## 457.646 Topics in Structural Reliability In-Class Material: Class 10

### **(a)** Second moment reliability index $\beta_{MVFOSM}$

#### MVFOSM

- Failure :  $g(\mathbf{x}) \le 0$  (NOT "elementary")
- Use ( ) & ( ) only. Therefore, can't compute P<sub>f</sub> (index, not method)
   Ang & Cornell (1974) ASCE Journal of Structural Engineering



i.e. equivalent limit-state functions could give different  $\beta_{MVFORM}$ 

$$g_{1}(x) = X_{1}^{2} + 3X_{2} < 0$$

$$g_{2}(x) = \frac{g_{1}(x)}{X_{1}^{2}} = 1 + 3\frac{X_{2}}{X_{1}^{2}} < 0$$
equivalent  $\Rightarrow$  the same  $\beta_{MVFORM}$ ?

#### Example: lack of invariance of second order reliability methods

Consider a structural reliability problem with two random variables  $X_1$  and  $X_2$ . The mean vector and the covariance matrix of  $X_1$  and  $X_2$  are

$$\mathbf{M}_{\mathbf{x}} = \begin{bmatrix} 5\\10 \end{bmatrix}, \quad \mathbf{\Sigma}_{\mathbf{x}\mathbf{x}} = \begin{bmatrix} 4 & 5\\5 & 25 \end{bmatrix}$$

 $\begin{aligned} \underline{\mathbf{Case 1:}} & g(X_1, X_2) = X_1^2 + 3X_2 \\ \text{Gradient } \nabla g = [2X_1 \quad 3]. \text{ At the mean point } \mathbf{X} = \mathbf{M}_{\mathbf{X}}, \ \nabla g = \begin{bmatrix} 10 \quad 3 \end{bmatrix}. \\ \text{First order approximation on } \mu_g \text{ and } \sigma_g^2: \\ \mu_g &\cong 5^2 + 3 \times 10 = 55 \\ \sigma_g^2 &\cong \nabla g \boldsymbol{\Sigma}_{\mathbf{X}\mathbf{X}} \nabla g^{\mathsf{T}} = 925 \\ \beta_{MVFOSM} &= \frac{\mu_g}{\sigma_g} = \frac{55}{\sqrt{925}} = 1.81 \\ P_f &= \Phi(-1.81) = 0.0351 \\ \\ \underline{\mathbf{Case 2:}} & g(X_1, X_2) = 1 + \frac{3X_2}{X_1^2} \\ \nabla g &= [-6X_2X_1^{-3} \quad 3X_1^{-2}]. \\ \text{At the mean point } \mathbf{X} = \mathbf{M}_{\mathbf{X}}, \ \nabla g &= [-0.48 \quad 0.12]. \\ \mu_g &\cong 1 + 3 \times 10/25 = 2.20 \\ \sigma_g^2 &\cong \nabla g \boldsymbol{\Sigma}_{\mathbf{X}\mathbf{X}} \nabla g^{\mathsf{T}} = 0.706 \\ \beta_{MVFOSM} &= \frac{\mu_g}{\sigma_g} = \frac{2.20}{\sqrt{0.706}} = 2.62 \end{aligned}$ 

Although the two limit-state functions are equivalent ones with the same failure domains, the second order reliability method yields different reliability indices and failure probability estimates.

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### Summary:

 $P_f = \Phi(-2.62) = 0.00440$ 

$$\beta_{SM} = \frac{\mu_M}{\sigma_M} = \frac{\mu_R - \mu_S}{\sqrt{\sigma_R^2 + \sigma_S^2 - 2\sigma_R \sigma_S \rho_{RS}}}$$
$$\beta_{SF} = \frac{\mu_F}{\sigma_F}, \text{ for LN } \beta_{SF} = \frac{\lambda_R - \lambda_S}{\sqrt{\zeta_R^2 + \zeta_S^2 - 2\zeta_R \zeta_S \rho_{\ln R \ln S}}}$$
$$\beta_{MVFOSM} = \frac{\mu_g^{FO}}{\sigma_g^{FO}} = \frac{g(\mathbf{M}_{\mathbf{X}})}{\nabla g(\mathbf{M}_{\mathbf{X}}) \Sigma_{\mathbf{XX}} \nabla g(\mathbf{M}_{\mathbf{X}})^{\mathrm{T}}} \quad (\text{Oct1974})$$

# ${\ensuremath{\textcircled{@}}}$ Hasofer-Lind Reliability Index, $\,\beta_{_{\mathit{HL}}}\,$ (JEM, May 1974)





### **Linear Limit-State Function**

$$g(\mathbf{x}) = a_0 + \mathbf{a}^{\mathrm{T}} \mathbf{x}$$
  
=  $a_0 + \mathbf{a}^{\mathrm{T}} ($  )  
=  $a_0 + \mathbf{a}^{\mathrm{T}} \mathbf{M} + \mathbf{a}^{\mathrm{T}} \mathbf{D} \mathbf{L} \mathbf{u}$   
=  $b_0 + \mathbf{b}^{\mathrm{T}} \mathbf{u} = G(\mathbf{u})$ 

VS

$$\beta = \frac{\mu_G}{\sigma_G} = \frac{b_0}{\|\mathbf{b}\|}$$



Can have +/\_ sign

always positive

For 
$$G(\mathbf{u}) = b_0 + \mathbf{b}^{\mathrm{T}}\mathbf{u}$$



 $b_o = G(\mathbf{0}) < 0$ (in failure domain)  $\beta < 0$  $b_o = G(\mathbf{0}) > 0$ (in safe domain)  $\beta > 0$  Seoul National University Dept. of Civil and Environmental Engineering Instructor: Junho Song junhosong@snu.ac.kr

i. 
$$\hat{\boldsymbol{\alpha}} = -\frac{\nabla G}{\|\nabla G\|}$$
 : "Negative normalized gradient vector"

: Unit row vector pointing toward the \_\_\_\_\_ domain

e.g. linear function : 
$$\hat{\boldsymbol{\alpha}} = -\frac{\mathbf{b}^{\mathrm{T}}}{\|\mathbf{b}\|}$$

ii.  $\mathbf{u}^*$  : "Design point"

"Most probable failure point (MPP)"

"Beta point"

e.g. linear function : 
$$\mathbf{u}^* \equiv -b_0 \frac{\mathbf{b}}{\|\mathbf{b}\|^2}$$

iii.

$$\beta_{HL} \equiv \hat{\alpha} \mathbf{u}^*$$

### Hasofer-Lind Reliability Index

 $\begin{cases} |\beta_{HL}| : \text{distance between origin and } \mathbf{u}^* \\ \text{sign} : \text{directions of } \hat{\boldsymbol{\alpha}} \text{ and } \mathbf{u}^* \end{cases}$ 

e.g. linear function : 
$$\beta_{HL} = \frac{b_0}{\|\mathbf{b}\|} \left( = \frac{\mu_G}{\sigma_G} \right)$$

$$P_{f} = F_{u_{g}}(-\beta_{HL})$$

$$\beta > 0 \quad 0 \quad \beta < 0$$
(reliable) (less reliable) What if  $\mathbf{X} \sim N$ 

What if 
$$\mathbf{X} \sim N(\mathbf{M}_{\mathbf{X}}, \sum_{\mathbf{X}\mathbf{X}})$$
 and  $g(\mathbf{x})$  linear?

$$\Rightarrow G, g \sim N$$
$$P_f = \Phi(-\beta_{HL})$$