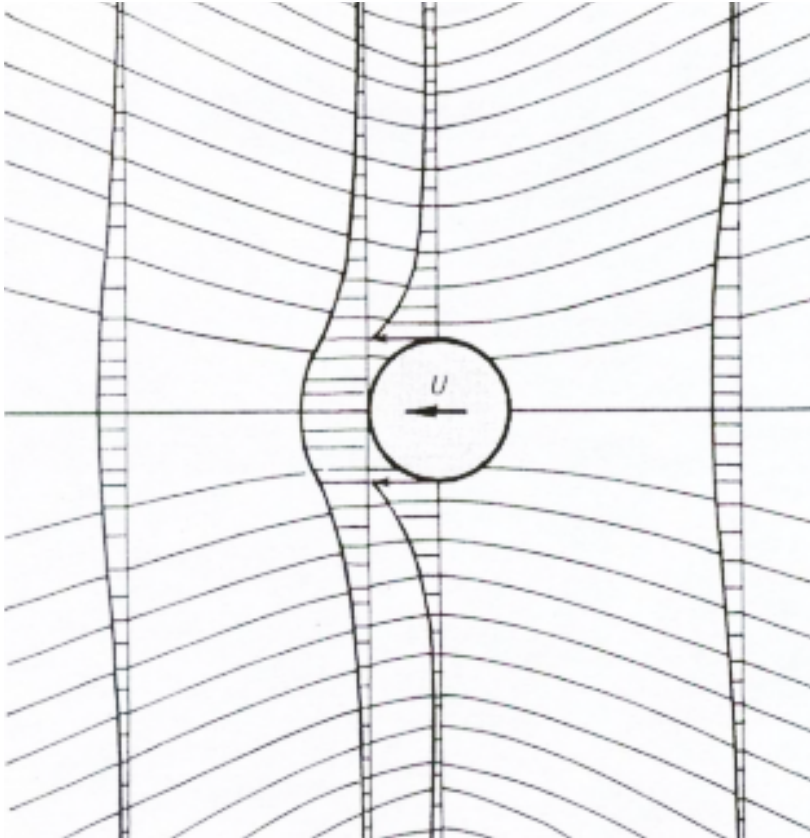


Creeping Flow around a Sphere

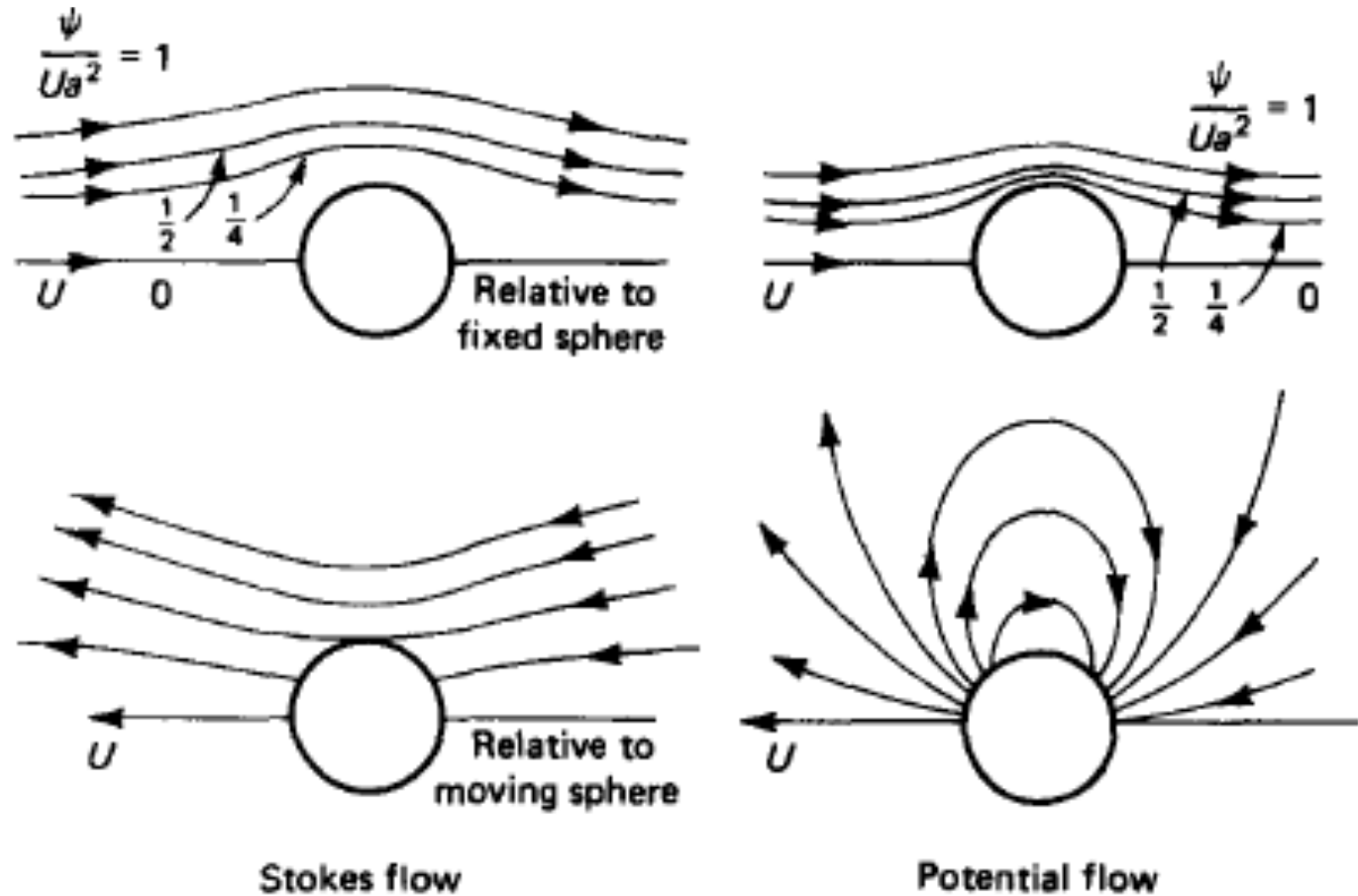
1



- Streamlines and velocity distributions in Stokes' solution of creeping flow due to a moving sphere
- This varies with Re_D
- There is no vortex shedding in the wake
- Viscous effects are felt everywhere



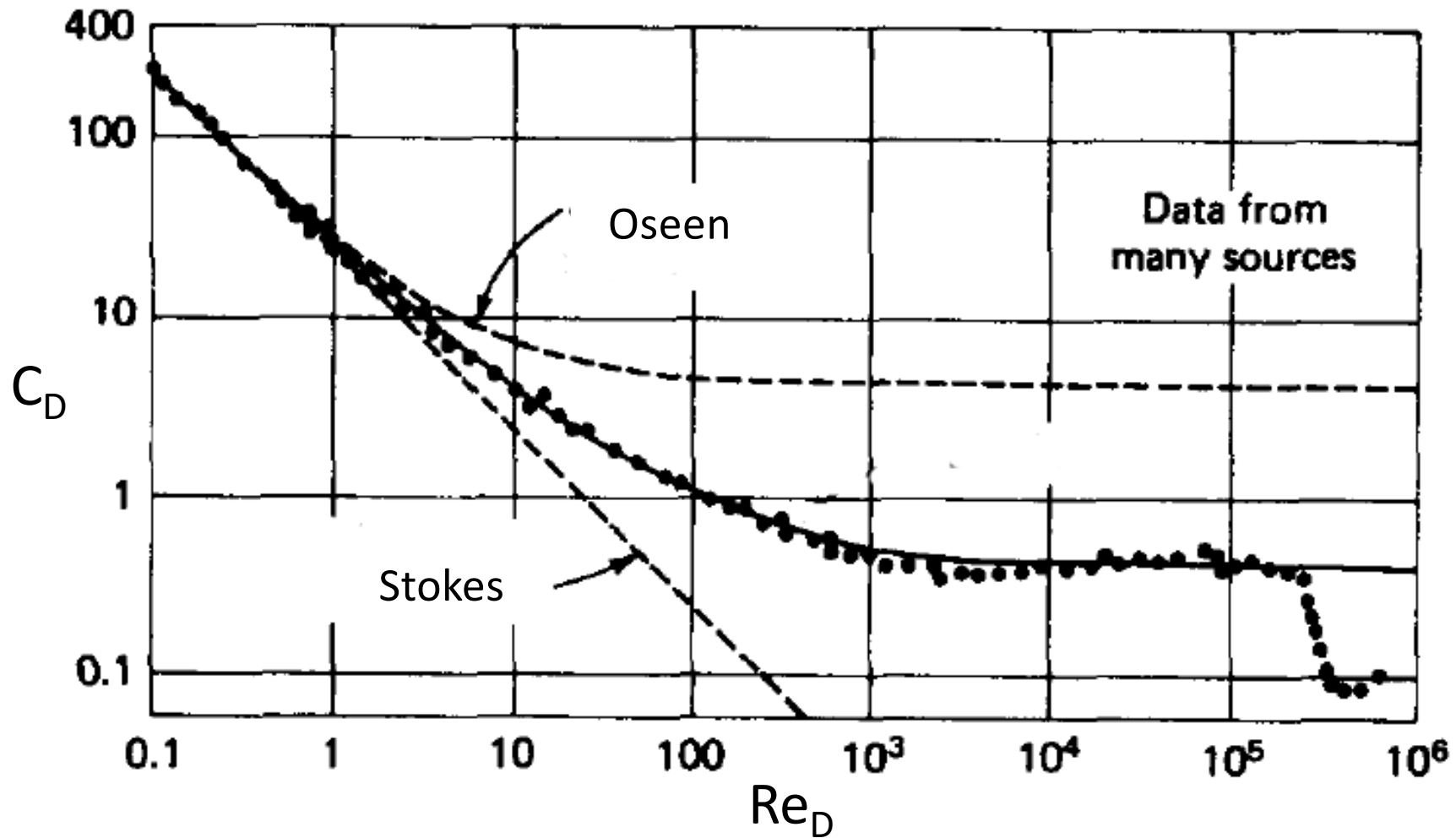
Creeping Flow around a Sphere



From White "Viscous Fluid Flow"



Creeping Flow around a Sphere



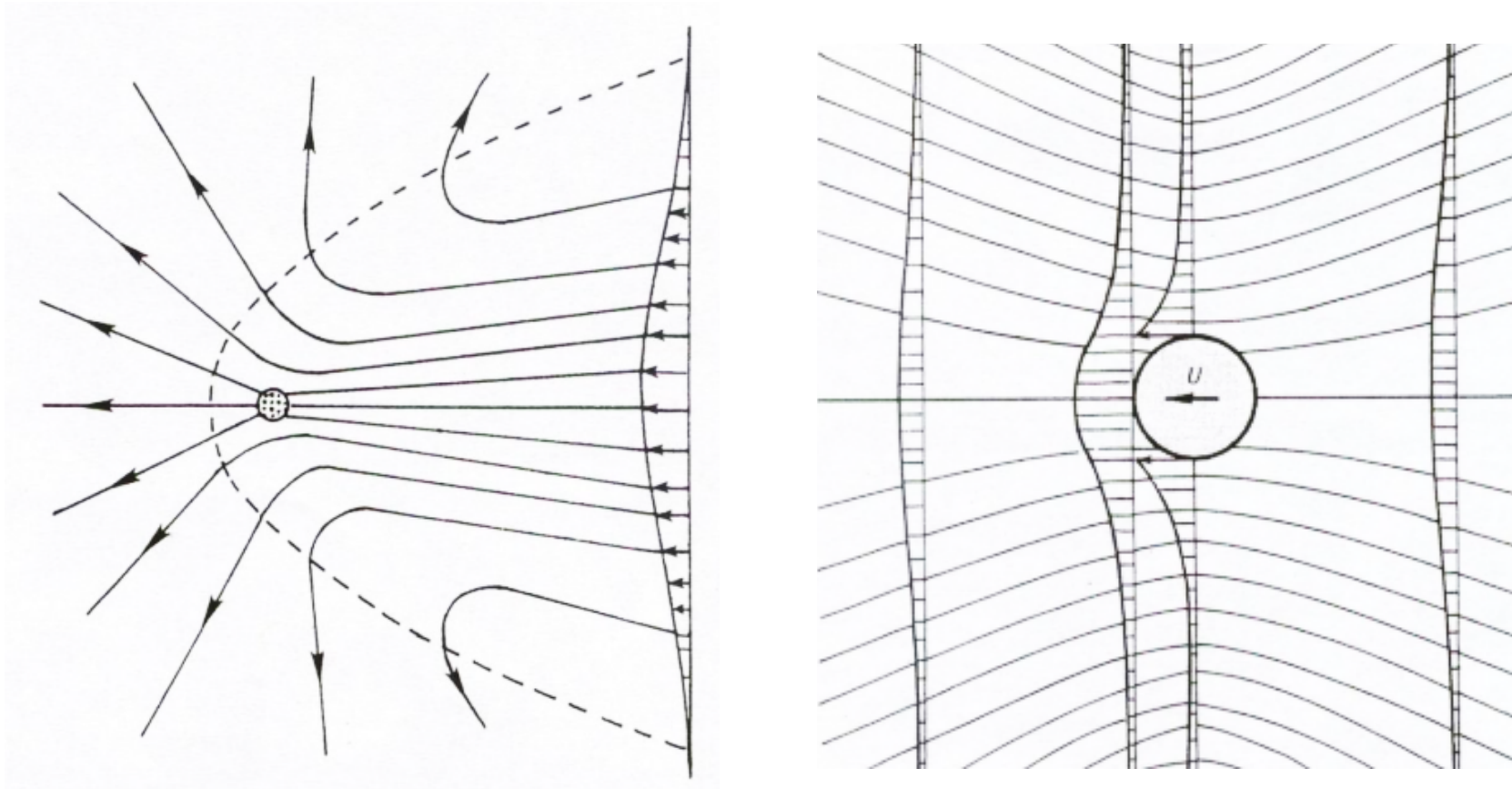
From White "Viscous Fluid Flow"



Creeping Flow around a Sphere

4

- Streamlines and velocity distributions in Oseen's solution of creeping flow due to a moving sphere.



- Note the upper stream and downstream asymmetry, a result of partial accounting for advection in the far field



* Non-uniformity of Stokes's Solution & Oseen's Improvement.

- as $r \rightarrow \infty$ (far away from the sphere): Stokes's sol. is NOT valid.

$$\frac{\text{inertia (advection)}}{\text{viscosity}} \sim Re \cdot \frac{r}{a}$$

$$\underline{\bar{u} \cdot \nabla \bar{u} = -\nabla p + \mu \nabla^2 \bar{u}} \quad (*)$$

↳ even if $Re \ll 1$,
if r/a is large enough
to have $r/a > \frac{1}{Re}$

→ inertia becomes important. $(Re \cdot \frac{r}{a} \gg 1)$
(at far-field) → limits of Stokes's solution.

• Oseen's Solution.

$$u = \underbrace{U_0}_{\text{free-stream}} + \underbrace{u'}_{\text{perturbation velocity } (\ll 1)} \quad v = v' \quad \omega = \omega' \quad \text{---} \textcircled{**}$$

free-stream

→ perturbation velocity ($\ll 1$)
(due to sphere)

momentum conservation

~~**~~ + ~~**~~
and
linearize.

$$\rho U_0 \frac{\partial u'_i}{\partial x_j} = - \frac{\partial p}{\partial x_i} + \mu \nabla^2 \bar{u}_i \quad ; \text{ Oseen's eq.}$$

$\bar{u} \cdot \nabla \bar{u}$ (linearized form)

$$\text{BC) } @ r = a, \quad u' = -U_0, \quad v' = \omega' = 0.$$

$$@ r \rightarrow \infty, \quad u' = v' = \omega' = 0.$$

$$\hookrightarrow C_D = \frac{24}{Re} \left(1 + \frac{3}{16} Re \right) ; \text{Oseen's sol.}$$

$$\text{cf) Stokes's sol} = C_D = \frac{24}{Re}.$$

MIDTERM. 10/31 (THU). 15:30 - 2 HOURS, 302-508.

(3) Flow past a circular cylinder(?)

Do we have a counter part of Stokes' solution for a sphere (3D) in 2D (i.e., circular cylinder)? No.

$\nabla^2 \bar{\omega} = 0$. in $r-\theta$ coordinates.



we seek $\psi(r, \theta) = f(r) \cdot \sin \theta$.

$$\left[\frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} \right] \psi = 0$$

$$\Rightarrow f(r) = Ar^3 + Br \cdot \log r + Cr + \frac{D}{r}$$

BC: ① $r \rightarrow \infty$, $f(r) = U_0 r$; $A = B = 0$, $C = U_0$.

② $r = a$, no-slip $\left(\frac{\partial \psi}{\partial r} = 0, \frac{\partial \psi}{\partial \theta} = 0 \right)$

\hookrightarrow No "D" can satisfy this BC!

\Rightarrow "Stokes' Paradox"

if we resort Stokes' approximation.

- valid @ $Re \rightarrow 0$.

- $\psi = \psi_0 + \psi_1 Re + \psi_2 Re^2 + \psi_3 Re^3 + \dots$

① in 3D ψ_0 exist. \rightarrow Stokes sol. \downarrow NOT valid
(sphere) as $r \rightarrow \infty$

ψ_1 was added.
(Oseen's improvement)

② in 2D (circular cylinder), ψ_0 does not exist
(\therefore inertia term can't be neglected at all).

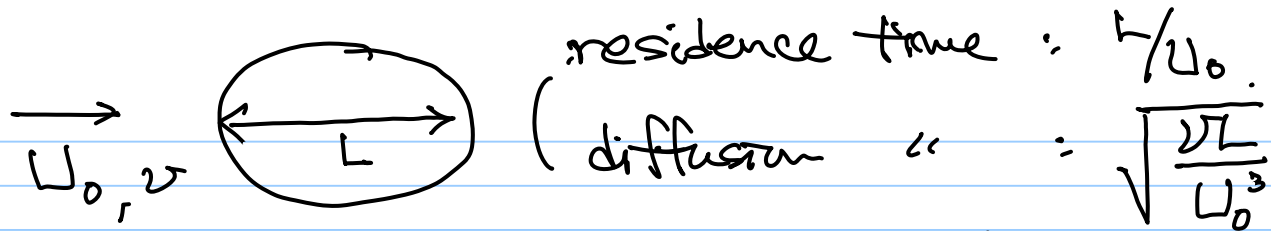
↑
MIDTERM
HW#2, etL.

BOUNDARY LAYERS

As $Re \uparrow$, convection of vorticity \gg diffusion of vorticity
(intra) (intra)

\Rightarrow viscous region becomes thin.

↳ outer: inviscid, irrotational \Rightarrow free-stream
(inner: viscous, rotational \Rightarrow boundary).



if diffusion time is much shorter than residence time.

$$\sqrt{\frac{2L}{U_0^3}} \ll \frac{L}{U_0} \rightarrow \sqrt{\frac{U_0 L}{\nu}} = \sqrt{Re} \gg 1$$

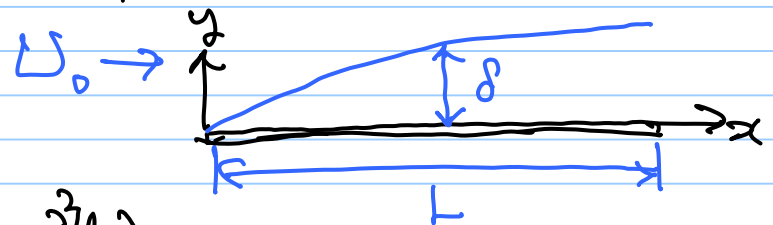
① order of magnitude analysis (Refer to Schlichting)

① 2D, ② incompressible, ③ flat-plate boundary-layer flow

④ thin boundary layer

$$\left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \right)$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} \right)$$



$$\left| \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial y} + \nu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} \right) \right.$$

w/ reference velocity, U_0 , $\hat{u} \equiv u/U_0$.

$$\hat{p} \equiv P/\rho U_0^2, \quad \hat{t} \equiv t/\tau, \quad \hat{x} \equiv x/L.$$

$$\Rightarrow \frac{\partial \hat{u}}{\partial \hat{x}} + \frac{\partial \hat{u}}{\partial \hat{y}} = 0$$

$\mathcal{O}(1)$
 $\mathcal{O}(f) \sim \mathcal{O}(0)$

$$\left(\frac{L}{U_0 \tau} \right) \frac{\partial \hat{u}}{\partial \hat{t}} + \hat{u} \frac{\partial \hat{u}}{\partial \hat{x}} + \hat{v} \frac{\partial \hat{u}}{\partial \hat{y}} = -\frac{\partial \hat{p}}{\partial \hat{x}} + \frac{1}{Re_L} \left(\frac{\partial^2 \hat{u}}{\partial \hat{x}^2} + \frac{\partial^2 \hat{u}}{\partial \hat{y}^2} \right)$$

$$\left(\frac{L}{U_0 \tau} \right) \frac{\partial \hat{u}}{\partial \hat{t}} + \hat{u} \frac{\partial \hat{u}}{\partial \hat{x}} + \hat{v} \frac{\partial \hat{u}}{\partial \hat{y}} = -\frac{\partial \hat{p}}{\partial \hat{y}} + \frac{1}{Re_L} \left(\frac{\partial^2 \hat{u}}{\partial \hat{x}^2} + \frac{\partial^2 \hat{u}}{\partial \hat{y}^2} \right), \quad Re_L \equiv \frac{U_0 L}{\nu}$$

Select L so that $f/L \ll 1$, ($f \ll L$) and $\frac{\partial \hat{u}}{\partial \hat{x}} \sim \mathcal{O}(1)$.

$$\hat{u} \equiv u/U_0 \sim \mathcal{O}(1). \rightarrow \hat{x} \sim \mathcal{O}(1), \hat{y} \equiv y/L \sim \mathcal{O}(\delta) \sim \mathcal{O}(0).$$

$$\rightarrow \frac{\partial \hat{u}}{\partial \hat{y}} \sim \mathcal{O}(1). \rightarrow \hat{u} \sim \mathcal{O}(\delta).$$

$$\rightarrow \frac{\partial \hat{u}}{\partial \hat{x}} \sim \mathcal{O}(\delta), \frac{\partial^2 \hat{u}}{\partial \hat{x}^2} \sim \mathcal{O}(\delta), \frac{\partial^2 \hat{u}}{\partial \hat{x}^2} \sim \mathcal{O}(1).$$

$$\frac{\partial \hat{u}}{\partial \hat{y}} \sim \mathcal{O}(1/\delta), \frac{\partial^2 \hat{u}}{\partial \hat{y}^2} \sim \mathcal{O}(1/\delta^2).$$

If $L/U_0 \gg 1$: Rayleigh BL.

$\ll 1$: Quasi-steady BL

$\mathcal{O} \rightarrow \infty$: Steady BL.

• Assume steady flow.

• from x-momentum: $\frac{1}{Re_L} \cdot \frac{1}{\delta^2} \sim O(1) \rightarrow Re_L \sim \frac{1}{\delta^2} \quad (Re_L \gg 1)$

• BL concept is valid at higher Re .

• from y-momentum: $\frac{1}{Re_L} \cdot \frac{1}{\delta} \sim O(\delta)$, $-\frac{\partial \hat{p}}{\partial \hat{y}} \sim O(\delta)$

$$\therefore \frac{\partial \hat{p} / \partial \hat{x}}{\partial \hat{p} / \partial \hat{y}} \sim O(\delta) \quad \therefore \frac{\partial \hat{p}}{\partial \hat{x}} \rightarrow \frac{\partial \hat{p}}{\partial \hat{y}}$$

$$\left(\frac{\partial u}{\partial x} + \frac{\partial u}{\partial y} = 0 \right.$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + \nu \frac{\partial^2 u}{\partial y^2}$$

; Prandtl's
Boundary-Layer eqn.