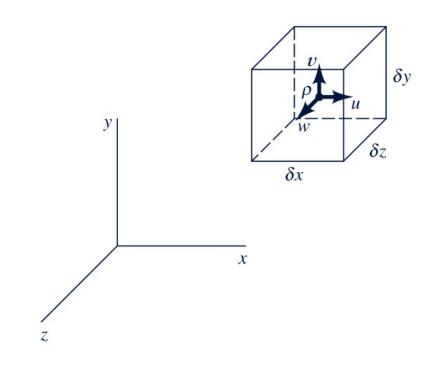
# **Chapter 6 Equations of Continuity and Motion**

### Session 6-2 Equation of motion







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- 6.2 Stream Function in 2-D, Incompressible Flows
- 6.3 Rotational and Irrotational Motion
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  - 6.6 Irrotational Motion
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- N-S equations are important in viscous flow problems.
- Laminar motion
- ~ orderly state of flow in which macroscopic fluid particles move in layers
- ~ viscosity effect is dominant
- ~ no-slip condition @ boundary wall
- ~ apply concept of the Newtonian viscosity
- ~ low Re

### [Ex]

- 1. Laminar flow between two parallel plates  $\rightarrow$  Couette flow
- 2. Laminar flow through a tube (pipe) of constant diameter  $\rightarrow$  Poiseuelle flow





[Re] Reynolds number = inertial force / viscous force = destabilizing force / stabilizing force

- Viscous force
- ~ dissipative
- ~ have a stabilizing or damping effect on the motion
- ~ use Reynolds number
- [Cf] Turbulent flow
  - ~ unstable flow
  - ~ instantaneous velocity is no longer unidirectional
  - ~ destabilizing force > stabilizing force





#### 6.5.1 Laminar flow between two parallel plates

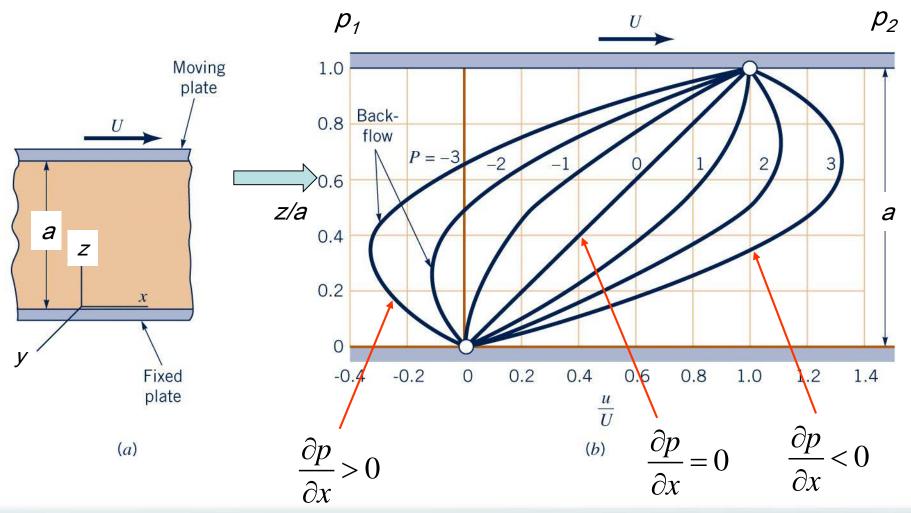
Consider the two-dimensional, <u>steady</u>, laminar flow between parallel plates in which either of two surfaces is moving at <u>constant velocity</u> and there is also an <u>external pressure gradient</u>.

Assumptions:

2-D flow (x, z)  $\rightarrow v = 0$ ;  $\frac{\partial()}{\partial y} = 0$ steady flow  $\rightarrow \frac{\partial()}{\partial t} = 0$ parallel flow  $\rightarrow w = 0$ ;  $\frac{\partial w}{\partial ()} = 0$ z-axis coincides with  $h \rightarrow \frac{\partial h}{\partial x} = \frac{\partial h}{\partial y} = 0$ ;  $\frac{\partial h}{\partial z} = 1$ 



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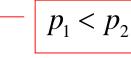






i)  $\frac{\partial p}{\partial x} < 0 \rightarrow$  pressure gradient <u>assists</u> the viscously induced motion to overcome the shear force at the lower surface

ii)  $\frac{CP}{\partial x} > 0 \rightarrow$  pressure gradient <u>resists</u> the motion which is induced by the motion of the upper surface







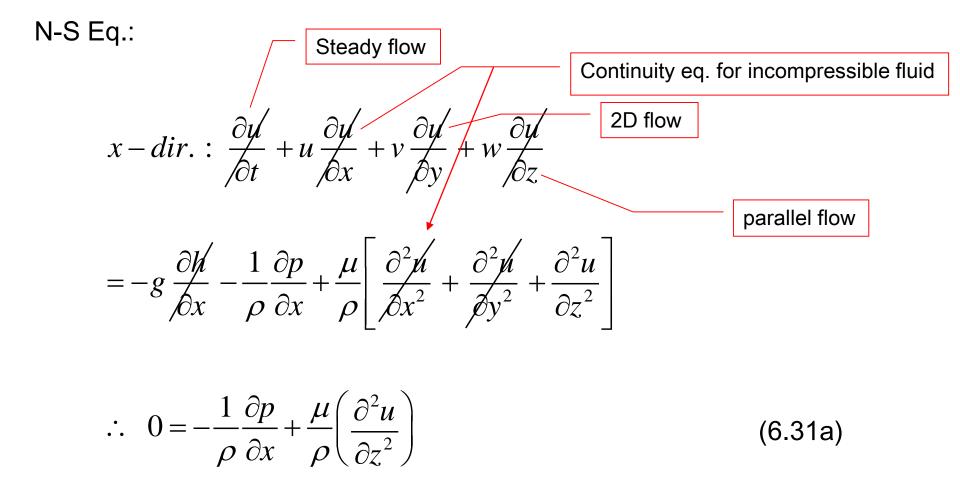
Continuity eq. for two-dimensional, parallel flow:

$$\frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0$$

$$\rightarrow \begin{cases} \frac{\partial^2 u}{\partial x^2} = 0\\ u = f(z) \text{ only} \end{cases}$$











$$z - dir.: \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z}$$
$$= -g \frac{\partial h}{\partial z} - \frac{1}{\rho} \frac{\partial p}{\partial z} + \frac{\mu}{\rho} \left[ \frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2} \right]$$

$$\therefore \quad 0 = -g - \frac{1}{\rho} \frac{\partial p}{\partial z}$$

(6.31b): 
$$\frac{\partial p}{\partial z} = -\rho g = -\gamma$$

$$\therefore \qquad p = -\gamma z + f(x)$$



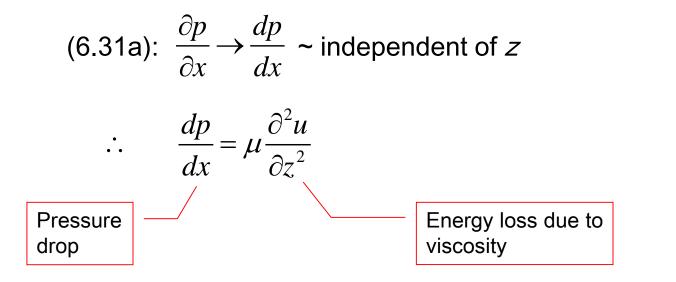
(6.31b)

(6.32)



 $\rightarrow$  hydrostatic pressure distribution normal to flow

 $\rightarrow$  For any orientation of *z*-axis. in case of a parallel flow, pressure is distributed hydrostatically in a direction normal to the flow.



(A)





Integrate (A) twice w.r.t. z to derive u(z)

$$\iint \frac{dp}{dx} dz dz = \iint \mu \frac{\partial^2 u}{\partial z^2} dz dz$$
$$\int \frac{dp}{dx} z dz = \int \mu \frac{\partial u}{\partial z} dz + \int C_1 dz$$
$$\frac{dp}{dx} \frac{z^2}{2} = \mu u + C_1 z + C_2$$

 $\mu \frac{\partial^2 u}{\partial z^2} = \frac{dp}{dx}$ 

(6.33)

Use the boundary conditions,

i) 
$$z = 0, \quad u = 0 \rightarrow \frac{dp}{dx} \times 0 = \mu(0) + C_2$$
  $\therefore C_2 = 0$ 





ii) 
$$z = a, \ u = U \rightarrow \frac{dp}{dx}\frac{a^2}{2} = \mu U + C_1 a$$

$$\therefore C_1 = \frac{1}{a} \left( \frac{dp}{dx} \frac{a^2}{2} - \mu U \right)$$

:. (6.33) becomes

$$\frac{dp}{dx}\frac{z^2}{2} = \mu u + \frac{1}{a}\left(\frac{dp}{dx}\frac{a^2}{2} - \mu U\right)z$$
$$\therefore \quad \mu u = \frac{z}{a}\mu U - \frac{dp}{dx}\left(\frac{az}{2} - \frac{z^2}{2}\right)$$



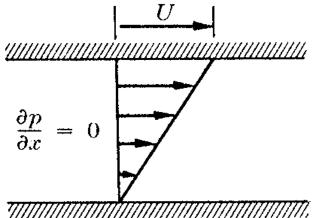


$$u(z) = u = \frac{U}{a}z - \frac{a}{2\mu}\frac{dp}{dx}\left(1 - \frac{z}{a}\right)z$$
(6.34)
Velocity
driven
Pressure
driven

i) If 
$$\frac{dp}{dx} = 0 \longrightarrow$$
 Couette flow (plane Couette flow)

$$u = \frac{U}{a}z \tag{6.35}$$

 $\rightarrow$  driving mechanism = U(velocity)

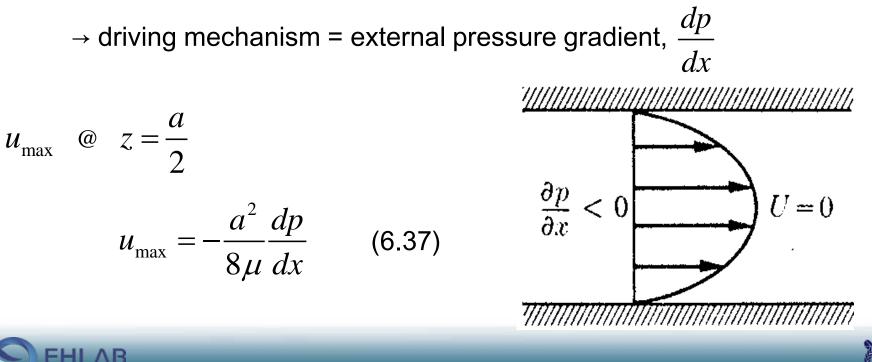






ii) If  $U = 0 \rightarrow 2$ -D Poiseuille flow (plane Poiseuille flow)

$$u = \frac{1}{2\mu} \frac{dp}{dx} (z - a) z \quad \sim \text{ parabolic} \tag{6.36}$$





$$V$$
 = average velocity

$$=\frac{Q}{A}=\frac{2}{3}u_{\max}=-\frac{a^2}{12\mu}\frac{dp}{dx}$$

(6.38)

#### [Re] detail

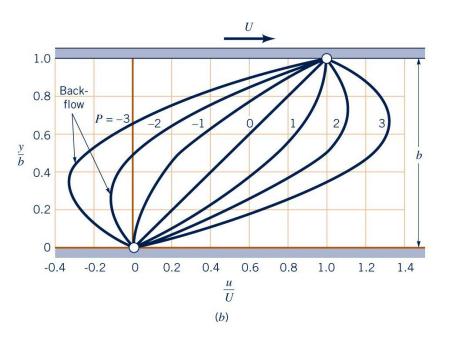
$$Q = \int_{0}^{a} u \, dz = \int_{0}^{a} \frac{1}{2\mu} \frac{dp}{dx} \left( z^{2} - az \right) dz = -\frac{1}{12\mu} \frac{dp}{dx} a^{3}$$
$$A = a \times 1 \qquad \therefore \quad V = \frac{Q}{A} = -\frac{a^{2}}{12\mu} \frac{dp}{dx} = \frac{2}{3} u_{\text{max}}$$





#### [Re] Dimensionless form

$$\frac{u}{U} = \frac{z}{a} - \frac{a^2}{2\mu U} \frac{dp}{dx} \frac{z}{a} \left(1 - \frac{z}{a}\right)$$
$$P = -\frac{a^2}{2\mu U} \frac{dp}{dx}$$
$$\frac{u}{U} = \frac{z}{a} + P \frac{z}{a} \left(1 - \frac{z}{a}\right)$$

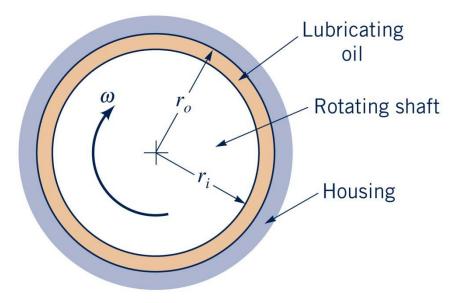






[Cf] <u>Couette flow</u> in the narrow gap of a journal bearing Flow between closely spaced concentric cylinders in which one cylinder is fixed and the other cylinder rotates with a constant angular velocity,  $\omega$ 

$$U = r_i \omega$$
$$a = r_o - r_i$$
$$\tau \approx \mu \frac{U}{a}$$





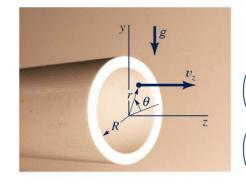


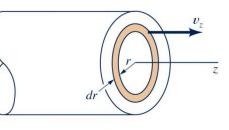
6.5.2 Laminar flow in a circular tube of constant diameter

- $\rightarrow$  Hagen-Poiseuille flow
- $\rightarrow$  Poiseuille flow: steady laminar flow due to pressure drop along a tube

Assumptions:

– use cylindrical coordinates





 $\frac{\partial p}{\partial p} < 0$ 

 $\partial x$ 

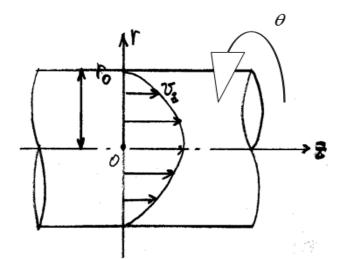


(*b*)





parallel flow 
$$\rightarrow \begin{array}{l} v_r = 0 \\ v_{\theta} = 0 \end{array}$$
  
Continuity eq.  $\rightarrow \begin{array}{l} \frac{\partial v_z}{\partial z} = 0 \\ \frac{\partial v_z}{\partial r} \neq 0 \end{array}$   
paraboloid  $\rightarrow \begin{array}{l} \frac{\partial v_z}{\partial \theta} = 0 \end{array}$   
steady flow  $\rightarrow \begin{array}{l} \frac{\partial v_z}{\partial t} = 0 \end{array}$ 







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### Eq. (6.29c) becomes

$$0 = -\frac{\partial p}{\partial z} + \rho g_z + \mu \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial v_z}{\partial r} \right)$$





#### Then (A) becomes

$$\frac{d}{dz}(p+\gamma h) = \mu \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial v_z}{\partial r} \right)$$
$$\frac{1}{\mu} \frac{d}{dz}(p+\gamma h)r = \frac{\partial}{\partial r} \left( r \frac{\partial v_z}{\partial r} \right)$$

Integrate (B) twice w.r.t. r to derive  $v_z(r)$ 

$$\frac{1}{\mu}\frac{d}{dz}(p+\gamma h)\frac{r^2}{2} = r\frac{\partial v_z}{\partial r} + C_1$$



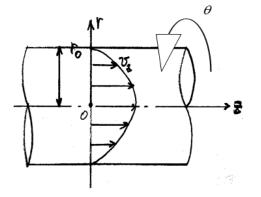


(B)

(C)

$$\frac{1}{2\mu}\frac{d}{dz}\left(p+\gamma h\right)r = \frac{\partial v_z}{\partial r} + \frac{C_1}{r}$$

$$\frac{1}{2\mu}\frac{d}{dz}(p+\gamma h)\frac{r^2}{2} = v_z + C_1 \ln r + C_2 \qquad (D)$$



#### Using BCs

$$r = 0, v_z = v_{z_{\text{max}}} \rightarrow (C): C_1 = 0$$
  
 $r = r_0, v_z = 0 \rightarrow (D): C_2 = \frac{1}{2\mu} \frac{d}{dz} (p + \gamma h) \frac{r_0^2}{2}$  (D1)





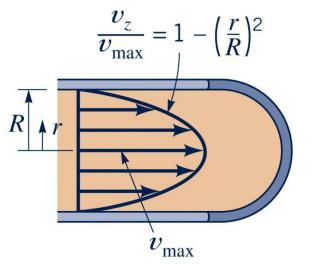
Then, substitute (D1) into (D) to obtain  $v_z$ 

piezometric pressure

$$v_{z} = \frac{1}{4\mu} \left[ -\frac{d}{dz} (p + \gamma h) \right] (r_{0}^{2} - r^{2})$$
 (6.39)

$$v_{z} = -\frac{d}{dz} \left( \frac{p + \gamma h}{4\mu} \right) \frac{r_{0}^{2}}{4\mu} \left[ 1 - \left( \frac{r}{r_{0}} \right)^{2} \right]$$

→ equation of a paraboloid of revolution









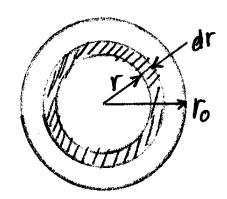
(1) maximum velocity,  $V_{z_{\text{max}}}$ 

$$v_{z_{\text{max}}}$$
 @  $r=0$ 

$$v_{z_{\text{max}}} = -\frac{d}{dz} (p + \gamma h) \frac{r_0^2}{4\mu}$$

(2) mean velocity,  $V_{z}$ 

$$dQ = v_z dA$$
$$= \frac{1}{4\mu} \left[ -\frac{d}{dz} (p + \gamma h) \right] (r_0^2 - r^2) 2\pi r dr$$



(6.40)

(6.41)





$$Q = \int_{0}^{r_{0}} \frac{1}{4\mu} \left[ -\frac{d}{dz} (p + \gamma h) \right] (r_{0}^{2} - r^{2}) 2\pi r dr$$

$$= \frac{\pi}{2\mu} \left[ -\frac{d}{dz} (p + \gamma h) \right] \left[ r_0^2 \frac{r^2}{2} - \frac{r^4}{4} \right]_r^{r_0}$$

.....

$$=\frac{\pi r_0^4}{8\mu} \left[ -\frac{d}{dz} (p + \gamma h) \right]$$

$$\therefore \quad V_z = \frac{Q}{A} = \frac{Q}{\pi r_0^2} = \frac{r_0^2}{8\mu} \left[ -\frac{d}{dz} (p + \gamma h) \right] = \frac{v_{z_{\text{max}}}}{2}$$
(E)  
[Cf] For 2 - D Poiseuille flow  $V = \frac{2}{3} u_{\text{max}}$ 



(3) Head loss per unit length of pipe

Total head = piezometric head + velocity head

Here, velocity head is constant.

Thus, total head loss = piezometric head change

$$\frac{h_f}{L} = \frac{1}{\gamma} \left[ -\frac{d}{dz} (p + \gamma h) \right] = \frac{8\mu V_z}{\gamma r_0^2} = \frac{32\mu V_z}{\gamma D^2}$$
(E)

$$\frac{h_f}{L} \equiv \frac{\Delta p}{\gamma}$$

(6.42)

where  $D = 2r_0 = \text{diameter}$ 





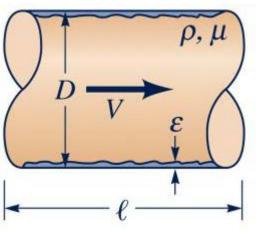
[Re] Consider Darcy-Weisbach Eq.

$$\frac{h_f}{L} = f \frac{1}{D} \frac{V_z^2}{2g}$$

$$h_f =$$
 head loss due to friction

- f =friction factor
- Combine (6.42) and (F)

$$\frac{32\mu V_z}{\gamma D^2} = f \frac{1}{D} \frac{V_z^2}{2g}$$



(F)

(6.43)





$$f = \frac{64}{V_z} \frac{\nu}{D} = \frac{64}{V_z D / \nu} = \frac{64}{\text{Re}} \quad \Rightarrow \text{For laminar flow}$$
(6.44)

(4) Shear stress

$$\tau_{zr} = \mu \left( \frac{\partial v_r}{\partial z} + \frac{\partial v_z}{\partial r} \right) = \mu \frac{\partial v_z}{\partial r}$$

Differentiate (6.39) w.r.t. r

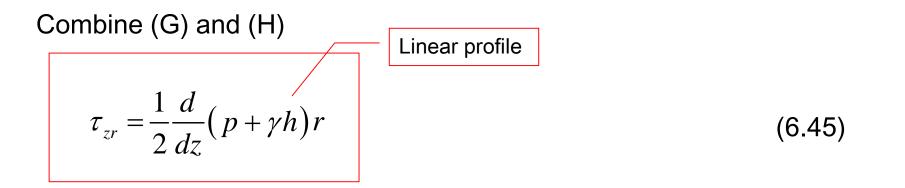
$$\frac{\partial v_z}{\partial r} = \frac{d}{dz} (p + \gamma h) \frac{1}{2\mu} r$$

(G)

(H)

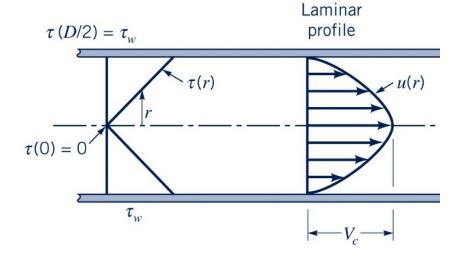






At center and walls

$$r = 0, \quad \tau_{zr} = 0$$
$$r = r_0, \quad \tau_{zr_{\text{max}}} = \frac{1}{2} \frac{d}{dz} (p + \gamma h) r_0$$



$$\tau_{zr} = \tau_{zr_{\max}} \frac{r}{r_0}$$



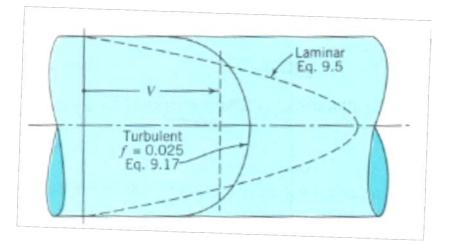


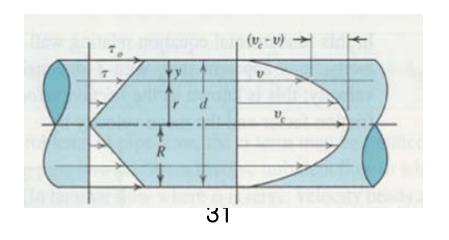
### Laminar flow :

$$v = v_c \left( 1 - \frac{r^2}{R^2} \right)$$
$$\tau = \tau_0 \left( 1 - \frac{y}{R} \right) = \frac{\tau_0 r}{R}$$

### Turbulent flow:

$$\frac{v_c - v}{v_*} = -\frac{1}{\kappa} \ln \frac{y}{R}$$
$$\tau = \tau_0 \left( 1 - \frac{y}{R} \right) = \frac{\tau_0 r}{R}$$









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