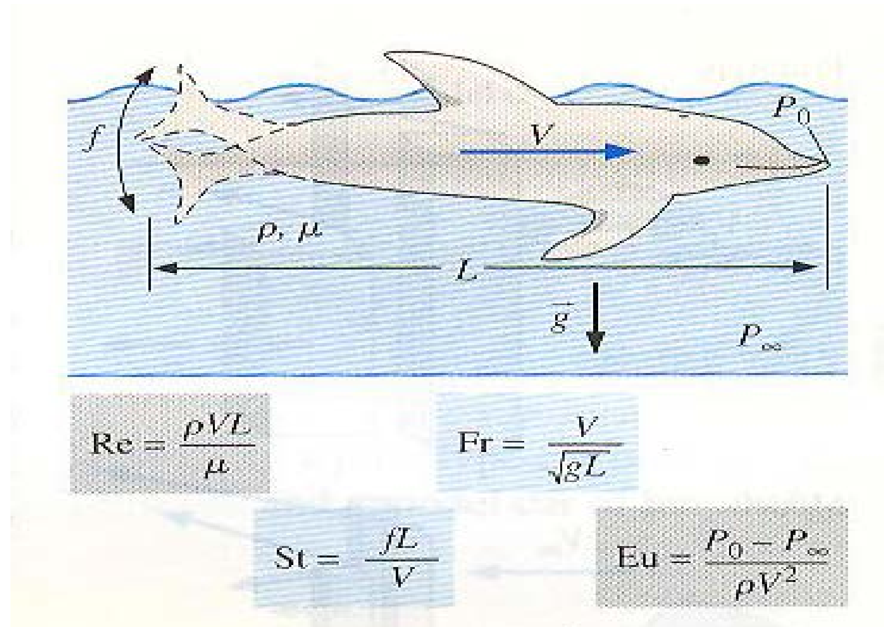
Chapter 8

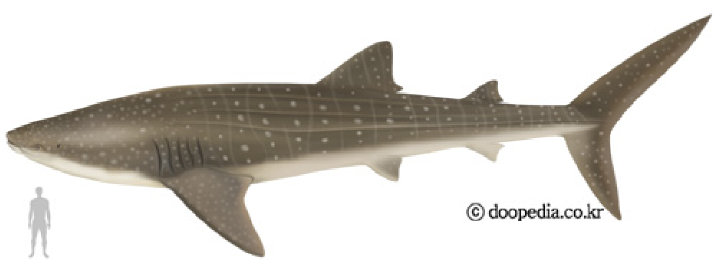
Similitude and Dimensional Analysis

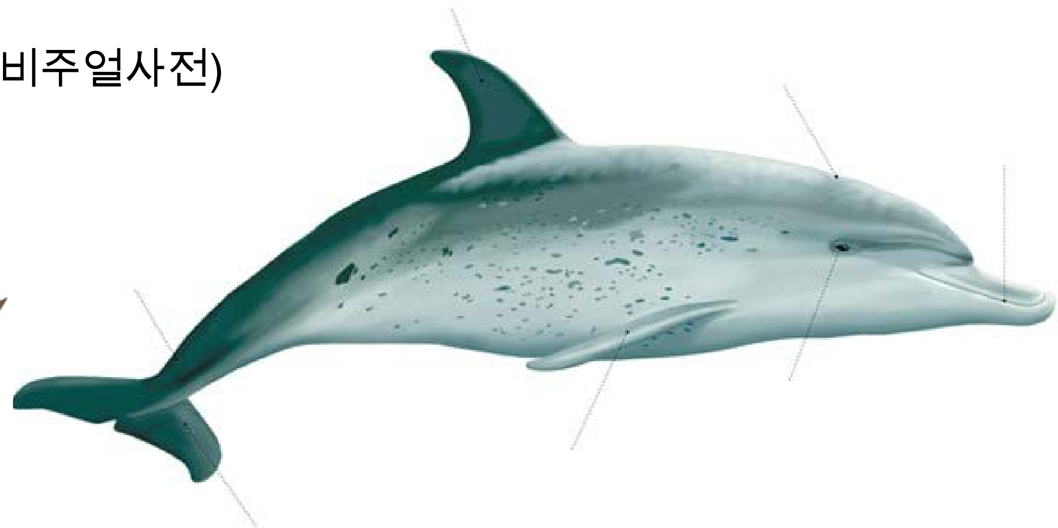


Chapter 8 Similitude and Dimensional Analysis

- 가슴지느러미 (pectoral fin): 헤엄치는 데 사용하는 골질 부속지. 안정감, 방향 감각, 정지, 체온 조절에 이용된다.
- 등지느러미 (dorsal fin): 헤엄치는 데 사용하는 등 중간의 부속지. 매우 촘촘한 섬유질 조직이며 안정감과 체온 조절을 담당한다.
- 꼬리지느러미 / 미기 (caudal fin): 힘차게 헤엄치는 데 사용되는 부속지. 단단한 연골로 이루어진 2개의 엽으로 갈라져 몸체의 뒤쪽 말단부에 수직으로 자리잡고 있으며, 추진 기능이 있다.
- 꼬리 (tail): 돌고래 몸의 말단 부분. 이 꼬리에 의해 수직 동작으로 전진할 수 있다. 척추에 붙은 강력한 근육으로 꼬리를 움직인다.

[Morphology of a dolphin] (브리태니커 비주얼사전)





Chapter 8 Similitude and Dimensional Analysis

Contents

Chapter 8 Similitude and Dimensional Analysis

Objectives

- Learn how to begin to interpret fluid flows
- Introduce concept of model study for the analysis of the flow phenomena that could not be solved by analytical (theoretical) methods
- Study laws of similitude which provide a basis for interpretation of model results
- Study dimensional analysis to derive equations expressing a physical relationship between quantities

8.0 Introduction

- 유체역학의 연구: 이론적 전개
  실험적 관찰
  - 자연계에서의 유체현상은 매우 복잡하므로 모든 변수를 고려할 수 없음
  - 중요한 변수만을 고려하고 나머지는 생략하는 <u>간략화 과정</u>이 필요함

  → **개념적 모형**
  - 개념적 모형의 수립 시 변수간의 함수 관계를 얻어 내는 작업이 필요함

  → **차원해석**
  - 개념적 모형을 이용하여 수학적 모형을 구성하고 이의 해를 구하는 작업이 이론적 연구임
  - 해석적인 연구가 불가능해서 실험을 수행하는 경우 원형과 실험 모형간의 상사성을 확보하는 것이 필요함

  → **상사법칙**

8.0 Introduction

Why we need to model the real system?

Most real fluid flows are <u>complex and can be solved only approximately</u>.

Real System

Set of assumptions

Conceptual Model ······ Simplified version of real system

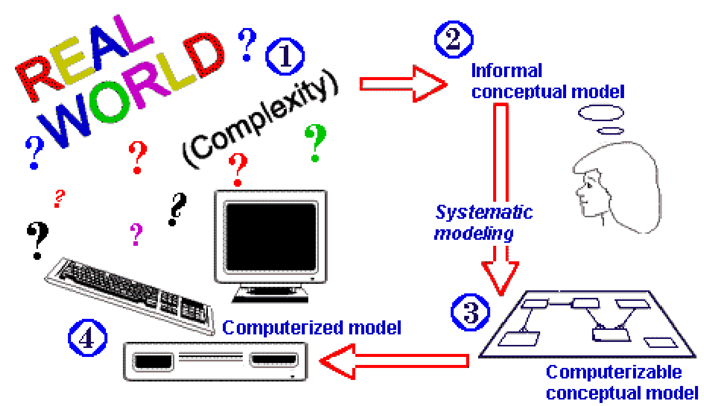
Field Study

Physical Modeling (Scaled and simplified version of prototype)

Mathematical Model [Governing equations + Boundary (initial) conditions]

Analytical solution

Numerical solution (model) (FDM/FEM/FVM)



8.0 Introduction

- Three dilemmas in planning a set of physical or numerical experiments

1) Number of possible and relevant variables or physical parameters in real system is huge and so the potential number of experiments is beyond our resources.
2) Many real flow situations are either too large or far too small for convenient experiment at their true size. → When testing the real thing (prototype) is not feasible, a physical model (scaled version of the prototype) can be constructed and the performance of the prototype simulated in the physical model.
3) The numerical models must be calibrated and verified by use of physical models or measurements in the prototype.

8.0 Introduction

▪ Model study

Physical models have been used for over a hundred years.

Models began to be used to study flow phenomena that could not be solved by analytical (theoretical) methods.

- *Laws of similitude (상사법칙)*

- provide a basis for interpretation of physical and numerical model results and crafting both physical and numerical experiments

- *Dimensional analysis (차원해석)*

- derive equations expressing a physical relationship between quantities

8.0 Introduction

[Example]

Civil and environmental engineering: models of hydraulic structures, river sections, estuaries and coastal bays and seas

Mechanical engineering: models of pumps and turbine, automobiles

Naval architect: ship models

Aeronautical engineering: model test in wind tunnels

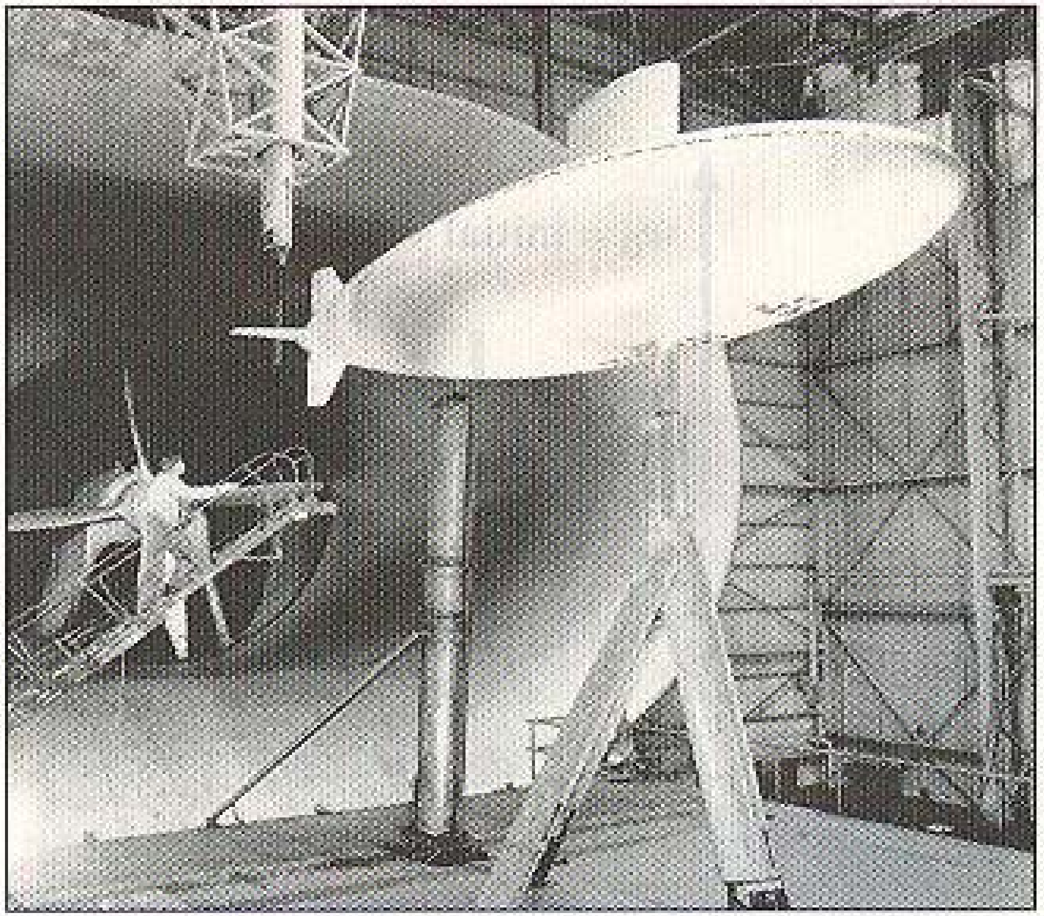
- Justification for models

1) Economics: A model, being small compared to the prototype, costs little.
2) Practicability: In a model, environmental and flow conditions can be rigorously controlled.

8.0 Introduction

한강(미사리~잠실수중보)
수리모형 (서일원 , 1995)

8.0 Introduction



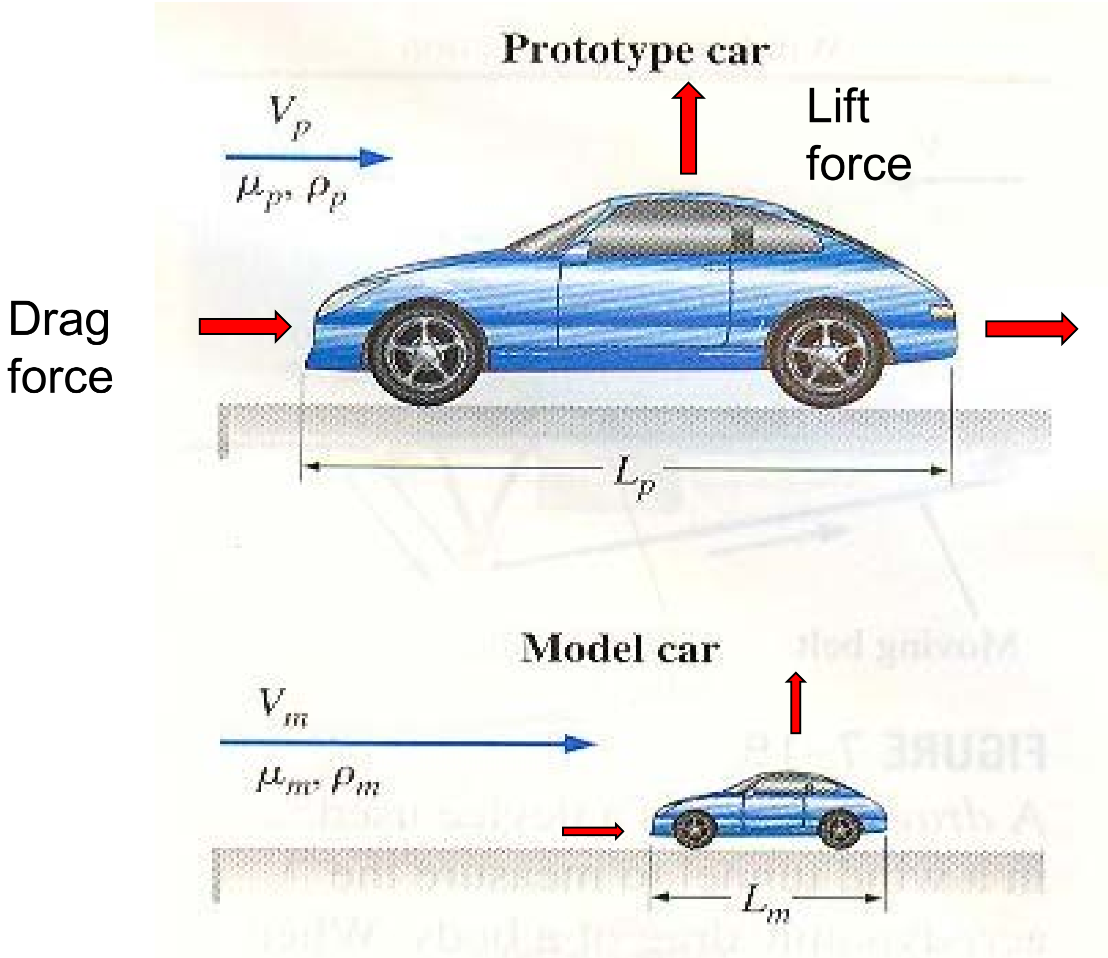
8.1 Similitude and Physical Models

Similitude of flow phenomena not only occurs between a prototype and its model but also may exist between various natural phenomena.

There are three basic types of similitude; all three must be obtained if complete similarity is to exist between fluid phenomena.

- Geometrical similarity (기하학적 상사성)
- Kinematic similarity (운동학적 상사성)
- Dynamic similarity (동력학적 상사성)

8.1 Similitude and Physical Models



8.1 Similitude and Physical Models

1) Geometrical similarity

~ Flow field and boundary geometry of model and of the prototype have the same shape.

→ The ratios between corresponding lengths in model and prototype are the same.

[Cf] Distorted model (왜곡모형)

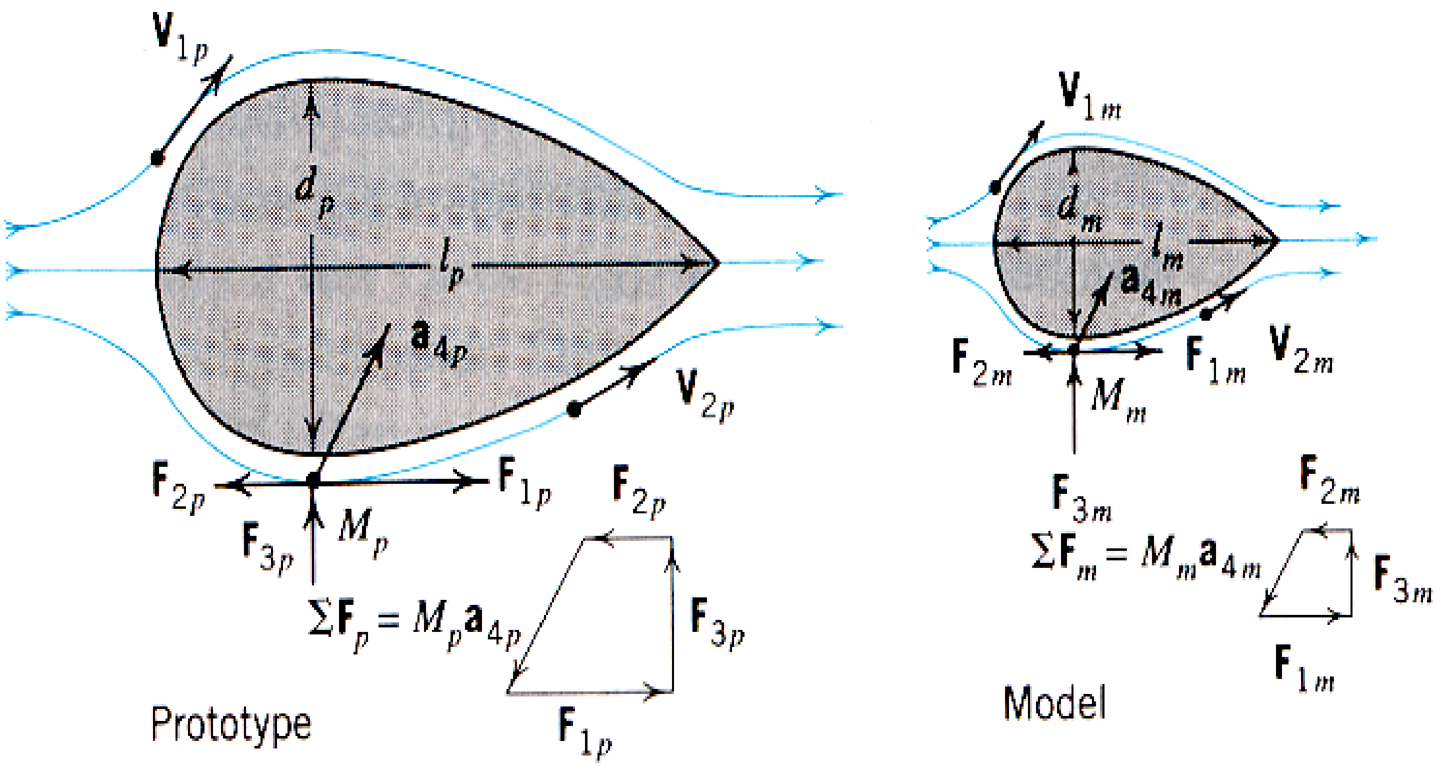
~ not geometrically similar $(l_r > d_r)$

~ The flows are not similar and the models have to be calibrated and adjusted to make them perform properly.

~ used models of rivers, harbor, estuary

~ Numerical models are usually used in their place.

8.1 Similitude and Physical Models



8.1 Similitude and Physical Models

For the characteristic lengths we have

$$d_r = \frac{d_p}{d_m} = \frac{l_p}{l_m} = l_r$$

$$d_r = 50;\ l_r = 50$$

$$A_r = 50^2;\ Vol_r = 50^3$$

- Area

$$\frac{A_p}{A_m} = \left(\frac{d_p}{d_m}\right)^2 = \left(\frac{l_p}{l_m}\right)^2$$

- Volume

$$\frac{Vol_p}{Vol_m} = \left(\frac{d_p}{d_m}\right)^3 = \left(\frac{l_p}{l_m}\right)^3$$

8.1 Similitude and Physical Models

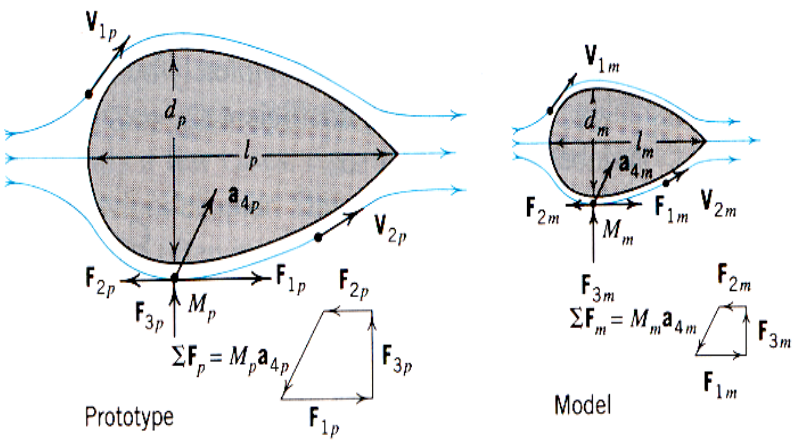
2) Kinematic similarity

In addition to the flowfields having the same shape, the ratios of corresponding velocities and accelerations must be the same through the flow.

→ Flows with geometrically similar streamlines are kinematically similar.

$$V_r = \frac{\vec{V}_{1p}}{\vec{V}_{1m}} = \frac{\vec{V}_{2p}}{\vec{V}_{2m}}$$

$$a_r = \frac{\vec{a}_{3p}}{\vec{a}_{3m}} = \frac{\vec{a}_{4p}}{\vec{a}_{4m}} \qquad (8.1)$$



8.1 Similitude and Physical Models

3) Dynamic similarity

In order to maintain the geometric and kinematic similarity between flowfields, the forces acting on corresponding fluid masses must be related by ratios <u>similar to those for kinematic similarity</u>.

Consider <u>gravity, viscous and pressure forces</u>, and apply <u>Newton's 2nd law</u>

$$F_r = \frac{\vec{F}_{1p}}{\vec{F}_{1m}} = \frac{\vec{F}_{2p}}{\vec{F}_{2m}} = \frac{\vec{F}_{3p}}{\vec{F}_{3m}} = \frac{M_p \vec{a}_{4p}}{M_m \vec{a}_{4m}} \qquad (8.2)$$

Define inertia force as the product of the mass and the acceleration

$$\vec{F}_I = M\,\vec{a}$$

8.1 Similitude and Physical Models

4) Complete similarity

~ requires simultaneous satisfaction of geometric, kinematic, and dynamic similarity.

→ Kinematically similar flows must be geometrically similar.

→ If the mass distributions in flows are similar, then kinematic similarity (density ratio for the corresponding fluid mass are the same) guarantees complete similarity from Eq. (8.2).

From Fig. 8.1, it is apparent that

$$\vec{F}_{1p} + \vec{F}_{2p} + \vec{F}_{3p} = M_p \, \vec{a}_{4p} \qquad \text{(a)}$$

$$\vec{F}_{1m} + \vec{F}_{2m} + \vec{F}_{3m} = M_m \, \vec{a}_{4m} \qquad \text{(b)}$$

8.1 Similitude and Physical Models

If the ratios between three of the four corresponding terms in Eq.(a) and Eq.(b) are the same, the ratio between the corresponding fourth terms be the same as that the other three. Thus, one of the ratio of Eq.(8.2) is redundant. If the first force ratio is eliminated,

$$\frac{M_p \vec{a}_{4p}}{\vec{F}_{2p}} = \frac{M_m \vec{a}_{4m}}{\vec{F}_{2m}} \Rightarrow \left(\frac{F_I}{F_2}\right)_p = \left(\frac{F_I}{F_2}\right)_m \qquad (8.3)$$

$$\frac{M_p \vec{a}_{4p}}{\vec{F}_{3p}} = \frac{M_m \vec{a}_{4m}}{\vec{F}_{3m}} \Rightarrow \left(\frac{F_I}{F_3}\right)_p = \left(\frac{F_I}{F_3}\right)_m \qquad (8.4)$$

8.1 Similitude and Physical Models

- Forces affecting a flow field

Inertia force: $$F_I = M\,a = \rho\, l^3 \left(\frac{V^2}{l} \right) = \rho\, V^2\, l^2$$

Pressure force (→ Euler No.): $$F_p = (\Delta\, p) A = \Delta\, p\, l^2$$

Gravity force (→ Froude No.): $$F_G = M\, g = \rho\, l^3 g$$

Viscosity force (→ Reynolds No.): $$F_V = \mu \left(\frac{dv}{dy} \right) A = \mu \left(\frac{V}{l} \right) l^2 = \mu V\, l$$

Elasticity force (→ Cauchy No.): $$F_E = EA = E\, l^2$$

Surface tension (→ Weber No.): $$F_T = \sigma\, l$$

Here l and V are characteristic length and velocity for the system.

8.1 Similitude and Physical Models

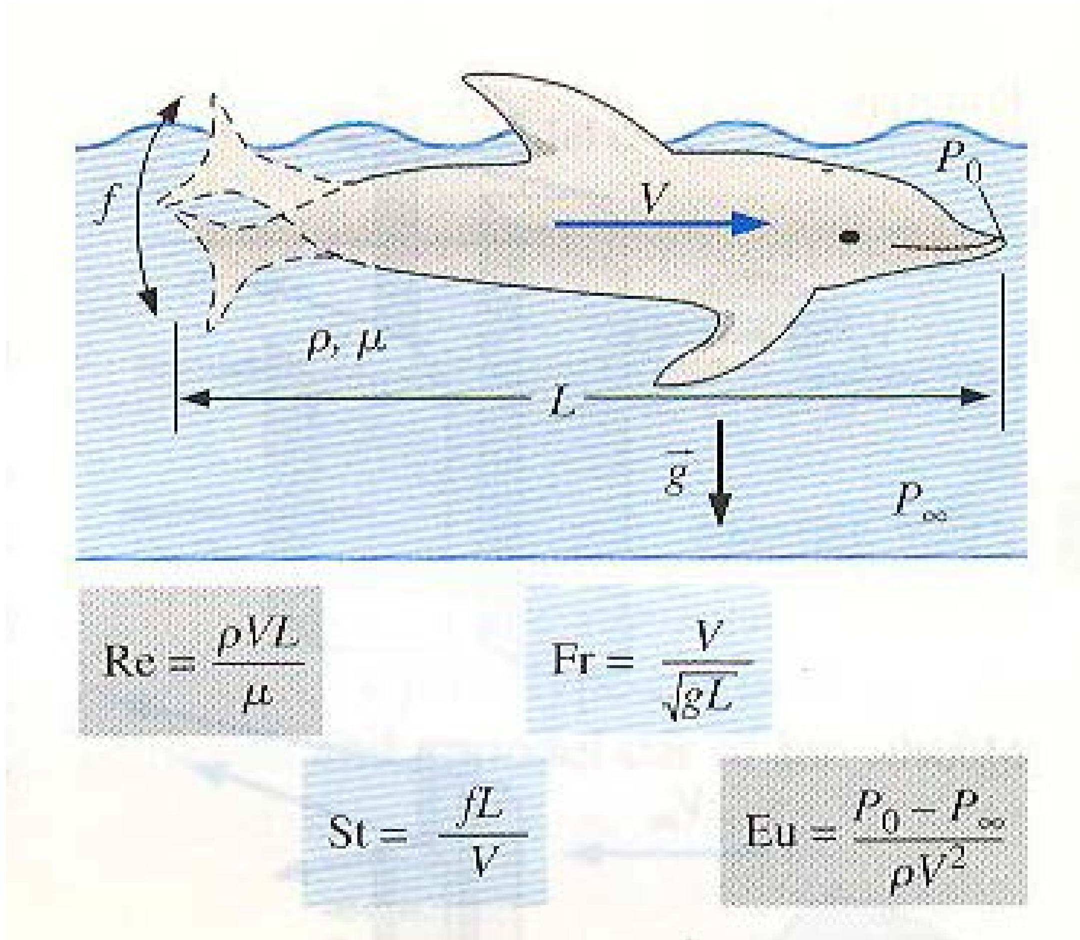
[Re] Other forces

Coriolis force of rotating system → Rossby number

Buoyant forces in stratified flow → Richardson number

Forces in an oscillating flow → Strouhal number

8.1 Similitude and Physical Models



8.1 Similitude and Physical Models

- Dynamic similarity

To obtain dynamic similarity between two flowfields when all these forces act, all corresponding force ratios must be the same in model and prototype.

(i) Pressure

$$\left(\frac{F_I}{F_p}\right)_p = \left(\frac{F_I}{F_p}\right)_m = \left(\frac{\rho V^2}{\Delta p}\right)_p = \left(\frac{\rho V^2}{\Delta p}\right)_m \tag{8.5}$$

Define Euler number, $Eu = V\sqrt{\dfrac{\rho}{2\Delta p}}$

$$Eu_p = Eu_m$$

8.1 Similitude and Physical Models

(ii) Viscous force

$$\left(\frac{F_I}{F_V}\right)_p = \left(\frac{F_I}{F_V}\right)_m = \left(\frac{\rho V l}{\mu}\right)_p = \left(\frac{\rho V l}{\mu}\right)_m \qquad (8.6)$$

Define Reynolds number, $Re = \dfrac{V l}{\nu}$

$Re_p = Re_m$ → Reynolds law

(iii) Gravity

$$\left(\frac{F_I}{F_G}\right)_p = \left(\frac{F_I}{F_G}\right)_m = \left(\frac{V^2}{g l}\right)_p = \left(\frac{V^2}{g l}\right)_m \qquad (8.7)$$

Define Froude number, $Fr = \dfrac{V}{\sqrt{g l}}$

$Fr_p = Fr_m$ → Froude law

8.1 Similitude and Physical Models

(iv) Elastic force

$$\left(\frac{F_I}{F_E}\right)_p = \left(\frac{F_I}{F_E}\right)_m = \left(\frac{\rho V^2}{E}\right)_p = \left(\frac{\rho V^2}{E}\right)_m \qquad (8.8)$$

Define Cauchy number, $Ca = \dfrac{\rho V^2}{E}$

$$Ca_p = Ca_m$$

[Cf] Define Mach number, $Ma = \sqrt{Ca} = \dfrac{V}{\sqrt{E/\rho}}$

$$Ma_p = Ma_m$$

(v) Surface tension

$$\left(\frac{F_I}{F_T}\right)_p = \left(\frac{F_I}{F_T}\right)_m = \left(\frac{\rho l V^2}{\sigma}\right)_p = \left(\frac{\rho l V^2}{\sigma}\right)_m \qquad (8.9)$$

Define Weber number, $We = \dfrac{\rho l V^2}{\sigma}$

$$We_p = We_m$$

8.1 Similitude and Physical Models

Only four of these equations are independent. → One equation is redundant according to the argument leading to Eq. (8.3) & (8.4). → If four equations are simultaneously satisfied, then dynamic similarity will be ensured and fifth equation will also be satisfied.

In most engineering problems (real world), some of the forces above (1) may not act, (2) may be of negligible magnitude, or (3) may oppose other forces in such a way that the effect of both is reduced.

→ In the problem of similitude a good understanding of fluid phenomena is necessary to determine how the problem may be simplified by the elimination of the irrelevant, negligible, or compensating forces.

8.1 Similitude and Physical Models

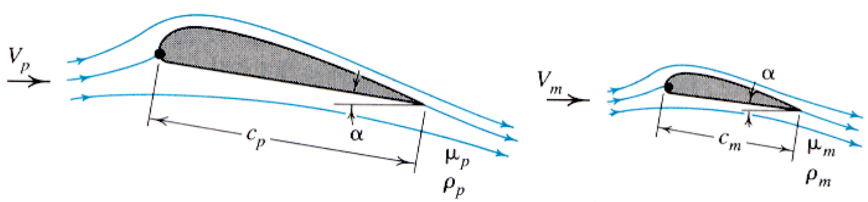
1. Reynolds similarity

~ used for flows in pipe, viscosity-dominant flow (관수로, 수중물체)

For low-speed submerged body problem, there are no surface tension phenomena, negligible compressibility effects, and gravity does not affect the flowfield.

→ Three of four equations are not relevant to the problem.

→ Dynamic similarity is obtained between model and prototype when the Reynolds numbers (ratio of inertia to viscous forces) are the same.



8.1 Similitude and Physical Models

(i) Low-speed submerged object

Reynolds similarity

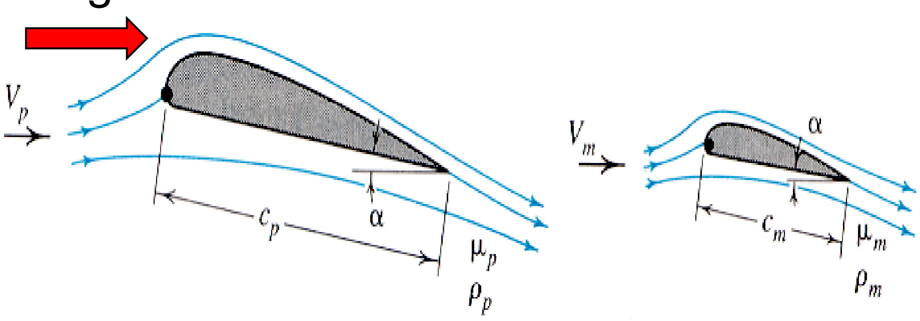
$$\left(\frac{V\,l}{\nu}\right)_p = Re_p = Re_m = \left(\frac{V\,l}{\nu}\right)_m \qquad (8.10)$$

Ratio of any corresponding forces will also be the same.

Consider drag force, $D = C\rho\, V^2 l^2$ 차원해석

$$\left(\frac{D}{\rho V^2 l^2}\right)_p = \left(\frac{D}{\rho V^2 l^2}\right)_m$$

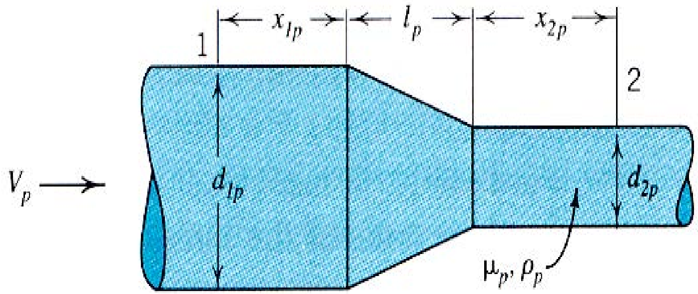
Drag force



8.1 Similitude and Physical Models

(ii) Flow of incompressible fluids in pipes

Geometric similarity:



$$\left(d_2/d_1\right)_p = \left(d_2/d_1\right)_m$$

$$\left(\frac{l}{d_1}\right)_p = \left(\frac{l}{d_1}\right)_m$$

Assume roughness pattern is similar, surface tension and elastic effect are nonexistent.

Gravity does not affect the flow fields

Accordingly dynamic similarity results when Reynolds similarity, Eq. (8.10) is satisfied.

$$Re_p = Re_m$$

8.1 Similitude and Physical Models

Eq. (8.11) is satisfied automatically.

$$Eu = \left(\frac{F_I}{F_P}\right)_p = \left(\frac{F_I}{F_P}\right)_m \quad \rightarrow \quad \left(\frac{p_1 - p_2}{\rho V^2}\right)_p = \left(\frac{p_1 - p_2}{\rho V^2}\right)_m \qquad (8.11)$$

◈ **Reynolds law**

① Velocity:

$$Re_p = Re_m \qquad \left(\frac{Re_p}{Re_m} = 1,\ Re_r = 1\right)$$

$$\left(\frac{Vd}{\nu}\right)_p = \left(\frac{Vd}{\nu}\right)_m \quad \rightarrow \quad \frac{V_m}{V_p} = \frac{\nu_m}{\nu_p}\frac{1}{\frac{d_m}{d_p}} = \frac{\nu_m}{\nu_p}\frac{d_p}{d_m}$$

$$\text{If} \quad \nu_m = \nu_p \quad \rightarrow \quad \boxed{\frac{V_m}{V_p} = \left(\frac{d_m}{d_p}\right)^{-1}}$$

8.1 Similitude and Physical Models

② Discharge: $Q = VA$

$$\frac{Q_m}{Q_p} = \left(\frac{d_m}{d_p}\right)^2 \frac{V_m}{V_p} = \left(\frac{d_m}{d_p}\right)^2 \frac{\nu_m}{\nu_p} \frac{1}{\frac{d_m}{d_p}} = \frac{\nu_m}{\nu_p} \frac{d_m}{d_p}$$

③ Time:

$$\frac{t_m}{t_p} = \frac{\frac{l_m}{V_m}}{\frac{l_p}{V_p}} = \frac{l_m}{l_p} \frac{1}{\frac{V_m}{V_p}} = \frac{l_m}{l_p} \frac{1}{\frac{\nu_m}{\nu_p}} \frac{d_m}{d_p} = \frac{\nu_p}{\nu_m} \left(\frac{l_m}{l_p}\right)^2$$

8.1 Similitude and Physical Models

④ Force:

$$\frac{F_m}{F_p}=\frac{\left(M_m l_m / t_m^2\right)}{\left(M_p l_p / t_p^2\right)}=\frac{\left(\rho_m l_m^3 l_m / t_m^2\right)}{\left(\rho_p l_p^3 l_p / t_p^2\right)}=\left(\frac{\mu_m}{\mu_p}\right)^2\left(\frac{\rho_p}{\rho_m}\right)$$

⑤ Pressure:

$$\frac{P_m}{P_p}=\left(\frac{\mu_m}{\mu_p}\right)^2\left(\frac{\rho_p}{\rho_m}\right)\left(\frac{l_p}{l_m}\right)^2$$

8.1 Similitude and Physical Models

[IP 8.1] p. 298 Water flow in a horizontal pipeline

Water flows in a 75 mm horizontal pipeline at a mean velocity of 3 m/s.

Prototype: Water $0^{\circ}C$

$$\mu_p = 1.781\times10^{-3}\ \mathrm{Pa\cdot s}$$

$$\rho_p = 99.8\ \mathrm{kg/m^3}$$

$$v_p = \frac{1.781\times10^{-3}}{998.8} = 1.78\times10^{-6}\ \mathrm{m^2/s}$$

$$d_p = 75\,\mathrm{mm},\quad V_p = 3\,\mathrm{m/s},\quad \Delta p = 14\ \mathrm{kPa},\quad l_p = 10\,\mathrm{m}$$

Model: <u>Gasoline</u> $20^{\circ}C$

$$\mu_m = 2.9\times10^{-4}\,\mathrm{Pa\cdot s}$$ (Table A 2.1)

$$\rho_m = 0.68\times998.8 = 679.2\,\mathrm{kg/m^3}$$

$$v_m = 4.27\times10^{-7}\,\mathrm{m^2/s}$$

$$d_m = 25\,\mathrm{mm}$$

8.1 Similitude and Physical Models

[Sol] Use Reynolds similarity; $\mathrm{Re}_p = \mathrm{Re}_m$

$$\frac{V_m}{V_p} = \frac{v_m}{v_p}\left(\frac{d_m}{d_p}\right)^{-1} = \frac{4.27\times10^{-7}}{1.78\times10^{-6}} / \left(\frac{25}{75}\right) = 0.753 \qquad d_r = \frac{d_m}{d_p} = 0.333$$

$$\therefore V_m = 0.753(3) = 2.26\,\mathrm{m/s}$$

$$Eu_p = Eu_m$$

$$\left(\frac{\Delta p}{\rho V^2}\right)_p = \left(\frac{\Delta p}{\rho V^2}\right)_m$$

$$\frac{14}{[998.8\times(3)^2]} = \frac{\Delta p_m}{[679.2\times(2.26)^2]}$$

$$\therefore \Delta p_m = 5.4\ \mathrm{kPa}$$

8.1 Similitude and Physical Models

2. Froude similarity

~ open channel flow, free surface flow, gravity-dominant flow.

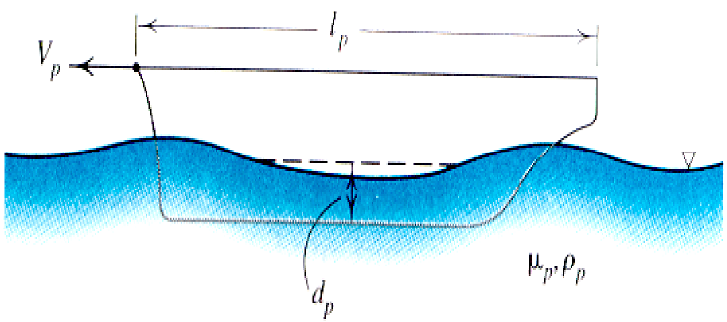
For flow field about an object moving on the surface of a liquid such as ship model (William Froude, 1870)

~ Compressibility and surface tension may be ignored.

~ Frictional effects are assumed to be ignored.

$$Fr_p = \left(\frac{V}{\sqrt{g\,l}}\right)_p = Fr_m = \left(\frac{V}{\sqrt{g\,l}}\right)_m$$

$$\frac{V_m}{V_p} = \sqrt{\frac{g_m}{g_p}\frac{l_m}{l_p}}$$



8.1 Similitude and Physical Models

◈ Froude law

① Velocity

$$\boxed{\frac{V_m}{V_p} = \sqrt{\frac{g_m}{g_p}\frac{l_m}{l_p}}}$$

② Time $t = \dfrac{l}{V}$

$$\frac{t_m}{t_p} = \frac{l_m}{l_p}\frac{V_p}{V_m} = \frac{l_m}{l_p}\sqrt{\frac{g_p}{g_m}\frac{l_p}{l_m}} = \sqrt{\frac{g_p}{g_m}\frac{l_m}{l_p}}$$

③ Discharge $Q = VA$

$$\frac{Q_m}{Q_p} = \frac{V_m}{V_p}\left(\frac{l_m}{l_p}\right)^2 = \sqrt{\frac{g_m}{g_p}\frac{l_m}{l_p}}\left(\frac{l_m}{l_p}\right)^2 = \left(\frac{g_m}{g_p}\right)^{0.5}\left(\frac{l_m}{l_p}\right)^{2.5}$$

8.1 Similitude and Physical Models

④ Force

$$\frac{F_m}{F_p} = \left(\frac{\rho_m}{\rho_p}\right)\left(\frac{l_m}{l_p}\right)^3$$

⑤ Pressure

$$\frac{P_m}{P_p} = \left(\frac{\rho_m}{\rho_p}\right)\left(\frac{l_m}{l_p}\right)$$

[IP 8.2] p. 301 ship model (free surface flow)

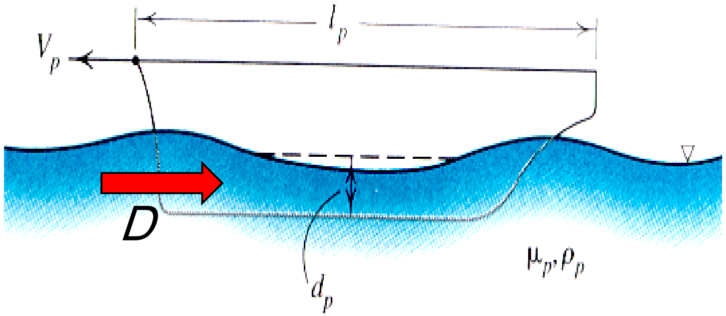
$$l_p = 120 \text{ m} \quad l_m = 3 \text{ m} \quad V_p = 56 \text{ km/h} = 15.56\, m/s \quad D_m = 9 \text{ N}$$

,

Find model velocity and prototype drag.

8.1 Similitude and Physical Models

[Sol] Use Froude similarity



$$\left(\frac{V}{\sqrt{g\,l}}\right)_p = \left(\frac{V}{\sqrt{g\,l}}\right)_m$$

$$l_r = \frac{l_m}{l_p} = \frac{3}{120} = \frac{1}{40}$$

$$V_m = V_p \sqrt{\frac{(g\,l)_m}{(g\,l)_p}} = \frac{56\times10^3}{3600}\left(\frac{3}{120}\right)^{1/2} = 2.46 \text{ m/s}$$

- Drag force ratio

$$\left(\frac{D}{\rho V^2 l^2}\right)_p = \left(\frac{D}{\rho V^2 l^2}\right)_m$$

$$D_p = D_m \frac{\left(\rho V^2 l^2\right)_p}{\left(\rho V^2 l^2\right)_m} = 9\times\left(\frac{56\times10^3/3600}{2.46}\right)^2\times\left(\frac{120}{3}\right)^2 = 575.8 \text{ kN}$$

8.1 Similitude and Physical Models

[Re] Combined action of gravity and viscosity

For ship hulls, the contribution of wave pattern and frictional action to the drag are the same order.

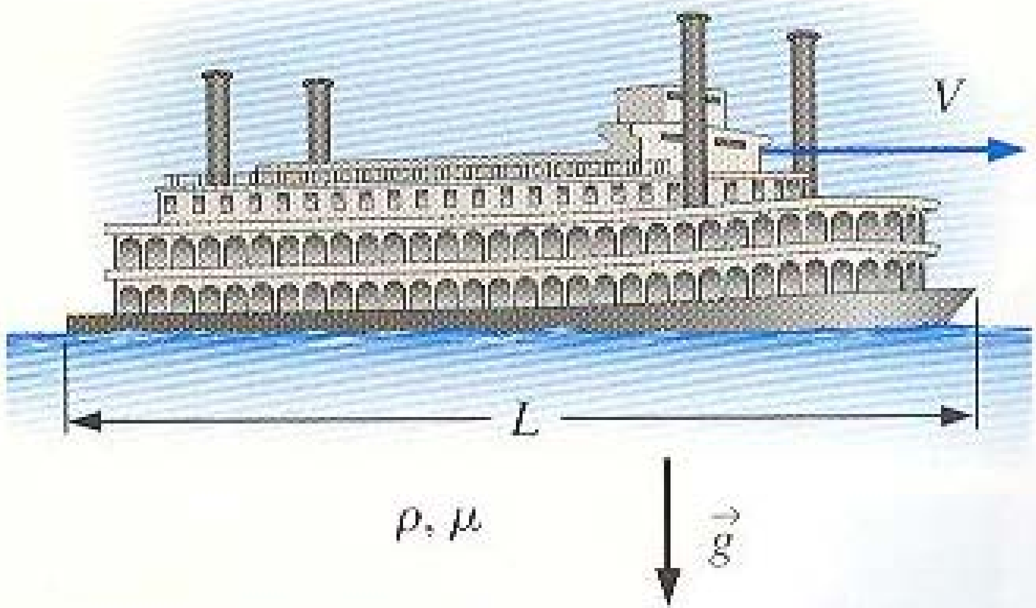
→ Frictional effects cannot be ignored.

→ This problem requires both Froude similarity and Reynolds similarity.

$$Fr_p = Fr_m = \left(\frac{v}{\sqrt{g\,l}}\right)_p = \left(\frac{v}{\sqrt{g\,l}}\right)_m \quad \rightarrow \quad \frac{V_m}{V_p} = \sqrt{\frac{g_m}{g_p}\frac{l_m}{l_p}} \qquad \text{(a)}$$

$$Re_p = Re_m = \left(\frac{V\,l}{\nu}\right)_p = \left(\frac{V\,l}{\nu}\right)_m \quad \rightarrow \quad \frac{V_m}{V_p} = \frac{\nu_m}{\nu_p}\frac{l_p}{l_m} \qquad \text{(b)}$$

8.1 Similitude and Physical Models



$$\mathrm{Re} = \frac{\rho V L}{\mu} = \frac{VL}{\nu}$$

$$\mathrm{Fr} = \frac{V}{\sqrt{gL}}$$

8.1 Similitude and Physical Models

Combine (a) and (b)

$$\sqrt{\frac{g_m}{g_p}\frac{l_m}{l_p}} = \frac{\nu_m}{\nu_p}\frac{l_p}{l_m} \rightarrow \quad \frac{\nu_m}{\nu_p} = \left(\frac{g_m}{g_p}\right)^{0.5}\left(\frac{l_m}{l_p}\right)^{1.5}$$

This requires

(a) A liquid of appropriate <u>viscosity must be found for the model test</u>.

(b) If same liquid is used, then model is as large as prototype.

8.1 Similitude and Physical Models

For $g_m = g_p$

$$\frac{\nu_m}{\nu_p} = \left(\frac{l_m}{l_p}\right)^{1.5} \quad \rightarrow \quad \nu_m = \nu_p \Big/ \left(\frac{l_m}{l_p}\right)^{1.5}$$

If $\quad \frac{l_m}{l_p} = \frac{1}{10} \quad \rightarrow \quad \nu_m = \frac{\nu}{31.6}$

Water: $\mu = 1.0 \times 10^{-3}\ \mathrm{Pa \cdot s} \rightarrow 0.32 \times 10^{-4}\ \mathrm{Pa \cdot s}$

Hydrogen is close: $\mu = 0.21 \times 10^{-4}\ \mathrm{Pa \cdot s}$

~ choose only one equation → Reynolds or Froude law

~ correction (correcting for scale effect) is necessary.

8.1 Similitude and Physical Models

[I.P.8.3] p. 301 Model of hydraulic overflow structure → spillway model

$$Q_p = 600 \text{ m}^3/\text{s}$$

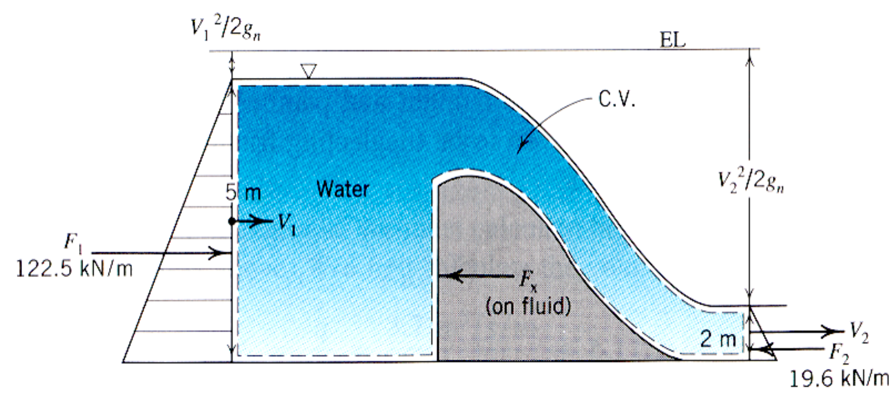
$$l_r = \frac{l_m}{l_p} = \frac{1}{15}$$

[Sol] Since gravity is dominant, use Froude similarity.

$$\frac{Q_m}{Q_p} = \left(\frac{g_m}{g_p}\right)^{0.5}\left(\frac{l_m}{l_p}\right)^{2.5}$$

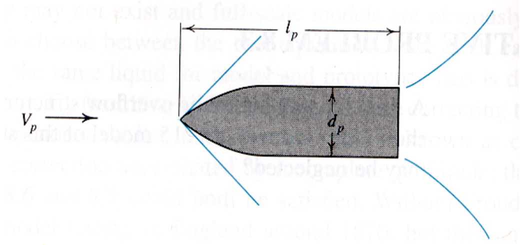
$$Q_m = Q_p\left(\frac{l_m}{l_p}\right)^{2.5} = 600\left(\frac{1}{15}\right)^{2.5}$$

$$= 0.69 \text{ m}^3/\text{s} = 690 \text{ l/s}$$



8.1 Similitude and Physical Models

3. Mach similarity



Similitude in <u>compressible fluid flow</u>

~ <u>gas, air</u>

~ Gravity and surface tension are ignored.

~ Combined action of resistance and elasticity (compressibility)

$$Re_p = Re_m \rightarrow \frac{V_p}{V_m} = \frac{\nu_p}{\nu_m}\frac{l_m}{l_p} \qquad \text{(a)}$$

$$Ma_p = Ma_m = \left(\frac{V}{a}\right)_p = \left(\frac{V}{a}\right)_m$$

8.1 Similitude and Physical Models

$$where\ a = \text{sonic velocity} = \sqrt{\frac{E}{\rho}}$$

$$\frac{V_p}{V_m} = \frac{a_p}{a_m} \qquad \text{(b)}$$

Combine (a) and (b)

$$\frac{l_p}{l_m} = \left(\frac{\nu_p}{\nu_m}\right)\left(\frac{a_m}{a_p}\right)$$

→ gases of appropriate viscosity are available for the model test.

8.1 Similitude and Physical Models

- Velocity

$$\frac{V_m}{V_p} = \frac{a_m}{a_p} = \sqrt{\frac{E_m}{E_p}\frac{\rho_p}{\rho_m}}$$

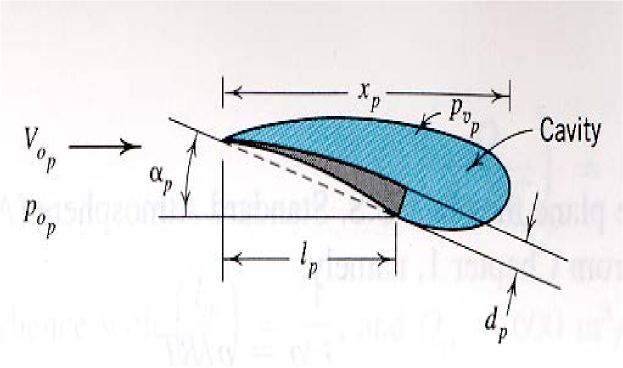
- Time

$$\frac{T_m}{T_p} = \frac{l_m}{l_p}\frac{V_p}{V_m} = \sqrt{\frac{E_p}{E_m}\frac{\rho_m}{\rho_p}}\ \frac{l_m}{l_p}$$

- Discharge

$$\frac{Q_m}{Q_p} = \left(\frac{l_m}{l_p}\right)^2 \frac{V_p}{V_m} = \sqrt{\frac{E_p}{E_m}\frac{\rho_m}{\rho_p}}\ \left(\frac{l_m}{l_p}\right)^2$$

8.1 Similitude and Physical Models



4. Euler Similarity

~ Modeling of prototype cavitation

~ For cavitation problem,

vapor pressure must be included.

[Ex.1] cavitating hydrofoil model in a water tunnel

Here gravity, compressibility, and surface tension are neglected.

Dynamic similitude needs Reynolds similarity and Euler similarity.

8.1 Similitude and Physical Models

$$Re_p = Re_m = \left(\frac{Vl}{\nu}\right)_p = \left(\frac{Vl}{\nu}\right)_m$$

$$\sigma_p = \sigma_m = \left(\frac{p_0 - p_v}{\rho V_0^2}\right)_p = \left(\frac{p_0 - p_v}{\rho V_0^2}\right)_m$$

$\sigma \quad = \dfrac{p_0 - p_v}{\rho V^2}$ = cavitation number

p_0 = absolute pressure

p_v = vapor pressure

~ Virtually impossible to satisfy both equation.

~ Cavitation number must be the same in model and prototype.

8.2 Dimensional Analysis

Dimensional analysis

~ mathematics of the dimensions of quantities

~ is closely related to laws of similitude

~ based on Fourier's principle of dimensional homogeneity (1882)

- 차원 동차성의 원리

An equation expressing a physical relationship between quantities must be dimensionally homogeneous.

→ The dimensions of each side of equation must be the same.

8.2 Dimensional Analysis

~ <u>cannot produce analytical solutions </u>to physical problems.

~ powerful tool in formulating problems which defy analytical solution and <u>must be solved experimentally</u>.

~ It points the way toward a <u>maximum of information from a minimum of experiment</u> by the <u>formation of dimensionless groups</u>, some of which are identical with the force ratios developed with the laws of similitude.

- 물리현상을 설명하는 변수들의 수를 줄여서 무차원 형태로 만드는 것
- 최종적으로 무차원 수들간의 함수관계를 얻어 내는 과정

8.2 Dimensional Analysis

- *Basic dimension (기본차원)*

~ directly relevant to fluid mechanics

~ independent fundamental dimensions

length, L

mass, M or force, F

time, t

thermodynamic temperature T

Newton′s 2nd law

$$F = M\,a = \frac{M\,L}{t^2}$$

~ There are only <u>three independent</u> fundamental dimensions , *M, L, t*.

8.2 Dimensional Analysis

(1) Rayleigh method

~ early development of a dimensional analysis

Suppose that power, P, derived from hydraulic turbine is dependent on Q , γ , E_T

Suppose that the relation between these four variables is unknown but it is known that these are the only variables involved in the problem.

$$P = f\left(Q , \gamma , E_T \right) \qquad \text{(a)}$$

Q = flow rate

γ = specific weight of the fluid

E_T = unit mechanical energy by unit weight of fluid (Fluid system → turbine)

8.2 Dimensional Analysis

Principle of dimensional homogeneity

→ Quantities involved cannot be added or subtracted since their dimensions are different.

Eq. (a) should be a combination of products of power of the quantities.

$$P = C\, Q^a\, \gamma^b\, E_T^c \tag{b}$$

where C = dimensionless constant ~ cannot be obtained by dimensional methods

a, b, c = unknown exponents

8.2 Dimensional Analysis

Eq. (b) can be written dimensionally as

$$(\text{Dimensions of } P) = (\text{Dimensions of } Q)^a (\text{Dimensions of } \gamma)^b (\text{Dimensions of } E_T)^c$$

$$\frac{ML^2}{t^3} = \left(\frac{L^3}{t}\right)^a \left(\frac{MLt^{-2}}{L^3}\right)^b (L)^c \qquad \text{(c)}$$

Using the principle of dimensional homogeneity, the exponent of each of the fundamental dimensions is the same on each side of the equation.

$$M: \ 1 = b$$

$$L: \ 2 = 3a - 2b + c$$

$$t: \ -3 = -a - 2b$$

8.2 Dimensional Analysis

Solving for *a, b*, and *c* yields

$$a = 1,\ b = 1,\ c = 1$$

Resubstituting these values Eq. (b) gives

$$P = C\ Q\ \gamma\ E_T \qquad \text{(d)}$$

$C =$ dimensionless constant that can be obtained from

① a <u>physical analysis of the problem</u>

② an <u>experimental measurement</u> of P, Q, γ, E_T

8.2 Dimensional Analysis

(2) Buckingham theorem

~ generalized method to find useful dimensionless groups of variables to describe process (Buckingham, 1915)

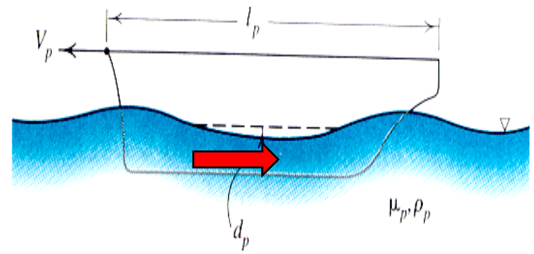
▪ Buckingham's Π - Theorem

- For fluid problems, n variables are functions of each other.
- If the number of independent basic dimensions is m.(대개는 m=3)
- Then, application of dimensional analysis allows expression of the functional relationship in terms of (n-m) distinct dimensionless groups.

8.2 Dimensional Analysis

[Ex] Drag on a ship

$$f\left(D,\ \rho,\ \mu, g, l, V\right)=0$$



f(역학적 인자, 유체의 고유성질, 중력가속도, 기하학적 인자, 운동학적 인자) = 0
역학적 인자: *F, E, P, p, M, T*
유체의 고유성질: ρ, μ
기하학적 인자: *L, d, H*
운동학적 인자: *V, a, Q*

$n = 6$

$m = 3$ = repeating variables; $M(\rho)$, $L(l)$, $t(V)$

Other variables $D,\ \mu,\ g$ appear only in the unique group describing the ratio of inertia force to force related to the variable.

8.2 Dimensional Analysis

- Procedure:

1) Find the largest number of variables which do not form a dimensionless group.

For drag problem, number of independent dimensions is $m = 3$, V, l, ρ cannot be formed into a Π group.

2) Determine the number of Π groups to be formed: $n\text{-}m = 3$

3) Combine sequentially the variables that cannot be formed into a dimensionless group, with each of the remaining variables to form the requisite Π - groups.

8.2 Dimensional Analysis

$$\Pi_1 = f_1(D, \rho, V, l)$$

$$\Pi_2 = f_2(\mu, \rho, V, l)$$

$$\Pi_3 = f_3(g, \rho, V, l)$$

4) Determine the detailed form of the dimensionless groups using principle of dimensional homogeneity.

i) Π_1

$$\Pi_1 = D^a \rho^b V^c l^d \qquad \text{(a)}$$

Since Π_1 is dimensionless, writing Eq. (a) dimensionally

$$M^0 L^0 t^0 = \left(\frac{ML}{t^2}\right)^a \left(\frac{M}{L^3}\right)^b \left(\frac{L}{t}\right)^c (L)^d \qquad \text{(b)}$$

8.2 Dimensional Analysis

The following equations in the exponents of the dimensions are obtained

$$M:\ 0 = a + b$$

$$L:\ 0 = a - 3b + c + d$$

$$t:\ 0 = -2a - c$$

Solving these equations in terms of *a* gives

$$b = -a, c = -2a,\ d = -2a$$

$$\Pi_1 = D^a \rho^{-a} V^{-2a} l^{-2a} = \left(\frac{D}{\rho l^2 V^2} \right)^a$$

8.2 Dimensional Analysis

The exponent may be taken as any convenient number other than zero.

If $a = 1$, then

$$\boxed{\Pi_1 = \frac{D}{\rho l^2 V^2}} \qquad \text{(c)}$$

ii) Π_2

$$\Pi_2 = \mu^a \rho^b V^c l^d$$

$$M^0 L^0 t^0 = \left(\frac{M}{Lt}\right)^a \left(\frac{M}{L^3}\right)^b \left(\frac{L}{t}\right)^c (L)^d$$

$$M \;:\; 0 = a + b$$

$$L \;:\; 0 = -a - 3b + c + d$$

$$t \;:\; 0 = -a - c$$

8.2 Dimensional Analysis

Solving these equations in terms of a gives

$$b = -a\,,\ c = -a\,,\ d = -a$$

$$\Pi_2 = \mu^a \rho^{-a} V^{-a} l^{-a} = \left(\frac{\mu}{\rho l V} \right)^a$$

If $a = -1$, then

$$\boxed{\Pi_2 = \frac{V l \rho}{\mu} = \mathrm{Re}} \qquad \text{(d)}$$

8.2 Dimensional Analysis

iii) Π_3

$$\Pi_3 = g^a l^b \rho^c V^d$$

$$M^0 L^0 t^0 = \left(\frac{L}{t^2}\right)^a L^b \left(\frac{M}{L^3}\right)^c \left(\frac{L}{t}\right)^d$$

$$M \ : \ 0 = c$$

$$L \ : \ 0 = a + b - 3c + d$$

$$t \ : \ 0 = -2a - d$$

Solving these equations in terms of *a* gives

$$b = a, \ c = 0, \ d = -2a$$

$$\Pi_3 = g^a l^a V^{-2a} = \left(\frac{g\,l}{V^2}\right)^a \qquad \text{(e)}$$

8.2 Dimensional Analysis

If a = -1/2, then

$$\Pi_3 = \frac{V}{\sqrt{g\,l}} = \mathrm{Fr}$$

Combining these three equations gives

$$f'\left(\frac{D}{\rho l^2 V^2},\ \mathrm{Re},\ \mathrm{Fr}\right) = 0$$

$$\boxed{\frac{D}{\rho l^2 V^2} = f''(\mathrm{Re},\ \mathrm{Fr})}$$

Reynolds Similarity

Froude Similarity

$$D = C_D \rho l^2 V^2$$

$$C_D = f''(\mathrm{Re},\ Fr)$$

- 무차원량간의 관계를 보여 줌
- 이 후 실험을 통해서 C_D를 결정하여 최종관계식을 유도함
- 실험 수행시 실험 조건을 무차원량으로 환산하여 수행함

8.2 Dimensional Analysis

Dimensional analysis

~ no clue to the functional relationship among $D/\rho l^2 V^2$, Re and Fr

~ arrange the numerous original variables into a relation between a smaller number of dimensionless groups of variables.

~ indicate how test results should be processed for concise presentation

[Problem 8.48] p. 320 Head loss in a pipe flow

Select all variable which affect the flow in pipe

- Fluid property: ρ, μ
- Geometric dimensions of system: d, l, b, h
- Forces and kinematics: $\Delta p, g, \tau, V$

8.2 Dimensional Analysis

$$f\left(h_L,\ \rho,\ \mu, d,\ l,\ V,\ g\right)=0$$

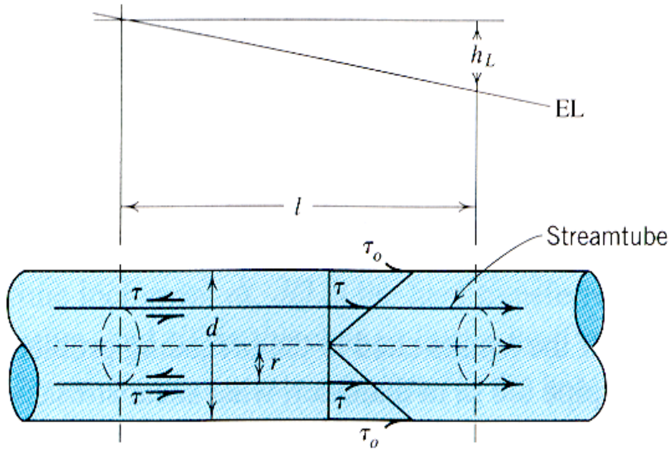
Repeating variables: $l,\ \rho, V$

$$\Pi_1 = f_1\left(h_L, l,\ \rho, V\right)$$

$$\Pi_2 = f_1\left(d, l,\ \rho, V\right)$$

$$\Pi_3 = f_3\left(\mu, l,\ \rho, V\right)$$

$$\Pi_4 = f_4\left(g, l,\ \rho, V\right)$$



(i) $\Pi_1 = h_L^a\, l^b \rho^c V^d$

$$M^0 L^0 t^0 = L^a L^b \left(\frac{M}{L^3}\right)^c \left(\frac{L}{t}\right)^d$$

$$M\ :\ 0 = c$$

8.2 Dimensional Analysis

$$M\ :\ 0 = c$$

$$L\ :\ 0 = a + b - 3c + d$$

$$t\ :\ 0 = -d$$

$$b = -a$$

$$\therefore \quad \Pi_1 = \left(\frac{h_L}{l}\right)^a$$

$$If \quad a = 1:\ \Pi_1 = \frac{h_L}{l}$$

8.2 Dimensional Analysis

(ii) $\Pi_2 = d^a l^b \rho^c V^d$

$$M^0 L^0 t^0 = L^a L^b \left(\frac{M}{L^3}\right)^c \left(\frac{L}{t}\right)^d$$

$$M\ :\ 0 = c \qquad ①$$

$$L\ :\ 0 = a + b - 3c + d \qquad ②$$

$$t\ :\ 0 = -d \qquad ③$$

$$② : 0 = a + b \qquad b = -a$$

$$\therefore \quad \Pi_2 = \left(\frac{d}{l}\right)^a$$

$$If \ \ a = 1 \ : \Pi_2 = \frac{d}{l}$$

8.2 Dimensional Analysis

(iii) $\Pi_3 = \mu^a l^b \rho^c V^d$

$$M^0 L^0 t^0 = \left(\frac{M}{LT}\right)^a L^b \left(\frac{M}{L^3}\right)^c \left(\frac{L}{t}\right)^d$$

$M : 0 = a + c$ ① $\rightarrow c = d \rightarrow c = -a$

$L : 0 = -a + b - 3c + d$ ②

$t : 0 = -a - d \rightarrow d = -a$ ③

② $d + b - 3d + d = 0 \quad b = d \rightarrow b = -a$

$\therefore \quad \Pi_3 = \mu^a l^{-a} \rho^{-a} V^{-a}$

$If \quad a = -1 \qquad \therefore \quad \Pi_3 = \dfrac{l \rho V}{\mu} = \mathrm{Re}$

8.2 Dimensional Analysis

(iv) $\Pi_4 = g^a l^b \rho^c V^d$

$$M^0 L^0 t^0 = \left(\frac{L}{t^2}\right)^a L^b \left(\frac{M}{L^3}\right)^c \left(\frac{L}{t}\right)^d$$

$M\ :\ 0 = c$ ①

$L\ :\ 0 = a + b - 3c + d$ ②

$t\ :\ 0 = -2a - d$ ③

③ $d = -2a$

② $0 = a + b - 0 - 2a \rightarrow \quad b = a$

8.2 Dimensional Analysis

$$\Pi_4 = g^{a} l^{a} V^{-2a} = \left(\frac{g^{l}}{V^2}\right)^{a}$$

$$If \quad a = -\frac{1}{2}: \quad \Pi_4 = \frac{V}{\sqrt{g\,l}} = \mathrm{Fr}$$

$$f\left(\frac{h_L}{l}, \frac{l}{d}, \mathrm{Re}, \mathrm{Fr}\right) = 0$$

$$\frac{h_L}{l} = f'\left(\frac{l}{d}, \mathrm{Re}, \mathrm{Fr}\right)$$

- Darcy-Weibach equation

$$\frac{h_L}{l} = f''(\mathrm{Re})\left(\frac{l}{d}\right)^{1}(\mathrm{Fr})^{2} = f\,\frac{l}{d}\frac{V^2}{gl}$$

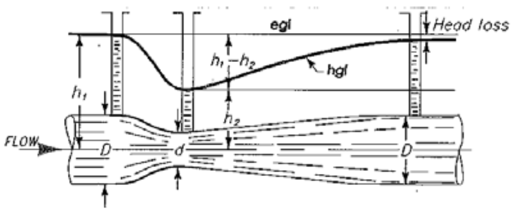
$$\boxed{h_L = f\,\frac{l}{d}\frac{V^2}{2g}}$$

$$f = fn(\mathrm{Re}) = \text{friction factor}$$

Homework Assignment # 8

Homework Assignment # 8

Due: 1 week from today



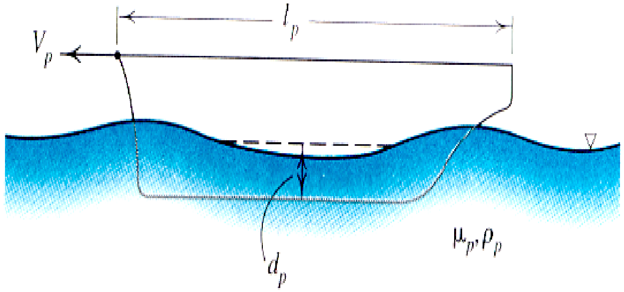
1. (Prob. 8.6)

A large Venturi meter (section 14.12) for air flow measurement has $d_1 = 1.5\ \mathrm{m}$ and $d_2 = 0.9\ \mathrm{m}$. It is to be calibrated using a 1:12 model with water the flowing fluid. When 0.07 $\mathrm{m^3/s}$ pass through the model, the drop in pressure from section 1 to section 2 is 172 kPa. Calculate the corresponding flowrate and pressure drop in the prototype. Use densities and viscosities for air and water given in Appendix 2 (altitude zero) Assume that these properties do not change. Assume the water temperature 15^{o}C.

Homework Assignment # 8

2. (Prob. 8.14)

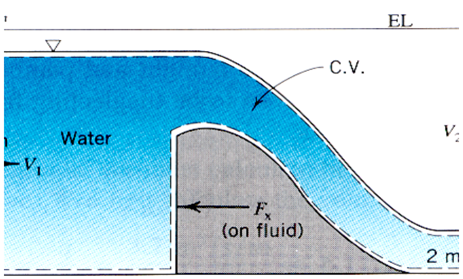
A ship model 1 m long (with negligible skin friction) is tested in a towing basin at a speed of 0.6 m/s. To what ship velocity does this correspond if the ship is 60 m long? A force of 4.45 N is required to tow the model; what propulsive force does this represent in the prototype?



Homework Assignment # 8

3. (Prob. 8.20)

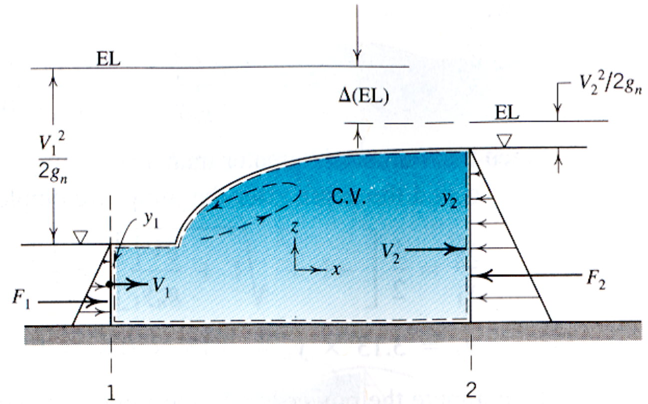
An overflow structure 480 m long is designed to pass a flood flow of 3,400 m^3/s. A 1:20 model of the cross section of the structure is built in a laboratory channel 0.3 m wide. Calculate the required laboratory flowrate if the actions of viscosity and surface tension may be neglected. When the model is tested at this flowrate, the pressure at a point on the model is observed to be 50mm of mercury vacuum; how should this be interpreted for the prototype?



Homework Assignment # 8

4. (Prob. 8.24)

A hydraulic jump from 0.6 m to 1.5 m is to be modeled in a laboratory channel at a scale of 1 :10. What (two-dimensional) flowrate should be used in the laboratory channel? What are the Froude numbers upstream and downstream from the jump on model and prototype?



Homework Assignment # 8

5. (Prob. 8.30)

A cavitation zone is expected on an overflow structure when the flowrate is 140 m^3/s, atmospheric pressure 101.3 kPa, and water temperature 5°C. The cavitation is to be reproduced on a 1:20 model of the structure operating in a vacuum tank with water at 50°C. Disregarding frictional and surface-tension effects, determine the flowrate and absolute pressure (kPa) to be used in the tank for dynamic similarity.

6. (Prob. 8.56)

For a hydraulic jump (Fig. 10.23), derive by dimensional analysis an expression for y_2 if y_2 depends only on q, y_1, g_n, μ, and ρ. Compare the resulting expression with Eq. 10.24.

Homework Assignment # 8

7. (Prob. 8.59)

The force, F, exerted by the flowing liquid on this two-dimensional sluice gate is to be studied by dimensional analysis. Assuming the flow frictionless (ideal fluid), derive an expression for this force in terms of the other variables relevant to the problem.