# Reactors II

## Today's lecture

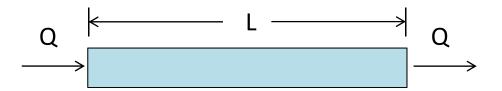
#### Plug flow reactor

- Concept
- PFR analysis for 1<sup>st</sup> order reaction
- PFR analysis for Monod kinetics

#### Continuous-stirred tank reactor

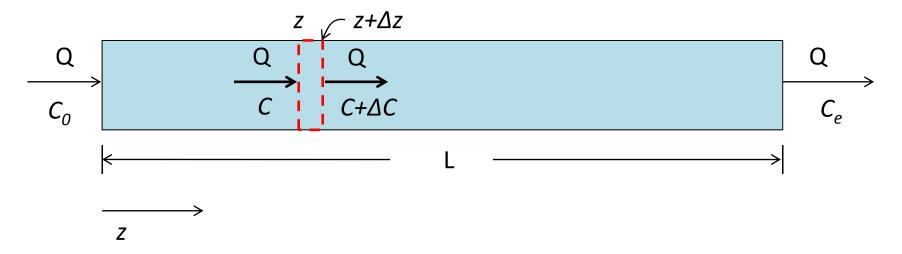
- CSTR analysis for 1<sup>st</sup> order reaction
- PFR vs. CSTR
- CSTR analysis for Monod kinetics

## Reactor analysis: PFR



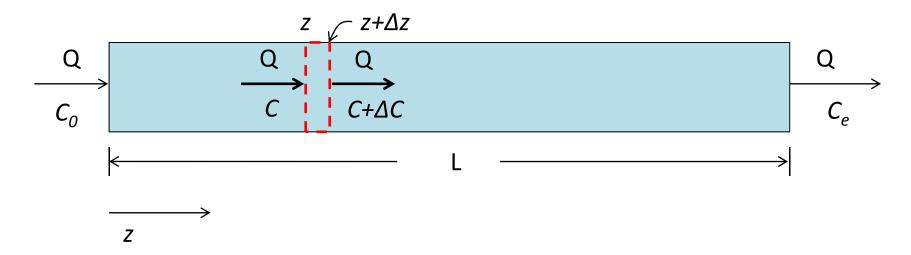
- Plug flow reactor (PFR)
  - assumption: no mixing in the direction of flow & completely mixed in the direction perpendicular to the flow
  - reactors get close to PFR as the length gets longer than the width and depth (e.g., rivers)

## PFR, first-order reaction



• Take control volume as a thin plate perpendicular to the flow at z=z with a dimension of  $\Delta z$  in z dir.

## PFR, first-order reaction



$$C/C_0 = e^{-k\theta} \longrightarrow$$

Same form as the batch reactor (why??)

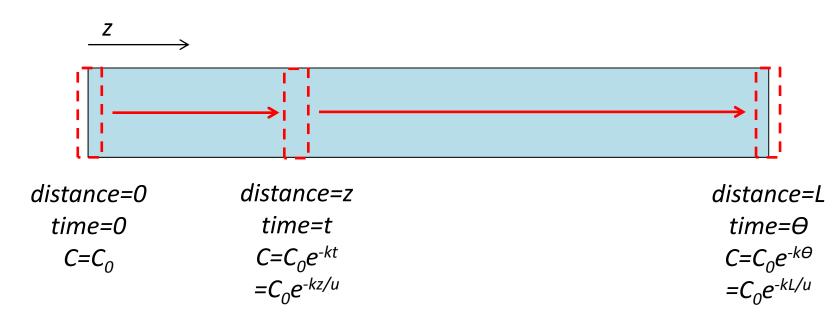
where, 
$$\theta \equiv \frac{V}{Q} = \frac{A \cdot L}{A \cdot u} = \frac{L}{u}$$
  $\theta = \text{hydraulic retention time, HRT [T]}$   $V = \text{reactor volume [I]}^3$ 

 $V = reactor\ volume\ [L^3]$ 

 $u = flow \ velocity \ [LT^{-1}]$ 

 $A = cross-sectional area [L^2]$ 

## PFR, first-order reaction



- We model plug flow reactor as a movement of a "plug"
- The plug has a cross sectional area same as the reactor dimension and an infinitesimal dimension in z-dir (a thin plate)
- Complete mixing within the plug → batch reactor moving in the direction of flow

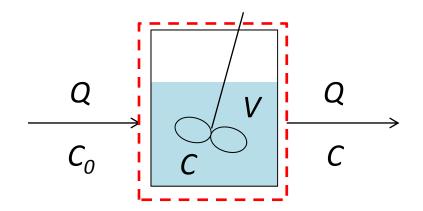
## PFR, Monod – Semi-analytical solution

#### Assuming decay is negligible,

$$\frac{z}{u} = -\frac{1}{\hat{q}} \left\{ \left( \frac{K}{X_a^0 + YS^0} + \frac{1}{Y} \right) ln(X_a^0 + YS^0 - YS) - \left( \frac{K}{X_a^0 + YS^0} \right) ln \frac{SX_a^0}{S^0} - \frac{1}{Y} lnX_a^0 \right\}$$

[5.26] in the textbook

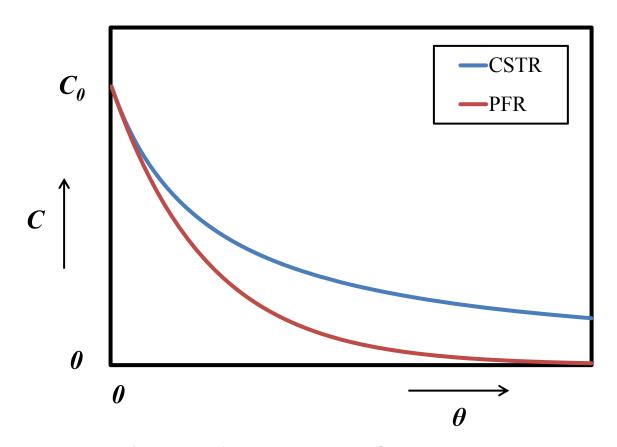
## Reactor analysis: CSTR, 1st order



At steady state,

$$C = \frac{C_0}{1 + k\theta}$$

#### PFR vs. CSTR



PFR shows better performance esp. at high HRTs

For 1<sup>st</sup> order reaction,

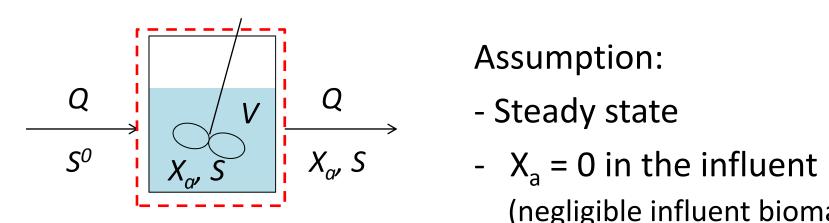
CSTR:

$$C = \frac{C_0}{1 + k\theta}$$

PFR:

$$C = C_0 e^{-k\theta}$$

## Reactor analysis: CSTR, Monod kinetics



#### **Assumption:**

- (negligible influent biomass)

$$S = K \frac{1 + b\theta}{Y\hat{q}\theta - (1 + b\theta)}$$

No  $S_0$  or  $X_a$  in the equation!

$$X_a = Y \frac{S^0 - S}{1 + b\theta}$$