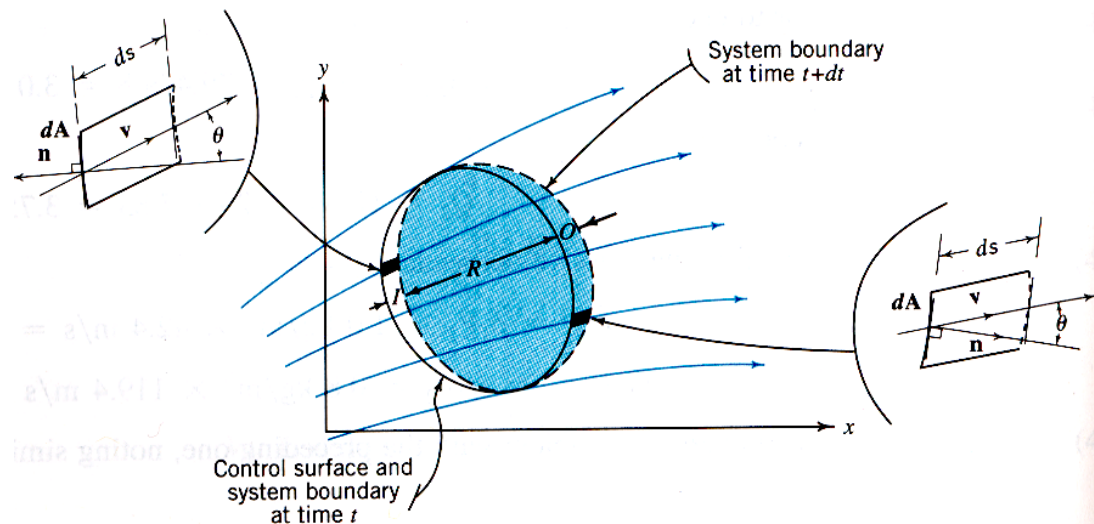


Chapter 4

Continuity, Energy, and Momentum Equations



Chapter 4 Continuity, Energy, and Momentum Equations

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4.4 The Moment of Momentum Equation for Finite Control Volumes

Objectives

- Apply finite control volume to get integral form of continuity, energy, and momentum equations
- Compare integral and point form equations
- Derive the simplified equations for continuity, energy, and momentum equations

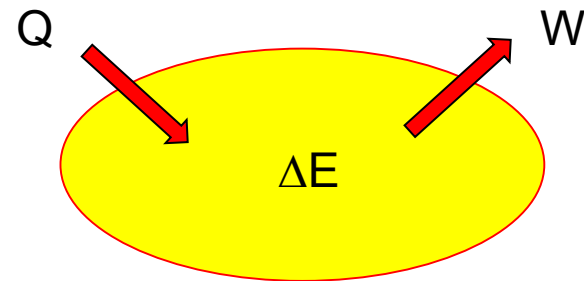
4.2 The General Energy Equation

4.2.1 The 1st law of thermodynamics

- The 1st law of thermodynamics:

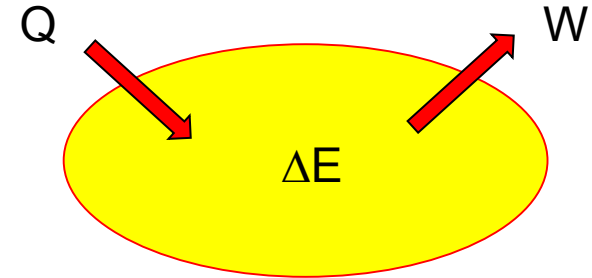
The difference between the heat added to a system of masses and the work done by the system depends only on the initial and final states of the system (→ change in energy).

→ Conservation of energy



4.2 The General Energy Equation

$$\delta Q - \delta W = dE \quad (4.14)$$



where δQ = heat added to the system from surroundings

δW = work done by the system on its surroundings

δE = increase in energy of the system

4.2 The General Energy Equation

[Re]

- property of a system: position, velocity, pressure, temperature, mass, volume
- state of a system: condition as identified through properties of the system

Consider time rate of change

$$\frac{\delta Q}{dt} - \frac{\delta W}{dt} = \frac{dE}{dt} \quad (4.15)$$

4.2 The General Energy Equation

- Work

$W_{pressure}$ = work of normal stresses acting on the system boundary

W_{shear} = work of tangential stresses done at the system boundary
on adjacent external fluid in motion

W_{shaft} = shaft work done on a rotating element in the system

- Energy

Consider e = energy per unit mass = $E/mass$

e_u = **internal energy** associated with fluid temperature = u

e_p = **potential energy** per unit mass = gh

where h = local elevation of the fluid

e_q = **kinetic energy** per unit mass = $\frac{q^2}{2}$

4.2 The General Energy Equation

$$u + \frac{p}{\rho} = \text{enthalpy}$$

$$e = e_u + e_p + e_q = u + gh + \frac{q^2}{2} \quad (4.16)$$

- **Internal energy**

= activity of the molecules comprising the substance

= force existing between the molecules

~ depend on temperature and change in phase

4.2 The General Energy Equation

4.2.2 General energy equation

$$\frac{\delta Q}{dt} - \frac{\delta W}{dt} = \frac{dE}{dt} \quad (4.15)$$

Consider work done

$$\frac{\delta W}{dt} = \frac{\delta W_{pressure}}{dt} + \frac{\delta W_{shaft}}{dt} + \frac{\delta W_{shear}}{dt} \quad (4.15a)$$

$\frac{\delta W_{pressure}}{dt}$ = net rate at which work of pressure is
done by the fluid on the surroundings (유체 압력이 외부에 한 일)

$$= \text{work flux}_{out} - \text{work flux}_{in}$$

$$= \oint_{CS} p (\vec{q} \cdot d\vec{A})$$

4.2 The General Energy Equation

[Cf] Mass conservation from RTT

$$\frac{dE}{dt} = \oint_{CS} e\rho(\vec{q} \cdot d\vec{A}) + \frac{\partial}{\partial t} \int_{CV} (e\rho dV) = 0$$

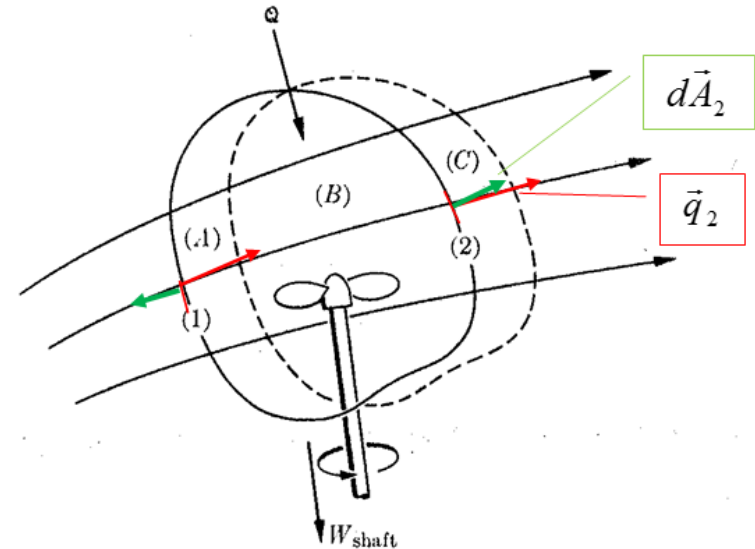
$$\frac{\partial}{\partial t} \int_{CV} (e\rho dV) = -\oint_{CS} e\rho(\vec{q} \cdot d\vec{A})$$

$$-\oint_{CS} \rho\vec{q} \cdot d\vec{A}$$

= net flux of matter through the control surface

(외부에서 유입된 질량 - 유출된 질량)

= flux in - flux out



4.2 The General Energy Equation

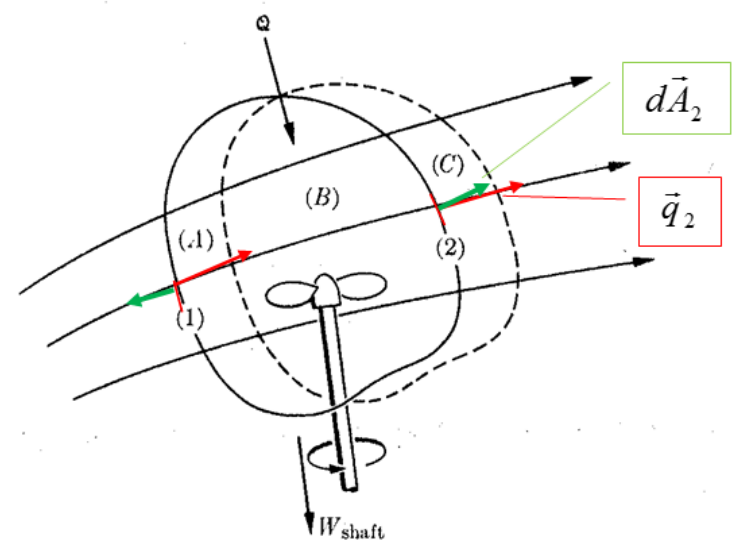
$$\vec{q} \cdot d\vec{A} = \begin{cases} \text{positive for outflow into CV} \\ \text{negative for inflow} \end{cases}$$

$$\vec{q} \cdot d\vec{A} = Q = L^3 / t$$

$$p(\vec{q} \cdot d\vec{A}) = \frac{F}{L^2} \frac{L^3}{t} = FL / t = E / t$$

Thus, (4.15a) becomes

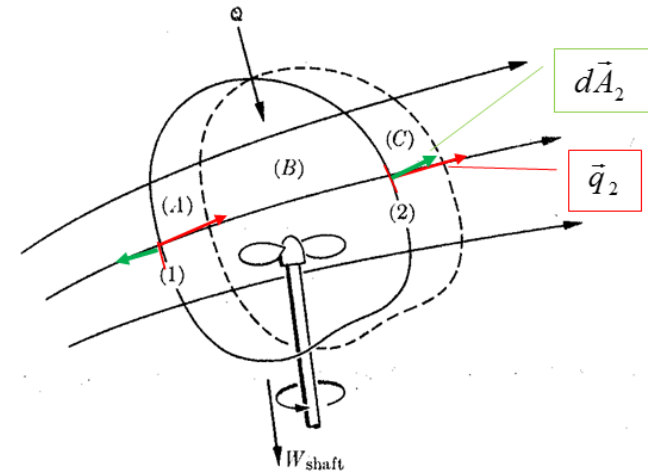
$$\frac{\delta W}{dt} = \oint_{CS} p(\vec{q} \cdot d\vec{A}) + \frac{\delta W_{shaft}}{dt} + \frac{\delta W_{shear}}{dt} \quad (4.15b)$$



4.2 The General Energy Equation

Now, consider energy change term

$$\begin{aligned} \frac{dE}{dt} &= \text{total rate change of stored energy} \\ &= \text{net rate of energy flux through C.V.} \\ &+ \text{time rate of change inside C.V.} \end{aligned}$$



$$\frac{dE}{dt} = \oint_{CS} e\rho(\vec{q} \cdot d\vec{A}) + \frac{\partial}{\partial t} \int_{CV} (e\rho dV)$$

(4.15c)

← Reynolds Transport Theorem

$$e = E / \text{mass}; \quad \rho(\vec{q} \cdot d\vec{A}) = \text{mass} / \text{time}$$

$$e\rho(\vec{q} \cdot d\vec{A}) = E / t$$

4.2 The General Energy Equation

Substituting (4.15b) and (4.15c) into Eq. (4.15) yields

$$\frac{\delta Q}{dt} - \frac{\delta W_{shaft}}{dt} - \frac{\delta W_{shear}}{dt} - \oint_{CS} p(\vec{q} \cdot d\vec{A})$$

$$= \oint_{CS} e\rho(\vec{q} \cdot d\vec{A}) + \frac{\partial}{\partial t} \int_{CV} (e\rho dV)$$

$$\frac{\delta Q}{dt} - \frac{\delta W_{shaft}}{dt} - \frac{\delta W_{shear}}{dt} \quad (4.16)$$

$$= \oint_{CS} \left(\frac{p}{\rho} + e \right) \rho (\vec{q} \cdot d\vec{A}) + \frac{\partial}{\partial t} \int_{CV} (e\rho dV) \quad (4.17)$$

4.2 The General Energy Equation

Assume potential energy $e_p = gh$ (due to gravitational field of the earth)

$$\text{Then } e = u + gh + \frac{q^2}{2}$$

Then, Eq. (4.17) becomes

$$\begin{aligned} & \frac{\delta Q}{dt} - \frac{\delta W_{shaft}}{dt} - \frac{\delta W_{shear}}{dt} \\ & = \oint_{cs} \left(\frac{p}{\rho} + u + gh + \frac{q^2}{2} \right) \rho (\vec{q} \cdot d\vec{A}) + \frac{\partial}{\partial t} \int_{cv} e \rho dV \end{aligned} \quad (4.17)$$

4.2 The General Energy Equation

- Application: generalized apparatus

At boundaries normal to flow lines \rightarrow no shear

$$\rightarrow W_{shear} = 0 \quad (4.18)$$

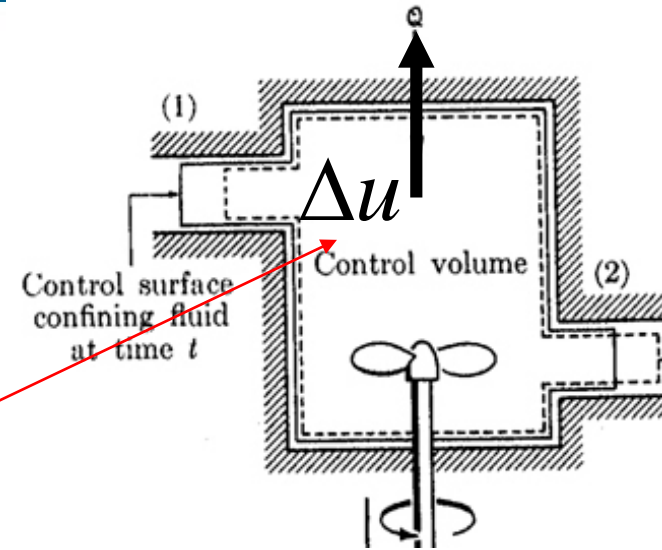
$$\frac{\delta Q}{dt} - \frac{\delta W_{shaft}}{dt} = \oint_{CS} \left(\frac{p}{\rho} + u + gh + \frac{q^2}{2} \right) \rho (\vec{q} \cdot d\vec{A}) + \frac{\partial}{\partial t} \int_{CV} e \rho dV \quad (4.19)$$

For steady motion,

$$\frac{\delta Q}{dt} - \frac{\delta W_{shaft}}{dt} = \oint_{CS} \left(\frac{p}{\rho} + u + gh + \frac{q^2}{2} \right) \rho (\vec{q} \cdot d\vec{A}) \quad (4.20)$$

4.2 The General Energy Equation

- ❖ Effect of friction
 - This effect is accounted for implicitly.
 - This results in a degradation of mechanical energy into heat which may be transferred away (Q , heat transfer), or may cause a temperature change
 - modification of internal energy
- Thus, Eq. (4.20) can be applied to both viscous fluids and non-viscous fluids (ideal frictionless processes).

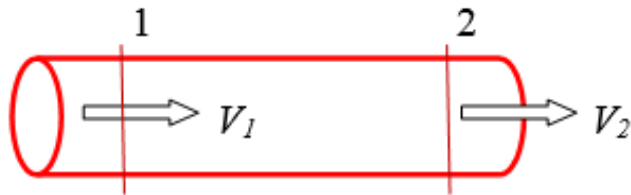


4.2 The General Energy Equation

4.2.3 1 D Steady flow equations

For flow through conduits, properties are uniform normal to the flow direction.

→ one-dimensional steady flow



$$\frac{\delta Q}{dt} - \frac{\delta W_{shaft}}{dt} = \oint_{CS} \left(u + \frac{p}{\rho} + gh + \frac{q^2}{2} \right) \rho (\vec{q} \cdot d\vec{A})$$

Integrated form of Eq. (4.20) = ② - ①

$$\frac{heat}{dt} - \frac{\delta W_{shaft}}{dt} = \left[u + \frac{p}{\rho} + gh + \frac{V^2}{2} \right]_{\text{②}} \rho Q - \left[u + \frac{p}{\rho} + gh + \frac{V^2}{2} \right]_{\text{①}} \rho Q$$

4.2 The General Energy Equation

where $\frac{V^2}{2}$ = average kinetic energy per unit mass

Section 1: $\int_1 \rho (\vec{q} \cdot d\vec{A}) = -\rho Q$ = mass flow rate into CV

Section 2: $\int_2 \rho (\vec{q} \cdot d\vec{A}) = \rho Q$ = mass flow from CV

Divide by ρQ (mass/time)

$$M = \rho Q dt$$

$$\frac{\text{heat transfer}}{\text{mass}} - \frac{W_{\text{shaft}}}{\text{mass}} = \left[u + \frac{p}{\rho} + gh + \frac{V^2}{2} \right]_{\textcircled{2}} - \left[u + \frac{p}{\rho} + gh + \frac{V^2}{2} \right]_{\textcircled{1}}$$

4.2 The General Energy Equation

Divide by g

$$\frac{\text{heat transfer}}{\text{weight}} - \frac{W_{shaft}}{\text{weight}} = \left[\frac{u}{g} + \frac{p}{\gamma} + h + \frac{V^2}{2g} \right]_{\textcircled{2}} - \left[\frac{u}{g} + \frac{p}{\gamma} + h + \frac{V^2}{2g} \right]_{\textcircled{1}}$$

(4.21)

- Energy Equation for 1-D steady flow: Eq. (4.21)
 - use average values for p , γ , h , u , and V at each flow section
 - use K_e (energy correction coeff.) to account for non-uniform velocity distribution over flow cross section

4.2 The General Energy Equation

$$K_e \frac{\rho}{2} V^2 Q = \int \frac{\rho}{2} q^2 dQ \quad \text{---- kinetic energy/time} = \frac{1}{2} \frac{mV^2}{t}$$

$$K_e = \frac{\int \frac{\rho}{2} q^2 dQ}{\frac{\rho}{2} V^2 Q} \geq 1 \quad (4.22)$$

$$\frac{\text{heat transfer}}{\text{weight}} - \frac{W_{shaft}}{\text{weight}} = \left[\frac{p}{\gamma} + h + K_e \frac{V^2}{2g} \right]_{\textcircled{2}} - \left[\frac{p}{\gamma} + h + K_e \frac{V^2}{2g} \right]_{\textcircled{1}} + \frac{u_2 - u_1}{g} \quad (4.23)$$

$$K_e = \begin{cases} 2, & \text{for laminar flow (parabolic velocity distribution)} \\ 1.06, & \text{for turbulent flow (smooth pipe)} \end{cases}$$

4.2 The General Energy Equation

For a fluid of uniform density γ

$$\frac{p_1}{\gamma} + h_1 + K_{e_1} \frac{V_1^2}{2g} = \frac{p_2}{\gamma} + h_2 + K_{e_2} \frac{V_2^2}{2g} + \frac{W_{shaft}}{weight} - \frac{\text{heat transfer}}{weight} + \frac{u_2 - u_1}{g}$$

(4.24)

→ unit: m (energy per unit weight)

For viscous fluid;

$$-\frac{\text{heat transfer}}{weight} + \frac{u_2 - u_1}{g} = H_{L_{1-2}}$$

→ loss of mechanical energy

~ irreversible in liquid

4.2 The General Energy Equation

Then, Eq. (4.24) becomes

$$\frac{p_1}{\gamma} + h_1 + K_{e_1} \frac{V_1^2}{2g} = \frac{p_2}{\gamma} + h_2 + K_{e_2} \frac{V_2^2}{2g} + \Delta H_M + \Delta H_{L_{1-2}} \quad (4.24a)$$

where ΔH_M = shaft work transmitted from the system to the outside

$$H_1 = H_2 + \Delta H_M + \Delta H_{L_{1-2}} \quad (4.24b)$$

where H_1, H_2 = weight flow rate average values of total head

4.2 The General Energy Equation

❖ Bernoulli Equation

Assume

- ① ideal fluid → friction losses are negligible
- ② no shaft work → $\Delta H_M = 0$
- ③ no heat transfer and internal energy is constant → $\Delta H_{L_{1-2}} = 0$

$$\frac{p_1}{\gamma} + h_1 + K_{e_1} \frac{V_1^2}{2g} = \frac{p_2}{\gamma} + h_2 + K_{e_2} \frac{V_2^2}{2g} \quad (4.25)$$

$$H_1 = H_2$$

4.2 The General Energy Equation

If $K_{e1} = K_{e2} = 1$, then Eq. (4.25) reduces to

The diagram shows the general energy equation (4.26) with four labels in red boxes pointing to specific terms in the equation:

- work**: points to the $\frac{p_1}{\gamma}$ term on the left side.
- Pressure head**: points to the h_1 term on the left side.
- Potential head**: points to the h_2 term on the right side.
- Velocity head**: points to the $\frac{V_2^2}{2g}$ term on the right side.

$$H = \frac{p_1}{\gamma} + h_1 + \frac{V_1^2}{2g} = \frac{p_2}{\gamma} + h_2 + \frac{V_2^2}{2g} \quad (4.26)$$

~ total head along a conduct is constant

4.2 The General Energy Equation

- Grade lines

1) Energy (total head) line (E.L) ~ H above datum

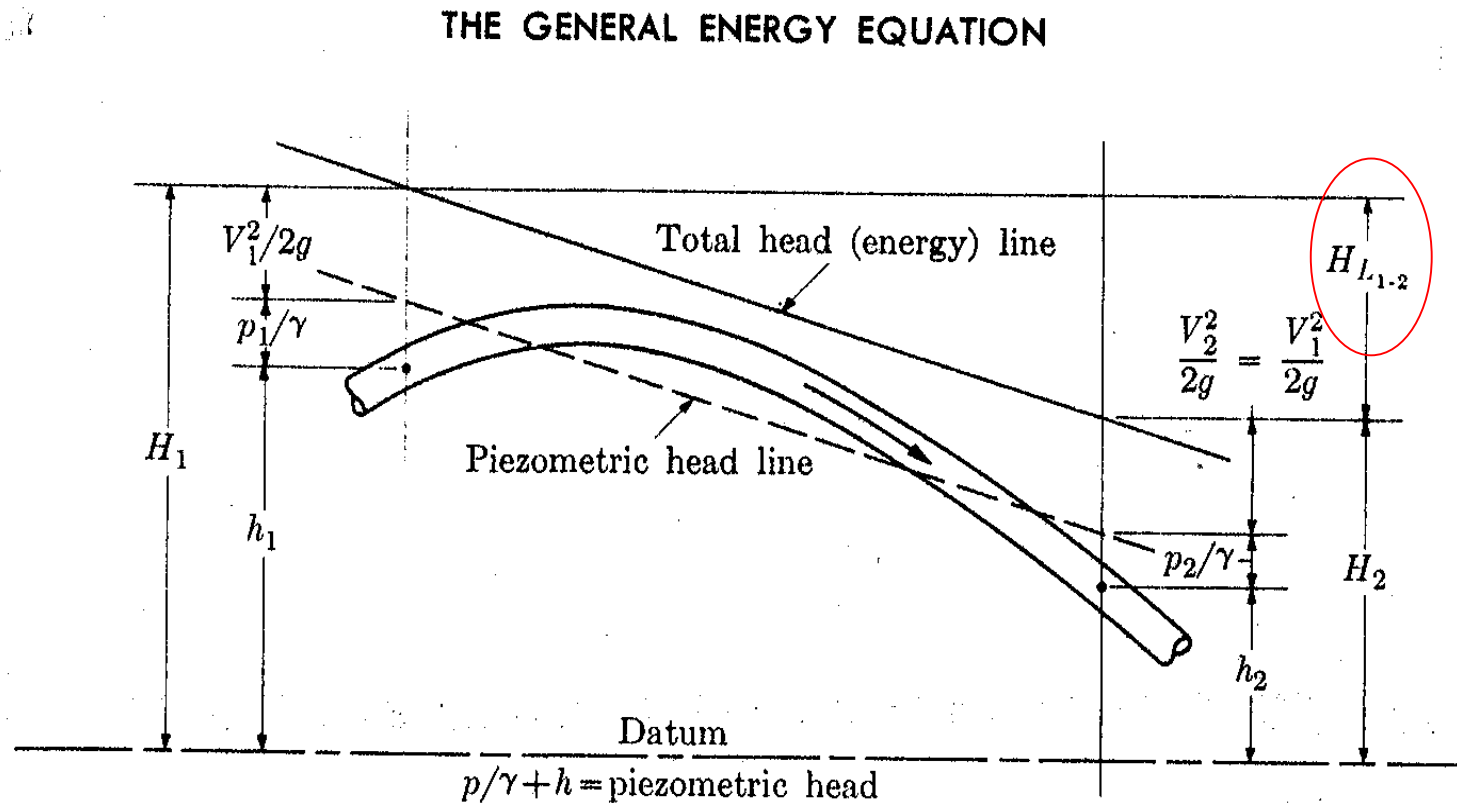
2) Hydraulic (piezometric head) grade line (H.G.L.)

$$= \left(\frac{p}{\gamma} + h \right) \text{above datum}$$

For flow through a pipe with a constant diameter

$$V_1 = V_2 \quad \rightarrow \quad \frac{V_1^2}{2g} = \frac{V_2^2}{2g}$$

4.2 The General Energy Equation



4.2 The General Energy Equation

- 1) If the fluid is real (viscous fluid) and if no energy is being added, then the energy line may never be horizontal or slope upward in the direction of flow.
- 2) Vertical drop in energy line represents the head loss or energy dissipation.