

Design of Piezoelectric Active Structures

Lecture 5:

Examples of Actuated Structures

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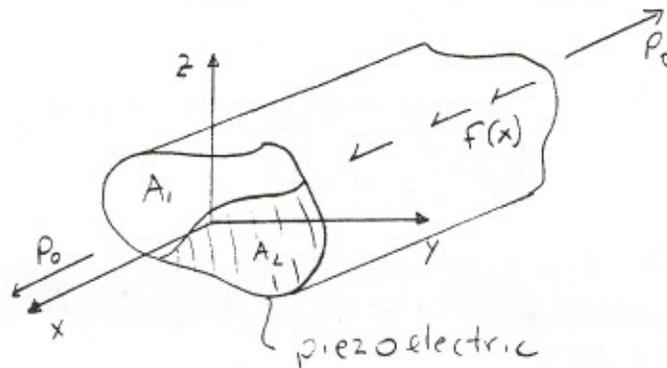
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Outline

- Extension of Rods
- Bending Beams
- Transverse Shear Model
- Torsion of Beams
- Anisotropic Plates
- Shells

Extension of Rods - I

- Consider inhomogeneous rod



- Let piezo be poled in x direction. "Longitudinal case"
- Strain Displacement: axial extension

$$u = u_0(x)$$

$$S_1 = \frac{du_0}{dx}$$

$$E_1 = \frac{v_0}{l} \cdot x$$

> all others zero?
may allow poisson's
contraction
 $S_2 = S_3 = \nu S_1$

- Stress Resultants (interior)

$$P = \int_A T_1 dA = P_1 + P_2$$

Note: equilibrium says $P_0 = P$

Extension of Rods II

- Constitutive Relations

full blown

$$\begin{bmatrix} T \\ D \end{bmatrix} = \begin{bmatrix} c^E & -e_1 \\ e & \epsilon^s \end{bmatrix} \begin{bmatrix} S \\ E \end{bmatrix}$$

assuming $S_1 \neq 0$, assuming only $E_1 \neq 0$

Note: properties have to be rotated so poling (3 direction) lines up with x axis.

- Energy Principle

$$\int_{\ell} \int_A \{ -(T \delta S) + D \delta E \} dA dx + P_o \delta u(x = \ell) + \int_{\ell} f_x \delta u dx = 0$$

since only S_1 and E_1 exist, this can be simplified. Also: material properties are different in each section so

$$\int_A (\cdot) da = \int_{A_1} da + \int_{A_2} da$$

plugging in assuming $A_1 = \text{structure}$, $A_2 = \text{piezo}$

$$\int_{\ell} \left[\int_A (-c_{11} S_1 \delta S_1) da + \int_{A_2} \{ -(c_{33}^E S_1 - \rho_{33} E_1) \delta S_1 + (\rho_{33} S_1 + \epsilon_{33}^s E_1) \delta E_1 \} da + f_x du \right] dx + P_o \delta u(x = \ell) = 0$$

Extension of Rods - III

- Integrating over cross section
(introduce section properties)

$$\bar{c} = A_1 c_{11} + A_2 c_{33}^E$$

$$\bar{e} = A_2 e_{33}$$

$$\bar{\epsilon} = A_2 \epsilon_{33}^3$$

get

$$\int_{\ell} [-(\bar{c} S_1 - \bar{e} E_1) \delta S_1 + (\bar{e} S_1 + \bar{\epsilon} E_1) \delta E_1 + f_x \delta u] dx \\ + P_o \delta u (x=\ell) = 0$$

- 2 options:

1) continuous - $u(x) \Rightarrow$ differential equation for rod

2) discrete - assume

$$u(x) = \frac{u_o x}{\ell} \Rightarrow \delta S_1 = \frac{\delta u_o}{\ell}$$

$$\varphi = \frac{v_o x}{\ell} \Rightarrow \delta E_1 = \frac{\delta v_o}{\ell}$$

Discrete Representation

$$\int_l \left\{ \underbrace{\left(\bar{c} \frac{u_0}{l} - \bar{e} \frac{v_0}{l} \right)}_{\text{arbitrary variations}} \frac{\delta u_0}{l} + \underbrace{\left(\bar{e} \frac{u_0}{l} + \bar{\epsilon} \frac{v_0}{l} \right)}_{\text{arbitrary variations}} \frac{\delta v_0}{l} + f_x \frac{\delta u_0}{l} x \right\} dx + P_0 \delta u_0 = 0$$

you get

$$\delta u_0 : \frac{\bar{c}}{l} u_0 + \bar{e} \frac{v_0}{l} + \int_x f_x \cdot \frac{x}{l} dx + P_0 = 0 \quad \text{Actuator Eqn.}$$

$$\delta v_0 : \frac{\bar{e}}{l} u_0 + \bar{\epsilon} \frac{v_0}{l} = 0 \quad \text{Sensor Eqn.}$$

or in matrix form

$$\begin{bmatrix} \bar{c} & -\bar{e} \\ \bar{e} & \bar{\epsilon} \end{bmatrix} \begin{bmatrix} \frac{u}{l} \\ \frac{v}{l} \end{bmatrix} = \begin{bmatrix} P_0 + \int_x f_x \cdot \frac{x}{l} dx \\ 0 \end{bmatrix}$$

no applied charge

- Free Expansion

$$\frac{u}{l} = S_0 = \frac{\bar{e}}{\bar{c}} \frac{v}{l} = \left(\frac{A_2}{A_1 c_{11} + A_2 c_{33}} \right) \underbrace{e_{33} E_0}_{\text{induced stress}}$$

st. (stress)
cut down