

(20점)

1. If each of the following statements is true, please mark O at the end of each statement. If false or incorrect, mark X and make corrections.
 - 1) Transmission lines are usually long in terms of wavelength and are represented by distributed parameters, while waveguides are normally short and are described by field quantities.
 - 2) A lossless transmission line is distortionless, and has zero α and X_o , constant u_p and R_o .
 - 3) When phase constant is proportional to frequency, transmission lines and single-conductor waveguides are dispersive.
 - 4) Comparing with the phase velocity of unguided plane wave in the dielectric medium, the phase velocity on a lossless or distortionless transmission line is the same, while the phase velocity of both TM and TE modes in a uniform waveguide is greater.
 - 5) Input impedance of a very short open-circuited line is purely inductive.
 - 6) The circuit conditions for an infinite line and for a matched line are the same at the input (sending) end.
 - 7) The distance between neighboring voltage maxima and voltage minima is $\lambda/2$ of a standing wave when a transmission line is not matched.
 - 8) The Smith chart can be used either as an impedance chart or as an admittance chart, and is applicable to transmission lines having any characteristic resistance.
 - 9) The point representing an open-circuit, P_{oc} , is at (1, 0) on a Smith admittance chart.
 - 10) TEM waves cannot exist in a single-conductor dielectric-filled waveguide of any cross section.
 - 11) Since a waveguide lets only waves with higher frequencies than a cutoff frequency propagate through it, it can act as a high-pass filter.
 - 12) For TM modes in rectangular waveguides, neither m nor n can be zero, and the wave impedance is less than the intrinsic impedance of the guide medium.
 - 13) The cutoff frequencies for TM_{nr} and TE_{nr} modes in a circular wave guide are not always the same.
 - 14) The subscripts m and n of TM_{mn} and TE_{mn} modes denote, respectively, the number of wavelengths of field variations in the x- and y-directions in rectangular waveguides.
 - 15) TM_{101} and TE_{110} modes cannot exist in a rectangular cavity resonator referring to the z-axis.

(30점)

2. For uniform two-wire transmission lines with time-harmonic variations,
- Draw the equivalent circuit of a differential length Δz for distributed circuit analysis.
 - Set up circuit equations for $v(z,t)$ and $i(z,t)$ from Kirchhoff's laws.
 - For cosine-reference time-harmonic variations, $v(z,t) = \text{Re}[V(z)e^{j\omega t}]$ and $i(z,t) = \text{Re}[I(z)e^{j\omega t}]$, show that the Helmholtz-type wave equation for $V(z)$ is $\frac{d^2 V(z)}{dz^2} - \gamma^2 V(z) = 0$, and express $\gamma = \alpha + j\beta$ in terms of R, L, G, C , and ω .
 - Find the general solution for $V(z)$.
 - Define the characteristic impedance Z_o of the transmission line.
 - Determine α, β, Z_o for the distortionless lossy transmission lines.
 - Define the matched line for a finite transmission line connected to a load impedance Z_L .

(15점)

3. Answer the following questions and explain how you've got the answers by using and drawing the Smith Chart.

A given lossless transmission line of 0.1875 (m) long and short-circuited has the characteristic impedance of 5 (Ω).

- Determine the voltage reflection coefficient in polar form.
- Find the input impedance at 600 (MHz).
- Determine the corresponding input admittance for the line in (b).
- Find the standing-wave ratio.
- Find all locations of the voltage maximum and the voltage minimum on the line, respectively.

(35점)

4. For an air-filled (ϵ_o, μ_o) $a \times b$ ($a = \sqrt{3} b$) rectangular waveguide operating at the frequency $f = 3.6$ GHz for a TM wave traveling along the z -direction,

- Set up a BVP (boundary-value problem) for finding the phasor $E_z^o(x,y)$.
- Find a general solution for $E_z^o(x,y)$ by solving this BVP.
- Determine eigenvalues for $h^2 = \gamma^2 + k^2$ and eigenmodes for $E_z^o(x,y)$.
- Show that a transverse component field $H_x^o(x,y)$ of this TM wave can be

determined by calculating $H_x^o = \frac{j\omega\epsilon_o}{h^2} \frac{\partial E_z^o}{\partial y}$ which is derived from the x-component of Faraday's law and the y-component of Ampere's law.

- Determine the dispersion relation and find the cutoff frequency for TM_{mn} mode.
- Find the dominant mode and calculate the cutoff frequency of the dominant mode.
- Find the cutoff wavelength λ_c of the dominant mode.
- If the operating frequency $f = 3.6$ GHz is at least 20% higher than the cutoff frequency of the dominant mode, give a typical design for the dimension a .