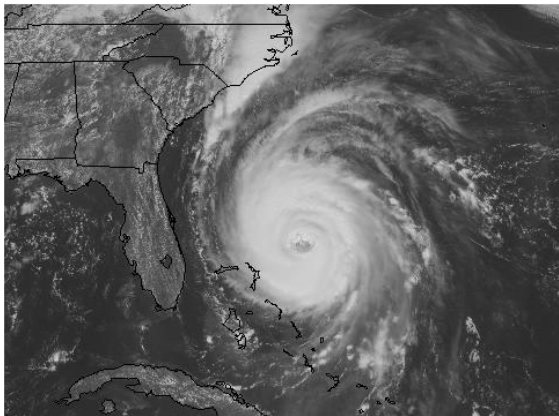
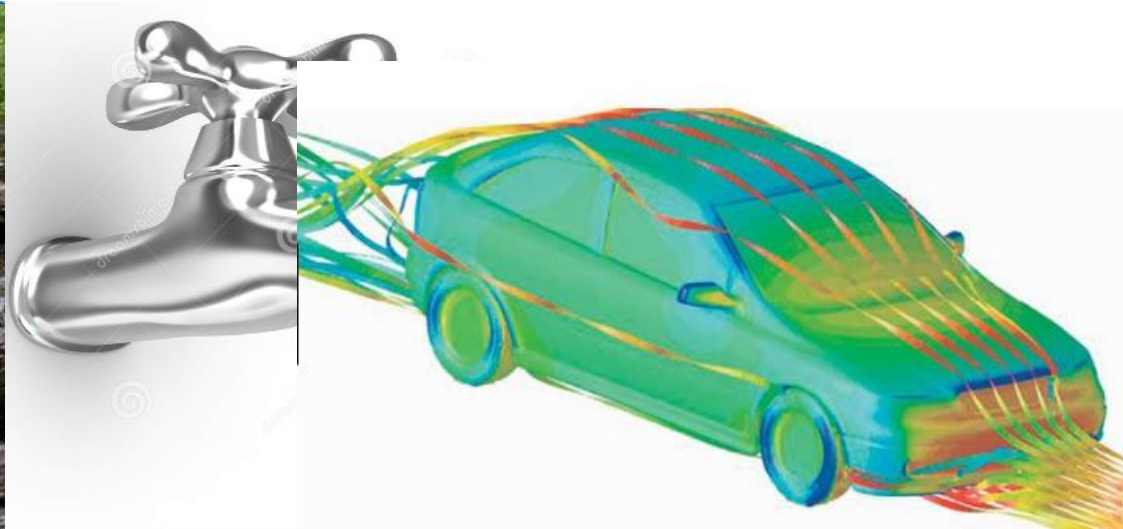


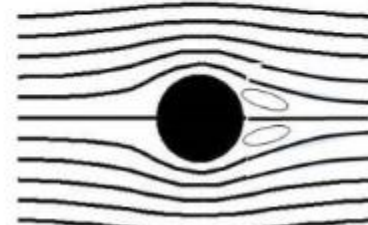
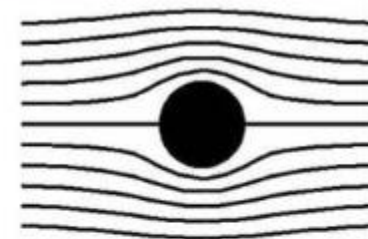
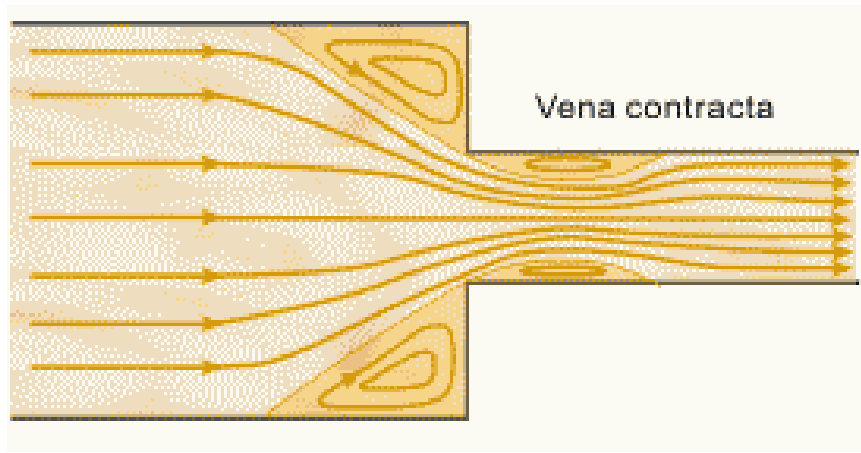
# 유변학

흐름과 유체

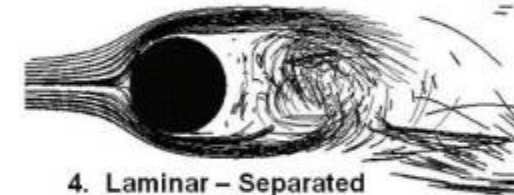
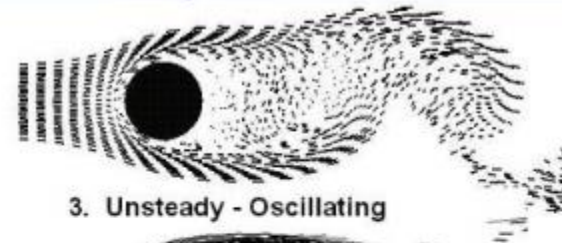
**흐름 (flow)**



 NASA Dryden Flight Research Center Photo Collection  
<http://www.dfrc.nasa.gov/gallery/photo/index.html>  
 NASA Photo: EC99-44921-1 Date: 1999  
 X-33 artist concept - 1999



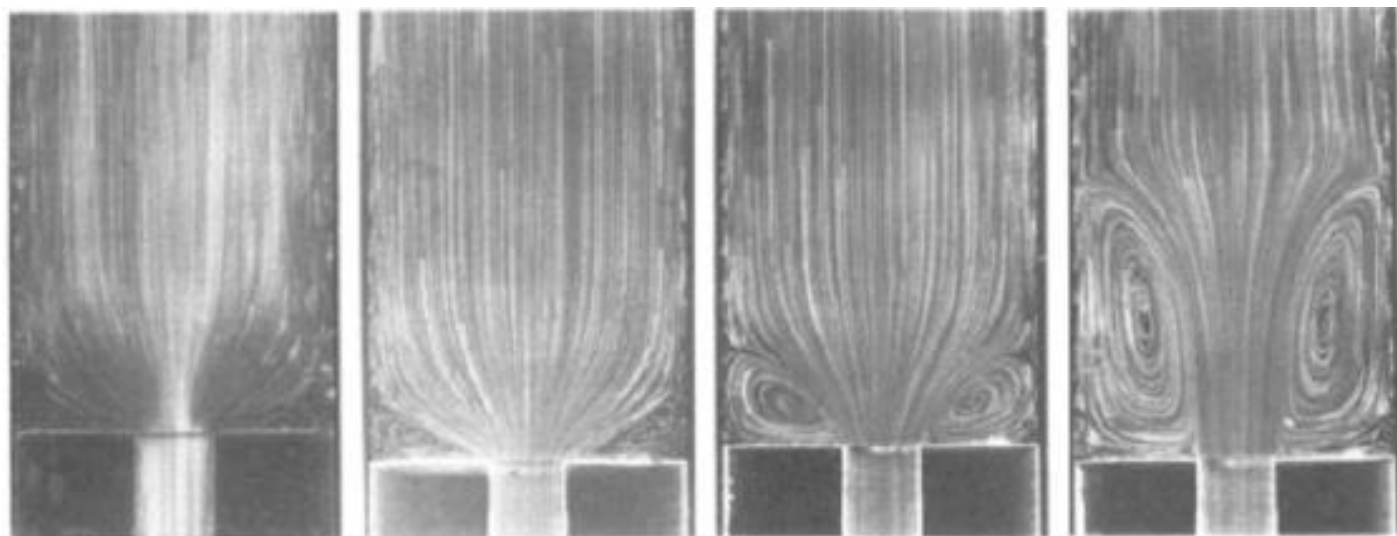
2. Separated - Steady



4. Laminar - Separated



5. Turbulent - Separated



$$\lambda\dot{\gamma} = 0.63$$

$$\lambda\dot{\gamma} = 0.96$$

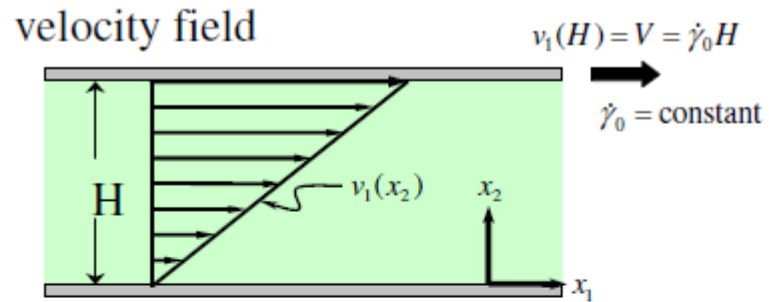
$$\lambda\dot{\gamma} = 1.43$$

$$\lambda\dot{\gamma} = 1.63$$

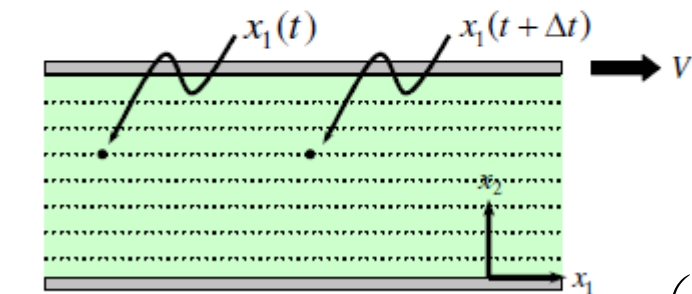
# flow

- shear flow
  - simple shear flow
- elongational flow
  - uniaxial elongational flow
  - biaxial stretching flow
  - planar elongational flow

# simple shear flow



$$\mathbf{v} = \begin{pmatrix} \dot{\gamma}_{21} x_2 \\ 0 \\ 0 \end{pmatrix}$$



$$\dot{\gamma} = \nabla \mathbf{v} + (\nabla \mathbf{v})^T = \begin{pmatrix} \frac{\partial v_1}{\partial x_1} & \frac{\partial v_2}{\partial x_1} & \frac{\partial v_3}{\partial x_1} \\ \frac{\partial v_1}{\partial x_2} & \frac{\partial v_2}{\partial x_2} & \frac{\partial v_3}{\partial x_2} \\ \frac{\partial v_1}{\partial x_3} & \frac{\partial v_2}{\partial x_3} & \frac{\partial v_3}{\partial x_3} \end{pmatrix} + \begin{pmatrix} \frac{\partial v_1}{\partial x_1} & \frac{\partial v_1}{\partial x_2} & \frac{\partial v_1}{\partial x_3} \\ \frac{\partial v_2}{\partial x_1} & \frac{\partial v_2}{\partial x_2} & \frac{\partial v_2}{\partial x_3} \\ \frac{\partial v_3}{\partial x_1} & \frac{\partial v_3}{\partial x_2} & \frac{\partial v_3}{\partial x_3} \end{pmatrix} = \begin{pmatrix} 0 & \dot{\gamma}_{21} & 0 \\ \dot{\gamma}_{21} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

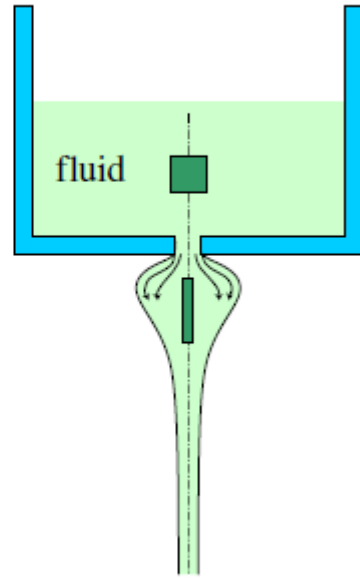
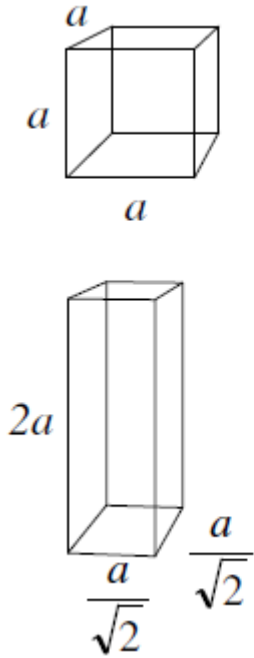
# Newtonian fluid

$$\boldsymbol{\tau} = \begin{pmatrix} \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & \tau_{33} \end{pmatrix} = -\mu \dot{\boldsymbol{\gamma}} = -\mu \begin{pmatrix} 0 & \dot{\gamma}_{21} & 0 \\ \dot{\gamma}_{21} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\tau_{21} = \tau_{12} = -\mu \dot{\gamma}_{21} = -\mu \frac{\partial v_1}{\partial x_2}$$

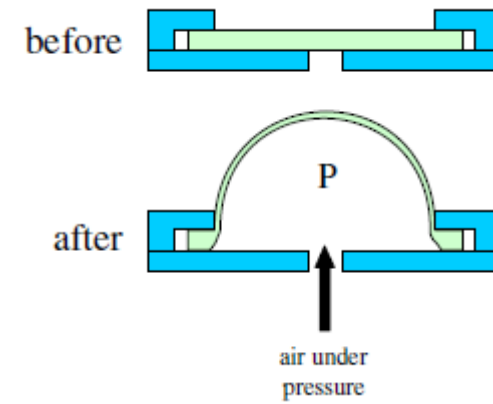
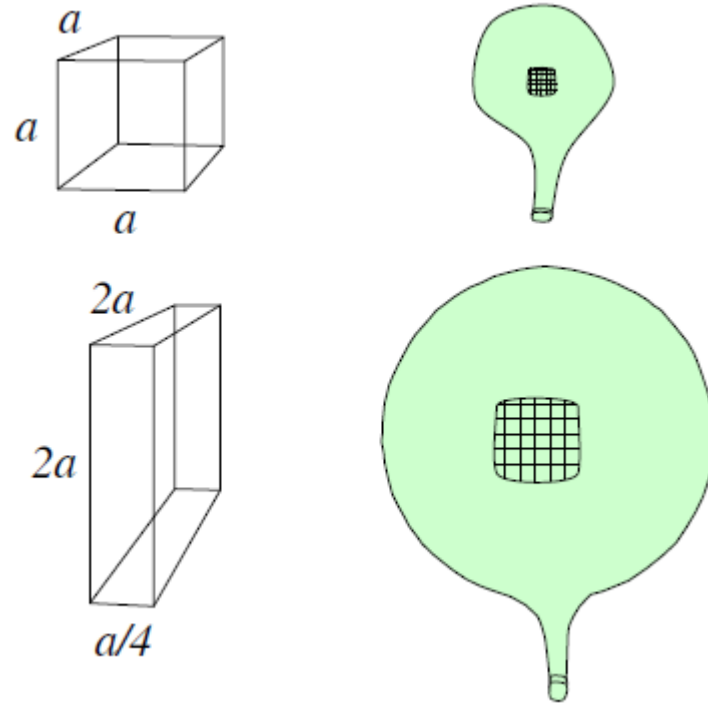


# uniaxial elongational flow



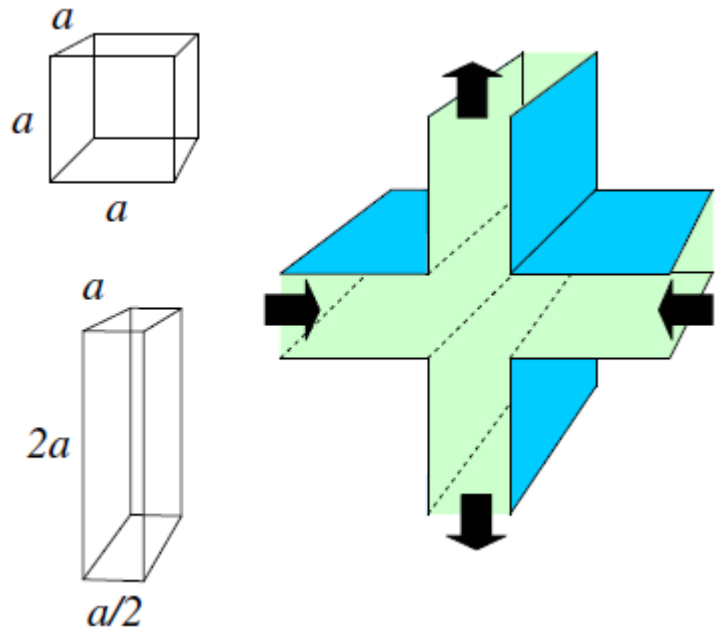
$$\underline{v} \equiv \begin{pmatrix} -\frac{\dot{\epsilon}(t)}{2}x_1 \\ -\frac{\dot{\epsilon}(t)}{2}x_2 \\ \dot{\epsilon}(t)x_3 \end{pmatrix}_{123} \quad \dot{\epsilon}(t) > 0$$

# biaxial stretching flow



$$\underline{v} \equiv \begin{pmatrix} -\frac{\dot{\epsilon}(t)}{2}x_1 \\ -\frac{\dot{\epsilon}(t)}{2}x_2 \\ \dot{\epsilon}(t)x_3 \end{pmatrix}_{123} \quad \dot{\epsilon}(t) < 0$$

# planar elongational flow



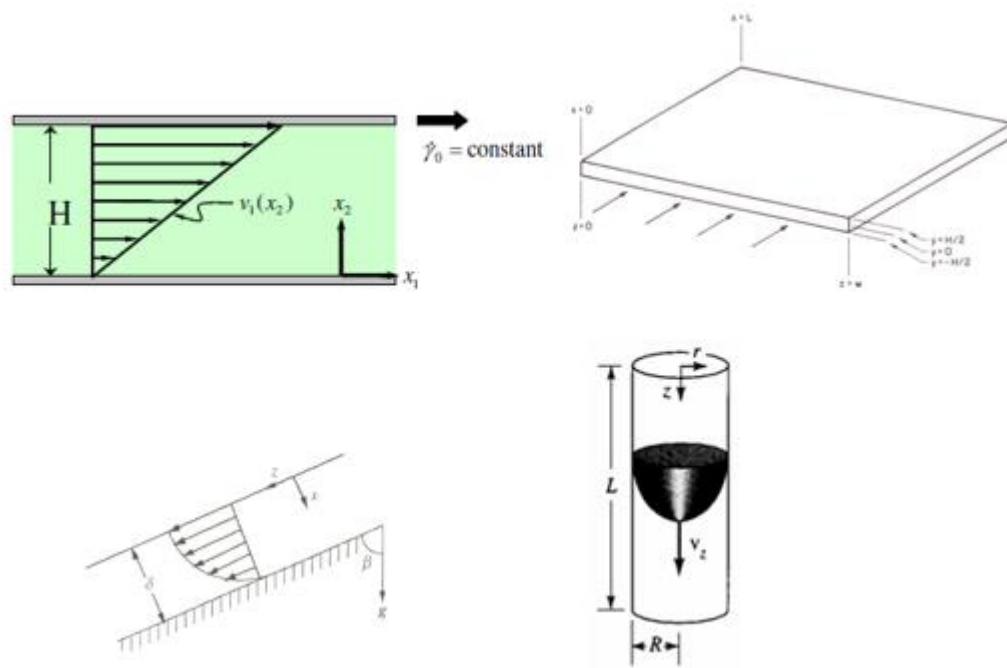
$$\underline{v} \equiv \begin{pmatrix} -\dot{\mathcal{E}}(t)x_1 \\ 0 \\ \dot{\mathcal{E}}(t)x_3 \end{pmatrix}_{123} \quad \dot{\mathcal{E}}(t) > 0$$

$$\underline{v} = \begin{pmatrix} -\frac{1}{2}\dot{\mathcal{E}}(t)(1+b)x_1 \\ -\frac{1}{2}\dot{\mathcal{E}}(t)(1-b)x_2 \\ \dot{\mathcal{E}}(t)x_3 \end{pmatrix}_{123}$$

Elongational flow:  $b=0$ ,  $\dot{\mathcal{E}}(t) > 0$

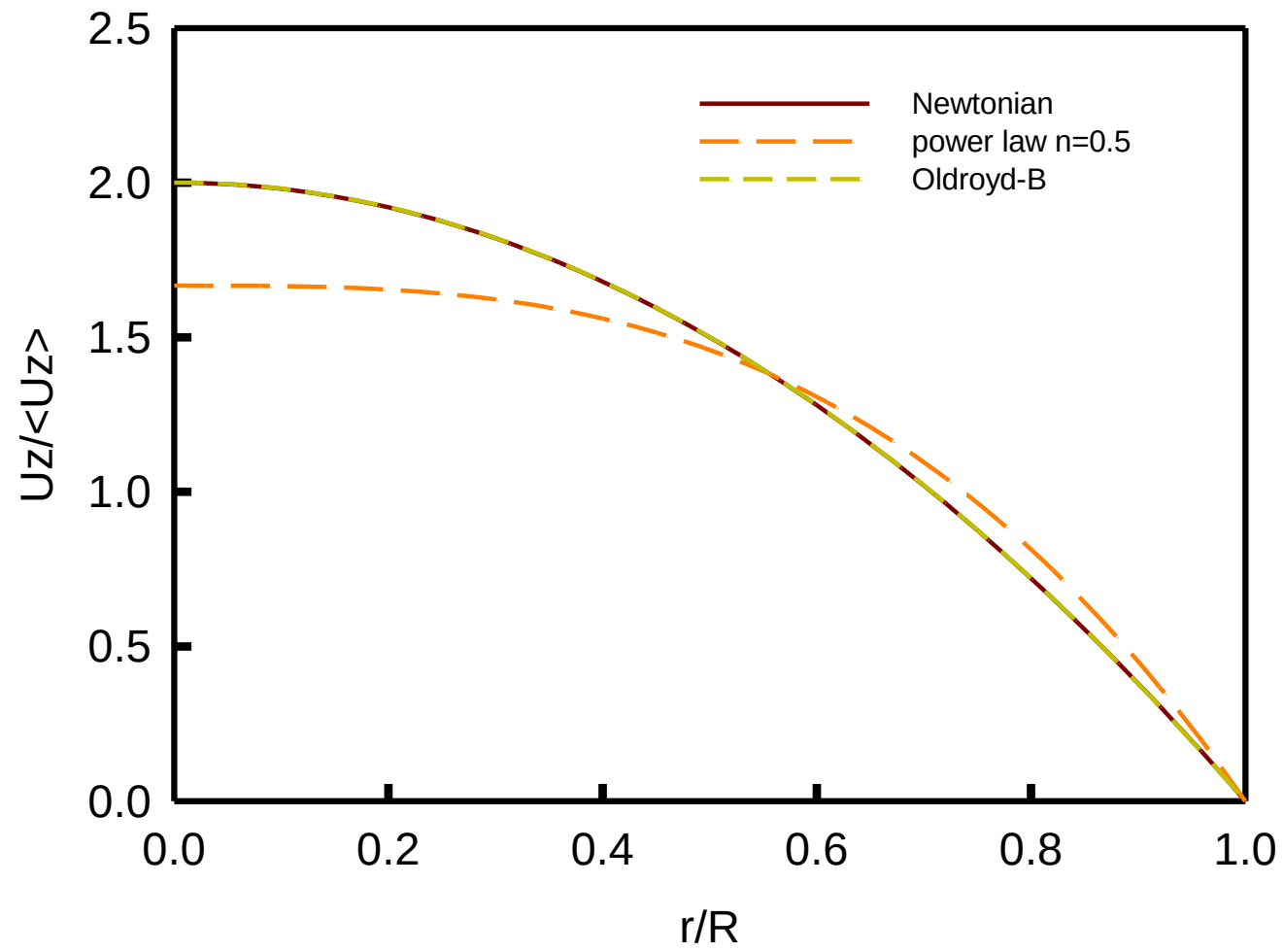
Biaxial stretching:  $b=0$ ,  $\dot{\mathcal{E}}(t) < 0$

Planar elongation:  $b=1$ ,  $\dot{\mathcal{E}}(t) > 0$



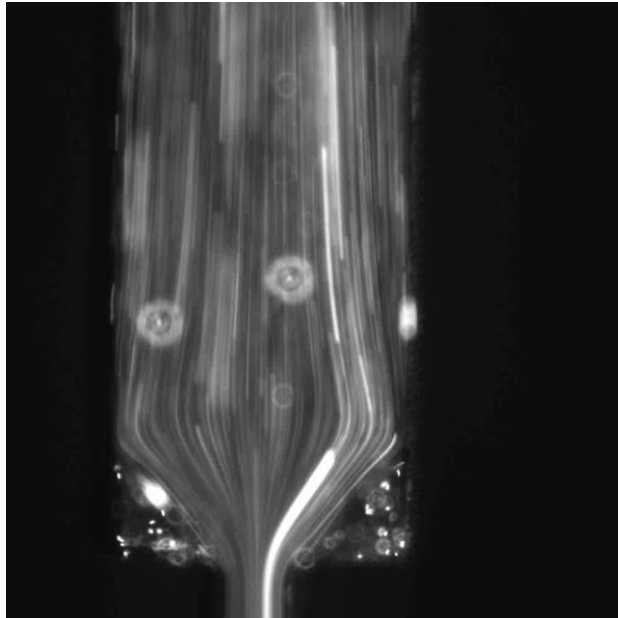
|                     | 뉴턴유체                                                                                                   | power-law유체                                                                                                                                                          |
|---------------------|--------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| a) 위판을 당겨준<br>평판유동  | $v_1 = \frac{V}{H} x_2$                                                                                | $v_1 = \frac{V}{H} x_2$                                                                                                                                              |
| b) 압력에 의한<br>평판유동   | $v_x = \frac{ \Delta P  h^2}{2\eta L} \left( 1 - \left( \frac{y}{H} \right)^2 \right)$                 | $v_x = \frac{n h}{n+1} \left( \frac{H  \Delta P }{m L} \right)^{1/n} \left( 1 - \left( \frac{ y }{H} \right)^{\frac{(n+1)}{n}} \right)$                              |
| c) 기울어진<br>사면에서의 유동 | $v_z = \frac{\rho g \delta^2 \sin \theta}{2\eta} \left( 1 - \left( \frac{x}{\delta} \right)^2 \right)$ | $v_z = \frac{n \delta}{n+1} \left( \frac{\rho g \sin \theta}{m} \right)^{1/n} \delta^{(1+n)/n} \left( 1 - \left( \frac{y}{\delta} \right)^{\frac{(1+n)}{n}} \right)$ |
| d) 파이프에서의<br>유동     | $v_z = \frac{ \Delta P  R^2}{4\eta L} \left( 1 - \left( \frac{r}{R} \right)^2 \right)$                 | $u_z = \frac{n R}{n+1} \left( \frac{R  \Delta P }{2 m L} \right)^{1/n} \left( 1 - \left( \frac{r}{R} \right)^{\frac{n+1}{n}} \right)$                                |

\*  $\rho$ : 유체의 밀도,  $\dot{\gamma}$ : 유체의 점도,  $g$ : 중력가속도

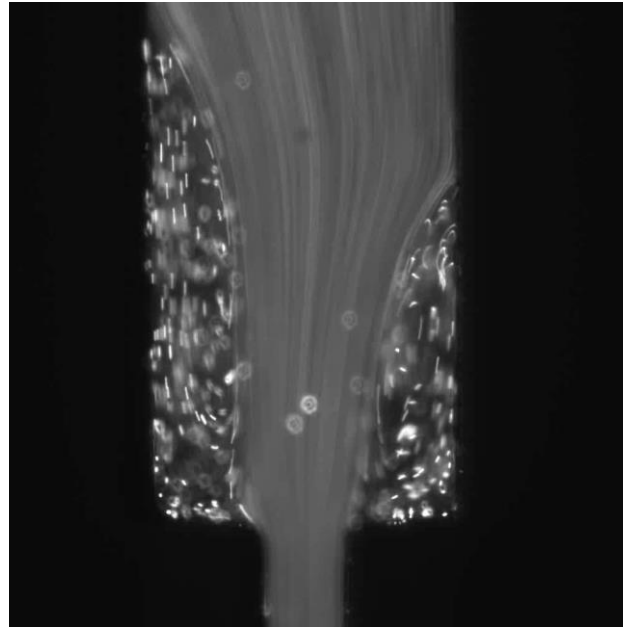


**55vol% well-dispersed  
alumina suspension at 0.3 /s**

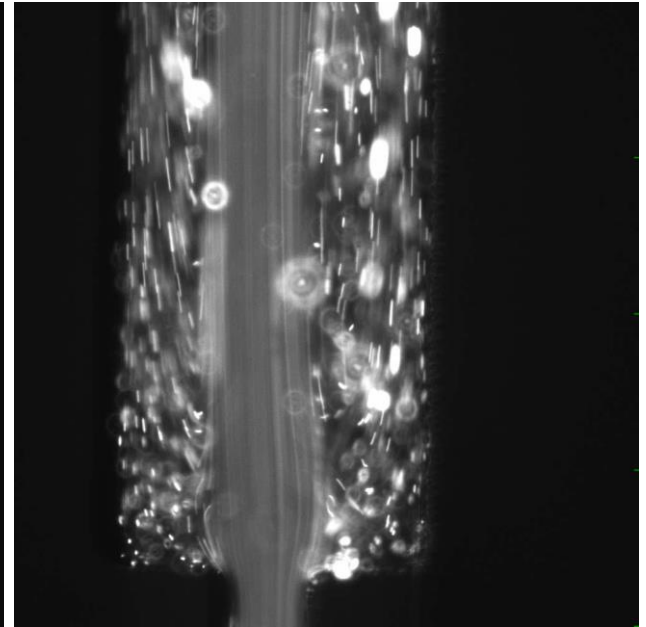




5M 0.7wt% PEO  
 $Wi = 79$



5M 1.0wt% PEO  
 $Wi = 130$



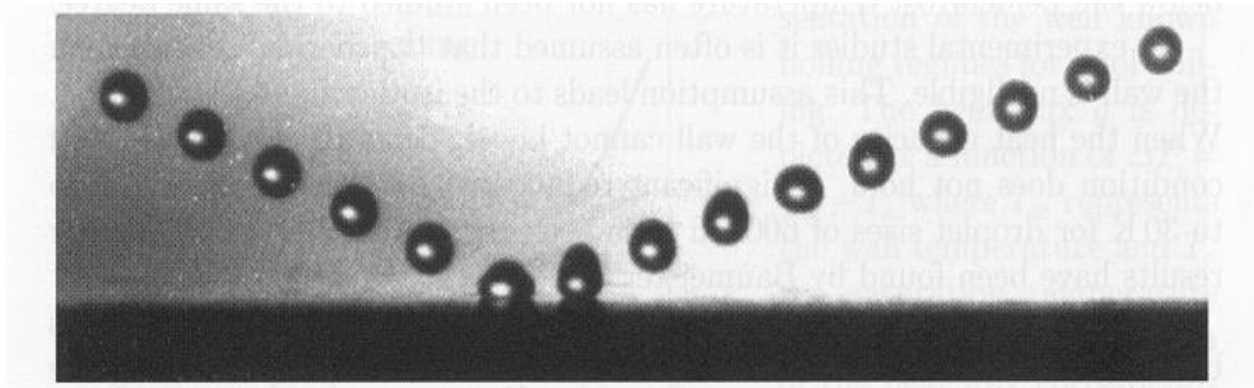
5M 0.7wt% PEO  
 $Wi = 145$



**유체 (fluid)**

# 유변학

- 물질 (복잡유체)의 유동과 변형에 관한 학문
- 고체/액체
- 탄성/점성
- 후크의 법칙/ 뉴턴의 법칙



# 막대오름 현상



$$= \begin{pmatrix} T_{11} & T_{12} & T_{13} \\ T_{21} & T_{22} & T_{23} \\ T_{31} & T_{32} & T_{33} \end{pmatrix}$$

# 샴푸



# 녹말용액에서 걷기



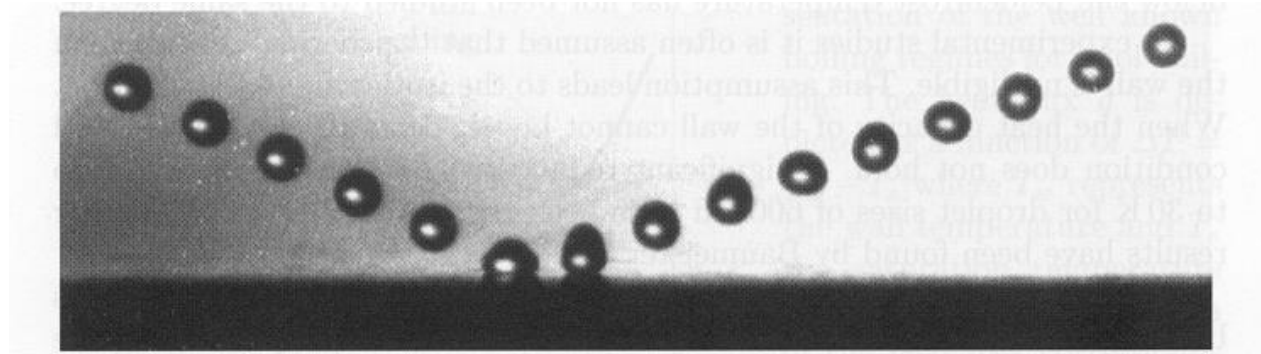
# 빅뱅이론



# 점탄성

- 구약성서 사사기:  
"The mountains flowed before the Lord"  
"주님 앞에서 산이 진동하였다"
- Deborah 수,  $De$  = 물질의 특성시간 / 공정의 특성시간

$$De = \lambda / t$$

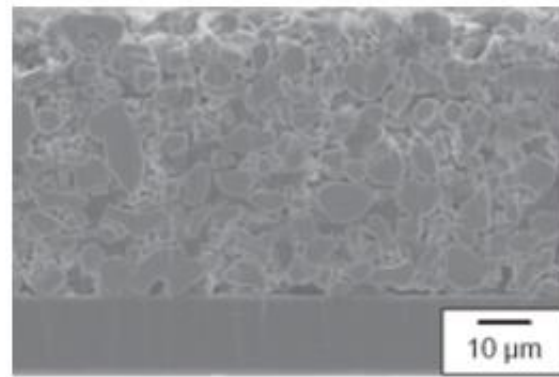




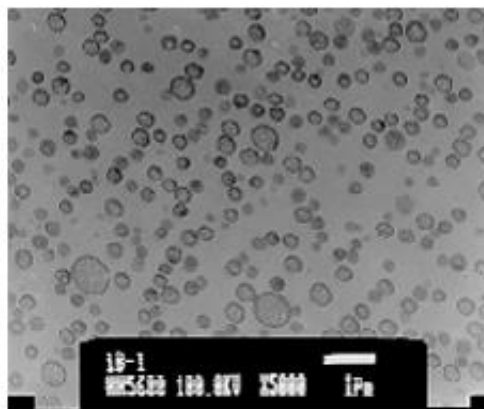




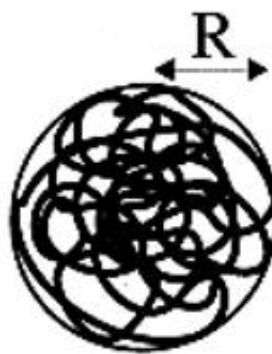
(a) 샴푸



(b) 배터리 전극

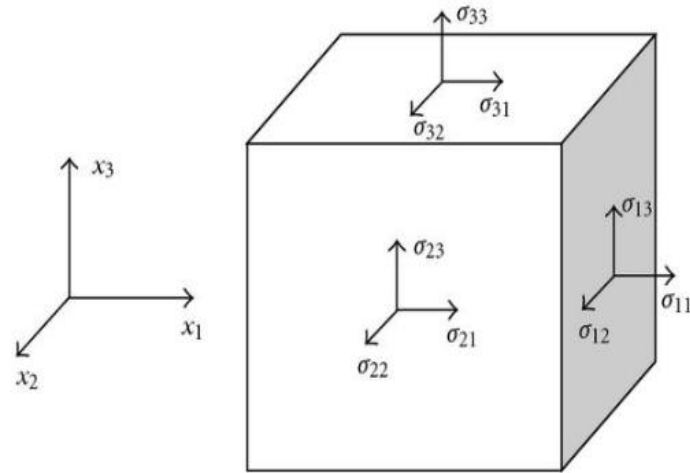


(c) ABS 수지



(d) 고분자

응력(stress): 단위면적 당 작용하는 힘



$$\underline{\underline{\tau}} = \begin{pmatrix} \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & \tau_{33} \end{pmatrix}_{123}$$

What is measured is the total stress,  $\underline{\underline{\Pi}}$  :

$$\underline{\underline{\Pi}} = \begin{pmatrix} p + \tau_{11} & \tau_{12} & \tau_{13} \\ \tau_{21} & p + \tau_{22} & \tau_{23} \\ \tau_{31} & \tau_{32} & p + \tau_{33} \end{pmatrix}_{123}$$

First normal stress  
difference

$$N_1 \equiv \Pi_{11} - \Pi_{22} = \tau_{11} - \tau_{22}$$

Second normal stress  
difference

$$N_2 \equiv \Pi_{22} - \Pi_{33} = \tau_{22} - \tau_{33}$$

SHEAR:

$$\underline{\underline{\tau}} = \begin{pmatrix} \tau_{11} & \tau_{12} & 0 \\ \tau_{21} & \tau_{22} & 0 \\ 0 & 0 & \tau_{33} \end{pmatrix}_{123}$$

In shear flow, three stress  
quantities are measured

$$\tau_{21}, N_1, N_2$$

In elongational flow, two stress  
quantities are measured

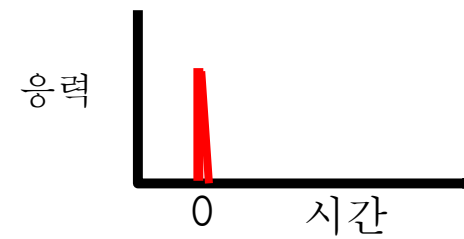
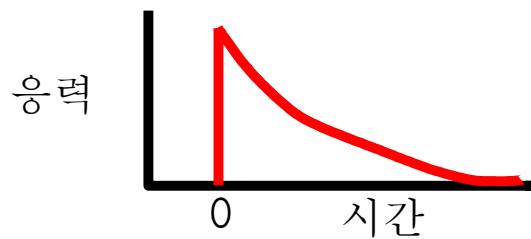
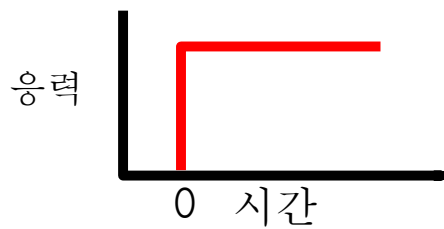
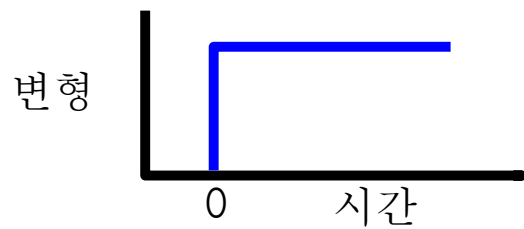
$$\tau_{33} - \tau_{11}, \tau_{22} - \tau_{11}$$

ELONGATION:

$$\underline{\underline{\tau}} = \begin{pmatrix} \tau_{11} & 0 & 0 \\ 0 & \tau_{22} & 0 \\ 0 & 0 & \tau_{33} \end{pmatrix}_{123}$$

# 물질의 완화특성

고체 ----- 액체  
 이상고체 ----- 대부분의 물질 ----- 이상액체  
 탄성 ----- 점탄성 ----- 점성



# 물질의 완화특성

고체 ----- 액체  
 이상고체 ----- 대부분의 물질 ----- 이상액체  
 탄성 ----- 점탄성 ----- 점성

---


$$\tau = G\gamma$$

$$\tau = \eta\dot{\gamma}$$

$$\tau_p + We \left( \frac{\partial \tau_p}{\partial t} + u \cdot \nabla \tau_p - (\nabla u)^T \cdot \tau_p - \tau_p \cdot \nabla u \right) = \beta \left( \nabla u + (\nabla u)^T \right)$$