

## Precision Machine Design-Acoustic Isolation

Ultra-precision machines are also influenced by the acoustic wave or sound pressure wave, when they are exposed to acoustic noise environment.

In this case, the best solution is to move away machines from the noisy environment, in order to escape from the noise headache.

Otherwise, proper acoustic enclosures are to be designed to give isolation from acoustic disturbance, which is called as acoustic isolation.

This chapter is to deliver the knowledge and methods for acoustic isolation or noise control in view of the precision machine design.

### Acoustic wave or sound wave:

Sound is a propagation of air pressure through media.

Once sound is generated, then propagated through media in the form of lateral wave of pressure in the direction of travelling.

Followings are some terminology for sound or acoustic wave.

Let  $C$  be the speed of sound, or speed of acoustic wave;

$$C=f\lambda$$

where  $\lambda$ =wavelength of sound wave,

$f$ =frequency of wave [Hz]

One octave band with central frequency  $f_c$  indicates

$$f_c 2^{-1/2} \leq f \leq f_c 2^{1/2}$$

One third octave band with central frequency  $f_c$  indicates

$$f_c 2^{-1/6} \leq f \leq f_c 2^{1/6}$$

$$C=[E/\rho]^{1/2} \text{ for solid media,}$$

where  $E$ =Young's modulus,  $\rho$  is the density

$$C=[\gamma P/\rho]^{1/2} \text{ for gas media}$$

where  $\gamma$ =ratio of specific heat= $C_p/C_v$ ,  $P$ =Pressure,  $\rho$ =Density

$C = 331.5 + 0.6T$  for air [m/s]

where T is temperature of air [°C]

Hearable pressure range:  $2 \times 10^{-5} \text{ Pa} \sim 60 \text{ Pa}$ , where  $1 \text{ Pa} = 1 \text{ N/m}^2$

Hearable freq. range:  $20 \text{ Hz} \sim 20,000 \text{ Hz}$

SPL (Sound Pressure Level) =  $20 \text{ Log}_{10} P_e/P_o$  [dB]

where  $P_o$  is  $2 \times 10^{-5} \text{ Pa}$ ,  $P_e$  is the effective pressure

PWL (Power Level) =  $10 \text{ Log}_{10} W/W_0$  [dB]

where  $W$  = power of sound in [W],  $W_0 = 1 \times 10^{-12} \text{ W}$

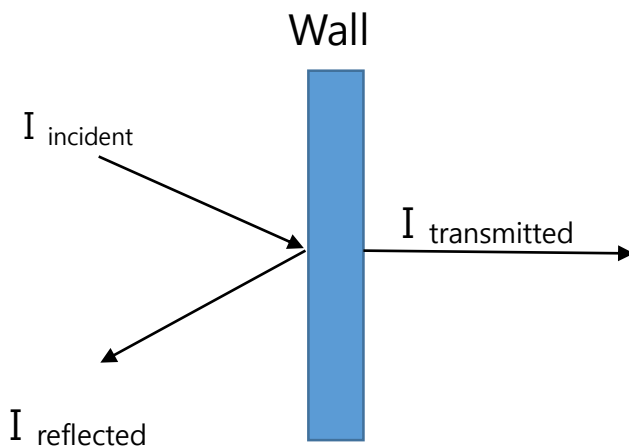
IL (Sound Intensity Level) =  $10 \text{ Log} I/I_0$  [dB]

where  $I$  = Intensity of sound [ $\text{W/m}^2$ ]

$I_0 = 1 \times 10^{-12} \text{ W/m}^2$

## Transmission of Sounds through Structures

This section is mainly sourced from Lamancusa's PDF file on Noise Control (source: [https://www.mne.psu.edu/lamancusa/me458/9\\_trans.pdf](https://www.mne.psu.edu/lamancusa/me458/9_trans.pdf))



### Transmission Coefficient, $\tau$

$$\tau = I_{\text{transmitted}} / I_{\text{incident}}$$

where  $\tau$  is a frequency dependent physical property of material.

When the wall or partition consist of several materials, then the composite transmission loss,  $\tau_{\text{composite}}$ , is calculated as

$$\tau_{\text{composite}} = \frac{\sum \tau_i S_i}{\sum S_i} \text{ for } i=1,2..n$$

where  $\tau_i$  = Transmission Loss of each material

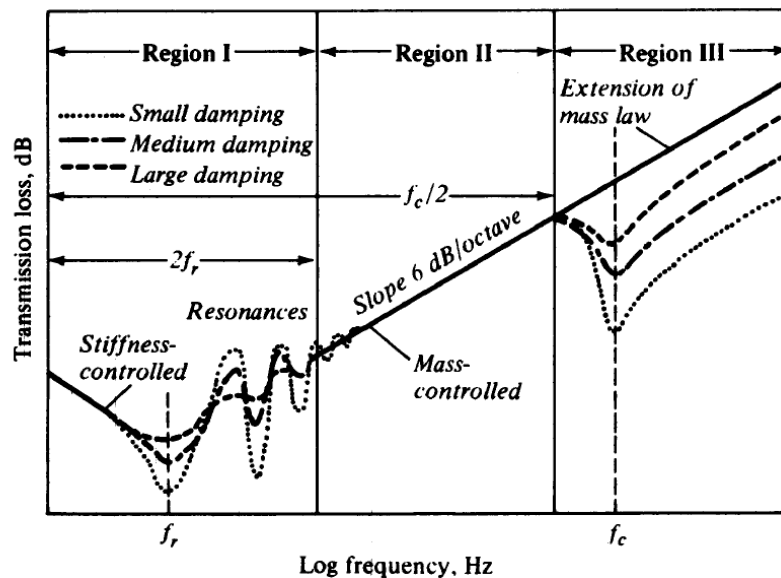
$S_i$  = Area of each material

## STL(Sound Transmission Loss)

= Log ratio of the incident to the transmitted energy

= $10 \log_{10} 1/\tau$  in [dB]

The STL is highly depending on the frequency, and theoretical STL is typically shown in fig.



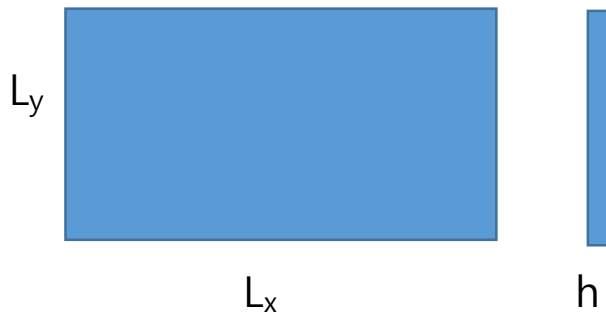
Theoretical Transmission Loss for an infinite homogeneous panel

(source: [https://www.mne.psu.edu/lamancusa/me458/9\\_trans.pdf](https://www.mne.psu.edu/lamancusa/me458/9_trans.pdf))

Region1: This region, stiffness controlled region, is mainly influenced by the bending stiffness, resonance, and damping of the panel, and this region spans the frequency range upto twice of resonant frequency,  $f_r$ , of the panel.

For the resonant freq,  $f_r$ , of panel can be analytically obtained as the lowest natural frequency;

Natural freq. of a rectangular plate of  $L_x \times L_y \times h$ ,



The natural frequency,  $F$ , of simple supported plate is;

$$F(N_x, N_y) = [\pi/2][Eh^2/(12\rho)]^{1/2}[(N_x/L_x)^2 + (N_y/L_y)^2]$$

where  $E$ =Young's modulus;  $\rho$ =density;

$N_x$ =number of half sine waves along x axis

$N_y$ =number of half sine wave along y axis

The Mode shapes of the plate is;

$$Z(x,y) = A \sin N_x \pi x / L_x \sin N_y \pi y / L_y$$

Region2: This region, mass controlled region, is mainly influenced by the mass of the panel, and follows fairly well the curve of slope 6dB/octave. The STL is theoretically given by

$$STL = 10 \text{ Log } \{1 + [\omega \rho_s / 2 \rho c]^2\} \text{ [dB]} \quad \text{eq}$$

where  $\omega$ =sound frequency [rad/sec]

$\rho c$ =Impedance of medium (density X velocity)

=415 rayls for air at standard temperature and pressure, and

1 rayl =1 Pa/m/s

$\rho_s$ =mass of panel for unit surface area

This equation indicates STL increase 6dB when either sound frequency( $\omega$ ) or panel mass per unit area( $\rho_s$ ) is doubled,

or Slope=6dB/octave in Log graph

[ $\therefore$  when  $\omega \rightarrow 2\omega$ ;

$$STL' = 10 \log [2\omega\rho_s/2\rho c]^2 = 10 \{ \log 4 + \log [\omega\rho_s/2\rho c] \}$$

$$= 10 \log 4 + 10 \log [\omega\rho_s/2\rho c] = 6 + STL$$

$\therefore$  STL increase by 6 when freq. doubles]

In this region, the frequency ranges from  $2f_r$  to  $f_c/2$ , where  $f_c$  is the critical frequency that will be explained in region 3.

Region 3: This region is influenced by the coincident effects, in which the sound wavelength coincides with the structural wavelength such as bending waves (or flexural waves) that

deform the structure transversely as they propagate in longitudinal direction. It is also called as radiation of sound wave.

For a homogeneous infinite plate,

the critical frequency,  $f_c$ , is

$$f_c = 5.2e10 \rho / hE \quad [\text{Hz}]$$

where  $\rho$  = weight density [lbf/in<sup>3</sup>],  $h$  = plate thickness [in],

$E$  = Young's modulus [psi]

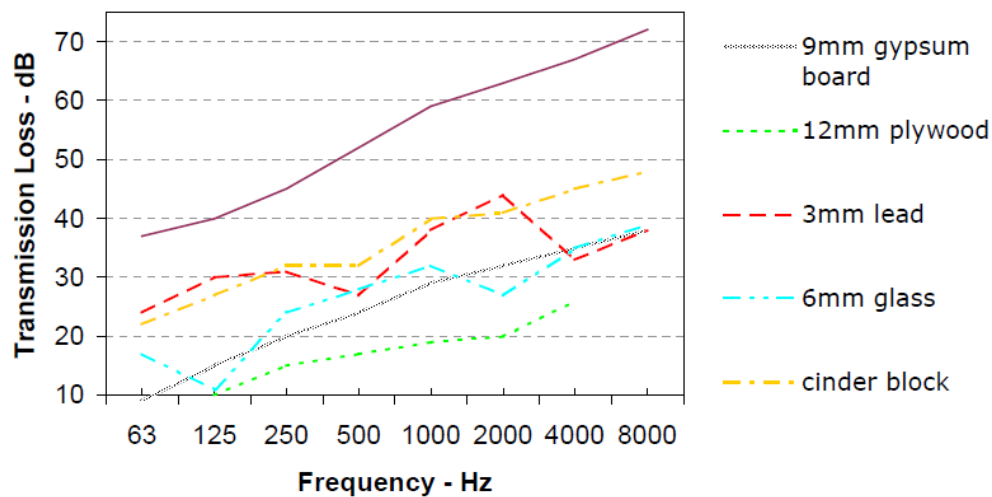
$f_c = 500/h$  for glass, steel, Al (all have similar  $\rho/E$ );

$f_c = 790/h$  for plywood

In this region, the frequency ranges upward from  $f_c/2$ .

Fig. shows practical a STL graph for typical materials for barrier.





## STL for typical materials

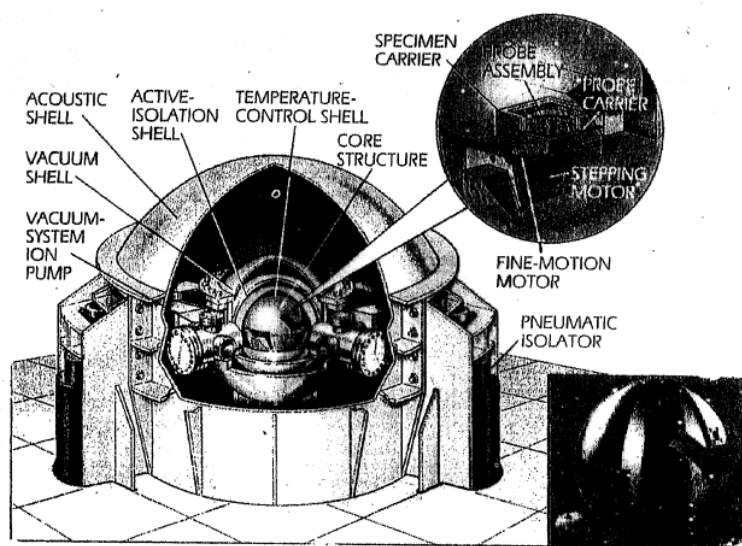
(Source: [https://www.mne.psu.edu/lamancusa/me458/9\\_trans.pdf](https://www.mne.psu.edu/lamancusa/me458/9_trans.pdf), Bies and Hansen)

In summary; acoustic isolation enclosure or barriers should be designed.

## Material properties for barrier material and the acoustic isolation:

- High density material gives high STL in mass controlled region
- Low bending stiffness material for high STL to give lower  $f_r$
- High internal damping material to prevent the resonant modes

Therefore, the ideal barrier material should have high density and low bending stiffness, (i.e. very limp). In the past, lead sheet or leaded vinyl was widely used until it was kicked out due to the environmental issue. Nowadays, loaded vinyl, that is impregnated with non-lead metal can be used. High density with low strength gives very high critical frequency, which is desirable. Gypsum board is a good barrier material and is more effective than plywood. Loaded vinyl or vinyl impregnated with metal fillings, is a common material for high STL.



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**SCHEMATIC OF M-CUBED**

## Vibration Isolation and Acoustic Isolation

(source: NIST's M-Cubed)