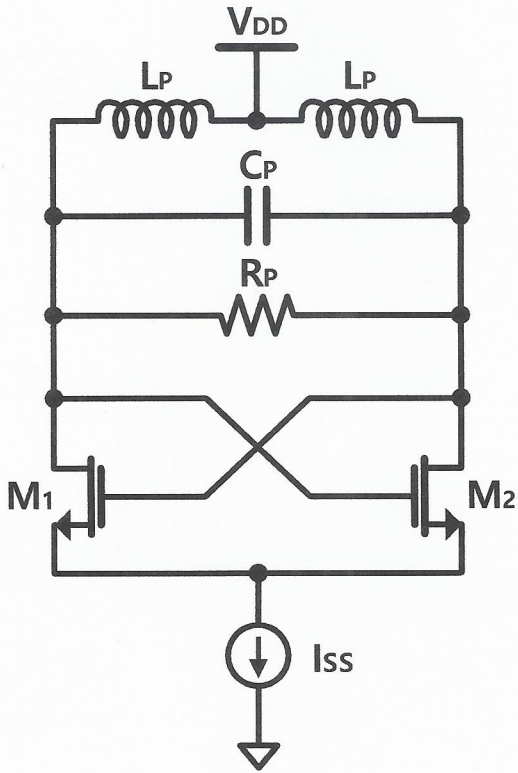
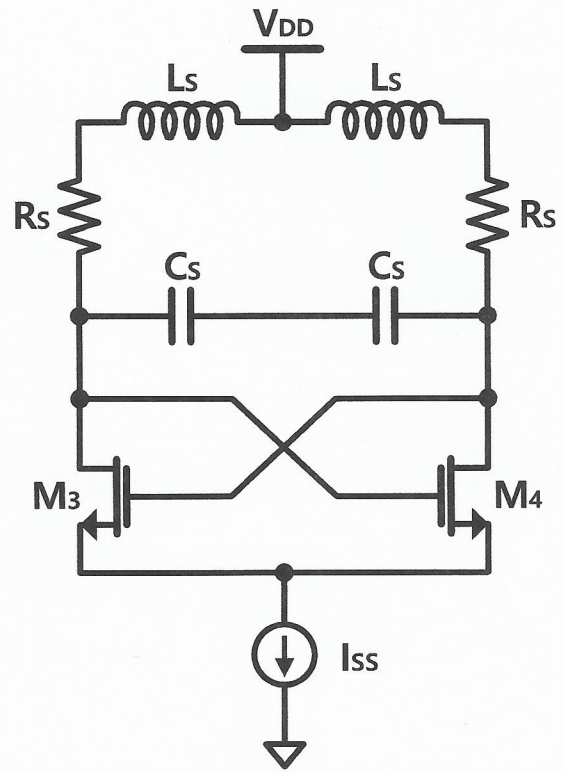


[1] Answer the following questions. Assume all the transistors are identical and $r_o = \infty$.

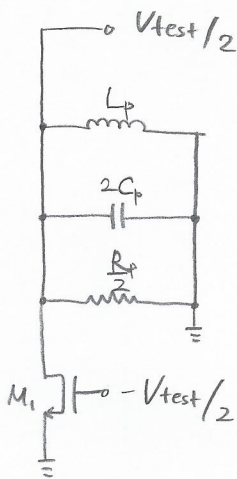


Circuit A

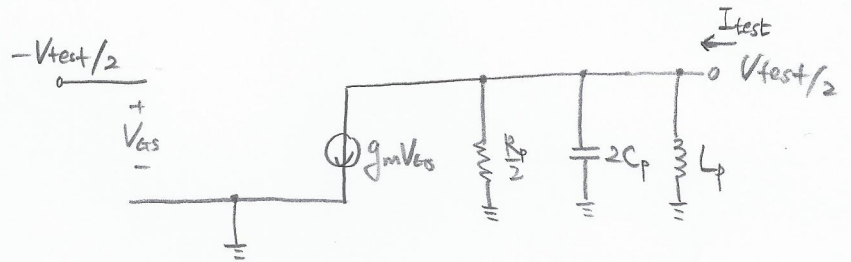


Circuit B

A. Find the oscillation frequency of the LC oscillator shown in Circuit A.



(Half-Circuit Analysis)



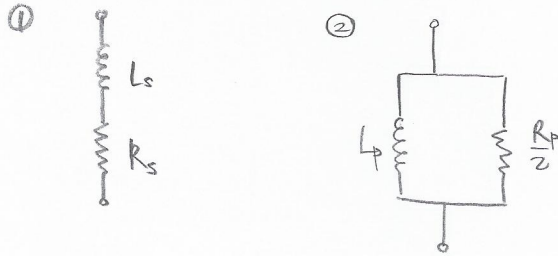
$$I_{test} = \frac{1}{2} V_{test} \left[-g_m + \frac{2}{R_p} + 2sC_p + \frac{1}{sL_p} \right]$$

$$\rightarrow \frac{V_{out}}{I_{out}} = \frac{\frac{1}{2} V_{test}}{I_{test}} = \frac{1}{-g_m + \frac{2}{R_p} + 2sC_p + \frac{1}{sL_p}} = \frac{R_p L_p}{R_p + (2L_p - g_m R_p L_p) s + 2R_p L_p C_p s^2}$$

$$\therefore \text{oscillation frequency } \omega_0 = \sqrt{\frac{1}{2L_p C_p}}$$

B. Determine the values of R_S , L_S , and C_S in terms of R_P , L_P , and C_P so that the impedance of Circuit B is the same as Circuit A. Use the oscillation frequency found from A. (Hint : Assume $R_P/2 \gg \omega L_P$)

$C_S = 2C_P$ 이고, ①과 ②가 서로 equivalent 하면 impedance가 서로 같아진다.



①의 impedance $Z_S = R_S + j\omega L_S$

②의 impedance $Z_P = j\omega L_P \parallel \frac{R_P}{2} = \frac{1}{\omega^2 L_P^2 + (\frac{R_P}{2})^2} \left\{ \omega^2 L_P^2 \left(\frac{R_P}{2}\right) + j\omega L_P \left(\frac{R_P}{2}\right)^2 \right\}$
 $\approx \frac{\omega^2 L_P^2}{(\frac{R_P}{2})^2} + j\omega L_P \quad (\because R_P/2 \gg \omega L_P)$

$\Rightarrow L_S = L_P, R_S = \frac{2\omega^2 L_P^2}{R_P}$ 이면 ①과 ②의 impedance가 서로 같아진다.

$\therefore \begin{cases} R_S = \frac{2\omega^2 L_P^2}{R_P} = \frac{L_P}{R_P C_P} \quad (\omega = \sqrt{\frac{1}{2L_P C_P}} \text{ 대입}) \\ L_S = L_P \\ C_S = 2C_P \end{cases}$

C. Determine whether the LC oscillator oscillates when $g_m=1\text{mS}$, $R_S=1\Omega$, and $L_S=1\mu\text{H}$, and $C_S=1\text{nF}$.

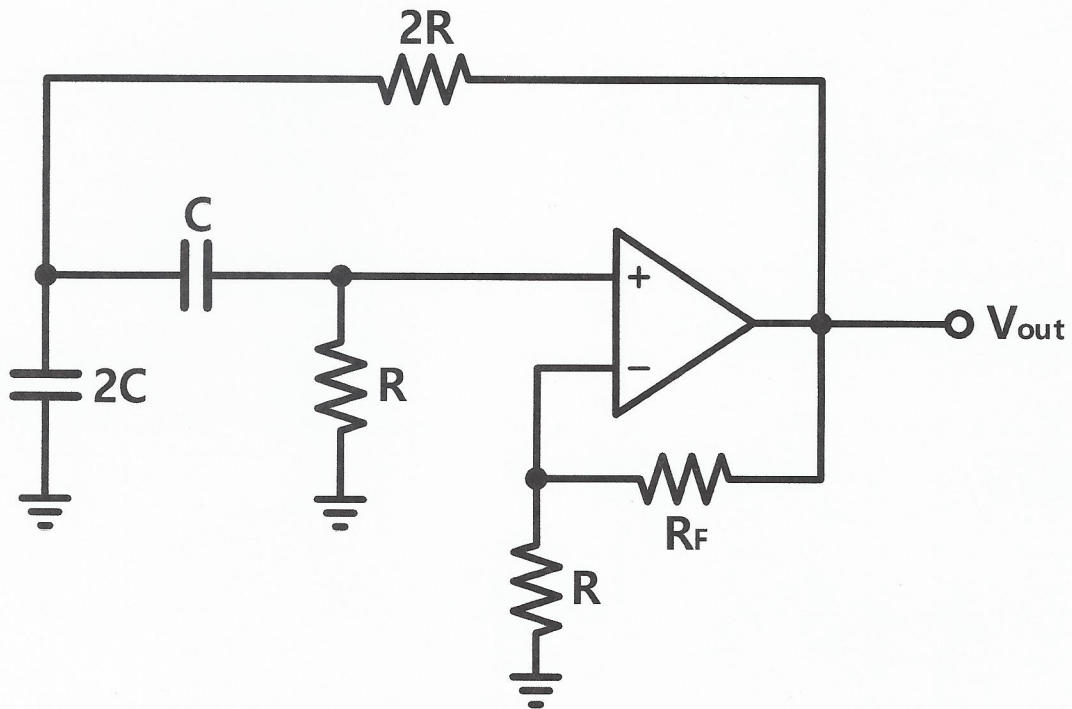
A의 식으로부터 $2L_P - g_m R_P \cdot L_P \leq 0$ 일 때, oscillation 하기 된다.

$(\Leftrightarrow g_m R_P \geq 2)$

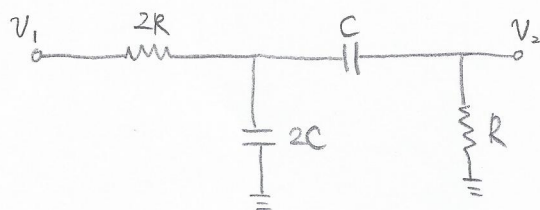
B로부터 $R_P = \frac{L_P}{R_S C_P} = \frac{2L_S}{R_S \cdot C_S}$
 $= \frac{2 \times 10^{-6}}{1 \times 10^{-9}} = 2 \times 10^3 (\Omega)$

$g_m R_P \geq 2$ 를 만족하므로 oscillation 한다.

[2] Answer the following questions. Assume the amplifier is ideal.



A. Derive the transfer function of the loop gain.



$$\begin{aligned} \frac{V_2}{V_1} &= \frac{\frac{1}{2sC} \parallel \left(\frac{1}{sC} + R\right)}{2R + \frac{1}{2sC} \parallel \left(\frac{1}{sC} + R\right)} \cdot \frac{R}{\frac{1}{sC} + R} \\ &= \frac{\frac{1+sRC}{(3+2sRC)sC}}{2R + \frac{1+sRC}{(3+2sRC)sC}} \cdot \frac{sRC}{1+sRC} \\ &= \frac{1+sRC}{4sRC^2 + 7sRC + 1} \cdot \frac{sRC}{1+sRC} = \frac{RCs}{4R^2C^2s^2 + 7RCs + 1} \end{aligned}$$

$$\begin{aligned} \therefore \text{Loop gain } H(s) &= \frac{V_2}{V_1} \cdot \left(1 + \frac{R_F}{R}\right) \\ &= \left(1 + \frac{R_F}{R}\right) \cdot \frac{RCs}{4R^2C^2s^2 + 7RCs + 1} \end{aligned}$$

B. Find the minimum value of R_F for starting oscillation. Assume $R=1k\Omega$, $C=1\mu F$.

positive feedback 이므로 $\angle H(s) = 0^\circ$ (or 360°) 인 ω_0 를 구하면,

$$\omega_0 = \frac{1}{2RC} \text{ 일 때, } \angle H(s) = 0^\circ \text{ 를 만족한다.}$$

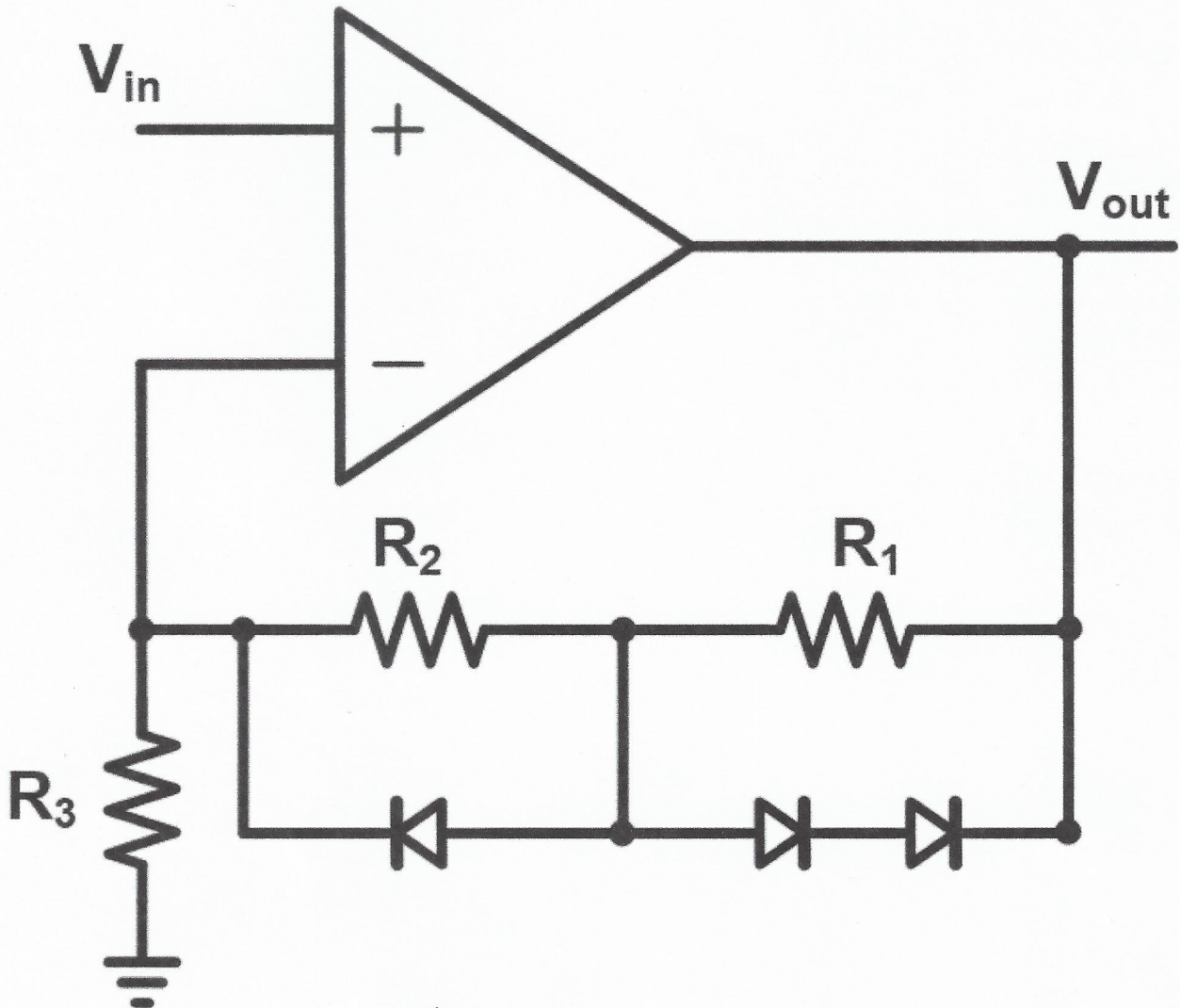
oscillation을 위해서는 $|H(j\omega_0)| \geq 1$ 의 조건을 만족해야 한다.

$$|H(j\omega_0)| = \left| \left(1 + \frac{R_F}{R}\right) \cdot \frac{1}{2} \right| \geq 1$$

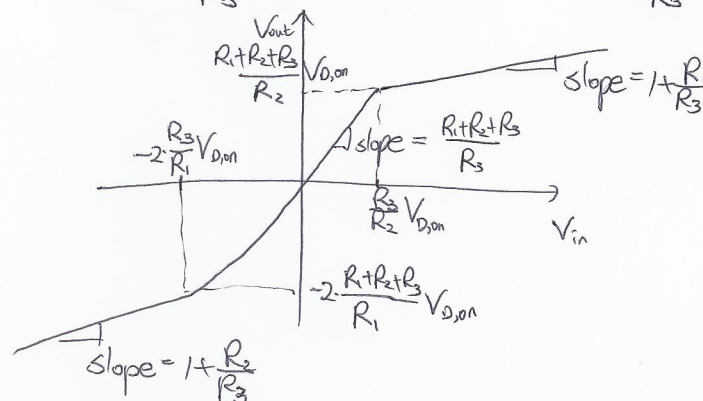
$$\Leftrightarrow R_F \geq 6R$$

\therefore oscillation을 위한 최소 $R_F = 6R = 6k\Omega$

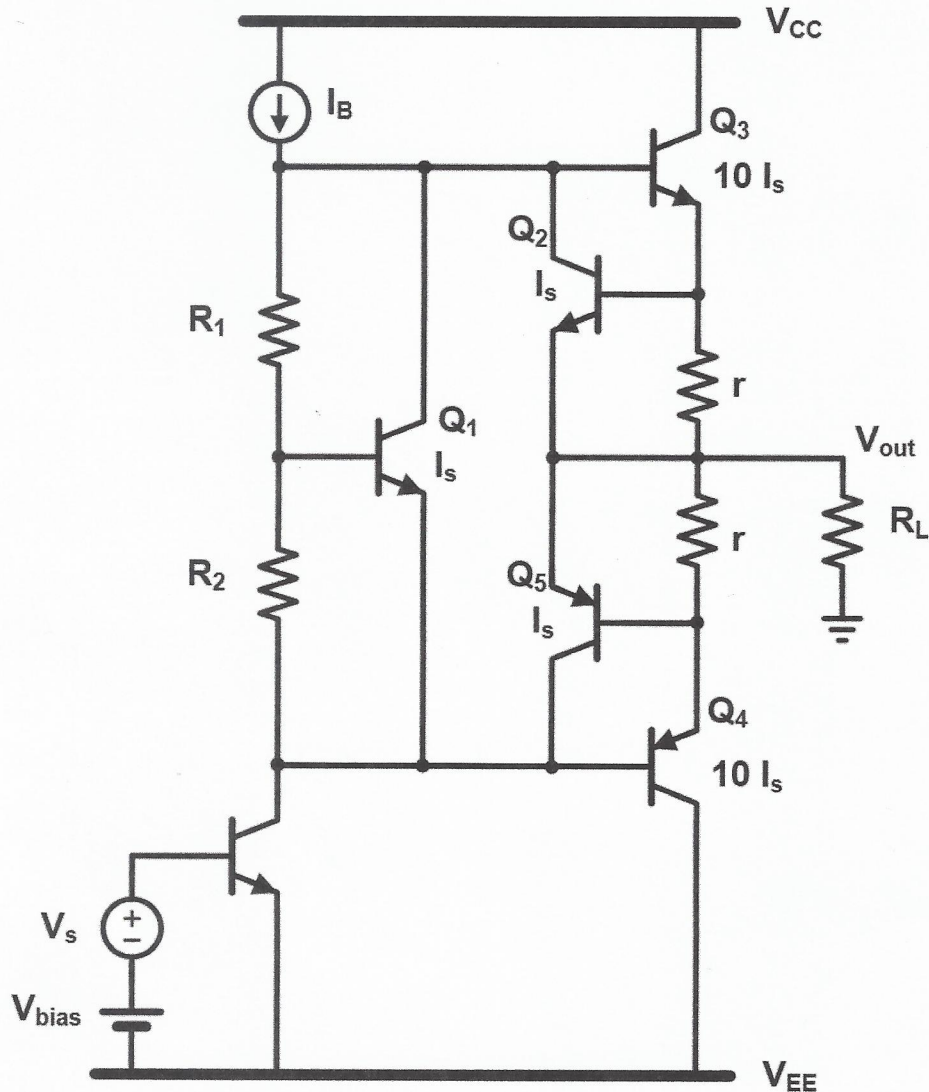
[1] Draw a $V_{in} - V_{out}$ curve of the circuit below. Specify the slope, condition of V_{in} or V_{out} when the diode turned on. (The voltage when the diode is turned on is $V_{D,ON}$)



- i) Diode off $V_{out} = \frac{V_{in}}{R_3} (R_1 + R_2 + R_3) = \left(1 + \frac{R_1 + R_2}{R_3}\right) V_{in}$
- ii) Diode on, $V_{in} > 0$ $\frac{V_{in}}{R_3} \cdot R_2 > V_{D,ON} \rightarrow V_{in} > \frac{R_3}{R_2} V_{D,ON}$
 $V_{out} = \frac{V_{in}}{R_3} (R_1 + R_3) + V_{D,ON} = \left(1 + \frac{R_1}{R_3}\right) V_{in} + V_{D,ON}$
- iii) Diode on, $V_{in} < 0$ $-\frac{V_{in}}{R_3} \cdot R_1 > 2V_{D,ON} \rightarrow V_{in} < -2\frac{R_3}{R_1} V_{D,ON}$
 $V_{out} = \frac{V_{in}}{R_3} (R_3 + R_2) - 2V_{D,ON} = \left(1 + \frac{R_2}{R_3}\right) V_{in} - 2V_{D,ON}$



[2] Consider the following output stage circuit. (Assume $V_A = \infty$)
 $V_T = 26\text{mV}$, $I_s = 1 \times 10^{-13}\text{A}$, $R_L = 10\Omega$, $V_{CC} = -V_{EE} = 42\text{V}$.



A. Find the resistor r , to limit the output current with 8 A. Assume Q2, Q5 is active when collector current is 1mA

$$V_{BE2, \text{active}} = V_T \ln \frac{I_{\text{active}}}{I_s} = 26\text{m} \ln \frac{10^{-3}}{10^{-13}} = 0.599\text{V}$$

$$r = \frac{V_{BE2, \text{active}}}{8\text{A}} = \frac{0.599}{8} = 0.0749\Omega$$

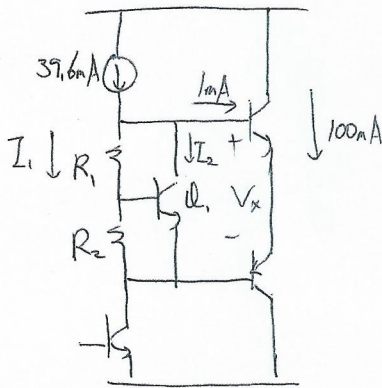
B. Find the minimum bias current I_B to deliver 80W power on 10Ω load with sinusoidal signal. Assume $\beta = 100$.

$$V_{\text{out}} = V_p \sin \omega t$$

$$\frac{1}{2} \frac{V_p^2}{R_L} = 80 \rightarrow V_p = 40\text{V}$$

$$(\beta + 1) I_B \geq \frac{40\text{V}}{10\Omega} \quad \therefore I_B \geq 39.6\text{mA}$$

- C. Find the R_1 using the bias current I_B of problem B, when the Quiescent current at the output is 100mA. (Quiescent current is the current when it is producing an output of zero, $V_{out} = 0$)
Assume $R_2 = 1k\Omega$, $r = 0\Omega$, and β of Q_1 is big enough, that is, $I_{C1} \approx I_{E1}$.)



$$V_x = 2 \cdot V_T \ln \frac{100mA}{10I_s} = 1,5205V$$

$$V_{BE, Q1} = V_T \ln \frac{I_2}{I_s} = 26mV \cdot \ln \frac{38,6mA - I_1}{10^{-13}}$$

$$\cancel{38,6mA} = I_1 + I_2 = I_1 = \frac{V_{BE, Q1}}{R_2} = \frac{26m}{1k} \ln \frac{38,6mA - I_1}{10^{-13}}$$

$$I_1 \approx 693\mu A$$

$$I_1 (R_1 + R_2) = V_x = 693\mu A (R_1 + 1k\Omega) = 1,5205V$$

$$\therefore R_1 = 1,194k\Omega$$

- D. Find the power efficiency when $V_{out} = 10 \sin \omega t$?

Ignore the power dissipation at pre-driver and assume that each transistor carries a negligible current around $V_{out} = 0$ and turns off for half of the period.

$$\eta = \frac{P_{out}}{P_{out} + P_{av,n} + P_{av,p} + 2 \cdot P_r}$$

$$P_{out} = \frac{1}{2} \cdot \frac{V_o^2}{R_L} = \frac{1}{2} \cdot \frac{100}{10} = 5W$$

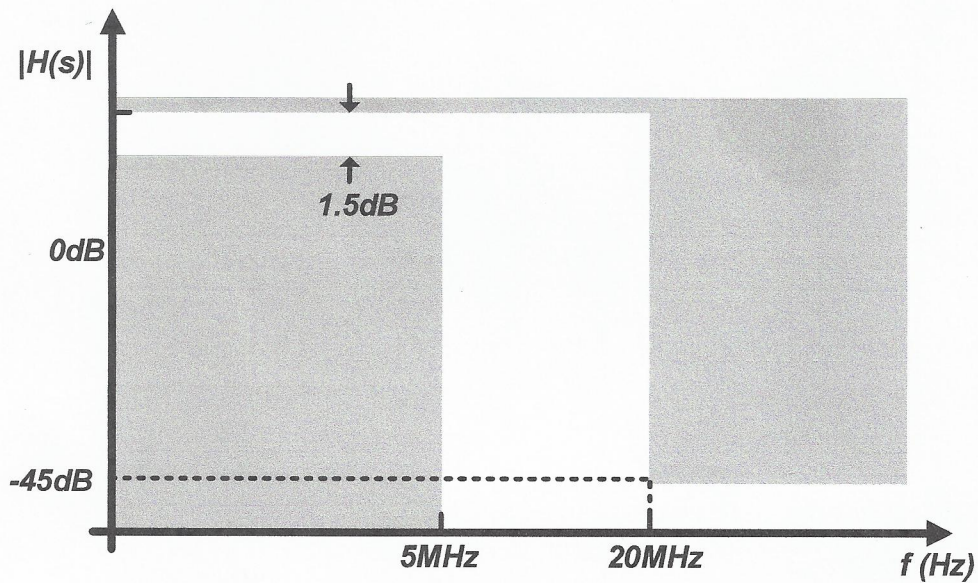
$$P_r = \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} I^2 \cdot r \, dt = \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} \left(\frac{10 \sin \omega t}{R_L} \right)^2 r \, dt = \frac{1}{4} 0,0895 = 0,021875W$$

$$P_{av,n} = \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} \left(V_{cc} - V_{out} - \frac{V_{out}}{R_L} \cdot r \right) \cdot \frac{V_{out}}{R_L} \, dt = \frac{10V_{cc}}{\pi R_L} - \frac{100}{4R_L} \left(1 + \frac{r}{R_L} \right)$$

$$= 10,847W$$

$$\therefore \eta = \frac{5}{10,847 \times 2 + 5 + 0,021875 \times 2} \Rightarrow 18,7\%$$

[1] Answer the following questions. [00 points]



Transfer function & Poles of the Butterworth Response

$$|H(j\omega)| = \frac{1}{\sqrt{1 + \left(\frac{\omega}{\omega_0}\right)^{2n}}}$$

$$p_k = \omega_0 \exp\left(\frac{j\pi}{2}\right) \exp\left(j\frac{(2k-1)\pi}{2n}\right), k = 1, 2, \dots, n$$

Transfer function & Poles of the Chebyshev Response

$$|H_{PB}(j\omega)| = \frac{1}{\sqrt{1 + \epsilon^2 \cos^2\left(n \cos^{-1}\left(\frac{\omega}{\omega_0}\right)\right)}} \quad |H_{SB}(j\omega)| = \frac{1}{\sqrt{1 + \epsilon^2 \cosh^2\left(n \cosh^{-1}\left(\frac{\omega}{\omega_0}\right)\right)}}$$

$$p_k = -\omega_0 \sin\frac{(2k-1)\pi}{2n} \sinh\left(\frac{1}{n} \sinh^{-1}\frac{1}{\epsilon}\right) + j\omega_0 \cos\frac{(2k-1)\pi}{2n} \cosh\left(\frac{1}{n} \sinh^{-1}\frac{1}{\epsilon}\right), k = 1, 2, \dots, n$$

Useful Equations

$$\sinh(x) = \frac{e^x - e^{-x}}{2}, \quad \cosh(x) = \frac{e^x + e^{-x}}{2}, \quad \sinh^{-1}(x) = \ln(x + \sqrt{x^2 + 1}), \quad \cosh^{-1}(x) = \ln(x + \sqrt{x^2 - 1})$$

A. Determine the minimum order of each filter (Butterworth Response & Chebyshev Response). Assume the bandwidth of Chebyshev filter is 5MHz. [00points]

< Butterworth >

$$\cdot |H(j\omega)|_{\omega=2\pi \cdot 5M} \geq -1.5dB = 0.841$$

$$\rightarrow \frac{1}{\sqrt{1 + \left(\frac{2\pi \times 5M}{\omega_0}\right)^{2n}}} = 0.841 \dots \textcircled{1}$$

$$\cdot |H(j\omega)|_{\omega=2\pi \cdot 20M} \leq -45dB = 5.6 \times 10^{-3}$$

$$\rightarrow \frac{1}{\sqrt{1 + \left(\frac{2\pi \cdot 20M}{\omega_0}\right)^{2n}}} = 5.6 \times 10^{-3} \dots \textcircled{2}$$

$$\Rightarrow \textcircled{1} \& \textcircled{2} : n \approx 4.058 \Rightarrow \text{minimum order} = 5$$

< Chebyshev >

$$\cdot \omega_0 = 2\pi \cdot 5M.$$

$$\cdot |H(j\omega)|_{\omega=2\pi \cdot 5M} = -1.5dB = 0.841$$

$$\rightarrow \frac{1}{\sqrt{1 + \epsilon^2}} = 0.841 \Rightarrow \epsilon \approx 0.643 \dots \textcircled{3}$$

$$\cdot |H(j\omega)|_{\omega=2\pi \cdot 20M} = -45dB = 5.6 \times 10^{-3}$$

$$\rightarrow \frac{1}{\sqrt{1 + \epsilon^2 \cosh^2\left(n \cdot \cosh^{-1}\left(\frac{2\pi \cdot 20M}{\omega_0}\right)\right)}} = 5.6 \times 10^{-3} \dots \textcircled{4}$$

$$\textcircled{3} \& \textcircled{4} \Rightarrow n \approx 3.06$$

$$\Rightarrow \text{minimum order} = 4$$

B. Using determined value of n above, get the range of the optimal natural frequency (ω_0) of the Butterworth filter. [00points]

From A, $\textcircled{1} : \frac{1}{\sqrt{1 + \left(\frac{2\pi \times 5M}{\omega_0}\right)^{2n}}} > 0.841 \Rightarrow \left(\frac{5M}{f_0}\right)^{10} < \frac{1}{(0.841)^2} - 1 = 0.414 \dots \textcircled{5}$

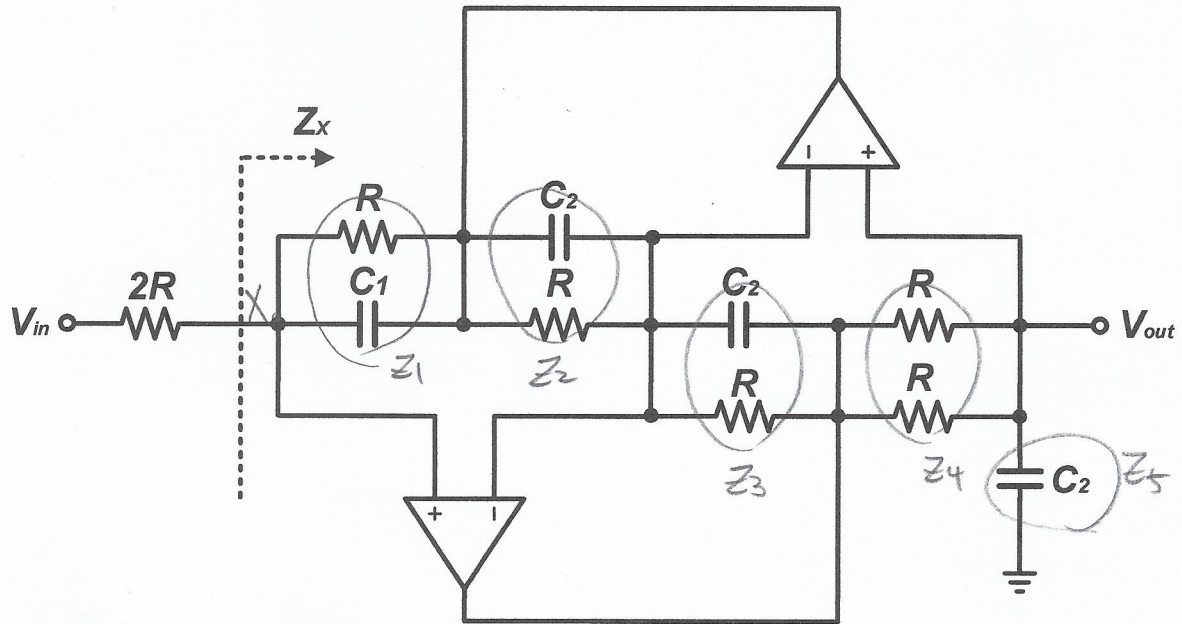
$\textcircled{2} : \frac{1}{\sqrt{1 + \left(\frac{2\pi \times 20M}{\omega_0}\right)^{2n}}} < 5.6 \times 10^{-3} \Rightarrow \left(\frac{20M}{f_0}\right)^{10} > \frac{1}{(5.6 \times 10^{-3})^2} - 1 = 31886.7 \dots \textcircled{6}$

$$\textcircled{5} \& \textcircled{6} \Rightarrow \frac{5M}{(0.414)^{\frac{1}{10}}} < f_0 < \frac{20M}{(31886.7)^{\frac{1}{10}}} \Rightarrow 5.46 \text{ MHz} < f_0 < 7.09 \text{ MHz}$$

$$\rightarrow \text{Optimum natural frequency } f_0 = \sqrt{(5.46M)(7.09M)} = 6.22 \text{ MHz.}$$

$$\rightarrow \text{Optimum natural frequency } \omega_0 = 2\pi \cdot f_0 = 39.09 \text{ Mrad/s}$$

[2] Answer the following questions. Assume all op-amps are ideal. [00 points]



A. Calculate $Z_x(s)$. [00 points]

$$Z_x(s) = \frac{Z_1 Z_3}{Z_2 Z_4} Z_5 = \frac{R}{(R(s+1))} \cdot \frac{1}{R/2} \cdot \frac{1}{C_2 s} = \frac{2}{C_2 s (R(s+1))}$$

B. Derive the transfer function $H(s)$. [00 points]

$$\begin{aligned} H(s) &= \frac{V_{out}}{V_{in}} = \frac{V_x}{V_{in}} \quad (\because V_x = V_{out}) \\ &= \frac{Z_x}{2R + Z_x} = \frac{\frac{2}{C_2 s (R(s+1))}}{2R + \frac{2}{C_2 s (R(s+1))}} = \frac{1}{R^2 C_1 C_2 s^2 + R C_2 s + 1} = \frac{\frac{1}{R C_1 C_2}}{s^2 + \frac{1}{R C_1} s + \frac{1}{R C_1 C_2}} \end{aligned}$$

C. Determine the sensitivity of Q to a change in C_1 , $S_{C_1}^Q$, and the sensitivity of ω_n to a change in R , $S_R^{\omega_n}$. [00 points]

$$\text{From B, } \omega_n = \frac{1}{R C_1 C_2} \rightarrow S_R^{\omega_n} = \frac{d\omega_n}{dR} \cdot \frac{R}{\omega_n} = -1$$

$$\frac{\omega_n}{Q} = \frac{1}{R C_1} \rightarrow Q = \sqrt{\frac{C_1}{C_2}} \rightarrow S_{C_1}^Q = \frac{dQ}{dC_1} \cdot \frac{C_1}{Q} = \frac{1}{2}$$

D. Design a Chebyshev filter of the problem 4 having high Q factor based on this filter structure, 'General Impedance Converter'. Every R is 1k ohm and you need to get the value of C₁, C₂.

From Problem 4, $\underline{\underline{\epsilon = 0.643, n=4}} \rightarrow \sinh^{-1} \frac{1}{\epsilon} \doteq 1.225$

$$\left\{ \begin{array}{l} \sinh\left(\frac{1}{n} \sinh^{-1} \frac{1}{\epsilon}\right) \doteq 0.311 \\ \cosh\left(\frac{1}{n} \sinh^{-1} \frac{1}{\epsilon}\right) \doteq 1.047 \end{array} \right.$$

$$P_{1,4} = -\omega_0 \cdot \sin \frac{\pi}{8} \cdot \sinh\left(\frac{1}{n} \sinh^{-1} \frac{1}{\epsilon}\right) \pm j \omega_0 \cos \frac{\pi}{8} \cosh\left(\frac{1}{n} \sinh^{-1} \frac{1}{\epsilon}\right)$$

$$= -0.119 \omega_0 \pm j 0.967 \omega_0$$

$$P_{2,3} = -\omega_0 \sin \frac{3\pi}{8} \cdot \sinh\left(\frac{1}{n} \sinh^{-1} \frac{1}{\epsilon}\right) \pm j \omega_0 \cos \frac{3\pi}{8} \cosh\left(\frac{1}{n} \sinh^{-1} \frac{1}{\epsilon}\right)$$

$$= -0.287 \omega_0 \pm j 0.401 \omega_0$$

Highest Q factor $\frac{1}{2}$ poles imaginary axis at $\pm j 0.401 \omega_0 \Rightarrow P_1, P_4$

$$H(s) = \frac{P_1 \cdot P_4}{(s - P_1)(s - P_4)} = \frac{0.949 \omega_0^2}{s^2 + 0.238 \omega_0 s + 0.949 \omega_0^2}$$

- Comparing with the result of the B.

$$\left(H(s) = \frac{\frac{1}{R^2 C_1 C_2}}{s^2 + \frac{1}{R C_1} s + \frac{1}{R^2 C_1 C_2}} \right)$$

$$\Rightarrow \frac{1}{R C_1} = 0.238 \cdot \omega_0 \Rightarrow C_1 = \frac{1}{R} \cdot \frac{1}{0.238 \omega_0} \doteq 133.7 \text{ pF}$$

$$\frac{1}{R^2 C_1 C_2} = 0.949 \omega_0^2 \Rightarrow C_2 = \frac{1}{R^2 C_1} \cdot \frac{1}{0.949 \cdot \omega_0^2} \doteq 8 \text{ pF}$$