445.204

Introduction to Mechanics of Materials (재료역학개론)

Chapter 6: Torsion

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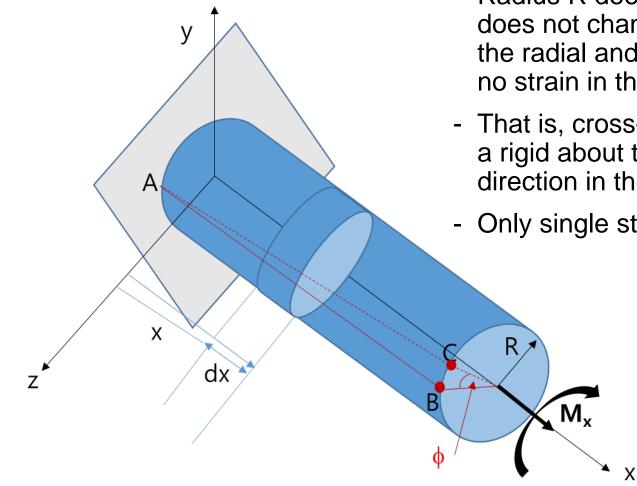
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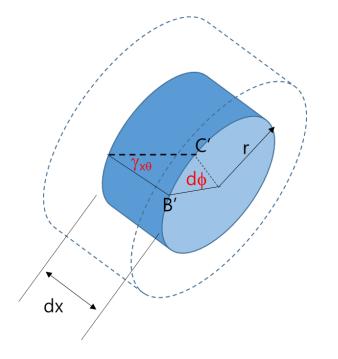
Torsion of circular shafts



Observation and assumptions

- Plane section remains plane during deformation; no warpage
- Radius R does not change, length does not change; i.e., normal strains in the radial and length are zeros; also no strain in the plane of cross section
- That is, cross-section simply rotates as a rigid about the axis of the shaft (or xdirection in the left figure)
- Only single strain component

Torsion of circular shafts



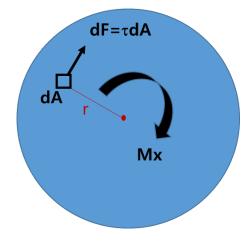
Angle of twist per unit length

$$\gamma_{x\theta} = \frac{B'C'}{dx} = \frac{rd\phi}{dx} = \frac{d\phi}{dx}r$$

Constitutive equation

$$\tau_{x\theta} = G\gamma_{x\theta} = G\frac{d\phi}{dx}r$$

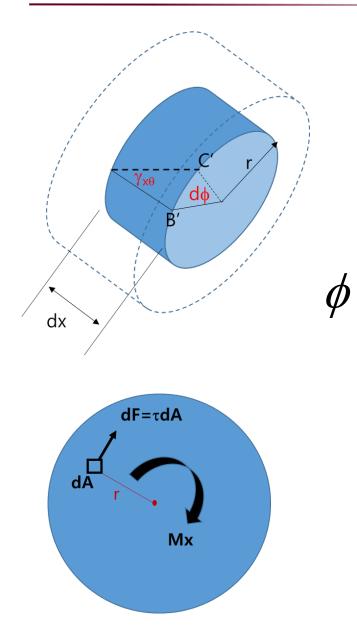
Equilibrium



$$M_{x} = \iint_{A} r\tau_{x\theta} dA = \iint_{A} r^{2}G \frac{d\phi}{dx} dA = G \frac{d\phi}{dx} \iint_{A} r^{2}dA = G \frac{d\phi}{dx} J$$
Polar moment

 $\frac{d\phi}{dx} = \frac{M_x}{GJ}$

Torsion of circular shafts



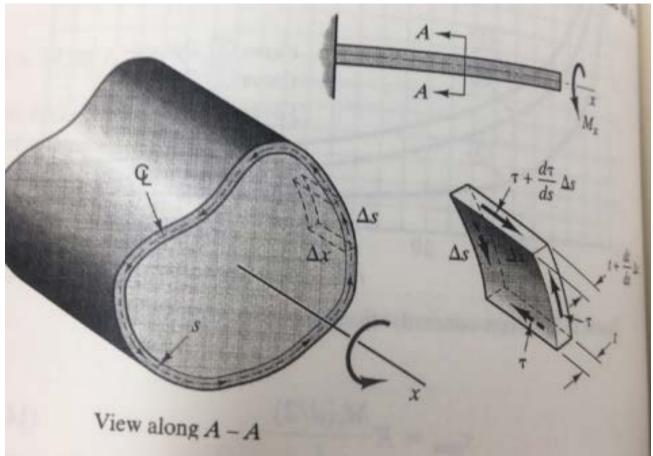
 $M_{\underline{x}}$ $d\phi$ GJ dx

Angle of twist for constant torque $\phi = \int_0^L d\phi = \int_0^L \frac{M_x}{GJ} dx = \frac{M_x L}{GJ}$ c.f. $\delta = \frac{PL}{EA}$ $=\frac{M_{x}r}{I}$ $\tau_{x\theta}$

Torsion of thin walled, non-circular closed shafts

Assumptions

- Tube is prismatic (or constant cross section)
- Wall thickness can be variable
- Define middle surface or midline (along this coordinate s is defined)

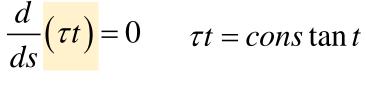


Torsion of thin walled, non-circular closed shafts

Applying equilibrium into the infinitesimal element

$$-\tau t \Delta x + \left(\tau + \frac{d\tau}{ds}\Delta s\right) \left(t + \frac{dt}{ds}\Delta s\right) \Delta x = 0$$

$$\left(\tau \frac{dt}{ds} + t \frac{d\tau}{ds}\right) \Delta s = 0$$

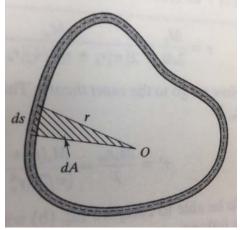


"Shear flow" is constant

Moment (torque) equilibrium

$$M_{x}\mathbf{i} = \oint \mathbf{r} \times (\tau t) d\mathbf{s} = (\tau t) \oint \mathbf{r} \times d\mathbf{s} = (\tau t) (2A\mathbf{i})$$

$$M_x = 2\tau tA$$
 $\tau = \frac{M_x}{2tA}$



A: total plane area enclosed by the midline s

Torsion of thin walled, non-circular closed shafts

Applying conservation of energy law, For the net rotation

$$\frac{1}{2}M_{x}\phi = \frac{1}{2}\int_{0}^{L}\tau \frac{\tau}{G}tdsdx$$
$$\phi = \frac{d\phi}{dx}L$$

$$M_{x}\left(\frac{d\phi}{dx}\right) = \frac{1}{G} \oint \tau^{2} t ds = \frac{1}{G} \oint \frac{M_{x}^{2}}{4t^{2}A^{2}} t ds$$

$$\left(\frac{d\phi}{dx}\right) = \frac{M_x}{4GA^2} \oint \frac{ds}{t} \implies \left(\frac{d\phi}{dx}\right) = \frac{M_x S}{4GA^2 t}$$

Constant thickness

Elastic-perfectly plastic torsion

From elastic circular shaft
$$\begin{aligned} \tau_{x\theta} &= \frac{M_x r}{J} \text{ or } M_x = \frac{\tau_{x\theta} J}{r} \\ T_{\max,el} &= \frac{\tau_s J}{R} = \frac{\tau_s}{R} \left(\frac{\pi}{2} R^4\right) = \frac{\pi}{2} R^3 \tau_s \\ T_{hinge} &= \int_0^{2\pi} \int_0^R r \tau_s \left(r dr d\theta\right) = 2\pi \tau_s \frac{R^3}{3} \\ \frac{T_{hinge}}{T_{\max,el}} &= \frac{4}{3} \\ T &= \int_0^{2\pi} \int_0^a r \left(\frac{r}{a} \tau_s\right) (r dr d\theta) + \\ \int_0^{2\pi} \int_a^R r(\tau_s) (r dr d\theta) = \frac{\pi \tau_s}{3} \left(2R^3 - \frac{1}{2}a^3\right) \end{aligned}$$

а

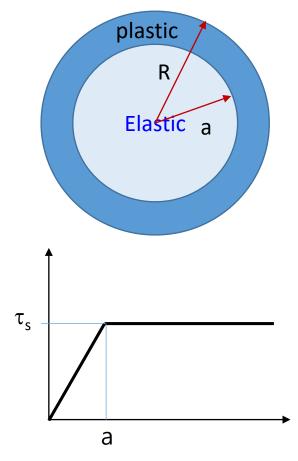
Elastic-perfectly plastic torsion

$$T = \int_0^{2\pi} \int_0^a r\left(\frac{r}{a}\tau_s\right) \left(rdrd\theta\right) + \int_0^{2\pi} \int_a^R r\left(\tau_s\right) \left(rdrd\theta\right) = \frac{\pi\tau_s}{3} \left(2R^3 - \frac{1}{2}a^3\right)$$

$$a = \left(4R^3 - \frac{6T}{\pi\tau_s}\right)^{1/3}$$
 Radius of elastic core

$$\gamma_{x\theta} = \frac{d\phi}{dx} r \quad \Rightarrow \frac{d\phi}{dx} = \frac{\gamma_{x\theta}}{r}$$

At r=a, $\gamma_{x\theta} = \frac{\tau_s}{G}$ Thus, $\frac{d\phi}{dx} = \frac{\tau_s}{Ga}$



Elastic-perfectly plastic torsion

Residual rate of twist

From,
$$\frac{d\phi}{dx} = \frac{M_x}{GJ}$$

$$\left(\frac{d\phi}{dx}\right)_{res} = \left(\frac{d\phi}{dx}\right)_{plastic} - \frac{T}{GJ}$$

Questions ?