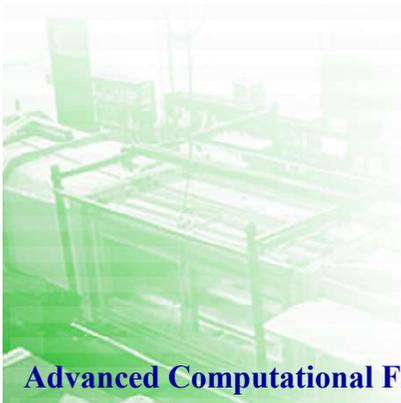




Chapter 1. Review on 'Introduction to CFD'



Chap. 1-1. Topics Covered

- **Classification of PDE**
 - Characteristics of 2nd-order linear PDE → Elliptic, Parabolic, and Hyperbolic PDE
- **Basic concept and linear stability**
 - Finite difference approximation of spatial and temporal derivatives
 - Truncation error and consistency → Fourier error analysis
 - Modified equation → numerical dissipation and numerical dispersion
 - General concept of stability → Von Neumann stability and Lax equivalence theorem
 - Domain of dependence/influence → CFD condition and stability
- **Discretization of Parabolic PDE**
 - Basic explicit/implicit schemes, and stability analysis
 - Splitting or factorized schemes for multi-D problems → ADI/AF-ADI in terms of delta/non-delta forms
 - Difference between delta and non-delta form for steady-state computations
- **Discretization of Elliptic PDE**
 - Relaxation methods depending on the choice of P with $A = P+B$ → Jacobi/G-S/ADI, and versions of over-relaxation
 - Similarity between relaxation method for elliptic PDE and time-marching method for parabolic PDE
 - Multigrid convergence acceleration → CGC strategy for linear elliptic PDE, V-/W-cycle

Chap. 1-2. Basic Theory of SCL

- **Hyperbolic PDEs**

- **Wave propagation problems with *limited D of Dep. and limited D. of Inf.***

- Formation, propagation and interaction of linear and nonlinear waves

- **Convection-dominated flows, compressible flows, convective flows admitting discontinuous solutions**

- **Scalar conservation law**

- Linear convection equation ($u_t + au_x = 0$)
- Burgers' equation ($u_t + uu_x = 0$)

- **Euler Equations**

- **General Form of SCL**

$$\frac{\partial u}{\partial t} + \frac{\partial f(u)}{\partial x} = \frac{\partial u}{\partial t} + a(u) \frac{\partial u}{\partial x} = 0 \quad \text{Eq. (*1)}$$

- u : conserved quantity, $f(u)$: convex flux function, $a(u) \equiv \frac{\partial f(u)}{\partial u}$: wave speed
- With I.C. of $u(x, 0) = u_0(x)$, the exact soln. of Eq. (*1) is $u(x, t) = u_0(x - a(u)t)$.
- $u(x, t) = \text{const}$ along the 'characteristic line' of $x - a(u)t = \text{const}$, with the wave speed of

$$\frac{dx}{dt} = a(u)$$

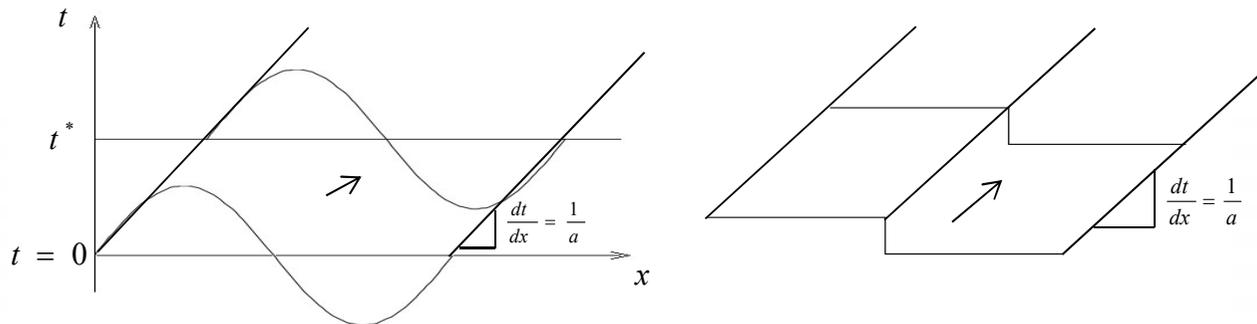
Chap. 1-2. Basic Theory of SCL

- **Ex 1) Linear wave equation**

- If $a(u) = a = \text{const}$, $f(u) = au$ and $u_t + au_x = 0$

$$\rightarrow u(x,t) = u_0(x - at) \text{ with } \frac{dx}{dt} = a = \text{const}$$

→ Initial profile moves with the same speed of a , and the initial shape is preserved.



- **Ex 2) Nonlinear wave equation**

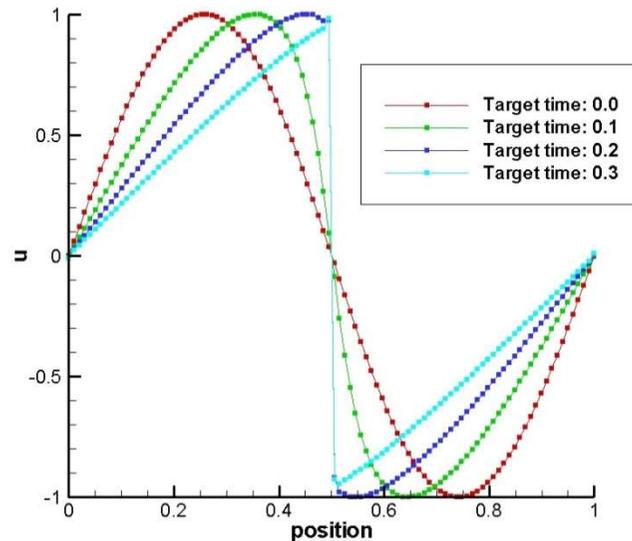
- If $a(u) = u \neq \text{const}$, $f(u) = \frac{u^2}{2}$ and $u_t + uu_x = 0$

$$\rightarrow u(x,t) = u_0(x - ut) \text{ with } \frac{dx}{dt} = u \neq \text{const}$$

→ Initial profile moves with the local speed of u , and a 'discontinuous' solution can be developed even with a 'smooth' initial profile.

Chap. 1-2. Basic Theory of SCL

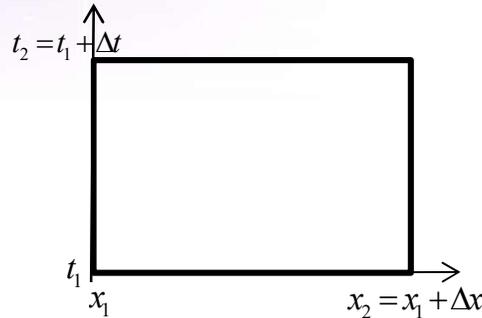
- **Ex 2) Nonlinear wave equation (cont'd)**
 - Problem of differentiability at discontinuity
 - A sinusoidal initial profile leading to a discontinuous saw-tooth profile



- **Behavior of the exact solution**
 - Assuming convex flux function ($f''(u) = a'(u) \geq 0$), extrema of the exact solution are determined by the initial condition, and after forming a discontinuity, they are decaying to $O(t^{-1/2})$ to create wider expansion region.
 - This is true to the case of intersection of discontinuities to create a single discontinuity.
 - In case of non-convex flux function for real gas flows or two-phase flows in porous media, intersection of discontinuities creates multiple discontinuities along with a new monotonic wave profile bounded by the multiple discontinuities.

Chap. 1-2. Basic Theory of SCL

- *Integration of SCL → Conservative Finite Volume Discretization*



$$\frac{\partial u}{\partial t} + \frac{\partial f(u)}{\partial x} = 0$$

$$\rightarrow \int_{t_1}^{t_2} \int_{x_1}^{x_2} \left(\frac{\partial u}{\partial t} + \frac{\partial f(u)}{\partial x} \right) dx dt = 0$$

$$\int_{x_1}^{x_2} u(x, t_2) dx - \int_{x_1}^{x_2} u(x, t_1) dx = \int_{t_1}^{t_2} f(u(x_1, t)) dt - \int_{t_1}^{t_2} f(u(x_2, t)) dt \quad \text{Eq. (*2)}$$

→ Conservation of u in (x, t) stating that

change of u over (x_1, x_2) during Δt = net flux across the boundary of x_1, x_2 during Δt

Introduce a finite volume computational cell with $(x_1, x_2) = (x_{j-1/2}, x_{j+1/2})$ and $(t_1, t_2) = (t^n, t^{n+1})$,

and define an approximate quantity averaged over $\Delta x = x_{j+1/2} - x_{j-1/2}$ and $\Delta t = t^{n+1} - t^n$

- cell-averaged value: $\frac{1}{\Delta x} \int_{x_{j-1/2}}^{x_{j+1/2}} u(x, t^n) dx \equiv u_j^n$,
- cell-interface numerical flux: $\frac{1}{\Delta t} \int_{t^n}^{t^{n+1}} f(u(x_{j+1/2}, t)) dt \equiv F_{j+1/2}$

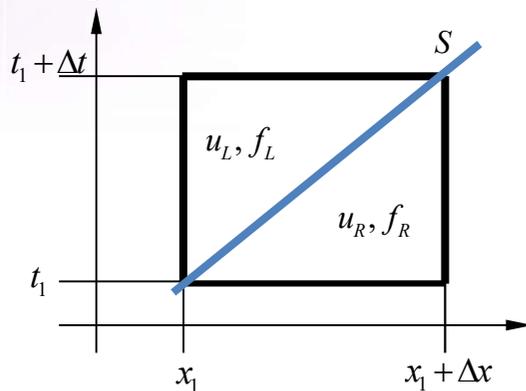
Then, Eq. (*2) can be discretized, called conservative finite volume discretization, as

$$\Delta x (u_j^{n+1} - u_j^n) = \Delta t (F_{j-1/2} - F_{j+1/2}) \rightarrow u_j^{n+1} = u_j^n - \frac{\Delta t}{\Delta x} (F_{j+1/2} - F_{j-1/2}) \quad \text{Eq. (*3)}$$

By applying the integral form of SCL (or using Eq. (*3)), problem of differentiability is avoided.

Chap. 1-2. Basic Theory of SCL

- **Integral conservative form and the condition for correct shock speed**



From Eq. (*3),

$$(u_L - u_R)\Delta x = (f_L - f_R)\Delta t$$

$$(f_R - f_L) = \frac{\Delta x}{\Delta t}(u_R - u_L) = S(u_R - u_L) \text{ with } S = \text{shock speed}$$

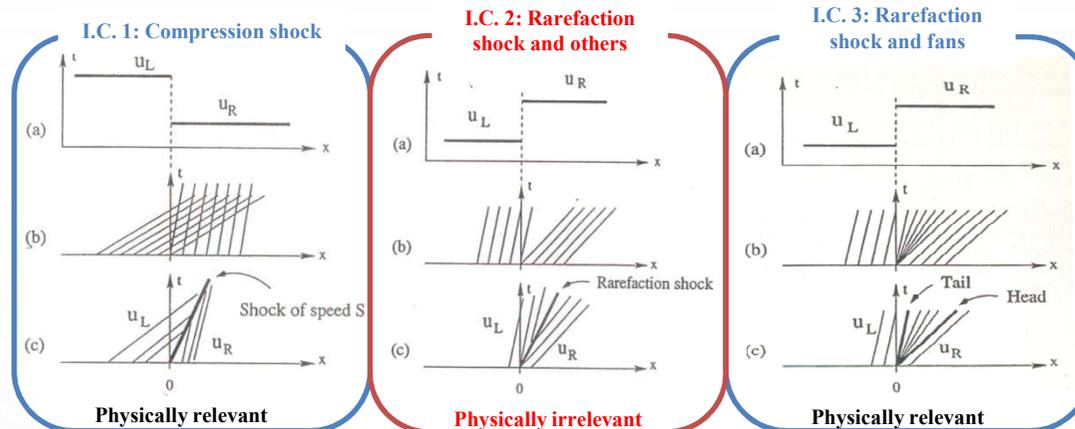
or $[f] = S[u] \rightarrow$ Rankine-Hugoniot relation for SCL

- Note that S is the shock speed averaged over Δx , Δt .

- **Integral form and the problem of non-uniqueness**

- Ex) Correct behavior of discontinuities under various initial conditions

$$S = \frac{[f]}{[u]} = \frac{\frac{1}{2}(u_L^2 - u_R^2)}{u_L - u_R} = \frac{1}{2}(u_L + u_R) \text{ for Burgers equation}$$



Chap. 1-2. Basic Theory of SCL

- **Flow physics from the 2nd law of thermodynamics states that expansion shock is not allowed. → entropy condition**

- Characteristics across discontinuity should converge. → For the right-moving shock with $u_L > u_R$, $u_L > S = [f]/[u] > u_R$. Thus, case III is the physically correct solution.

- More generally, the entropy condition by Oleinik can be considered to include non-convex cases.

$$(f(u) - f(u_L)) / (u - u_L) > S = [f]/[u] > (f(u_R) - f(u)) / (u_R - u)$$

- Ex) Consider a SCL with $u_0(x) = \begin{cases} 1 & \text{if } x < 0 \\ 0 & \text{if } x > 0 \end{cases}$

What would be the expected entropy solution for convex and non-convex flux functions?

- **How to implement ?**

- Solve a vanishing viscosity form $u_t + au_x = \varepsilon u_{xx}$ with some(?) $\varepsilon > 0$

- Design a numerical flux such that it contains a proper form of numerical viscosity

- Entropy function and entropy flux → entropy inequality

- Motivated by the entropy inequality of the Euler equations $(\rho s)_t + (\rho us)_x \geq 0$,

Consider the entropy inequality of SCL as $U(u)_t + F(u)_x \geq 0$

with $U(u)$: entropy function, $F(u)$: entropy flux.

Then, by requiring $\frac{dF}{du} = \frac{df}{du} \frac{dU}{du}$ and $\frac{d^2U}{du^2} \leq 0$, $U(u)$ and $F(u)$ satisfying the entropy inequality

can be obtained.

Chap. 1-2. Basic Theory of SCL

- **Conservation law and weak solution**

- Consider $u_t + \left(\frac{u^2}{2}\right)_x = 0$ vs. $(u^2)_t + \left(\frac{2}{3}u^3\right)_x = 0$

$$S_u = \frac{[f]}{[u]} = \frac{1}{2}(u_L + u_R) \quad \text{vs.} \quad S_{u^2} = \frac{[f(u^2)]}{[u^2]} = \frac{1}{2}(u_L + u_R) + \frac{1}{6} \frac{(u_L - u_R)^2}{u_L + u_R}$$

- Mathematically both equations are the same in smooth region, but not, in discontinuous region
 - Note that $U(u) = -u^2$ and $F(u) = -\frac{2}{3}u^3$ are actually the entropy function and entropy flux, respectively.

- **Conservative Scheme**

- **Applying the integral form of SCL over $(\Delta x, \Delta t)$**

$$u_j^{n+1} = u_j^n - \frac{\Delta t}{\Delta x} (F_{j+1/2} - F_{j-1/2}) \quad \text{Eq. (*3)}$$

- **For 1-D case with $\Omega = \text{JMAX} \times \Delta x$**

$$\sum_{j=1}^{\text{JMAX}} (\text{Eq. (*3)}) \text{ gives } \sum_{j=1}^{\text{JMAX}} u_j^{n+1} - \sum_{j=1}^{\text{JMAX}} u_j^n + \frac{\Delta t}{\Delta x} (F_{\text{JMAX}+1/2}^n - F_{1/2}^n) = 0,$$

if each cell-interface flux is *uniquely* and *consistently* determined from cell-averaged values

→ Change of u in the computational domain during Δt

= Net flux across the computational boundary during Δt

→ Discrete realization of the integral conservation law over the computational domain

Chap. 1-2. Basic Theory of SCL

- Ex) Non-conservative scheme and shock speed

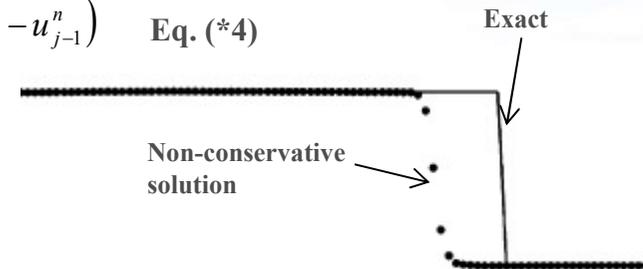
- For Burgers eqn. of $u_t + uu_x = 0$ with I.C. of $u_0(x) = \begin{cases} 1 & \text{if } x < 0 \\ 0 & \text{if } x \geq 0 \end{cases}$

- A non-conservative upwind scheme : $u_j^{n+1} = u_j^n - \frac{\Delta t}{\Delta x} u_j^n (u_j^n - u_{j-1}^n)$ Eq. (*4)

$$\text{with } u_j^0 = \begin{cases} 1 & \text{if } j < 0 \\ 0 & \text{if } j \geq 0 \end{cases}$$

- From Eq. (*4), $u_j^n = u_j^0$ for all n and $j \rightarrow S=0$

But from the R-H condition of SCL, $S = \frac{1}{2}(1+0) = 0.5$



- Consistency**

- General form of conservative scheme**

$$u_j^{n+1} = u_j^n - \frac{\Delta t}{\Delta x} \left(F_{j+1/2}(u_{j-p}^n, u_{j-p+1}^n, \dots, u_{j+q}^n) - F_{j-1/2}(u_{j-p-1}^n, u_{j-p}^n, \dots, u_{j+q-1}^n) \right) \quad \text{Eq. (*5)}$$

- Eq. (*5) is called consistent with SCL if $F_{j+1/2}$ goes to the true flux $f(u)$ in the constant flow.

$$F(\bar{u}, \bar{u}, \dots, \bar{u}) = f(\bar{u})$$

- A stronger condition to satisfy the consistency is the Lipschitz continuity of $F_{j+1/2}$, or that there is some $K > 0$ such that

$$\left| F(u_{j-p}, u_{j-p+1}, \dots, u_{j+q}) - f(u) \right| \leq K \max_{-p \leq i \leq q} |u_{j+i} - u|$$