## Midterm Examination

May 1st, 2008

1. Classify the discontinuities in rock mass and list 6 properties of the discontinuities with brief explanation. (10)
Classification: Fault, Joint, Bedding, Cleavage, Fracture(Natural -), Artificial discontinuities.
Properties: Orientation, Size, Frequency, Surface geometry, Genetic type, Infill material.
2. Convert strike/dip to dip direction/dip. (10)
1) $\mathrm{N} 20^{\circ} \mathrm{E} / 66^{\circ} \mathrm{SE} \rightarrow 110 / 66$
2) $\mathrm{N} 32^{\circ} \mathrm{W} / 60^{\circ} \mathrm{SW} \rightarrow 238 / 60$
3) $\mathrm{N} 40^{\circ} \mathrm{E} / 30^{\circ} \mathrm{NW} \rightarrow 310 / 30$
4) $\mathrm{N} 56^{\circ} \mathrm{W} / 27^{\circ} \mathrm{NE} \rightarrow 34 / 27$
3. Compare the equal- angle projection with equal- area projection. (10)
4. Compare the BIPS with televiewer . (10)
5. Compare scanline survey with window sampling in terms of sampling bias. (10)
6. From a scanline whose trend and plunge are $40^{\circ}$ and $0^{\circ}$, respectively, orientations of three joints are measured as below. (20)

| Joint | Dip direction <br> $(\mathrm{a})$ | Dip ( $\beta$ ) |
| :---: | :---: | :---: |
| 1 | 230 | 86 |


| 2 | 247 | 78 |
| :--- | :---: | :---: |
| 3 | 65 | 80 |

When a cartesian coordinate system is adopted so that $x, y$ and $z$ axes are parallel to east, north and upward, respectively,

| Joint | $X$ | $Y$ | $Z$ |
| :---: | :---: | :---: | :---: |
| 1 | -0.764 | -0.641 | 0.07 |
| 2 | -0.9 | -0.382 | 0.208 |
| 3 | -0.893 | -0.416 | -0.174 |
| Sum | -2.557 | -1.439 | 0.104 |

1) Calculate the unweighted mean normal vector.
$(-2.557,-1.439,0.104)=>(-0.871,-0.491,0.035)$
2) Calculate the weighted mean normal vector using Terzaghi correction.
scanline: $(\sin 40, \cos 40,0)=(0.643,0.766,0)$
$\mathrm{w} 1=1 / \cos$ theta1 $=1 / \mid(-0.764,-0.641,0.07) p 0.643,0.766,0) \mid=1 / 0.982$
$w 2=1 / \cos$ theta2 $=\mid(-0.9,-0.382,0.208) p 0.643,0.766,0) \mid=1 / 0.871$
$w 3=1 / \cos$ theta3 $=\mid(0.893,0.416,0.174) p 0.643,0.766,0) \mid=1 / 0.893$
weighted sum: $(-0.764,-0.641,0.07) / 0.982+(-0.9,-0.382,0.208) / 0.871-(0.893$, $0.416,0.174) / 0.893=(-2.811,-1.557,0.115)=>(-0.874,-0.484,0.036)$
7. Derive the Maximum Likelihood estimator of Fisher's $K$ of generalized truncated Fisher distribution when the angle from the center (mean orientation) of poles to the set boundary is . (30)


| d.f. ${ }^{\alpha}$ | . 995 | . 990 | . 975 | . 950 | . 050 | . 025 | . 010 | . 005 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $392704 \times 10^{-10}$ | $157088 \times 10^{-9}$ | $982069 \times 10^{-9}$ | $393214 \times 10^{-8}$ | 3.84146 | 5.02389 | 6.63490 | 7.87944 |
| 2 | . 0100251 | .0201007 | . 0506356 | . 102587 | 5.99147 | 7.37776 | 9.21034 | 10.5966 |
| 3 | . 0717212 | . 114832 | . 215795 | . 351846 | 7.81473 | 9.34840 | 11.3449 | 12.8381 |
| 4 | . 206990 | . 297110 | . 484419 | . 710721 | 9.48773 | 11.1433 | 13.2767 | 14.8602 |
| 5 | . 411740 | . 554300 | . 83121 i | 1.145476 | 11.0705 | 12.8325 | 15.0863 | 16.7 |
| 6. | . 675727 | . 872085 | 1.237347 | 1.63539 | 12.5916 | 14.4494 | 16.8119 | 18.5476 |
| 7 | . 989265 | 1.239043 | 1.68987 | 2.16735 | 14.0671 | 16.0128 | 18.4753 | 20.2777 |
| 8 | 1.344419 | 1.646482 | 2.17973 | 2.73264 | 15.5073 | 17.5346 | 20.0902 | 21.9550 |
| 9 | 1.734926 | 2.087912 | 2.70039 | 3.32511 | 16.9190 | 19.0228 | 21.6660 | 23.5893 |
| 10 | 2.15585 | 2.55821 | 3.24697 | 3.94030 | 18.3070 | 20.4831 | 23.2093 | 25.1882 |
| 11 | 2.60321 | 3.05347 | 3.81575 | 4.57481 | 19.6751 | 21.9200 | 24.7250 | 26.7569 |
| 12 | 3.07382 | 3.57056 | 4.40379 | $5: 22603$ | 21.0261 | 23.3367 | 26.2170 | 28.2995 |
| 13 | 3.56503 | 4.1069 | 5.00874 | 5.89186 | 22.3621 | 24.7356 | 27.6883 | 29.8194 |
| 14 | 4.07468 | 4.66043 | 5.62872 | 6.57063 | 23.6848 | 26.1190 | 29.1413 | 31.3193 |
| 15 | 4.60094 | 5.22935 | 6.26214 | 7.26094 | 24.9958 | 27.4884 | 30.5779 | 32.8013 |
| 16 | 5.14224 | 5.81221 | 6.90766 | 7.96164 | 26.2962 | 28.8454 | 31.9999 | 34.2672 |
| 17 | 5.69724 | 6.40776 | 7.56418 | 8.67176 | 27.5871 | 30.1910 | 33.4087 | 35.7185 37.1564 |
| 18 | 6.26481 | 7.01491 | 8.23075 | 9.39046 | 28.8693 | 31.5264 | 34.8053 | 37.1564 |
| 19 | 6.84398 | 7.63273 | 8.90655 | 10.1170 | 30.1435 | 32.8523 | 36.1908 | 38.5822 |
| 20 | 7.43386 | 8.26040 | 9.59083 | 10.8508 | 31.4104 | 34.1696 | 37.5662 | 39.9968 |
| 21 | 8.03366 | 8.89720 | 1028293 | 11.5913 | 32.6705 | 35.4789 | 38.9321 | 41.4010 |
| 22 | 8.64272 | 9.54249 | 10.9823 | 12.3380 | 33.9244 | 36.7807 | 40.2894 | 42.7956 |
| 23 | 9,26042 | 10.19567 | 11.6885 | 13.0505 | 35.1725 | 38.0757 | 41.6384 | 44.1813 |
| 24 | 9.8862: | 10.8564 | 12.4011 | 13.8484 | 36.4151 | 39.3641 | 42.9798 | 45.5585 |
| 25 | 10.5197 | 11.5240 | 13.1197 | 14,6114 | 37.6525 | 40.6465 | 44.3141 | 46.9278 |
| 26 | 11.1603 | 12.1981 | 13.8439 | 15.3791 | 38.8852 | 41.9232 | 45.6417 | 48.2899 |
| 27 | 11.8076 | 12.8786 | 14.5733 | 16.1513 | 40.1133 | 43.1944 | 46.9630 | 49.6649 |
| 28 | 12.4613 | 13.5648 | 15.3079 | 16.9279 | 41.3372 | 44.4607 | 48.2782 | 50.9933 |
| 29 | 13.1211 | 14.2565 | 16.0471 | 17.7083 | 42.5569 | 45.7222 | 49.5879 | 52.3356 |
| 30 | 13.7867 | 14.9535 | 16.7908 | 18.4926 | 43.7729 | 46.9792 | 50.8922 | 53.6720 |
| 40 | 20.7065 | 22.1643 | 24.4331 | 26.5093 | 55.7585 | 59.3417 | 63.6907 | 66.7659 |
| 50 | 27.9907 | 29,7067 | 32.3574 | 34.7642 | 67.5048 | 71.4202 | 76.1539 | 79.4900 |
| 60 | 35.5346 | 37.4848 | 40.4817 | 43.1879 | 79.0819 | 83.2976 | 88.3794 | 91.5517 |
| 70 | 43.2752 | 45.4418 | 48.7576 | 51.7393 | 90.5312 | 95.0231 | 100.425 | 104.215 |
| 80 | 51.1720 | 53.5400 | 57.1532 | 60.3915 | 101.879 | 106.629 | 112.329 | 116.321 |
| 90 | 59.1963 | 61.7541 | 65.6466 | 69.1260 | 113.145 | 118.136 | 124.116 | 128.299 |
| 100 | 67.3276 | 70.0648 | 74.2219 | 77.9295 | 124.342 | 129.561 | 135.807 | 140.169 |

Table A.4. Critical Values of $D_{n}{ }^{\alpha}$ in the Kolmogorov-Smirnov Test (After Hoel, 1962)

|  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| 5 | 0.20 | 0.10 | 0.05 | 0.01 |
| 10 | 0.45 | 0.51 | 0.56 | 0.67 |
| 15 | 0.32 | 0.37 | 0.41 | 0.49 |
| 20 | 0.27 | 0.30 | 0.34 | 0.40 |
| 25 | 0.23 | 0.26 | 0.29 | 0.36 |
| 30 | 0.21 | 0.24 | 0.27 | 0.32 |
| 35 | 0.19 | 0.22 | 0.24 | 0.29 |
| 40 | 0.18 | 0.20 | 0.23 | 0.27 |
| 45 | 0.17 | 0.19 | 0.21 | 0.25 |
| 50 | 0.16 | 0.18 | 0.20 | 0.24 |
| $>50$ | 0.15 | 0.17 | 0.19 | 0.23 |

