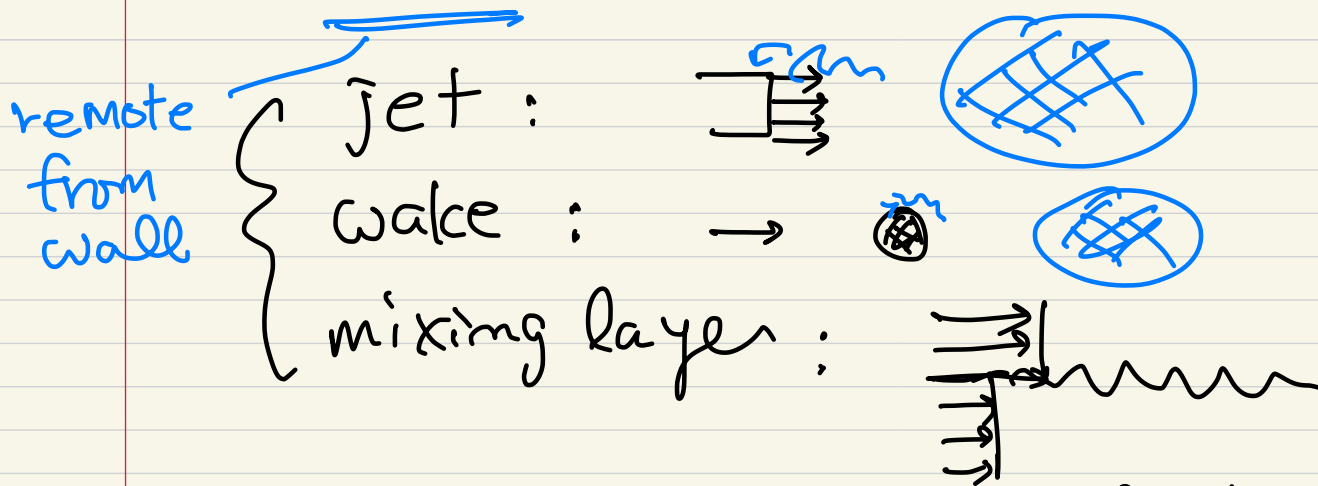
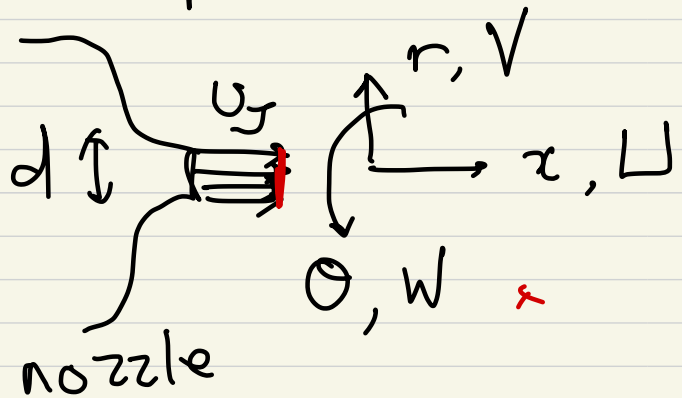


# Ch. 5 Free shear flows

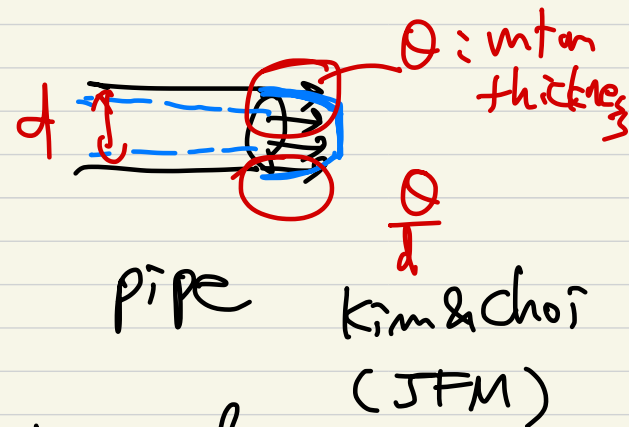


## 5.1 Round jet : experimental observations

### ① Description of flow

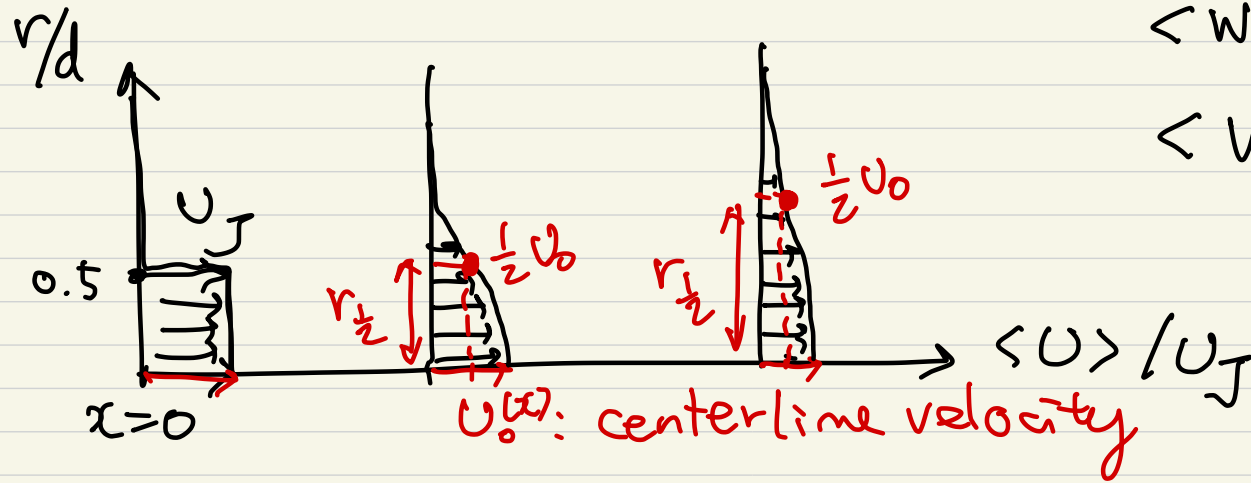


statistically stationary  
&  
axisymmetric



$$Re \equiv U_j d / \nu : \text{jet Reynolds number}$$

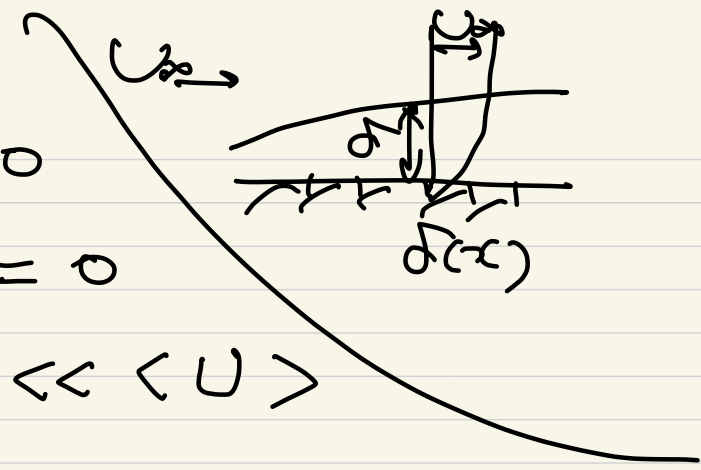
# ① Mean velocity field



$$W \neq 0$$

$$\langle W \rangle = 0$$

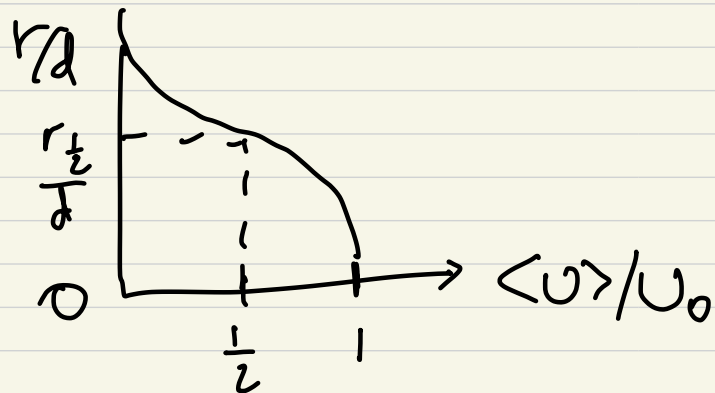
$$\langle V \rangle \ll \langle U \rangle$$



$$U(x, r, \theta, t)$$

• centerline velocity :  $U_0(x) = \langle U(x, 0, 0, t) \rangle$

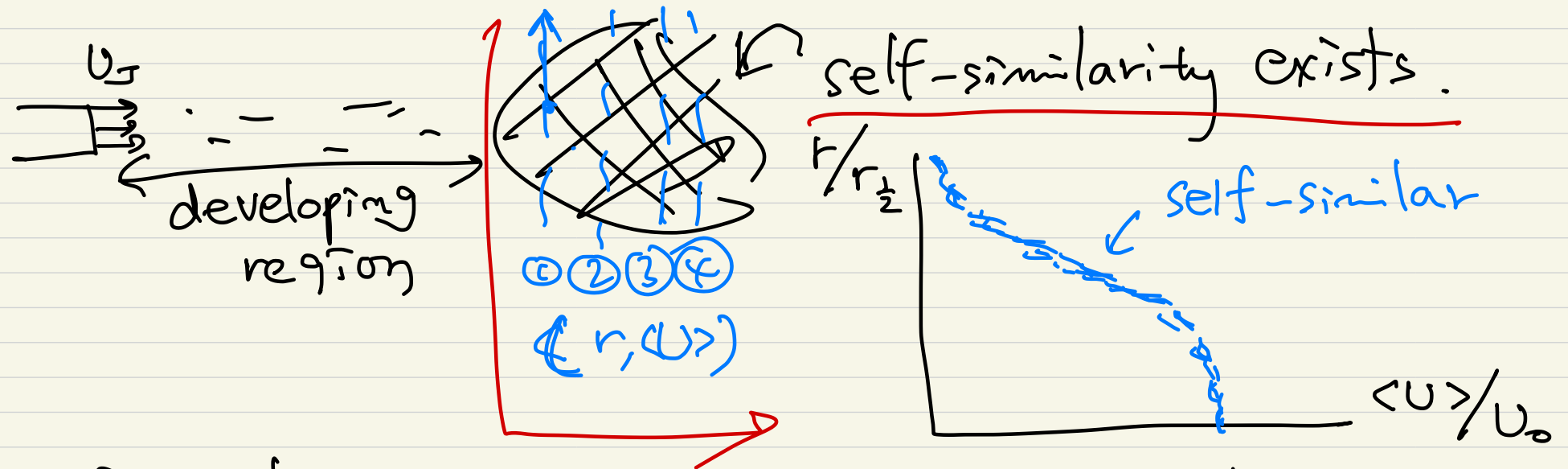
• Jet half-width  $r_{1/2}(x)$  :  $\langle U(x, r_{1/2}(x), \theta, t) \rangle = \frac{1}{2} U_0(x)$



As  $x \uparrow$ , jet decays (i.e.  $U_0(x)$  decreases)

& jet spreads (i.e.  $r_{1/2}(x)$  increases).

- Beyond the developing region ( $x > 30d$ )



- self-similarity: important concept in turbulent flow

$Q(x, y)$ : a quantity

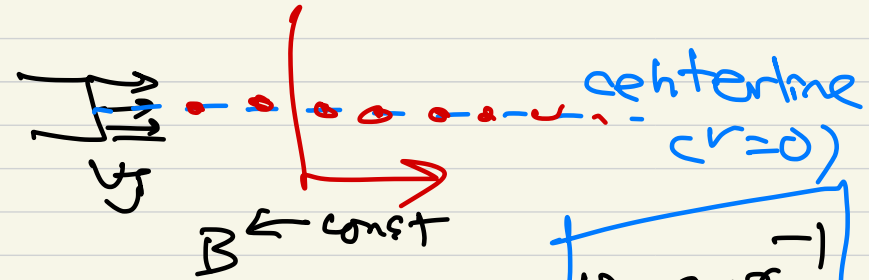
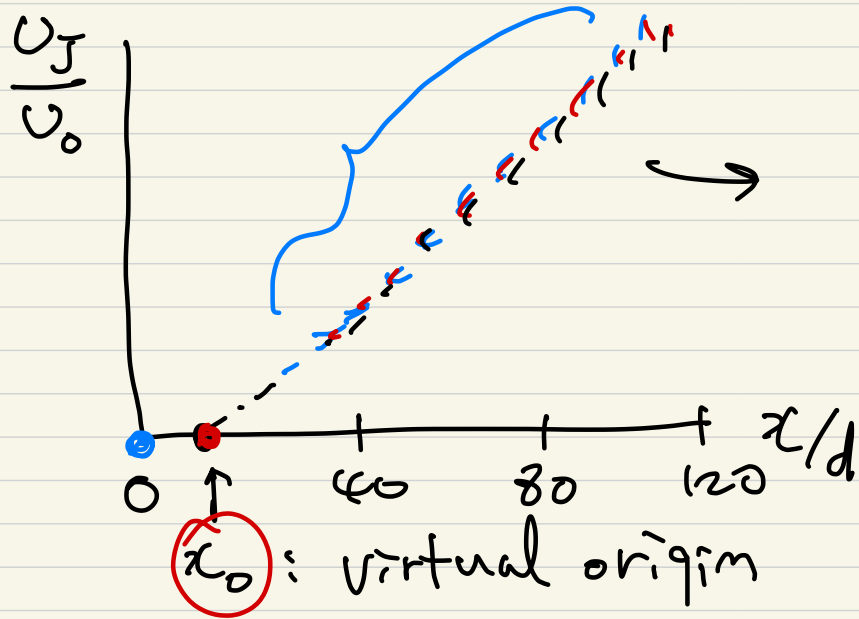
$Q_0(x)$  and  $\delta(x)$ : characteristic scales  
 $\uparrow$  length scale

Define  $\xi \equiv y / \delta(x)$

$\hat{Q}(\xi, x) \equiv Q(x, y) / Q_0(x)$

If  $\tilde{Q}(\xi, x) = \tilde{Q}(\xi)$ ,  $Q(x, y)$  is self-similar.

• Axial variation of scales

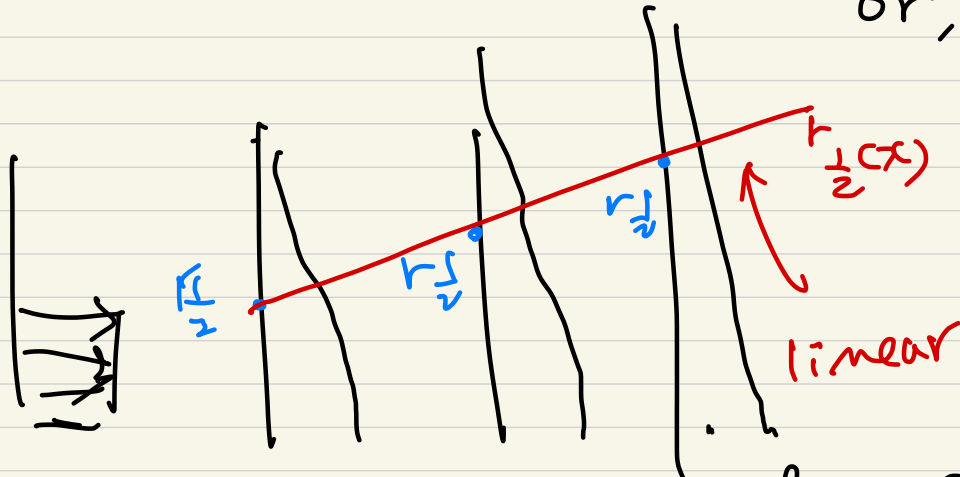


$$\frac{U_0(x)}{U_J} = \frac{B}{(x-x_0)/d} \rightarrow U_0 \sim x^{-1}$$

It is also found that the spreading rate  $S$

$$S \equiv \frac{dh_{1/2}(x)}{dx} = \text{const}$$

$$\text{or, } h_{1/2} = S(x-x_0) \rightarrow h_{1/2} \sim x$$



$h_{1/2} \cdot U_0$  is indep. of  $x$

local Reynolds number  $Re_0(x) = \frac{U_0(x) h_{1/2}(x)}{\nu}$  is indep. of  $x$ .

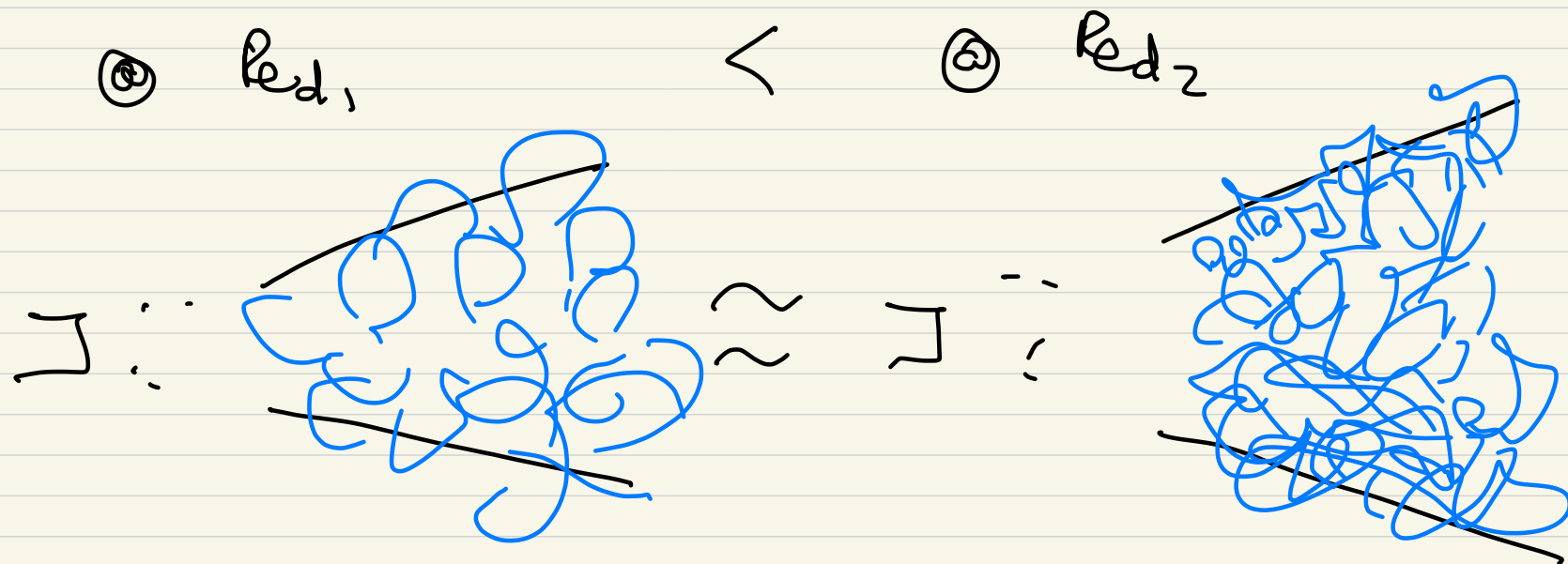
Red

• S and B have no dependence on  $Re \rightarrow Re_d$

(Table 5.1)  $Re_d = 11000 \sim 95500$

$B = 5.8 \sim 6.0$  &  $S = 0.094 \sim 0.1$

→ The mean vel. profile and spreading rate are indep. of  $Re_d$ , although small-scale structures are smaller at larger  $Re$  #



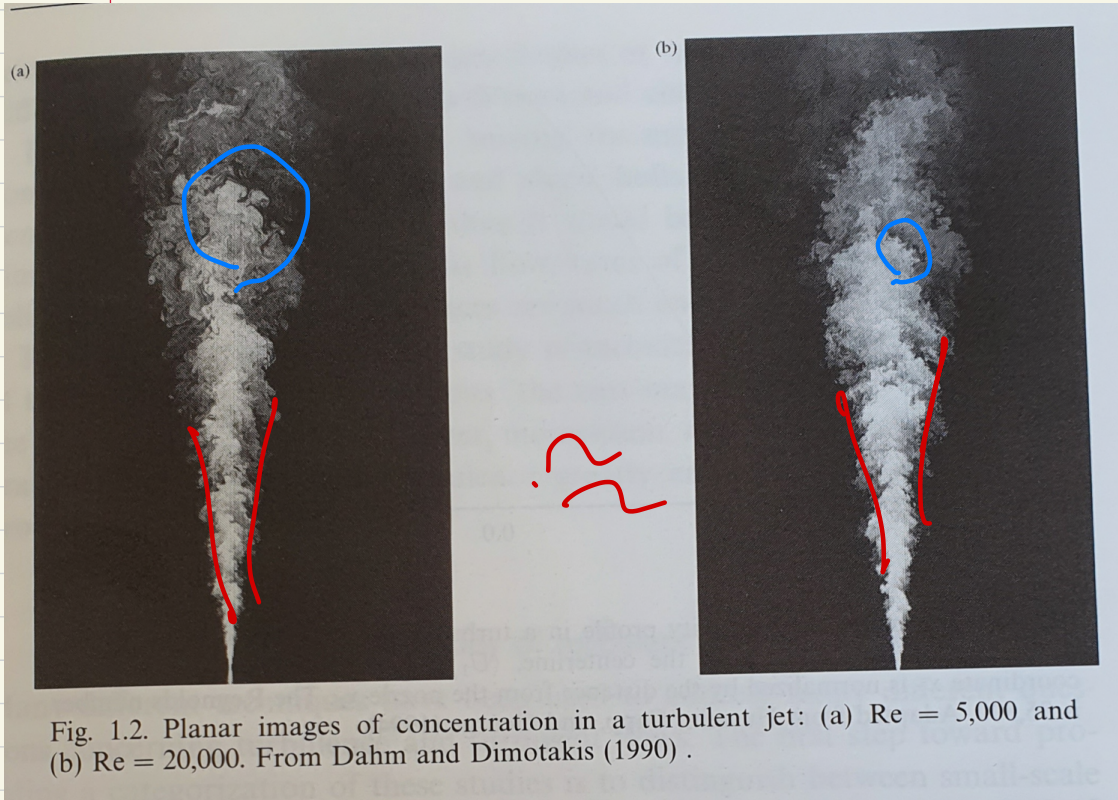


Fig. 1.2. Planar images of concentration in a turbulent jet: (a)  $Re = 5,000$  and (b)  $Re = 20,000$ . From Dahm and Dimotakis (1990).

$Re_d = 5,000$

$Re_d = 20,000$

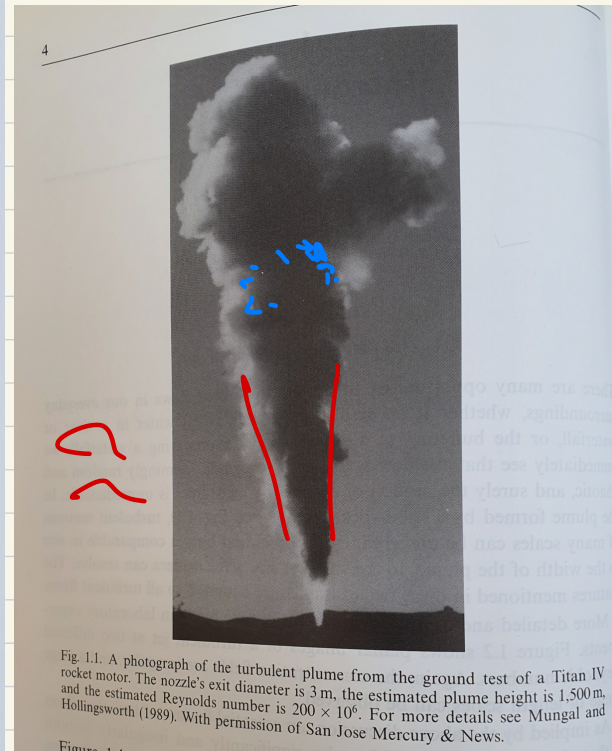
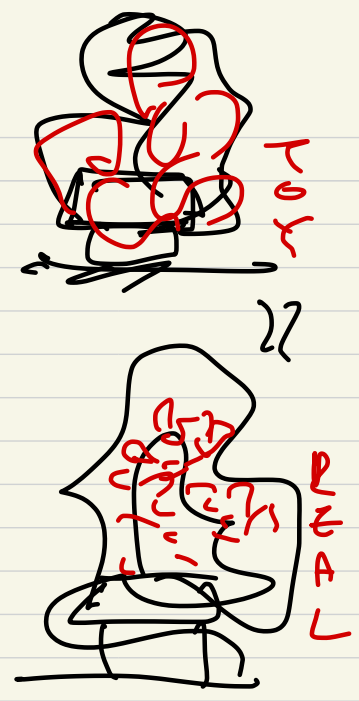


Fig. 1.1. A photograph of the turbulent plume from the ground test of a Titan IV rocket motor. The nozzle's exit diameter is 3 m, the estimated plume height is 1,500 m, and the estimated Reynolds number is  $200 \times 10^6$ . For more details see Mungal and Hollingsworth (1989). With permission of San Jose Mercury & News.

$Re_d = 200 \times 10^6$

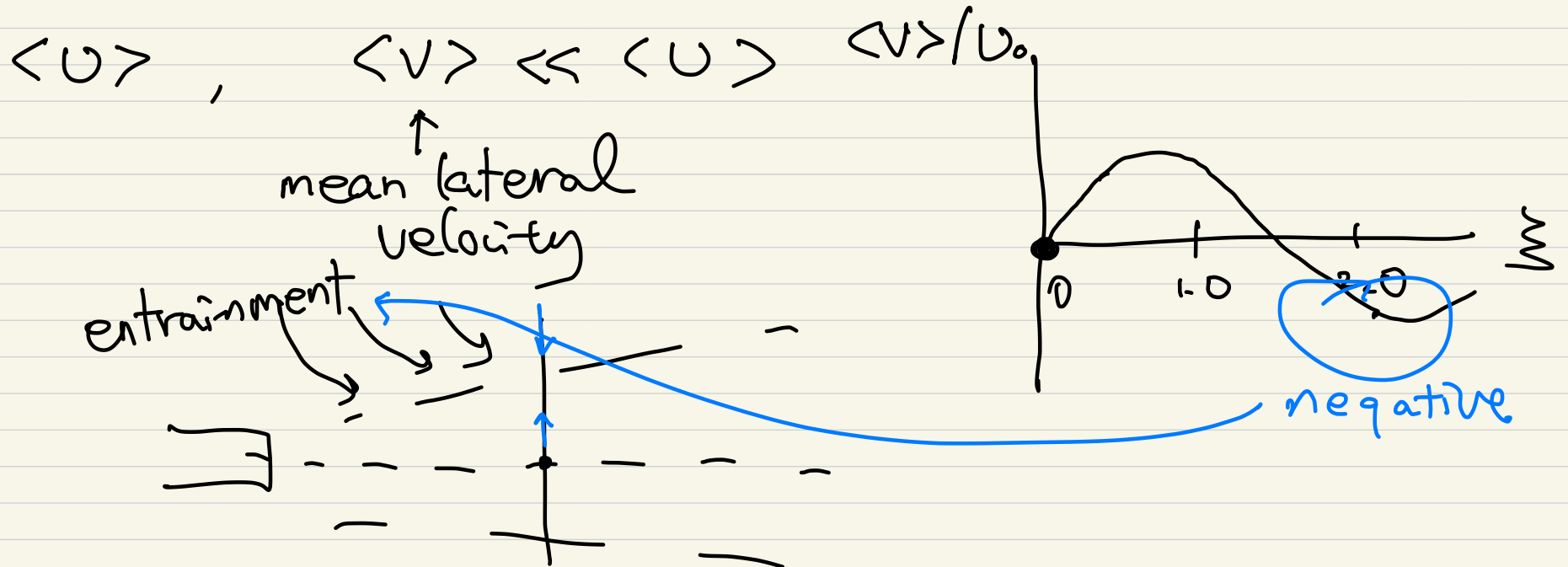
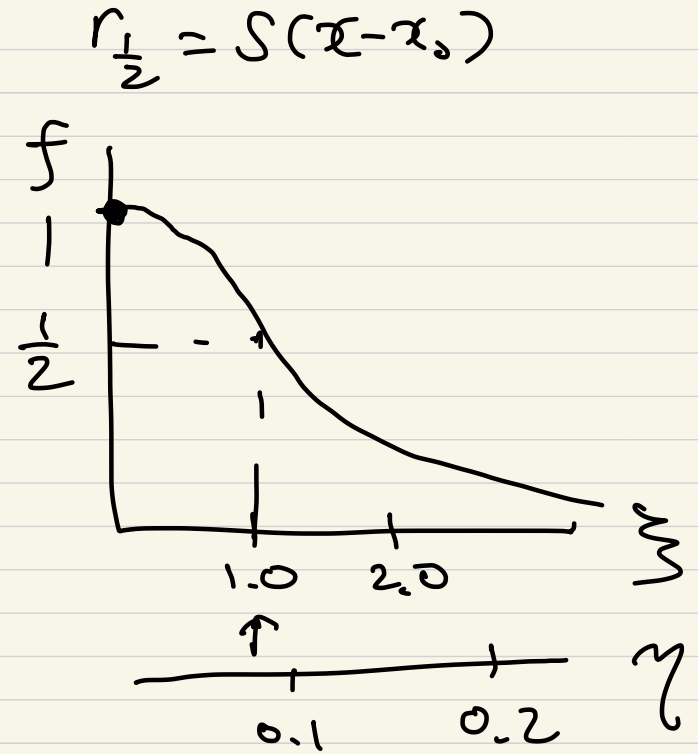


$$\xi = r/r_{1/2} \quad \text{or} \quad \eta = r/(x-x_0)$$

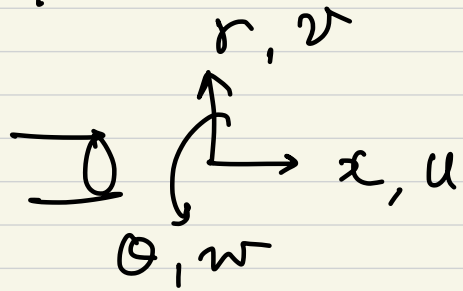
$$\rightarrow \eta = S \xi$$

$$f(\eta) = \bar{f}(\xi) = \frac{\langle U(x, r, 0) \rangle}{U_0(x)}$$

self-similar mean velocity profile



• Reynolds stresses



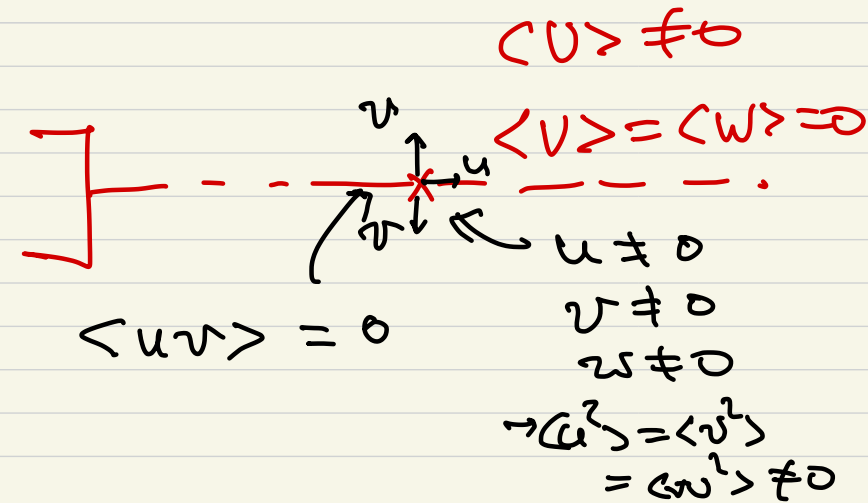
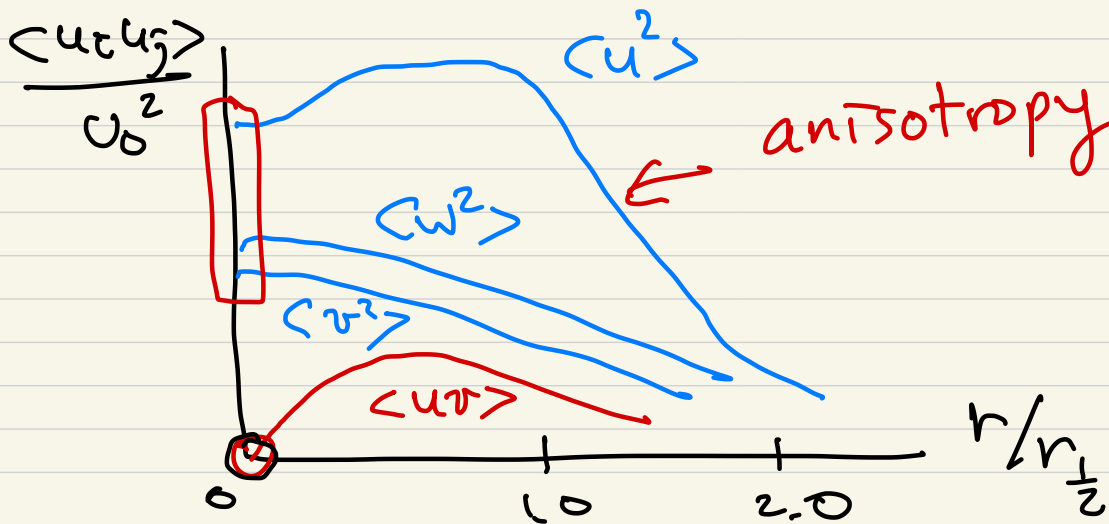
$$\begin{bmatrix} \langle u^2 \rangle & \langle uv \rangle & 0 \\ \langle uv \rangle & \langle v^2 \rangle & 0 \\ 0 & 0 & \langle w^2 \rangle \end{bmatrix}$$

due to circumferential symmetry

$u'_0(x) \equiv \langle u^2 \rangle_{r=0}^{1/2}$  : rms axial centerline vel. fluctuations

in self-similar region,  $u'_0(x) / U_0(x) \sim 0.25$

$\rightarrow u'_0 \sim U_0 \sim x^{-1} \quad \frac{\partial \langle u \rangle}{\partial x} = 0$



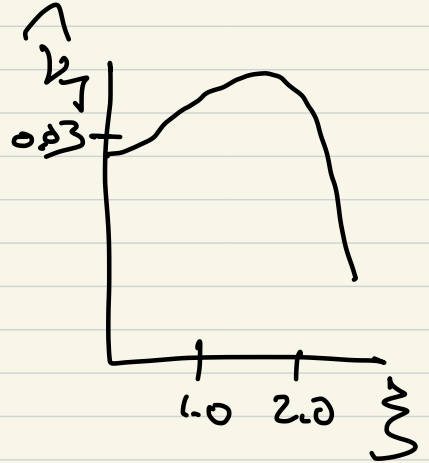


$$\langle uv \rangle \equiv - \underbrace{\nu_T}_{\sim} \frac{\partial \langle U \rangle}{\partial r} > 0 \quad \frac{\partial \langle U \rangle}{\partial r} < 0$$

of. bdry layer  
 $\langle uv \rangle < 0$

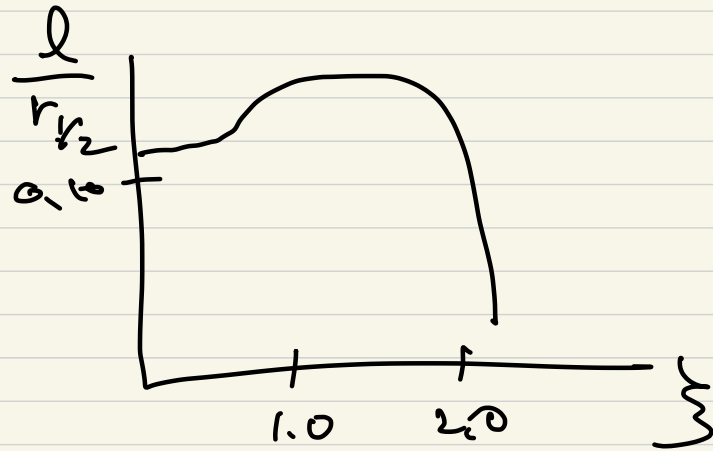
$$\hookrightarrow \nu_T \sim u \cdot l$$

$$\nu_T(x, r) = U_0(x) r_{\frac{1}{2}}(x) \hat{\nu}_T(\eta) \quad \hat{\nu}_T(\xi)$$



$\left. \begin{matrix} \langle uv \rangle \\ \langle U \rangle \end{matrix} \right\}$  self-similar  $\rightarrow \nu_T$  self-similar

$$\nu_T = u \cdot l = u' \cdot l$$



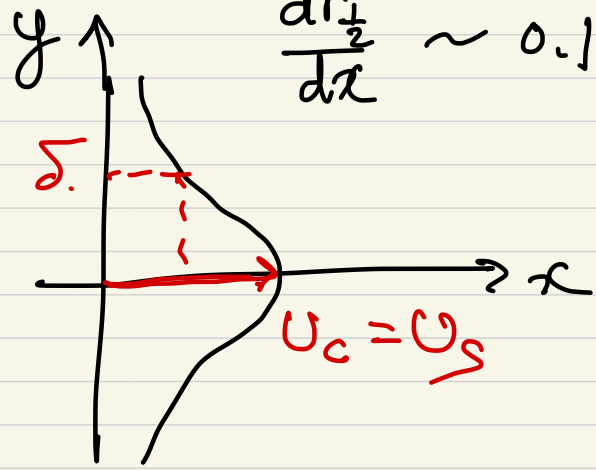
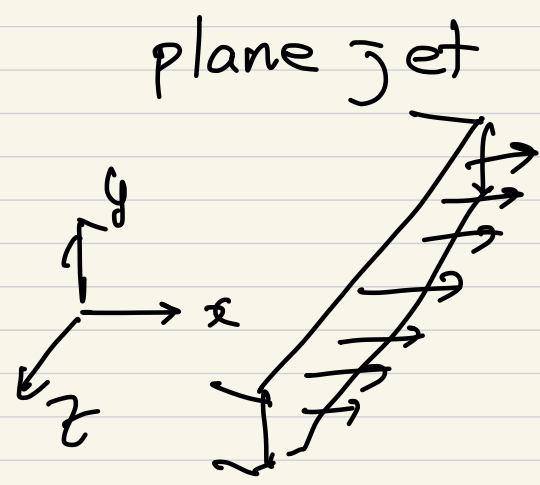
$$V = \langle V \rangle + v \quad \text{vs} \quad v = \bar{v} + v'$$

5.2 Round jet : mean momentum  $\langle V \rangle \ll \langle W \rangle$

① Boundary-layer eqs.

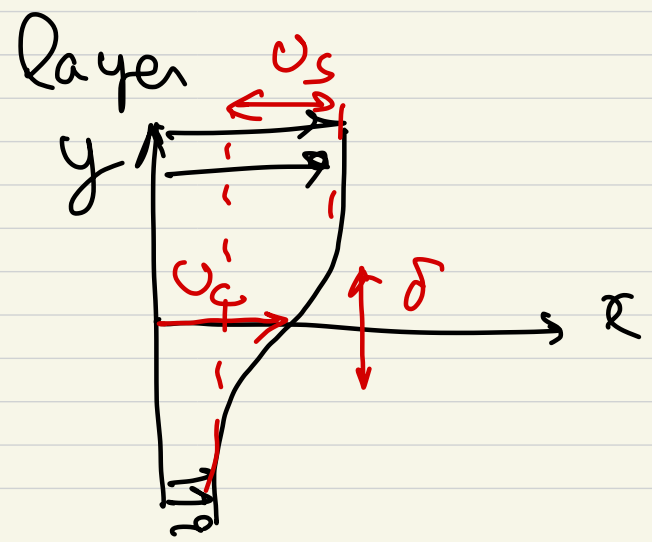
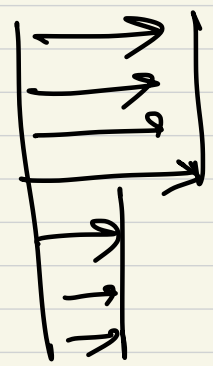
in turbulent jet,  $|\langle V \rangle| \approx 0.03 |\langle U \rangle|$

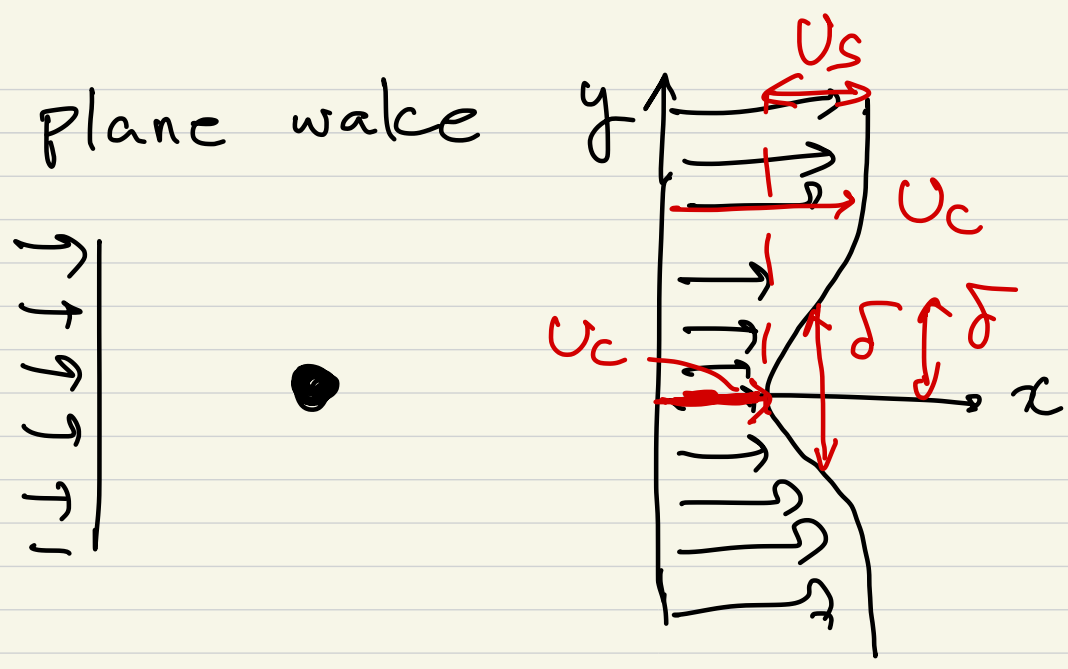
$\frac{dr_{\frac{1}{2}}}{dx} \sim 0.1 \leftarrow$  axial grad is very small



$\delta$  : char. flow width  
 $U_c$  : char. convection vel.  
 $U_s$  : char. vel. difference

plane mixing layer





boundary-layer approx.

$$|\langle u \rangle| \gg |\langle v \rangle|$$

$$\frac{\partial}{\partial y}(\cdot) \gg \frac{\partial}{\partial x}(\cdot)$$

