# Coastal Structures ('07 Fall) <br> Final Exam (12/18 12:00-12/19 10:00) 

## You have to solve this exam by yourself without talking to other persons.

1. (30) We would like to show that the probability density function of wave height $H$ is given by the Rayleigh probability density function for waves of narrow-band normal (or Gaussian) process. A narrow-band random process is defined as one whose spectral density function is sharply concentrated in the neighborhood of a certain frequency $\omega_{0}$. This implies that the random process $x(t)$ has a constant frequency, and they may be written as

$$
\begin{equation*}
x(t)=A(t) \cos \left[\omega_{0} t+\varepsilon(t)\right] \tag{1}
\end{equation*}
$$

where $A(t)$ is the amplitude and $\varepsilon(t)$ is the phase; both are random variables.
On the other hand, assuming that the random process $x(t)$ is a normal random process with zero mean and variance $\sigma^{2}, x(t)$ may be written as

$$
\begin{equation*}
x(t)=\sum_{n=1}^{\infty}\left(a_{n} \cos n \omega t+b_{n} \sin n \omega t\right) \tag{2}
\end{equation*}
$$

where

$$
\begin{align*}
& a_{n}=\frac{2}{T} \int_{0}^{T} x(t) \cos n \omega t d t  \tag{3}\\
& b_{n}=\frac{2}{T} \int_{0}^{T} x(t) \sin n \omega t d t \tag{4}
\end{align*}
$$

Here, the coefficients $a_{n}$ and $b_{n}$ are normally distributed with zero mean and variance $\sigma^{2}$.
(a) By writing $n \omega t$ as $\left(n \omega-\omega_{0}\right) t+\omega_{0} t$, express $x(t)$ in the form

$$
\begin{equation*}
x(t)=x_{c}(t) \cos \omega_{0} t-x_{s}(t) \sin \omega_{0} t \tag{5}
\end{equation*}
$$

and obtain the expressions of $x_{c}(t)$ and $x_{s}(t)$.
(b) Obtain the expressions of $x_{c}(t)$ and $x_{s}(t)$ in terms of $A(t)$ and $\varepsilon(t)$.
(c) We may write $x_{c}(t), x_{s}(t), A(t)$ and $\varepsilon(t)$ as the random variables $x_{c}, x_{s}, A$ and $\varepsilon$ for a given time $t$. Since $x_{c}$ and $x_{s}$ are the summations of normal random variables, they are also normally distributed. It can be proved that $x_{c}$ and $x_{s}$ are statistically independent normal random variables with zero mean and variance which is equal to twice the area under the spectral density function of $x(t)$.

That is,

$$
\begin{align*}
& E\left[x_{c}\right]=E\left[x_{s}\right]=0  \tag{6}\\
& E\left[x_{c} x_{s}\right]=0  \tag{7}\\
& E\left[x_{c}^{2}\right]=E\left[x_{s}^{2}\right]=\sigma^{2}=\int_{0}^{\infty} S(\omega) d \omega \tag{8}
\end{align*}
$$

where $S(\omega)$ = spectral density function of $x(t)$. For proofs, refer to Davenport and Root (1958) ${ }^{1}$.

When the random variables $X$ and $Y$ are the functions of other random variables $x$ and $y$, and the joint probability density function of $X$ and $Y$, $f(X, Y)$, is known, it can be transformed to the joint probability density function of $x$ and $y, f(x, y)$, by the following relationship:

$$
f(x, y)=[f(X, Y)]_{\substack{X=f n(x, y)  \tag{9}\\
Y=n n(x, y)}}\left|\begin{array}{cc}
\frac{\partial X}{\partial x} & \frac{\partial X}{\partial y} \\
\frac{\partial Y}{\partial x} & \frac{\partial Y}{\partial y}
\end{array}\right|
$$

We may write the joint probability density function $x_{c}$ and $x_{s}$ as

$$
\begin{equation*}
f\left(x_{c}, x_{s}\right)=\frac{1}{2 \pi \sigma^{2}} e^{-A^{2} / 2 \sigma^{2}} \quad-\infty<x_{c}<\infty \quad-\infty<x_{s}<\infty \tag{10}
\end{equation*}
$$

Obtain the joint probability density function $f(A, \varepsilon)$ using the above transformation.
(d) Obtain the marginal probability density function $f(A)$ by integrating $f(A, \varepsilon)$ from 0 to $2 \pi$ with respect to $\varepsilon$.
(e) Express $f(A)$ in terms of $H$ and $H_{r m s}$ and compare it with the Rayleigh probability density function $f(H)$ given by Eq. (7.18) in Dean \& Dalrymple's book.

[^0]2. (40) Two gages will be used to separate the incident and reflected waves in front of a structure as shown in Fig. 1 where $\Delta \ell=$ unknown distance between the two gages; $h=$ water depth; $S_{i}(f)=$ incident wave spectrum with $f=$ frequency; $H_{s}=$ incident significant wave height; and $T_{s}=$ incident significant wave period. The wavemaker is assumed to be ideal and generate $S_{i}(f)$ as specified as input to the wavemaker. The unknown gage spacing $\Delta \ell$ may be selected to maximize the incident wave energy resolved by the two gages.
\[

$$
\begin{equation*}
\text { maximize } E=\int_{f_{\min }}^{f_{\max }} S_{i}(f) d f \text { with respect to } \Delta \ell \tag{1}
\end{equation*}
$$

\]

where $f_{\text {max }}$ and $f_{\text {min }}$ are the maximum and minimum frequencies that can be resolved by the two gages on the basis of the recommendation in Goda's book (p 359).

To simplify the following analysis, $S_{i}(f)$ is assumed to be given by the Bretschneider-Mitsuyasu spectrum (Eq. (2.10) in Goda's book). Furthermore, the frequencies $f_{\max }$ and $f_{\min }$ are assumed to correspond to deep-water and shallowwater waves, respectively.

$$
\begin{equation*}
\tanh \left(k_{\max } h\right) \cong 1 ; \quad \tanh \left(k_{\min } h\right) \cong k_{\min } h \tag{2}
\end{equation*}
$$

where $k_{\max }$ and $k_{\min }$ are the wave numbers corresponding to $f_{\max }$ and $f_{\text {min }}$, respectively.
(a) Derive an equation based on Eq. (1) for the optimal gage spacing $\Delta \ell$. Show that the value of $\Delta \ell^{*}=\Delta \ell /\left(T_{s} \sqrt{g h}\right)$ is uniquely determined for given $L_{s}^{*}=T_{s} \sqrt{g / h}$.
(b) Find the value of $\Delta \ell$ for $h=0.4 \mathrm{~m}$ and $T_{s}=2 \mathrm{~s}$ and show that the assumptions given in Eq. (2) are satisfied approximately. You may need the Newton-Raphson iteration method.

3. (30) A structure is subjected to a characteristic load $S$ that has a mean value $\mu_{s}=$ 80 kN and is normally distributed with a standard deviation $\sigma_{s}=18 \mathrm{kN}$. For the type of structure we are designing, the characteristic resistance $R$ is known to have $\sigma_{r}=20 \mathrm{kN}$.
(a) We want to design the structure with the safety factor $\Gamma=\gamma_{r} \gamma_{s}=1.0, Z_{s}=0$ and $Z_{r}=-1.64$, so that the mean load can be resisted by the structure $95 \%$ of the time, where $Z_{s}=\left(S-\mu_{s}\right) / \sigma_{s}, Z_{r}=\left(R-\mu_{r}\right) / \sigma_{r}$, and $\gamma_{r}$ and $\gamma_{s}$ are the partial safety factors for resistance and load, respectively. Describe the design equation in the partial safety factor system. Calculate the mean resistance $\mu_{r}$ and the probability of failure $P_{f}$.
(b) We want to design the structure so that the probability of failure is the same as that calculated in part (a) but the mean load can be resisted by the structure $50 \%$ of the time. Calculate the safety factor $\Gamma$.
(c) In the case of $\Gamma=1.3, Z_{s}=0$ and $Z_{r}=-1.64$, calculate the mean resistance $\mu_{r}$ and the probability of failure $P_{f}$.


[^0]:    ${ }^{1}$ Davenport, W. B. and Root, W. L. (1958). An introduction to the theory of random signals and noise. McGraw-Hill, New York.

