

Selected Solutions of Mid-term Exam 2

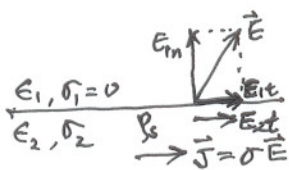
1. 1) ① $\oint_S \vec{E} \cdot d\vec{s} = \frac{Q}{\epsilon}$: The total outward flux of E-field over any closed surface in a dielectric is equal to the total charge enclosed in the surface divided by ϵ . (Gauss's law)

② $\oint_C \vec{E} \cdot d\vec{l} = 0$: The line integral of the static electric field intensity around any closed path vanishes

② is a path-independent integral (only end point dependent) which vanishes $\Rightarrow E$ is a conservative field.

② is derived from the surface integral of $\nabla \times \vec{E} = \vec{0}$ by using Stokes's theorem. $\nabla \times \vec{E} = \vec{0}$ satisfies a null vector identity $\nabla \times \nabla V = \vec{0}$ if $\vec{E} = -\nabla V$. Therefore, \vec{E} can be obtained from a scalar potential V .

2)



From $\nabla \times \vec{E} = \vec{0}$ and $\vec{J} = \sigma \vec{E}$,

$E_{1t} = E_{2t} = J_{2t} / \sigma_2$ $J_{1t} = 0$

From $\nabla \cdot \vec{D} = \rho_s$,

$D_{1n} = \rho_s$ or $E_{1n} = \rho_s / \epsilon_1$

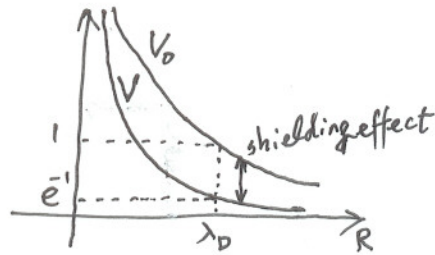
3) For a point charge in free space,

$V_0(R) = q / (4\pi\epsilon_0 R)$

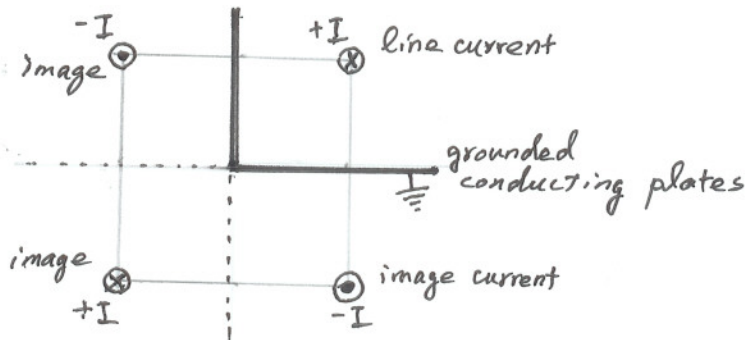
For a test charge in a plasma,

$V(R) = V_0 e^{-R/\lambda_D}$

where λ_D is the Debye length due to the shielding effect of the electron cloud around the test charge.



4)



5) Steady-state drift velocity of free electron in a conductor :

$\vec{u}_d = \mu \vec{E}$ where $\mu = q/mv$: mobility

Current density of free electron :

$\vec{J} = nq\vec{u}_d = \rho_v \vec{u}_d = \rho_v \mu \vec{E} = \sigma \vec{E}$: Ohm's law

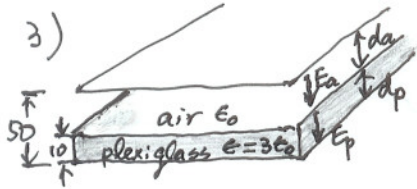
\therefore conductivity $\sigma = \rho_v \mu = \frac{nq^2}{mv}$

Both μ and σ are inversely proportional to collision freq. ν .

2. Breakdown voltage of a medium with a thickness d
 $V_b = E_b d$ where E_b is the dielectric strength.

1) For air, $V_b = E_{ba} d_a = (3 \times 10^6)(50 \times 10^{-3}) = \underline{1.5 \times 10^5 (V) = 150 (kV)}$

2) For plexiglass, $V_b = E_{bp} d_p = (2 \times 10^7)(50 \times 10^{-3}) = \underline{10^6 (V) = 1000 (kV)}$



$$V_b = E_{ba} d_a + E_{bp} d_p$$

Since $D_a = D_p \Rightarrow \epsilon_0 E_a = \epsilon E_p$

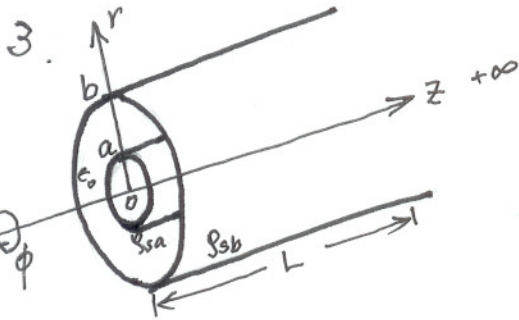
$$\Rightarrow E_a = \frac{\epsilon}{\epsilon_0} E_p = 3 E_p$$

$\Rightarrow E_a > E_p$ (High electric field intensity is applied in air, which means the breakdown occurs in air first.)

Therefore,

$$V_b = E_{ba} d_a + \frac{E_{ba}}{3} d_p = E_{ba} \left(d_a + \frac{d_p}{3} \right)$$

$$= 3 \times 10^6 \left(40 \times 10^{-3} + \frac{10 \times 10^{-3}}{3} \right) = \underline{1.3 \times 10^5 (V) = 130 (kV)}$$



Cylindrical symmetric ($\frac{\partial}{\partial \phi} = 0$);

$$\vec{E} = \hat{r} E_r$$

1) Applying Gauss's law, $\oint \vec{E} \cdot d\vec{s} = Q/\epsilon_0$

For $r < a$, $\oint E_r ds_r = 0$

$$\Rightarrow \int_0^L \int_0^{2\pi} E_r r d\phi dz = 0$$

$$\Rightarrow 2\pi r L E_r(r) = 0$$

$$\Rightarrow \underline{E_r(r) = 0}$$

For $a < r < b$, $\oint E_r ds_r = Q/\epsilon_0$

$$\Rightarrow \int_0^L \int_0^{2\pi} E_r r d\phi dz = \frac{2\pi a L \rho_{sa}}{\epsilon_0}$$

$$\Rightarrow 2\pi r L E_r(r) = 2\pi a L \rho_{sa} / \epsilon_0$$

$$\Rightarrow \underline{E_r(r) = \frac{a \rho_{sa}}{\epsilon_0 r}}$$

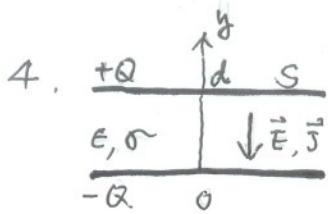
For $r > b$, $\oint E_r ds_r = Q/\epsilon_0$

Similarly, $2\pi r L E_r(r) = \frac{2\pi a L \rho_{sa}}{\epsilon_0} + \frac{2\pi b L \rho_{sb}}{\epsilon_0}$

$$\Rightarrow \underline{E_r(r) = \frac{a \rho_{sa} + b \rho_{sb}}{\epsilon_0 r}}$$

2) $E_r(r) = 0$ for $r > 0$,

$$\Rightarrow a \rho_{sa} + b \rho_{sb} = 0 \Rightarrow \underline{\frac{b}{a} = -\frac{\rho_{sa}}{\rho_{sb}}}$$



1) $C = Q/V$

$V = - \int_0^d \vec{E} \cdot d\vec{l} = \int_0^d E dy = Ed$

$D_n = \rho_s \Rightarrow \epsilon E = \frac{Q}{S} \Rightarrow E = Q/\epsilon S$

$\therefore C = Q/Ed = Q/(Q/\epsilon S) = \epsilon \frac{S}{d}$

2) $W_e = \int_V w_e dv = \int_V (\frac{\epsilon}{2} E^2) dv = \frac{1}{2} \int_V \epsilon (\frac{V}{d})^2 dv$
 $= \frac{1}{2} \epsilon (\frac{V}{d}) (Sd) = \frac{1}{2} (\epsilon \frac{S}{d}) V^2 = \frac{1}{2} CV^2$

3) $C = \frac{Q}{V} = \frac{\oint_S \epsilon \vec{E} \cdot d\vec{s}}{- \int_d \vec{E} \cdot d\vec{l}}$
 $R = \frac{V}{I} = \frac{- \int_d \vec{E} \cdot d\vec{l}}{\oint_S \sigma \vec{E} \cdot d\vec{s}}$

$\Rightarrow RC = \frac{\epsilon \oint_S \vec{E} \cdot d\vec{s}}{\sigma \oint_S \vec{E} \cdot d\vec{s}} = \frac{\epsilon}{\sigma}$

$\therefore R = \frac{\epsilon/\sigma}{C} = \frac{\epsilon/\sigma}{\epsilon S/d} = \frac{1}{\sigma} \frac{d}{S} = \eta \frac{d}{S}$

5. 1) BVP: $\nabla^2 V = 0$ in spherical symmetric fields ($\frac{\partial}{\partial \theta} = \frac{\partial}{\partial \phi} = 0$)

$\frac{1}{R^2} \frac{\partial}{\partial R} (R^2 \frac{\partial V}{\partial R}) = 0, R_i \leq R \leq R_o \text{ --- (1)}$

BCs: $V(R)|_{R=R_i} = V_o \text{ --- (2)}$

$V(R)|_{R=R_o} = 0 \text{ --- (3)}$

General solution of (1): $\frac{\partial V}{\partial R} = \frac{C_1}{R^2} \rightarrow V = -\frac{C_1}{R} + C_2 \text{ --- (4)}$

(2) in (4): $V_o = -C_1/R_i + C_2$
 $0 = -C_1/R_o + C_2 \Rightarrow C_1 = V_o / (\frac{1}{R_i} - \frac{1}{R_o}) \Rightarrow V(R) = \frac{V_o}{\frac{1}{R_o} - \frac{1}{R_i}} (\frac{1}{R} - \frac{1}{R_o})$

2) $\vec{J} = \sigma \vec{E}$: ohm's law and $\vec{E} = -\nabla V$

$\vec{E}(R) = \hat{R}(-\nabla V) = -\hat{R} \frac{\partial V}{\partial R} = \hat{R} \frac{V_o}{\frac{1}{R_i} - \frac{1}{R_o}} \frac{1}{R^2}$

$\therefore \vec{J}(R) = \sigma \vec{E}(R) = \hat{R} \frac{\sigma V_o}{\frac{1}{R_i} - \frac{1}{R_o}} \frac{1}{R^2}$

3) $R = V_o/I$

$I = \int_S \vec{J} \cdot d\vec{s}_R = \int_0^{2\pi} \int_0^\pi J_R R^2 \sin\theta d\theta d\phi = \frac{\sigma V_o}{\frac{1}{R_i} - \frac{1}{R_o}} \int_0^{2\pi} d\phi \int_0^\pi \sin\theta d\theta$
 $= \frac{4\pi\sigma V_o}{\frac{1}{R_i} - \frac{1}{R_o}}$

$\therefore R = V_o/I = \frac{1}{4\pi\sigma} (\frac{1}{R_i} - \frac{1}{R_o})$