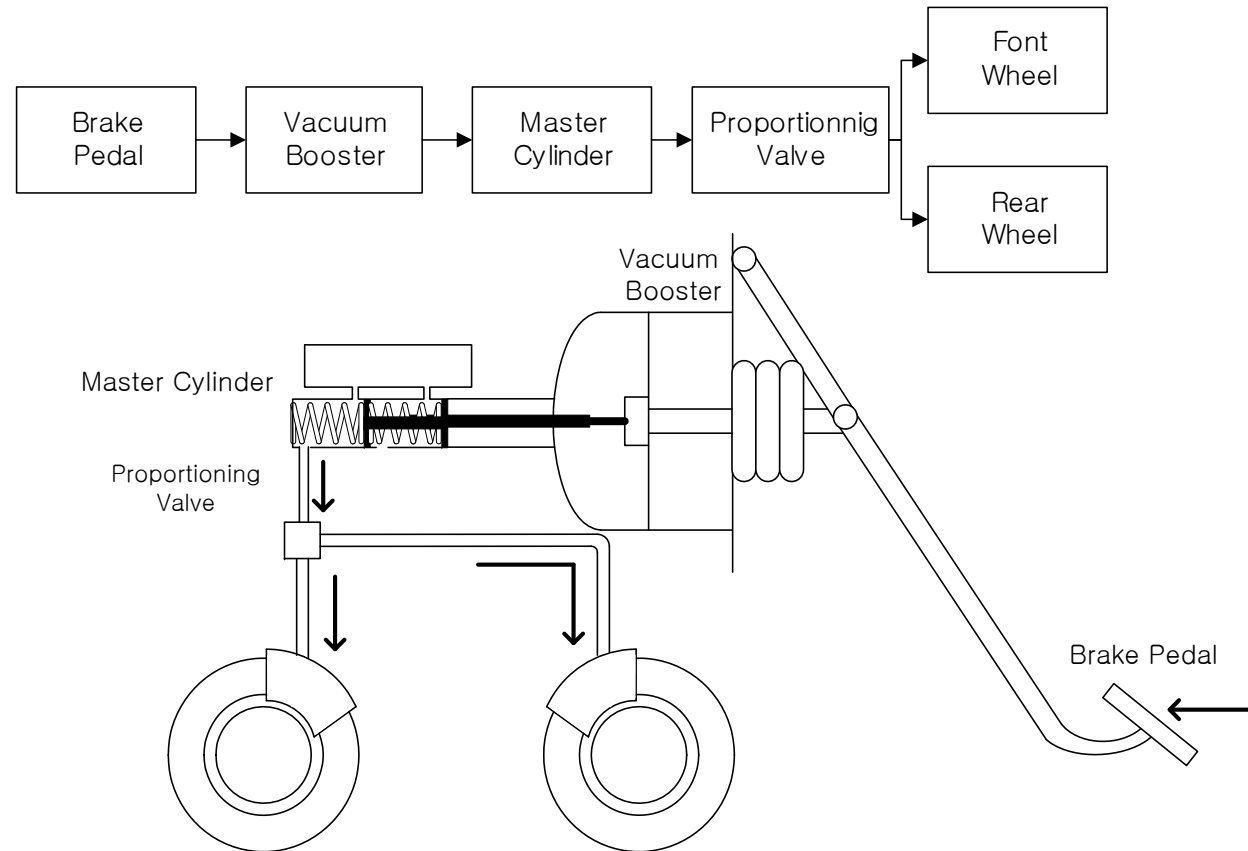


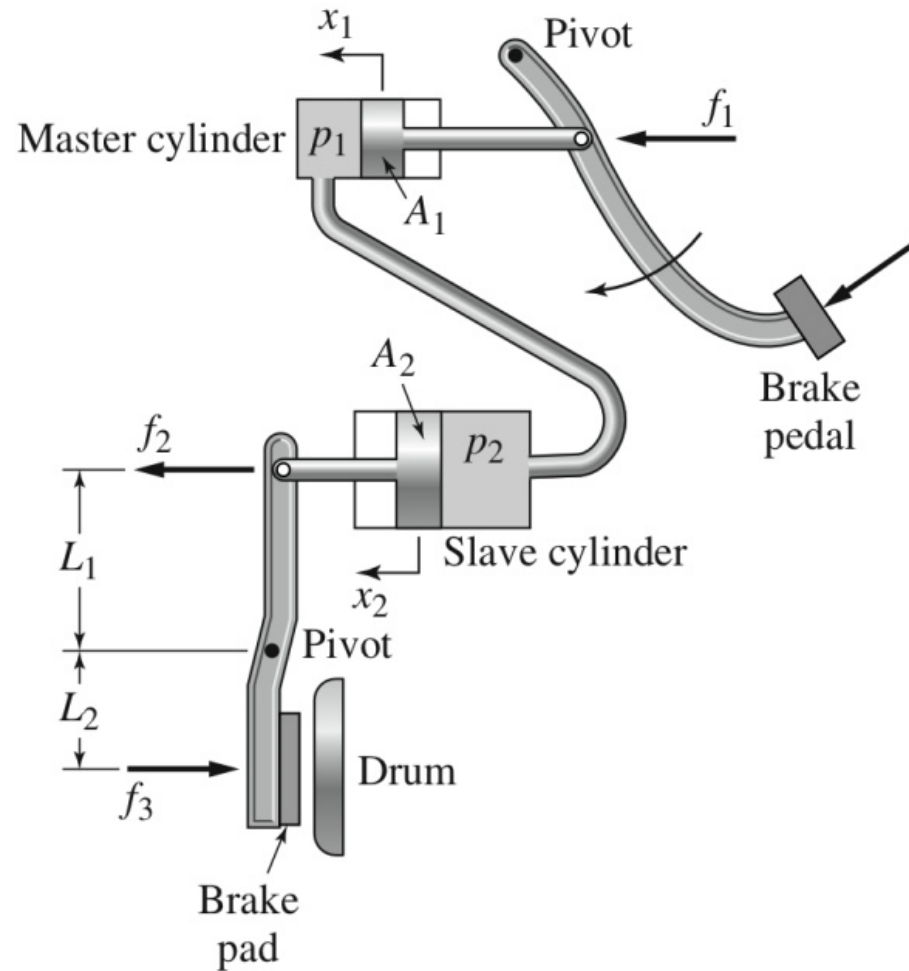
Fluid Systems I

Brake systems



Fundamental structure of a hydraulic brake

Conservation of Mass, Force and Pressure



Fluid Resistance

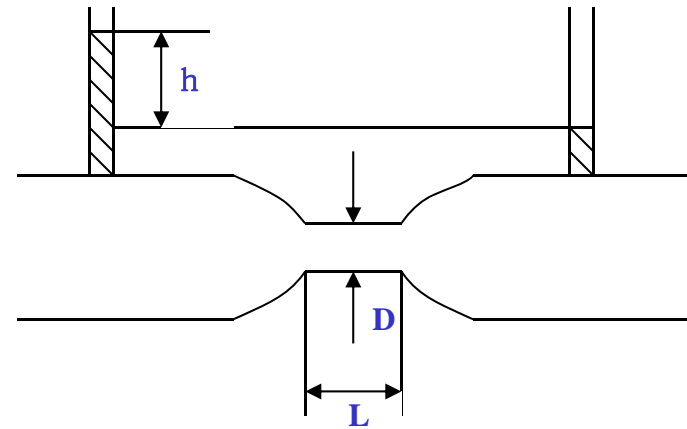
Electrical systems, resistance is defined as

$$i = \frac{v}{R}, \quad R = \frac{v}{i}$$

For fluid systems, R is defined as

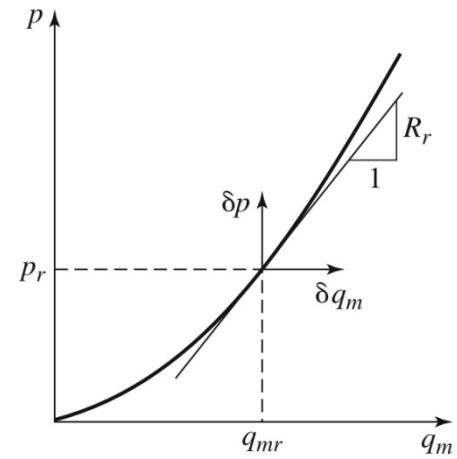
$$q_m = \frac{P}{R}, \quad R = \frac{P}{q_m}$$

Mass flow rate,
pressure difference



Fluid Resistance

$$R = \frac{\text{change in pressure}}{\text{change in flow rate}} = \left. \frac{dp}{dq_m} \right|_{q=q_{mr}}$$



Fluid Capacitance

Electrical systems,

$$\frac{dv}{dt} = \frac{1}{C} i$$

Fluid systems,

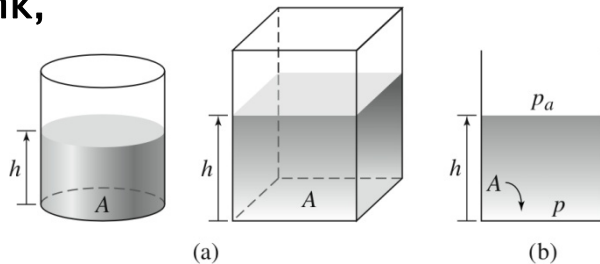
$$\frac{dp}{dt} = \frac{1}{C} q_m, \quad dp = \frac{1}{C} q_m dt, \quad C = \frac{q_m dt}{dp}$$

$$C = \frac{\text{change in stored mass}}{\text{change pressure}} = \frac{dm}{dp}$$

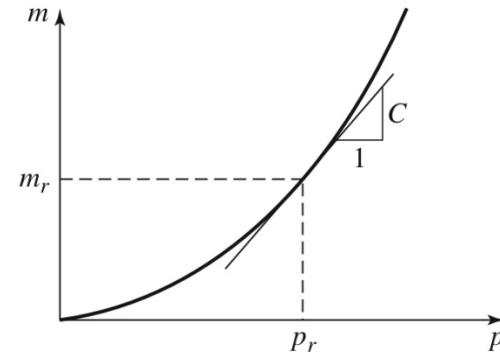
Fluid Capacitance

$$C = \frac{\text{change in stored mass}}{\text{change pressure}} = \frac{dm}{dp}$$

For a tank,



$$C = \rho A \frac{dh}{dp} = \rho A \frac{1}{\rho g} = \frac{A}{g}$$



General fluid capacitance

$$\frac{dm}{dt} = C \frac{dp}{dt} = q_{mi} - q_{mo}$$

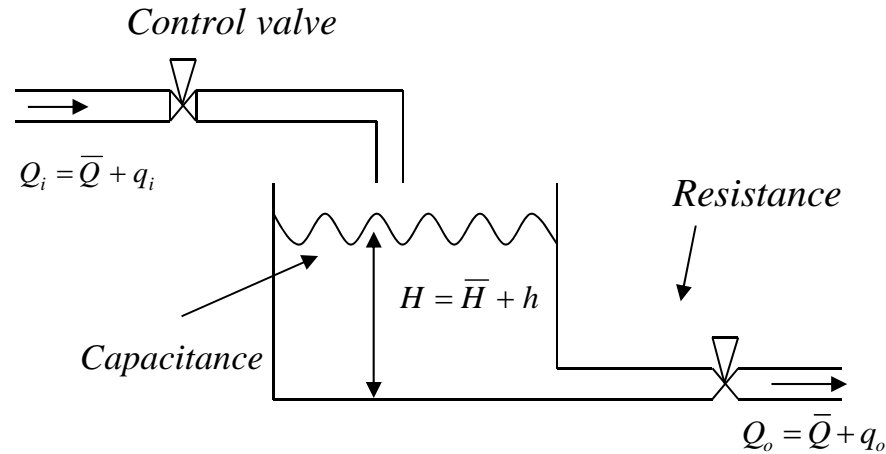
$$C \frac{dp}{dt} = \rho A \frac{dh}{dt} = q_{mi} - q_{mo}$$

For liquid level system, C is defined as

$$C = \frac{\text{change in liquid stored } m^3}{\text{change in head } m} = \rho A$$

use h(pressure head) , instead of p.

Liquid Level Systems



$$R = \frac{\text{change in level difference } m}{\text{change in flow rate } m^3 / s}$$

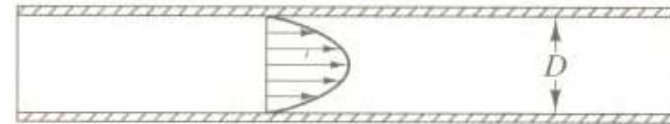
$$C = \frac{\text{change in liquid stored } m^3}{\text{change in head } m}$$

$$\text{Steady state : } Q_i = \bar{Q} = Q_o = \frac{\bar{H}}{R}$$

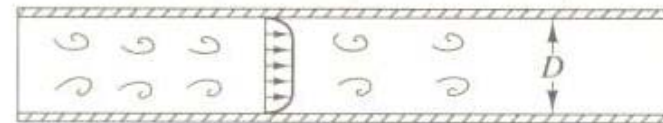
$$\text{consider, } Q_o = \frac{H}{R}, \quad Q_i - Q_o = C \frac{dH}{dt}$$

Basic Concepts

Laminar flow : When the viscous forces are dominant (slow flow, low Re) they are sufficient enough to keep all the fluid particles in line, then the flow is laminar.



Turbulent flow : It can be interpreted that when the inertial forces dominate over the viscous forces (when the fluid is flowing faster and Re is larger) then the flow is turbulent.



Reynolds number (Re) : The ratio of inertial forces to viscous forces.

It is used to determine whether a flow will be laminar or turbulent.

$$Re = \frac{\rho v D}{\mu}$$

μ : the dynamic viscosity of the fluid

ρ : density of the fluid

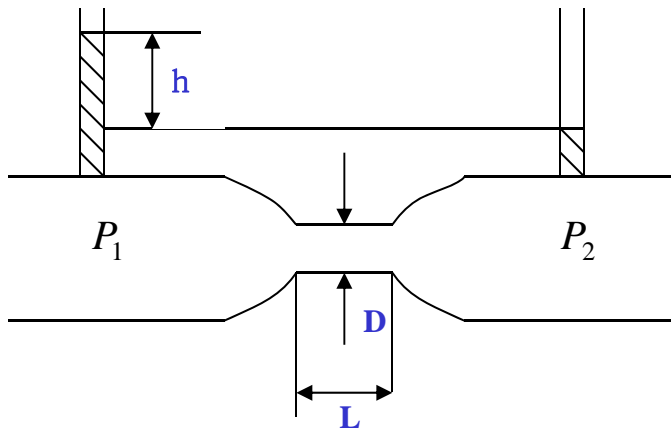
D : diameter

Re < 2000 : always laminar

Re > 4000 : always turbulent

Laminar Flow

Cylindrical pipe



$$P_1 - P_2 = \rho gh, \quad Q \frac{128\nu L}{g\pi D^4} = h$$

ν : viscosity,

L : length of pipe

D : diameter of pipe

$$Q = \frac{h}{R} = K_l h, \quad R = \frac{128\nu L}{g\pi D^4} \quad [s/m^2]$$

Q : steady – state flow rate

K_l : constant

h : steady – state head

Laminar Flow

Liquid level dynamics :

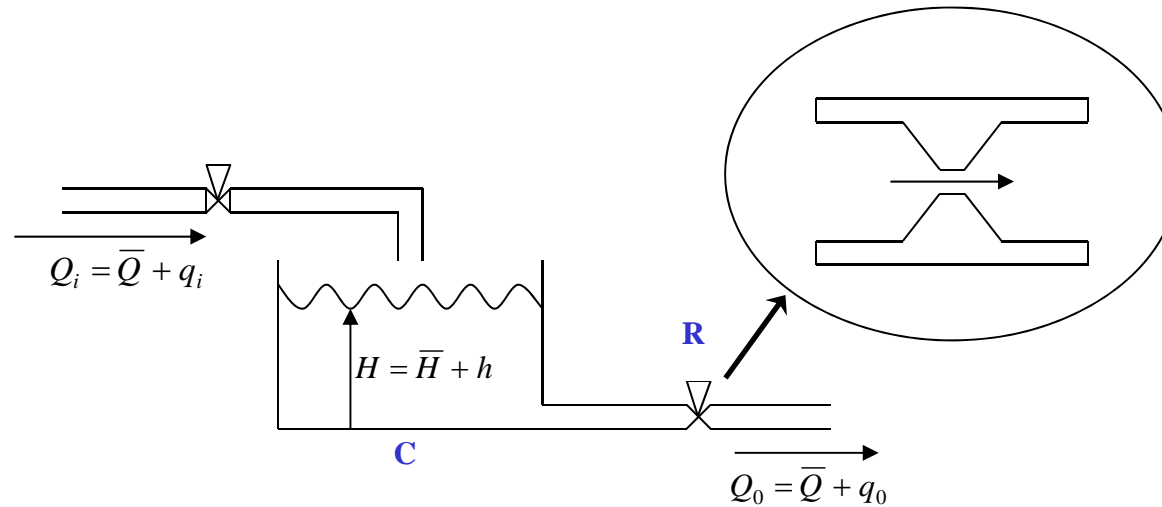
$$C \frac{dH}{dt} = Q_i - Q_o$$
$$= \bar{Q} + q_i - (\bar{Q} + q_o) = q_i - q_o$$

$$\frac{dH}{dt} = \frac{d}{dt}(\bar{H} + h) = \frac{dh}{dt}$$

$$Q_o = \bar{Q} + q_o = \frac{\bar{H} + h}{R}, \quad q_o = \frac{h}{R}$$

$$\rightarrow \frac{dh}{dt} = -\frac{1}{CR}h + \frac{1}{C}q_i$$

Turbulent Flow



$$Q = C_d \cdot a \cdot \sqrt{\frac{2}{\rho}(P_1 - P_2)}$$

ρ : density, a : area, C_d : discharge coefficient

steady state: $Q_i = \bar{Q} = Q_o = K_t \sqrt{\bar{H}}$

Turbulent Flow

Liquid level dynamics

$$C \frac{dH}{dt} = Q_i - Q_0 = \bar{Q} + q_i - K\sqrt{H}$$

$$\frac{dH}{dt} = \frac{1}{C} Q_i - \frac{1}{C} K\sqrt{H} = f(Q_i, H)$$

$$f(Q_i, H) = f(\bar{Q}_i, \bar{H}) + \left. \frac{\partial f}{\partial Q_i} \right|_{\bar{Q}, \bar{H}} (Q_i - \bar{Q}) + \frac{1}{2!} \frac{\partial^2 f}{\partial Q_i^2} (Q_i - \bar{Q})^2 + \dots$$

$$\dots + \left. \frac{\partial f}{\partial H} \right|_{\bar{Q}, \bar{H}} (H - \bar{H}) + \frac{1}{2!} \frac{\partial^2 f}{\partial H^2} (H - \bar{H})^2 + \dots$$

$$= \frac{1}{C} \bar{Q} - \frac{1}{C} K\sqrt{\bar{H}} + \left(\frac{1}{C} q_i - \frac{K}{C \cdot 2\sqrt{\bar{H}}} h \right) + \text{high order term}$$

Turbulent Flow

$$\frac{dH}{dt} = \frac{d\bar{H}}{dt} + \frac{dh}{dt}$$

$$\Rightarrow \frac{dh}{dt} = \frac{1}{C} q_i - \frac{K}{C \cdot 2\sqrt{\bar{H}}} h$$

$$q_o = \frac{h}{R}, \quad R = \frac{2\sqrt{\bar{H}}}{K} = \frac{2\bar{H}}{\bar{Q}}, \quad (\bar{Q} = K\sqrt{\bar{H}})$$

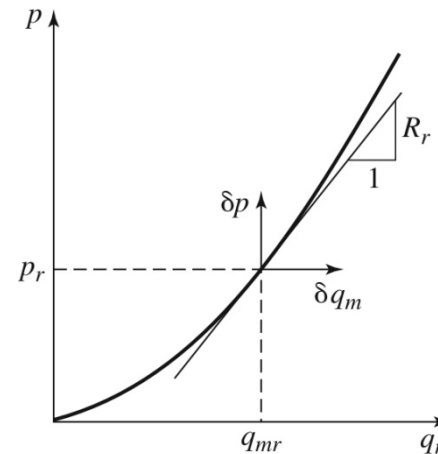
$$\therefore \begin{cases} \frac{dh}{dt} = -\frac{1}{CR} h + \frac{1}{C} q_i \\ q_o = \frac{h}{R} \end{cases} \quad \text{for small } q_i$$

Fluid Resistance(laminar flow vs turbulent flow)

$$R = \frac{\text{change in pressure}}{\text{change in flow rate}} = \left. \frac{dp}{dq_m} \right|_{q=q_{mr}}$$

$$q_m = \frac{p}{R} \quad \text{For laminar flow}$$

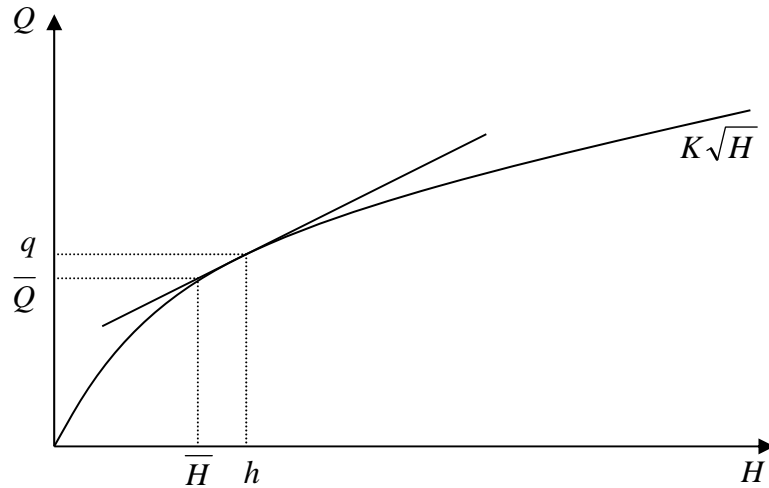
$$q_m = \sqrt{\frac{p}{R_t}} \quad \text{For turbulent flow}$$



For liquid level system, R is defined as

$$R = \frac{\text{change in level difference}}{\text{change in flow rate}} \frac{m}{m^3 / s} = \frac{dh}{dq_m}$$

Linearization



$$Q = \bar{Q} + q = K\sqrt{\bar{H}} + () \cdot h$$

$$y = f(x), \quad \bar{y} = f(\bar{x}), \quad x = \bar{x} + \Delta x$$

$$y = f(\bar{x}) + \left. \frac{\partial f}{\partial x} \right|_{\bar{x}} \cdot \Delta x + \frac{1}{2!} \left. \frac{\partial^2 f}{\partial x^2} \right|_{\bar{x}} \cdot \Delta x^2 + \dots$$

$$\approx \bar{y} + \left. \frac{\partial f}{\partial x} \right|_{\bar{x}} \cdot \Delta x$$

$$y - \bar{y} = \left. \frac{\partial f}{\partial x} \right|_{\bar{x}} (x - \bar{x}) = K(x - \bar{x})$$

$$y = f(x_1, x_2) \approx f(\bar{x}_1, \bar{x}_2) + \left. \frac{\partial f}{\partial x_1} \right|_{\bar{x}_1, \bar{x}_2} (x_1 - \bar{x}_1) + \left. \frac{\partial f}{\partial x_2} \right|_{\bar{x}_1, \bar{x}_2} (x_2 - \bar{x}_2)$$

$$= \bar{y} + K_1(x_1 - \bar{x}_1) + K_2(x_2 - \bar{x}_2)$$

$$\therefore y - \bar{y} = K_1(x_1 - \bar{x}_1) + K_2(x_2 - \bar{x}_2)$$

Summary of Liquid Level Systems

Laminar flow

$$\frac{dh}{dt} = -\frac{1}{CR}h + \frac{1}{C}q_i$$

$$\bar{Q} = K \cdot \bar{H} \quad R = \frac{\bar{H}}{\bar{Q}}$$

$$R = \frac{128\nu L}{g\pi D^4}$$

$$q_o = \frac{h}{R}$$

Turbulent flow

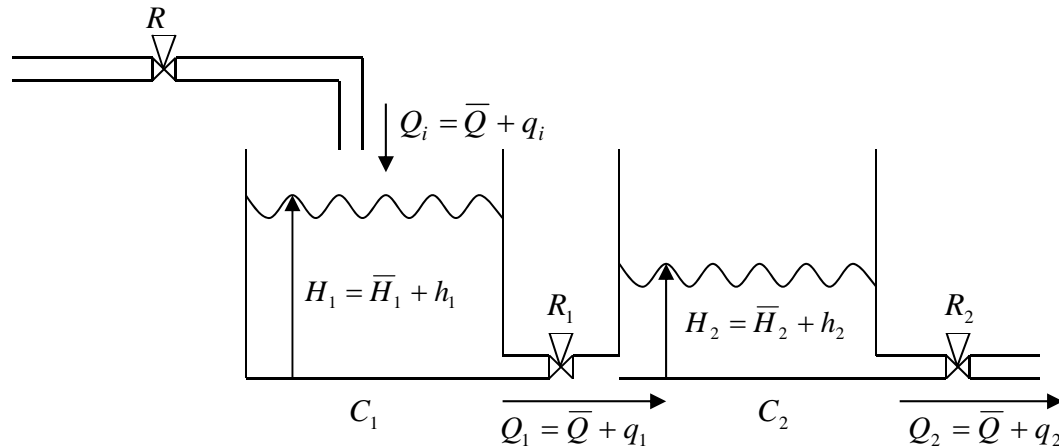
$$\frac{dh}{dt} = -\frac{1}{CR}h + \frac{1}{C}q_i$$

$$q_o = \frac{h}{R}$$

$$R = \frac{2\bar{H}}{\bar{Q}} = \frac{2\sqrt{\bar{H}}}{K} = \frac{2\sqrt{\bar{H}}}{C_d a \sqrt{2g}}$$

$$\left(\because \bar{Q} = K\sqrt{\bar{H}} = C_d a \sqrt{\frac{2}{\rho} \rho g \bar{H}} = C_d a \sqrt{2g} \sqrt{\bar{H}} \right)$$

Liquid Level Systems with Interaction



Steady state :

$$Q_i = \bar{Q} = Q_1 = Q_2$$

$$= \frac{\bar{H}_1 - \bar{H}_2}{R_1} = \frac{\bar{H}_2}{R_2}$$

Liquid level dynamics :

$$C_1 \frac{dH_1}{dt} = \bar{Q} + q_i - (\bar{Q} + q_1) \quad \rightarrow \quad C_1 \frac{dh_1}{dt} = q_i - q_1$$

$$Q_1 = \bar{Q} + q_1 = \frac{1}{R_1} (\bar{H}_1 + h_1 - (\bar{H}_2 + h_2)) \quad \rightarrow \quad q_1 = \frac{h_1 - h_2}{R_1}$$

$$C_2 \frac{dH_2}{dt} = \bar{Q} + q_1 - (\bar{Q} + q_2) \quad \rightarrow \quad C_2 \frac{dh_2}{dt} = q_1 - q_2$$

$$Q_2 = \bar{Q} + q_2 = \frac{\bar{H}_2 + h_2}{R_2} \quad \rightarrow \quad q_2 = \frac{h_2}{R_2}$$

Liquid Level Systems with Interaction

$$\therefore \begin{cases} \frac{dh_1}{dt} = -\frac{1}{C_1} \left(\frac{h_1 - h_2}{R_1} \right) + \frac{1}{C_1} q_i \\ \frac{dh_2}{dt} = \frac{1}{C_2} \left(\frac{h_1 - h_2}{R_1} \right) - \frac{1}{C_2} \frac{h_2}{R_2} \end{cases}$$

$$\text{Transfer Function} = \frac{Q_2(S)}{Q_i(S)} = \frac{1}{R_1 C_1 R_2 C_2 S^2 + (R_1 C_1 + R_2 C_2 + R_2 C_1) S + 1}$$