

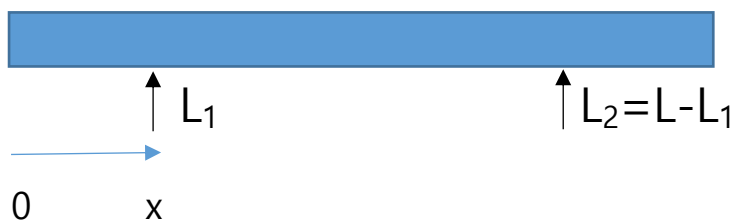
Precision Design –Airy support

Support positions and deformation:

Deformation varies with the supporting positions, thus it can be optimized for specific application

Beam of distributed load with double support

Weight per unit length= w , Length= L



Let $\langle x \rangle = x$ if $x \geq 0$, $\langle x \rangle = 0$ if $x < 0$

$$Q(x) = -w + wL/2 \langle x - L_1 \rangle_{-1} + wL/2 \langle x - L_2 \rangle_{-1}$$

$$V(x) = -\int Q(x) dx$$

$$= wx - wL/2 \langle x - L_1 \rangle^0 - wL/2 \langle x - L_2 \rangle^0 + C_1, \text{ and } C_1 = 0 (\because V(0) = 0)$$

$$M(x) = E I d^2 y / dx^2 = -\int V(x) dx$$

$$= -wx^2/2 + wL/2 \langle x - L_1 \rangle + wL/2 \langle x - L_2 \rangle + C_2, \text{ and } C_2 = 0 (\because M(0) = 0)$$

$$E I dy / dx = \int M(x) dx$$

$$= -wx^3/6 + wL/4 \langle x - L_1 \rangle^2 + wL/4 \langle x - L_2 \rangle^2 + C_3$$

$$Ely(x) = -wx^4/24 + wL/12 \langle x-L_1 \rangle^3 + wL/12 \langle x-L_2 \rangle^3 + C_3x + C_4,$$

Applying $y(x)=0$ at L_1 and L_2

$$Ely(L_1) = -wL_1^4/24 + C_3L_1 + C_4 = 0$$

$$Ely(L_2) = -wL_2^4/24 + C_3L_2 + C_4 = 0$$

Thus

$$C_3 = (wL/24)(L_1^2 + L_2^2) - (wL/12)(L_2 - L_1)^2$$

$$C_4 = wL^4/24 - C_3L_1 = (w/24)[L_1^4 - LL_1(L_2^2 + L_1^2) + 2LL_1(L_2 - L_1)^2]$$

Therefore,

$$\delta(x) = (w/24EI) [-x^4 + 2L \langle x-L_1 \rangle^3 + 2L \langle x-L_2 \rangle^3 + [L(L_2^2 + L_1^2) - 2L(L_2 - L_1)^2]x + L_1^4 - L_1L(L_2^2 + L_1^2) + 2LL_1(L_2 - L_1)^2]$$

Thus,

$$\delta(0) = (w/24EI) [L_1^4 - L_1L(L_2^2 + L_1^2) + 2LL_1(L_2 - L_1)^2] \quad \mathbf{eq(1)}$$

$$\delta(L/2) = (w/24EI) [-L^4/16 + 2L(L/2 - L_1)^3 + [L(L_2^2 + L_1^2) - 2L(L_2 - L_1)^2](L/2) + L_1^4 - L_1L(L_2^2 + L_1^2) + 2LL_1(L_2 - L_1)^2]$$

$$= (w/24EI) [-L^4/16 + L_1^4 + 2L(L_2 - L_1)^3/8 + (L_1^2 + L_2^2)(L^2/2 - L_1L) + (L_2 - L_1)^2(-L^2 + 2LL_1)]$$

$$\text{From } L/2 - L_1 = (L_2 - L_1)/2, \quad -L^2 + 2LL_1 = 2L(L_1 - L/2) = -2L(L_2 - L_1)/2 = -L(L_2 - L_1)$$

Thus,

$$\delta(L/2) = (w/24EI) [-L^4/16 + L_1^4 - (3/4)L(L_2 - L_1)^3 + (L_1^2 + L_2^2)L(L_2 - L_1)/2] \quad \mathbf{eq(2)}$$

For Double support case, $L_1=0$, $L_2=L$, then from eq(1), eq(2)

$$\delta(0)=0$$

$$\delta(L/2)= (wL^4/24EI) [-1/16-(3/4)+(1/2)]$$

$$= (wL^4/24EI) [(-1-12+8)/16]=-(5/384)wL^4/EI=-0.01302wL^4/EI$$

Airy Points Support:

Support for standard metre-bars to remove any bending at both ends, it means to locate L_1 , L_2 such that end faces of beams are vertical, that is $y'(0)=0$ and $y'(L)=0$. Thus,

$$Ely'(0)=C_3=0$$

$$Ely'(L)=-wL^3/6+wL(L-L_1)^2/4+ wL(L-L_2)^2/4=0$$

$$\text{Divide by } wL; -L^2/6+(L-L_1)^2/4+(L-L_2)^2/4=0,$$

$$*12/L^2, \text{ and remembering } L_1+L_2=L, \text{ and } L_1/L=x, L_2/L=1-x$$

$$-2+3(1-x)^2+3x^2=0, \text{ and } 6x^2-6x+1=0, \text{ thus } x=(3\pm\sqrt{3})/6$$

$$\text{Thus } L_1/L=(3-\sqrt{3})/6=0.211, L_2/L=(3+\sqrt{3})/6=0.788, \text{ and}$$

$$L_2-L_1=2\sqrt{3}L/6=0.577L: \text{ Airy Points Support}$$

At Airy points support,

$$\delta(0)= (w/24EI)[L_1^4-L_1L(L_2^2+L_1^2)+2LL_1(L_2-L_1)^2]$$

$$=(wL^4/24EI)[0.211^4-0.211(0.788^2+0.211^2)+2(0.211)(0.577)^2]$$

$$=(wL^4/24EI)[0.00206]$$

$$=0.000086(wL^4/EI)$$

$$\delta(L/2)= (w/24EI) [-L^4/16+L_1^4-(3/4)L(L_2-L_1)^3+(L_1^2+L_2^2)L(L_2-L_1)/2]$$

$$= wL^4/24EI[-1/16+0.211^4-0.75(0.577)^3+(0.211^2+0.788^2)(0.577)/2]$$

$$=(wL^4/24)[-0.0126]$$

$$\approx -0.000525wL^4/EI$$

Thus deflection, $\delta=\delta(0)-\delta(L/2)=0.000611 wL^4/EI$

For double support condition from eq(1), eq(2): $L_1=0, L_2=L$

$$\delta(0)=0$$

$$\delta(L/2)= (w/24EI)(-5L^4/16)=-5wL^4/384EI=-0.01302 wL^4/EI$$

\therefore About 4.7% ($\approx 0.000611/0.01302$) deflection when compared to the Double Support condition.

*Minimum straightness support points

The straightness due to bending deflection = $\delta_{\max} - \delta_{\min}$

To find the L_1, L_2 such that $\delta_{\max} - \delta_{\min}$ be minimum

This condition is to find L_1 such that $\delta(0) = \delta(L/2)$;

From eq(1), eq(2);

$$\text{Left} = 24EI\delta(0)/w = L_1^4 - L_1L(L_2^2 + L_1^2) + 2LL_1(L_2 - L_1)^2$$

$$\text{Right} = 24EI\delta(L/2)/w = -L^4/16 + L_1^4 - (3/4)L(L_2 - L_1)^3 + (L_1^2 + L_2^2)L(L_2 - L_1)/2$$

$/L^4$, and let $x = L_1/L$, then $L_2/L = 1 - x$, $(L_2 - L_1)/L = 1 - 2x$

$$x^4 - x[(1-x)^2 + x^2] + 2x(1-2x)^2 = -1/16 + x^4 - 0.75(1-2x)^3 + [x^2 + (1-x)^2](1-2x)/2$$

$$\text{Left} = x^4 - x(1-2x+2x^2) + 2x(1-4x+4x^2) = x^4 + 6x^3 - 6x^2 + x$$

$$\text{Right} = -1/16 + x^4 - 0.75[1 - 3(2x) + 3(2x)^2 - (2x)^3] - (2x^2 - 2x + 1)(x - 1/2)$$

$$= -1/16 + x^4 - (0.75 - 4.5x + 9x^2 - 6x^3) - (2x^3 - 3x^2 + 2x - 1/2)$$

$$= x^4 + 4x^3 - 6x^2 + 2.5x + (-1 - 12 + 8)/16$$

$$\text{Left} - \text{Right} = 2x^3 - 1.5x + 5/16 = 0$$

By solving the cubic equation by numerical method,

$$L_1 = 0.223L, L_2 = 0.777L, \text{ and } L_2 - L_1 = 0.554L.$$

$$\text{Then } \delta(0) = (w/24EI) [L_1^4 - L_1L(L_2^2 + L_1^2) + 2LL_1(L_2 - L_1)^2]$$

$$= (wL^4/24EI) [0.223^4 - (0.223)(0.777^2 + 0.223^2) + 2(0.223)(0.554)^2]$$

$$= wL^4/24EI(-0.00636) = (-0.000265)wL^4/EI$$

The straightness error $=\delta(L_1)-\delta(0)=-\delta(0)=0.000265wL^4/EI$

\therefore About 2% ($\cong 0.000265/0.01302$) of Double support case

Therefore, the supporting locations for beam elements give very strong influence on the beam bending or deformation, and thus better to be located at the optimum position.