

5. Electrode Processes 2

Learning subject

1. Butler-Volmer equation
2. Tafel plot
3. Mass transport

Learning objective

1. Understanding the relation between potential and current
2. Understanding Butler-Volmer equation and Tafel plot
3. Understanding limiting current from mass transport

1. Butler-Volmer equation

**Nernst equation : equilibrium expression → electrode reaction rate?
(kinetics)**

Electron transfer at an electrode

Reduction & oxidation at electrode are accomplished by heterogeneous electron transfer reactions since electron transfer occurs at the interface between electrode and solution → relationship between potential and rate of electrode reaction (which determine current)

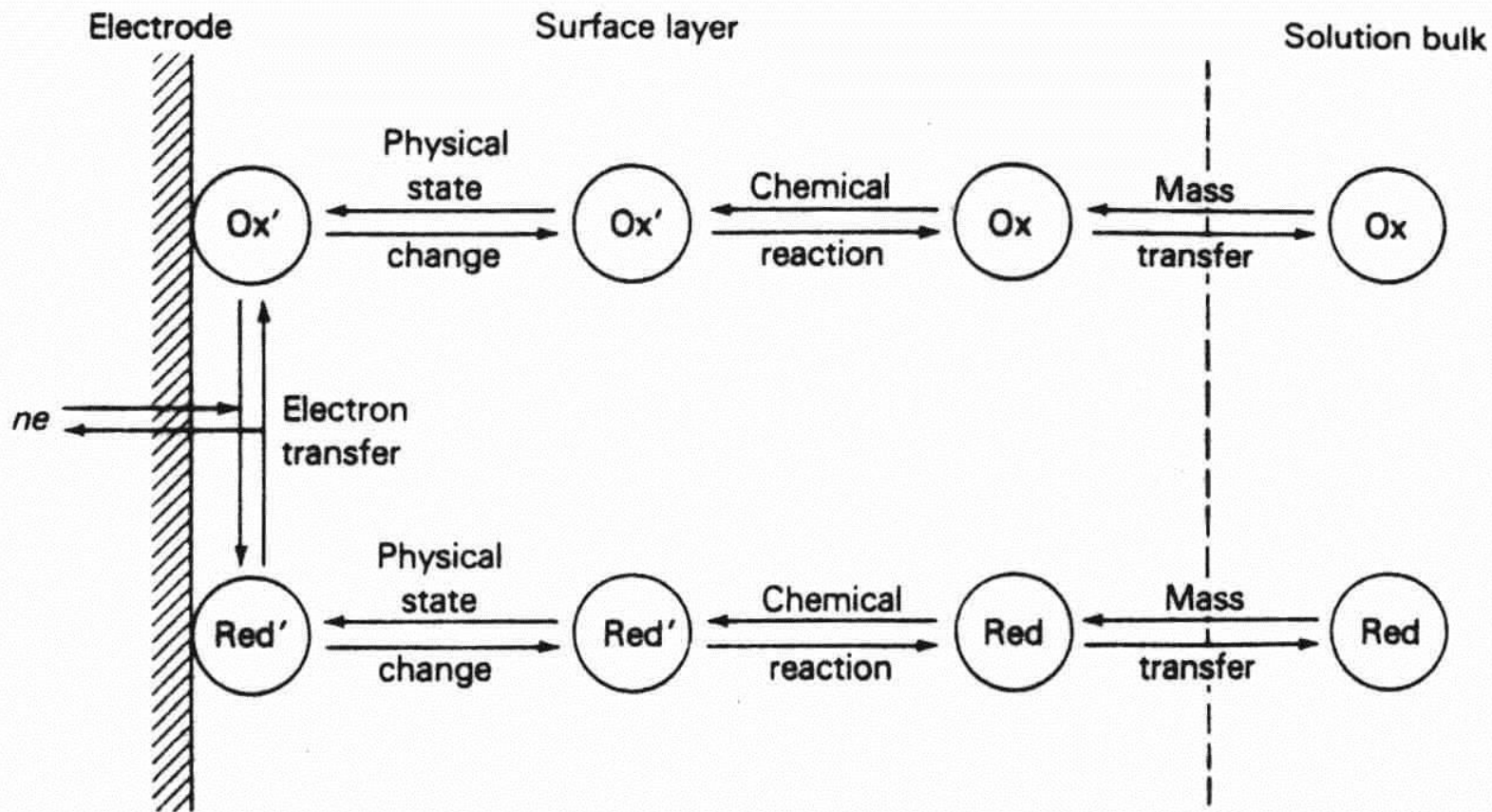
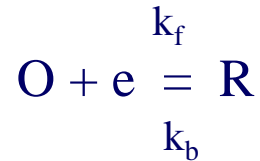


FIGURE 19-10 Steps in the reaction $\text{Ox} + ne \rightleftharpoons \text{Red}$ at an electrode. Note that the surface layer is only a few molecules thick. (Adapted from: A. J. Bard and L. R. Faulkner, *Electrochemical Methods*, p. 21, Wiley: New York, 1980. Reprinted by permission of John Wiley & Sons, Inc.)

Review of homogeneous kinetics

Dynamic equilibrium



Rate of the forward process

$$v_f \text{ (M/s)} = k_f C_A$$

Rate of the reverse reaction

$$v_b = k_b C_B$$

Rate const, k_f, k_b : s^{-1}

Net conversion rate of A & B

$$v_{\text{net}} = k_f C_A - k_b C_B$$

At equilibrium, $v_{\text{net}} = 0$

$$k_f/k_b = K = C_B/C_A$$

*kinetic theory predicts a const conc ratio at equilibrium, just as thermodynamics

At equilibrium, kinetic equations \rightarrow thermodynamic ones

\rightarrow dynamic equilibrium (equilibrium: nonzero rates of k_f & k_b , but equal)

Exchange velocity

$$v_0 = k_f(C_A)_{\text{eq}} = k_b(C_B)_{\text{eq}}$$

Relationship between current and heterogeneous rate constants

Faraday's law: chemical reaction \rightarrow electric **current** \rightarrow an indicator of **reaction rate**

Amount of electricity,

$$q = nFN$$

n: electron number, N: number of moles, F: Faraday constant (96485 C/mol)



$$q/2F = -\Delta N_{\text{PbSO}_4} = -\Delta N_{\text{H}_2\text{O}}/2 = \Delta N_{\text{PbO}_2} = \Delta N_{\text{HSO}_4^-} = \Delta N_{\text{H}^+}/3$$

The passage of two moles of electrons = destroy one mole of PbSO_4 , destroy two moles of water, create one mole of PbO_2 ...

If we generalize this result and apply it to the oxidation reaction,



Then,

$$q/nF = -\Delta N_{\text{R}} = \Delta N_{\text{O}}$$

$$I = dq/dt = nFdN/dt$$

$$I/nF = -dN_{\text{R}}/dt = dN_{\text{O}}/dt = \text{rate}$$



$$E_{\text{n}} = E^0 - RT/F \ln(c_{\text{R}}/c_{\text{O}})$$

depends on the concentrations of the two species and E^0

“=” means,



At E_{n} (E_{eq}), the rates

$$\mathbf{r_{ox}(E_{\text{n}}) = r_{rd}(E_{\text{n}})}$$

because no net reaction occurs. The rate r depend on the electrode potential E .

What exactly is meant by the “rate” of an electrode reaction?

At the potential of E,

$$\mathbf{r_{net}(E) = r_{ox}(E) - r_{rd}(E)}$$

net reaction rate: the rate at which R is destroyed , or the rate at which O is created, per unit area of electrode (unit of molm⁻²s⁻¹) “heterogeneous reaction rate”

$$r_{net}(E) = -(1/A)(dN_R/dt) = (1/A)(dN_O/dt)$$

$$\mathbf{r_{ox}(E) = k_{ox}(E)c_R^s}$$

“s” means that the concentrations at the electrode surface

k_{ox}(E): oxidative rate constant (ms⁻¹)

$$\mathbf{r_{rd}(E) = k_{rd}(E)c_O^s}$$

k_{rd}(E): reductive rate constant

$$r_{net}(E) = I/nAF = i/nF$$

From $r_{\text{net}}(E) = r_{\text{ox}}(E) - r_{\text{rd}}(E)$, $r_{\text{ox}}(E) = k_{\text{ox}}(E)c_{\text{R}}$, $r_{\text{rd}}(E) = k_{\text{rd}}(E)c_{\text{O}}$

Relate the faradaic **current** and **rate constants**

$$i = nF[k_{\text{ox}}c_{\text{R}}^s - k_{\text{rd}}c_{\text{O}}^s]$$

cf) $k_{\text{ox}} = k_{\text{a}}$ of anode, $k_{\text{rd}} = k_{\text{c}}$ of cathode

when $k_{\text{ox}}(E)c_{\text{R}}^s = k_{\text{rd}}(E)c_{\text{O}}^s \rightarrow$ zero current \rightarrow equilibrium

when $k_{\text{ox}}(E)c_{\text{R}}^s > k_{\text{rd}}(E)c_{\text{O}}^s \rightarrow$ anodic current (i_{a}) \rightarrow oxidation of R to O

when $k_{\text{ox}}(E)c_{\text{R}}^s < k_{\text{rd}}(E)c_{\text{O}}^s \rightarrow$ cathodic current (i_{c}) \rightarrow reduction of O to R

Potential dependence of heterogeneous rate constants

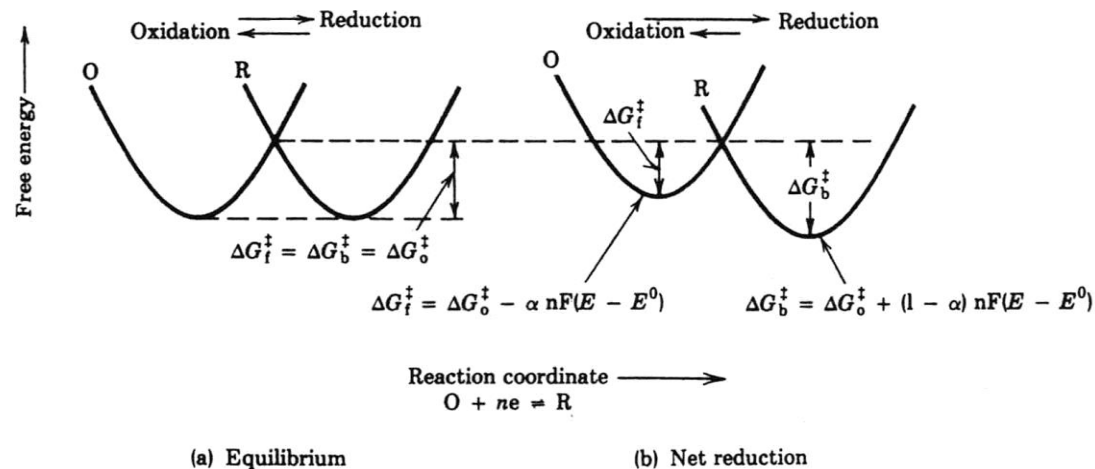


Transition state model,

$$k_{rd} = k_f = A \exp(-\Delta G_f^\ddagger / RT)$$

where ΔG_f^\ddagger is the free energy of activation and A is a frequency factor which accounts for the rate of collision of the electroactive molecule with the electrode surface

cf) $k_{ox} = k_b$ of anode, $k_{rd} = k_f$ since forward direction (\rightarrow) is reduction one.



(a) equilibrium between O and R

O \rightarrow R: pass over the activation free energy barrier, ΔG_f^\ddagger

R \rightarrow O: pass over the activation free energy barrier, ΔG_b^\ddagger

At equilibrium, $\Delta G_f^\ddagger = \Delta G_b^\ddagger \rightarrow$ probability of electron transfer is the same in each direction \rightarrow no net current $\rightarrow i_c + i_a = 0$

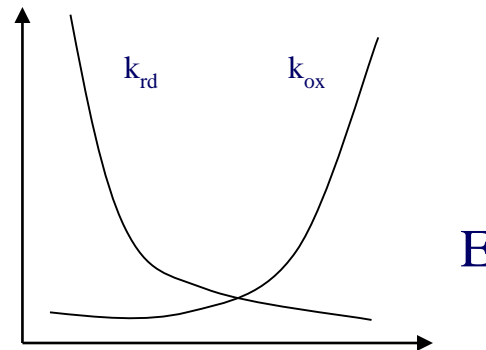
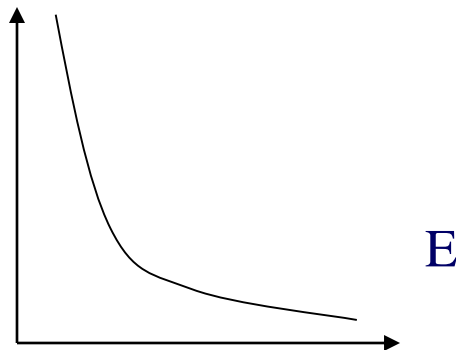
No net current means same rates between forward and backward (not zero current)
 \rightarrow **exchange current i_0** at equilibrium; $i_0 = i_c = -i_a$

$$i_0 \uparrow \text{ as } \Delta G \downarrow$$

(b) net reduction

applying negative potentials

reduction: more negative potential $\rightarrow k_f \uparrow, k_b \downarrow$



Negative potential $E \rightarrow$ lower ΔG_f^\ddagger and raise ΔG_b^\ddagger

Potential change $E - E^0 \rightarrow$ free energy change $-nF(E-E^0) \Rightarrow$ part of this energy change (factor α) \rightarrow decrease in the activation barrier for reduction (forward reaction) ; part (factor $(1 - \alpha)$) \rightarrow increase in the activation barrier for oxidation

$$\Delta G_f^\ddagger = \Delta G^{0\ddagger} - \alpha nF(E-E^0)$$

$$\Delta G_b^\ddagger = \Delta G^{0\ddagger} + (1-\alpha)nF(E-E^0)$$

Applying potential to the electrode \rightarrow activation free energy barrier

α ; “**transfer coefficient**” or “**symmetry factor**” since α is a measure of the symmetry of the energy barrier \rightarrow a symmetrical energy barrier ($\alpha = 0.5$), real systems: $0.3 \sim 0.7$ semiconductor: ~ 0 or ~ 1



Actually,



$\alpha, -(1-\alpha)$; orders of the reductive and oxidative processes

another interpretation of α : increasing electrochemical activity of electrons \rightarrow it accelerates the reductive process and retards the oxidative process $\rightarrow \alpha$ is the fraction of the increase r_{rd} , $(1-\alpha)$ is the fraction that diminishes r_{ox}
 $\alpha = 0.5$; perfect symmetric, these fractions are equal

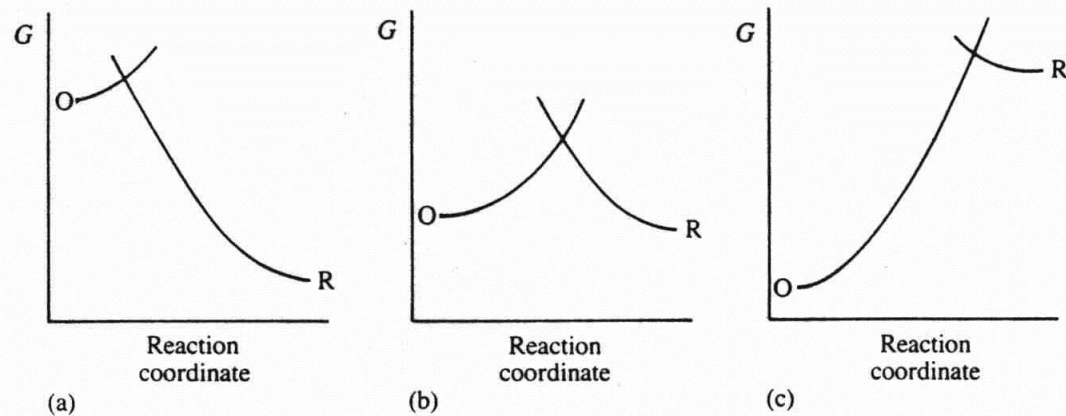


Fig. 4.4 Energy profiles for the cases (a) $\alpha_c \approx 0$; (b) $\alpha_c \approx \frac{1}{2}$; (c) $\alpha_c \approx 1$.

Arrhenius form,

$$k_f = k^0 \exp[-\alpha n F (E - E^0) / RT]$$

$$k_b = k^0 \exp[(1 - \alpha) n F (E - E^0) / RT]$$

Where k^0 is the standard rate constant, $k_f = k_b = k^0$ at E^0 . $k^0, \alpha \rightarrow$ rate constant.
 Relationship between potential and rate

Relationship between current and potential

$$i_c = nF c_O^s k_f \quad \text{and} \quad i_a = -nF c_R^s k_b$$

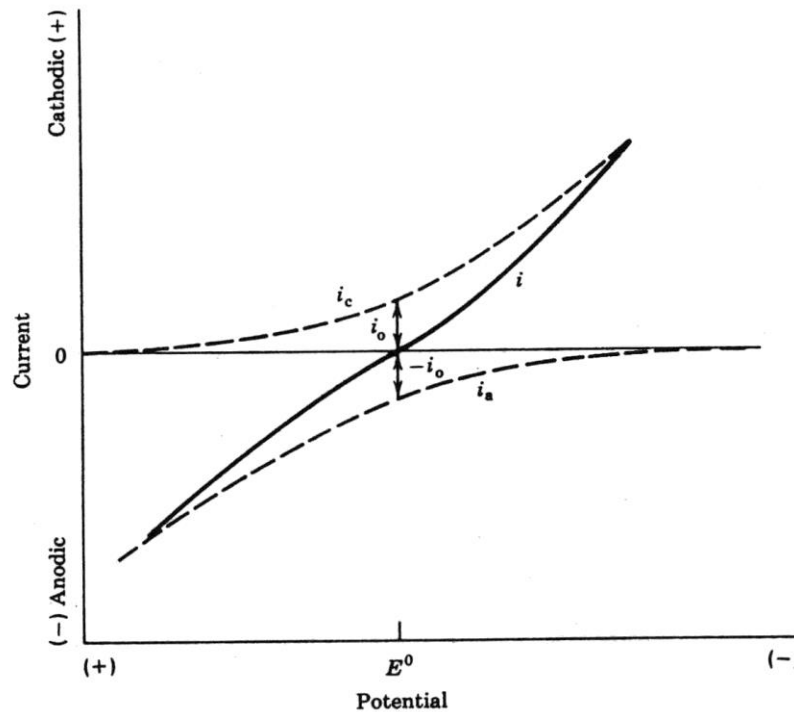
$$i_c = nF k^0 c_O^s \exp\{-\alpha nF(E-E^0)/RT\}$$
$$i_a = -nF k^0 c_R^s \exp\{(1-\alpha)nF(E-E^0)/RT\}$$

$$i = i_c + i_a$$

Butler-Volmer equation

$$i = nF k^0 [c_O^s \exp\{-\alpha nF(E-E^0)/RT\} - c_R^s \exp\{(1-\alpha)nF(E-E^0)/RT\}]$$

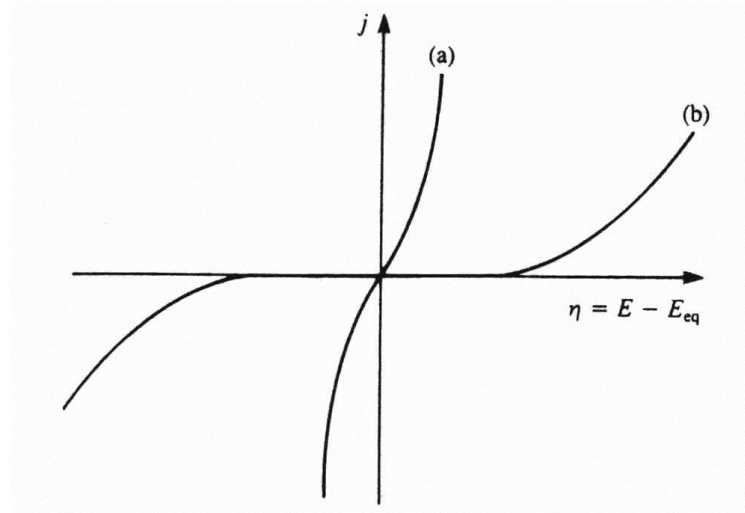
This relationship links the faradaic current, electrode potential, the concentrations of electroactive species at the electrode surface



i and i_c and i_a as a function of potential E ; negative $E \uparrow \rightarrow i_c \uparrow$ (forward reaction),
 positive $E \uparrow \rightarrow i_a \uparrow$ (backward)

k^0 ; $1 \sim 50 \text{ cm s}^{-1}$ for very fast reactions, $10^{-9} \text{ cm s}^{-1}$ for very slow reactions.

Exchange current density i_0 ; $10 \text{ Acm}^{-2} \sim 1 \text{ pAcm}^{-2}$



The effect of the value of k_0 on the current density close to E_{eq} (a) k_0 large (b) k_0 smaller

At equilibrium, zero net current, $i_c = -i_a$

Butler-Volmer equation (kinetics) \rightarrow Nernst equation (thermodynamics)

$$E = E^0 - (RT/nF)\ln(c_R^s/c_O^s)$$

$$i_0 = i_c = nFk^0c_O^s\exp\{-\alpha nF(E-E^0)/RT\} = i_a = -nFk^0c_R^s\exp\{(1-\alpha)nF(E-E^0)/RT\} \Rightarrow$$

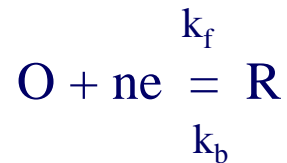
$$i_0 = nFk^0(c_O^s)^{1-\alpha}(c_R^s)^\alpha$$

high exchange current density \rightarrow high reaction rate

2. Tafel plot

Essentials of electrode reactions

*accurate kinetic picture of any dynamic process must yield an equation of the thermodynamic form in the limit of equilibrium



Equilibrium is characterized by the Nernst equation

$$E = E^{0'} + (RT/nF)\ln(C_o^*/C_R^*)$$

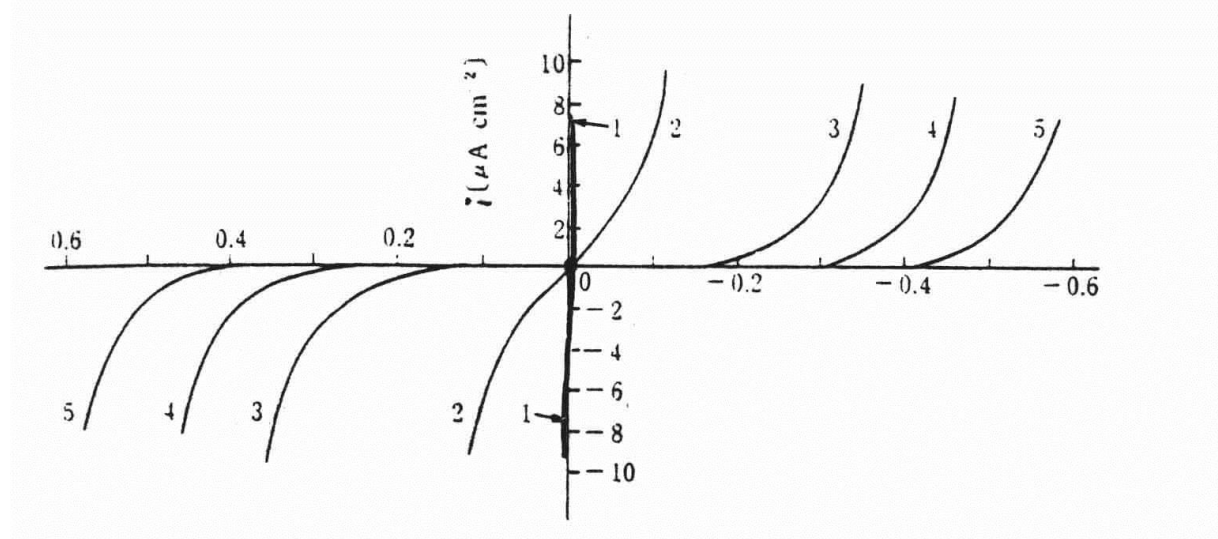
bulk conc

Kinetic: dependence of current on potential

Overpotential

$$\eta = a + b \log i$$

Tafel equation



The effect of exchange current density on overpotential

Butler-Volmer equation/ i_0

$$i = nFk^0 [c_O^s \exp\{-\alpha nF(E-E^0)/RT\} - c_R^s \exp\{(1-\alpha)nF(E-E^0)/RT\}]$$

and let $F/RT = f$, overpotential $\eta = E - E^0 \Rightarrow$ current-overpotential equation

$$i = i_0 [\exp(-\alpha n f \eta) - \exp((1-\alpha) n f \eta)]$$

$\eta \gg 0$ (oxidation, only O in bulk) $\rightarrow \exp(-\alpha n f \eta) \ll \exp((1-\alpha) n f \eta)$

$$i = -i_0 \exp((1-\alpha) n f \eta)$$

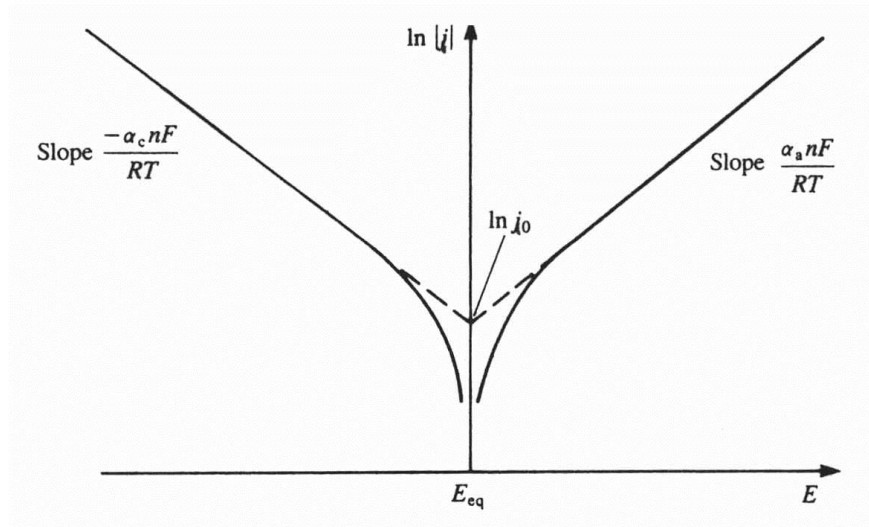
apply log,

$$\eta = -(RT/(1-\alpha)nF)\ln i_0 + (RT/(1-\alpha)nF)\ln |i|$$

for $\eta \ll 0$ (reduction), $\eta = (RT/\alpha nF)\ln i_0 - (RT/(\alpha nF))\ln |i|$

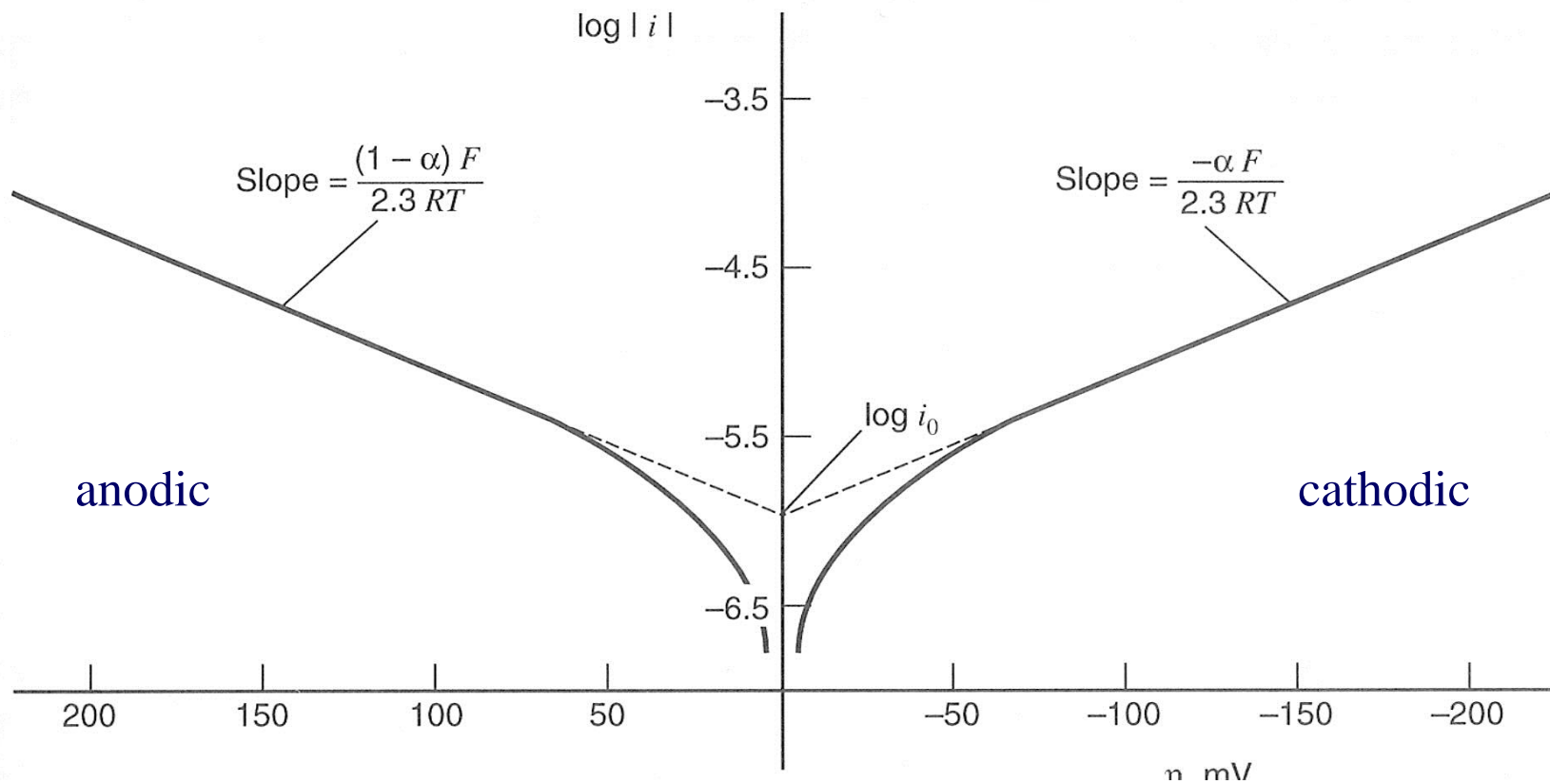
Tafel plot \rightarrow measure i_0 and α

$$E - E^0 = \eta = a \ln i_0 \pm b \ln |i|$$



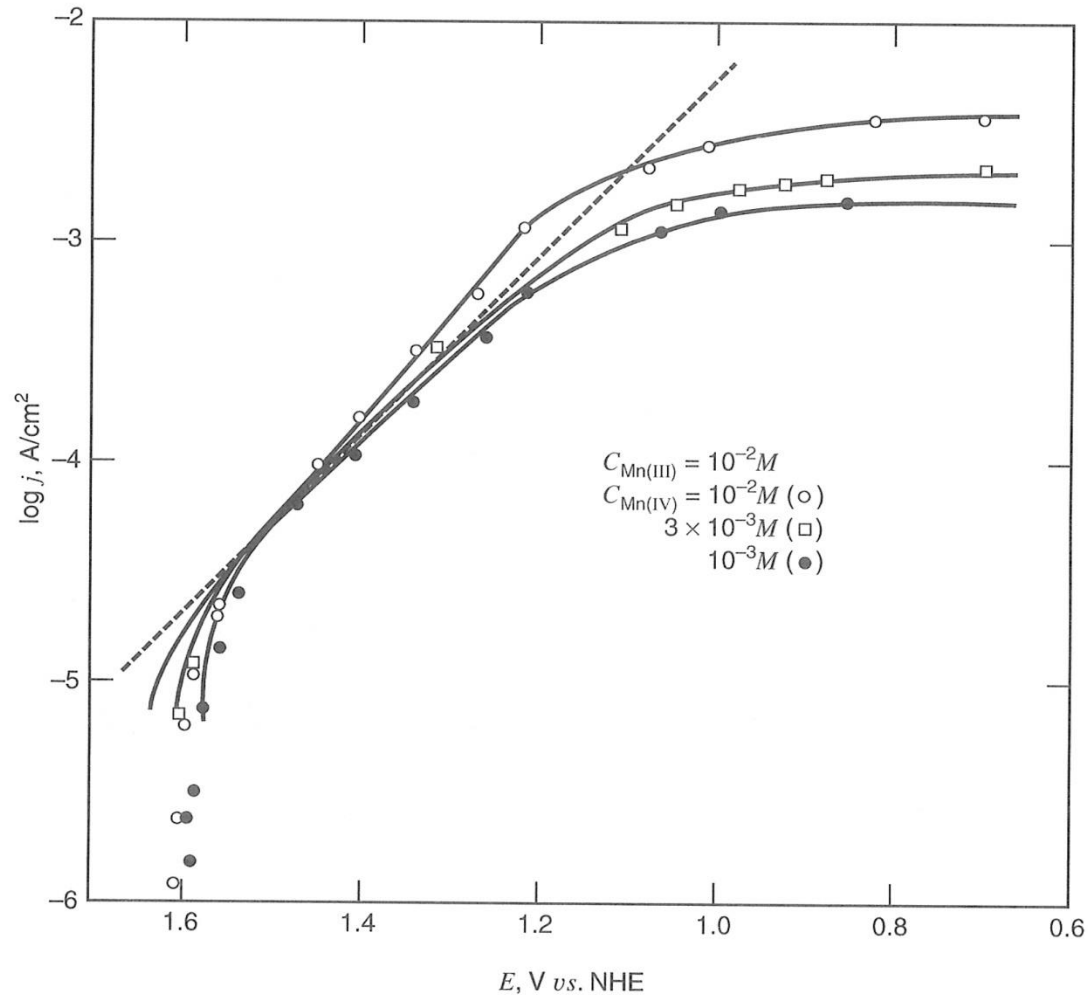
Plot of $\ln |i|$ vs. E showing how to measure i_0 and α from the slopes of the lines

Tafel plots (i vs. η) → evaluating kinetic parameters (e.g., i_0 , α)



e.g., real Tafel plots for Mn(IV)/Mn(III) system in concentrated acid

- At very large overpotential: mass transfer limitation



Summary of Butler–Volmer Kinetics and Useful Simplifications

1. General kinetics, applicable under all current density conditions; the general BV expression for η (solve numerically):

$$i_{\text{cell}} = i_o \left\{ \exp \left(\frac{\alpha_a F}{R_u T} \eta \right) - \exp \left(\frac{-\alpha_c F}{R_u T} \eta \right) \right\} \quad (4.52)$$

2. Low polarization, facile kinetics, linearized BV approximation (explicit η expression):

$$\eta = \pm \frac{i}{i_o} \frac{R_u T}{(\alpha_a + \alpha_c) F} \quad (4.53)$$

3. High polarization, Tafel approximation (explicit η expression):

$$\eta = \frac{R_u T}{\alpha_j F} \ln \left(\frac{i}{i_o} \right) \quad (4.54)$$

4. Both regions, $\alpha_a = \alpha_c$ sinh simplification (explicit η expression):

$$\frac{R_u T}{\alpha F} \sinh^{-1} \left(\frac{i_{\text{cell}}}{2i_o} \right) = \eta \quad (4.55)$$

3. Mass Transport

Mass transport

$$\text{rate} = k_a C_R^s - k_c C_O^s$$

Electrochemical reaction at electrode/solution interface: molecules in bulk solution must be transported to the electrode surface → “mass transfer”

$$C_O^b = C_O^s = C_R^s = C_R^b$$

Mechanisms for mass transport:

- (a) Migration: movement of a charged body under the influence of an electric field (a gradient of electric potential)
- (b) Diffusion: movement of species under the influence of gradient of chemical potential (i.e., a concentration gradient)
- (c) Convection: stirring or hydrodynamic transport

Nernst-Planck equation (diffusion + migration + convection)

$$J_i(x) = -D_i(\partial C_i(x)/\partial x) - (z_i F/RT)D_i C_i(\partial \phi(x)/\partial x) + C_i v(x)$$

Where $J_i(x)$; the flux of species i ($\text{molsec}^{-1}\text{cm}^{-2}$) at distance x from the surface, D_i ; the diffusion coefficient (cm^2/sec), $\partial C_i(x)/\partial x$; the concentration gradient at distance x , $\partial \phi(x)/\partial x$; the potential gradient, z_i and C_i ; the charge and concentration of species i , $v(x)$; the velocity (cm/sec)

1. Steady state mass transfer

steady state, $(\partial C/\partial t) = 0$; the rate of transport of electroactive species is equal to the rate of their reaction on the electrode surface

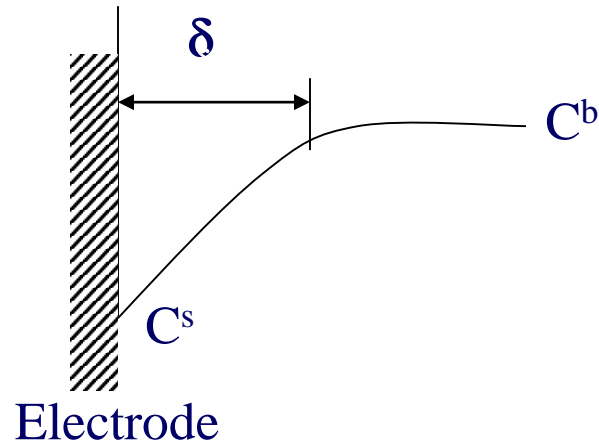
In the absence of migration,



The rate of mass transfer,

$$v_{mt} \propto (\partial C_R(x)/\partial x)_{x=0} = (C_R^b - C_R^s)/\delta$$

where x is distance from the electrode surface & δ : diffusion layer



$$v_{mt} = m_R [C_R^b - C_R^s]$$

where C_R^b is the concentration of R in the bulk solution, C_R^s is the concentration at the electrode surface

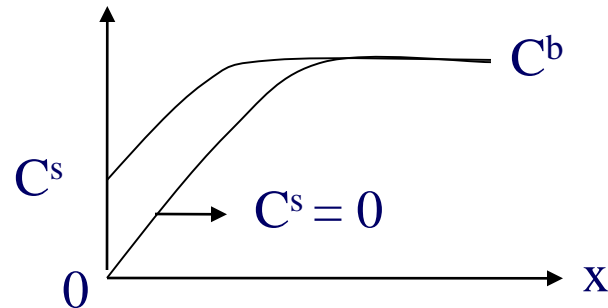
m_R is “mass transfer coefficient”

$$i = nFm_R [C_R^b - C_R^s]$$

$$i = -nFm_O [C_O^b - C_O^s]$$

largest rate of mass transfer of R when $C_R^s = 0 \rightarrow$ “limiting current”

$$i_{l,a} = nFm_R C_R^b$$



$$C_R^s / C_R^b = 1 - (i / i_{l,a})$$

And

$$C_R^s = [1 - (i / i_{l,a})] [i_{l,a} / nFm_R] = (i_{l,a} - i) / (nFm_R)$$

Same method,

$$C_O^s / C_O^b = 1 - (i / i_{l,c})$$

$$i_{l,c} = nFm_O C_O^b$$

$$C_O^s = [1 - (i / i_{l,c})] [i_{l,c} / nFm_O] = (i_{l,c} - i) / (nFm_O)$$

Put these equations to $E = E^0 - (RT/nF)\ln(C_R^s/C_O^s)$

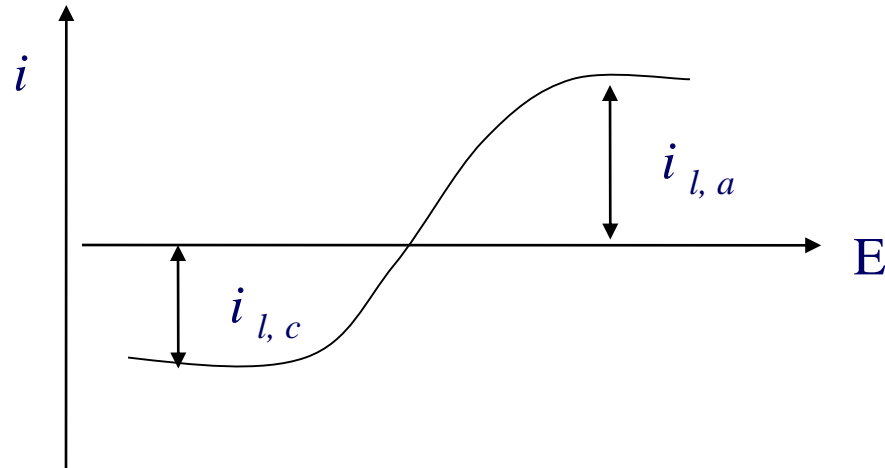
$$E = E^0 - (RT/nF)\ln(m_O/m_R) - (RT/nF)\ln[(i_{l,a} - i)/(i - i_{l,c})]$$

Let

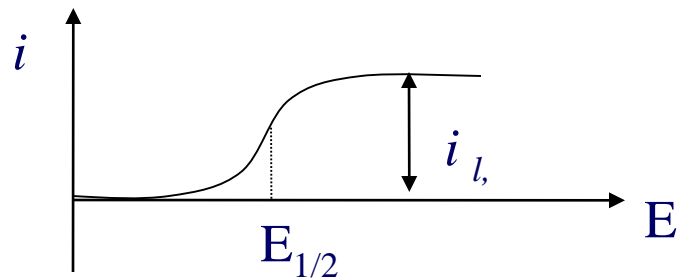
$$E_{1/2} = E^0 - (RT/nF)\ln(m_O/m_R)$$

Then,

$$E = E_{1/2} - (RT/nF)\ln[(i_{l,a} - i)/(i - i_{l,c})]$$



$E_{1/2}$, half-wave potential, independent of C_O^b and $C_R^b \rightarrow$ characteristic of the R/O system.



Reversibility:

reversible: $k^0 \gg m_O$ or $m_R \rightarrow$ kinetic rate constant \gg mass transport rate constant \rightarrow system is at equilibrium at the electrode surface and it is possible to apply the Nernst equation at any potential

irreversible: $k^0 \ll m_O$ or m_R

2. Non-steady state mass transport: diffusion control

The rate of diffusion depends on the concentration gradients

$$J = -D(\partial C/\partial x) \quad \text{Fick's first law}$$

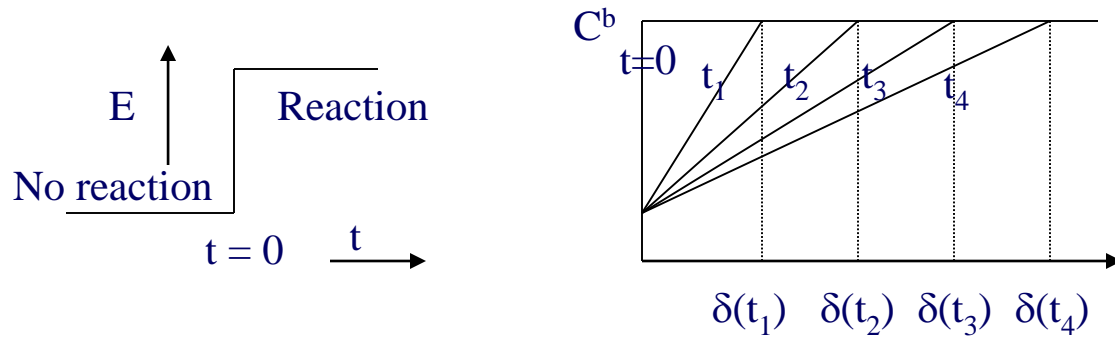
D: diffusion coefficient (cm²/sec)

The variation of concentration with time due to diffusion → Fick's second law

$$\partial C/\partial t = -D(\partial^2 C/\partial x^2) \quad \text{1-D}$$

$$J = -D(\partial C/\partial x) = i/nF$$
$$D(\partial C/\partial x) = D(C^b - C^s)/\delta = i/nF$$

Time-dependent, applying potential step E



Moles of species in diffusion layer = $\int i dt / nF \approx [C^b - C^s](A\delta(t)/2)$

Differentiating,

$$i/nF = [C^b - C^s](A d\delta(t)/2 dt) = D(C^b - C^s)/\delta(t)$$

$$d\delta(t)/dt = 2D/\delta(t), \delta(t) = 0 \text{ at } t = 0$$

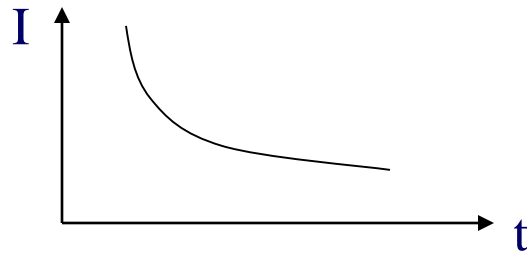
$$\delta(t) = 2\sqrt{(Dt)}$$

$$i/nF = (D^{1/2}/2t^{1/2}) [C^b - C^s]$$

diffusion layer grows with $t^{1/2}$ and current decays with $t^{-1/2}$

potential step (chronoamperometry), planar electrode: Cottrell equation (in Table)

constant current \rightarrow potential variation at time (chronopotentiometry): Sand equation ($t = \tau$ (transition time) at $C^s = 0$)



1. Polarization curve

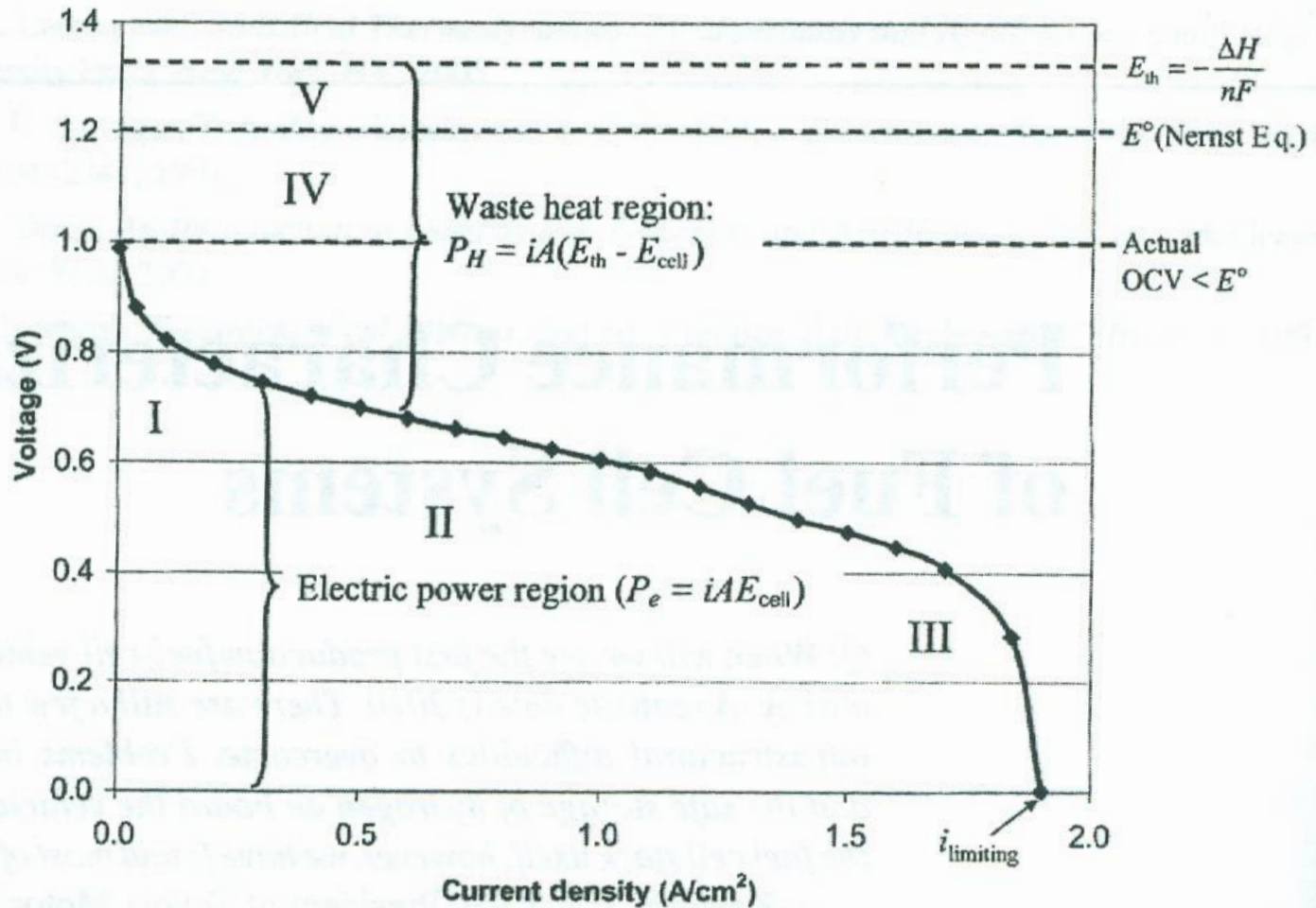


Figure 4.1 Typical polarization curve for fuel cell with significant kinetic, ohmic, concentration, and crossover potential losses.

hydrogen-air FC

-5 regions

- (i) Region I: activation (kinetic) overpotential at the electrodes
- (ii) Region II: ohmic polarization. Electric & ionic conduction loss
- (iii) Region III: concentration polarization. Mass transport limitations
- (iv) Region IV. Departure from Nernst thermodynamic equilibrium potential; undesired species crossover through electrolyte, internal currents from electron leakage, other contamination or impurity
- (v) Region V: the departure from the maximum thermal voltage; a result of entropy change which cannot be engineered

-Regions I, II, III are not discrete → all modes of loss contribute throughout the entire current range

-Heat: current x (thermal voltage – FC voltage)

& electrical generation: cell current x FC voltage

-FC voltage:

$$E_{\text{cell}} = E^{\circ}(T, P) - \eta_{a,a} - |\eta_{a,c}| - \eta_r - \eta_{m,a} - |\eta_{m,c}| - \eta_x \quad (4.1)$$