

Ship Stability

Ch. 7 Inclining Test

Spring 2016

Myung-II Roh

Department of Naval Architecture and Ocean Engineering
Seoul National University

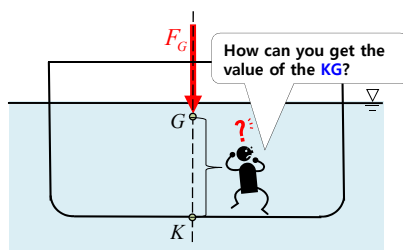
Contents

- Ch. 1 Introduction to Ship Stability
- Ch. 2 Review of Fluid Mechanics
- Ch. 3 Transverse Stability Due to Cargo Movement
- Ch. 4 Initial Transverse Stability
- Ch. 5 Initial Longitudinal Stability
- Ch. 6 Free Surface Effect
- Ch. 7 Inclining Test**
- Ch. 8 Curves of Stability and Stability Criteria
- Ch. 9 Numerical Integration Method in Naval Architecture
- Ch. 10 Hydrostatic Values and Curves
- Ch. 11 Static Equilibrium State after Flooding Due to Damage
- Ch. 12 Deterministic Damage Stability
- Ch. 13 Probabilistic Damage Stability

Ch. 7 Inclining Test

The Problem of Finding an Accurate Vertical Center of Gravity (KG)

The problem of **finding an accurate KG** for a ship is a serious one for the ship's designer.



K: Keel
G: Center of gravity

✓ Any difference in the weight of structural parts, equipment, or welds in different ship will produce a different KG.

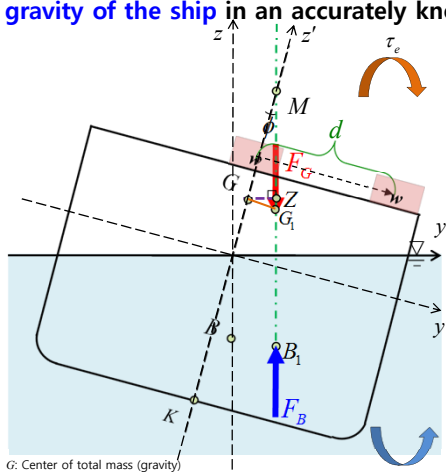


There is an accurate method of finding KG for any particular ship and that is **the inclining test**.

Required Values to Find the KG (1/3)

$\tau_r = F_B \cdot GZ$
 $GZ \approx GM \cdot \sin \phi \text{ (at small angle } \phi)$
 $GM = KB + BM - KG$

The purpose of the inclining test is to determine the position of the center of gravity of the ship in an accurately known condition.



Required values to find the KG

- Draft
- Total weight (F_G)
- Hydrostatic values (KB, BM)
- Weight (w)
- Distance (d)
- Angle of inclination (ϕ)*

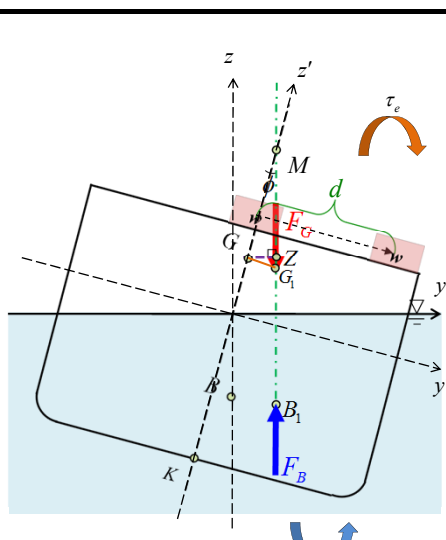
G: Center of total mass (gravity)
 B: Center of buoyancy at initial position
 G_1 : New position of center of total mass (gravity) after the weight has been moved
 B_1 : New position of center of buoyancy after the ship has been inclined
 Z: The intersection of vertical line through the center of buoyancy with the transversally parallel line to a waterline through center of total mass (gravity)
 M: The intersection of a vertical line through the center of buoyancy at previous position(B) with a vertical line through the present position of the center of buoyancy(B_1) after the ship has been inclined transversally through a small angle

τ_r : Heeling moment
 τ_r : Righting moment

5

Required Values to Find the KG (2/3)

$\tau_r = F_B \cdot GZ$
 $GZ \approx GM \cdot \sin \phi \text{ (at small angle } \phi)$
 $GM = KB + BM - KG$



Shift of center of total mass (gravity)

$$GG_1 = \frac{w \cdot d}{F_G}$$

Heeling moment produced by total weight

$$\tau_h = F_G \cdot GG_1 \cos \phi$$

Righting moment produced by buoyant force

$$\tau_r = F_B \cdot GZ \approx F_B \cdot GM \sin \phi$$

Static equilibrium of moment

$$F_G \cdot GG_1 \cos \phi = F_B \cdot GM \sin \phi$$

(\because Static equilibrium : $F_G = F_B$)

$$\therefore GM = \frac{GG_1}{\tan \phi} = \frac{w \cdot d}{F_G \cdot \tan \phi}$$

Inclining test formula

Naval Architectural Calculation, Spring 2016, Myung-Il Roh

sydlab 6

Required Values to Find the KG (3/3)

$\tau_r = F_B \cdot GZ$
 $GZ \approx GM \cdot \sin \phi$ (at small angle ϕ)
 $GM = KB + BM - KG$

Inclining experiment formula

$$GM = \frac{w \cdot d}{F_G \cdot \tan \phi}$$

KG

$$KG = KB + BM - GM$$

$$= \underset{\text{Known}}{KB} + \underset{\text{Known}}{BM} - \frac{w \cdot d}{\underset{\text{Known}}{F_G} \cdot \tan \phi}$$

The angle of inclination can be measured when we perform the inclining test.

Naval Architectural Calculation, Spring 2016, Myung-Il Roh **sydlab** 7

Derivation of Inclining Test Formula (1/5)

$\tau_r = F_B \cdot GZ$
 $GZ \approx GM \cdot \sin \phi$ (at small angle ϕ)
 $GM = KB + BM - KG$

Suppose that the center of gravity is located at K . Then the KN represents the righting arm.

$$GZ = KN$$

$$= KN_0 + N_0N$$

$$= KB \cdot \sin \phi + \delta y_B' \cdot \cos \phi + \delta z_B' \cdot \sin \phi$$

These terms have positive effect to the restoring moment arm.

8

Derivation of Inclining Test Formula (2/5)

$\tau_r = F_B \cdot GZ$
 $GZ \approx GM \cdot \sin \phi$ (at small angle ϕ)
 $GM = KB + BM - KG$

$GZ = KN$
 $= KN_0 + N_0N$
 $= KB \cdot \sin \phi + \delta y_B' \cdot \cos \phi + \delta z_B' \cdot \sin \phi$

$KG = \delta z_G'$
 $GZ = KN - KG'$
 $= KB \cdot \sin \phi + \delta y_B' \cdot \cos \phi + \delta z_B' \cdot \sin \phi - \delta z_G' \cdot \sin \phi$

This term has negative effect to the restoring moment arm.

Derivation of Inclining Test Formula (3/5)

$\tau_r = F_B \cdot GZ$
 $GZ \approx GM \cdot \sin \phi$ (at small angle ϕ)
 $GM = KB + BM - KG$

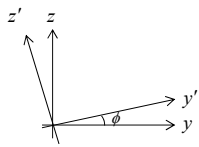
$GZ = KN - KG'$
 $= KB \cdot \sin \phi + \delta y_B' \cdot \cos \phi + \delta z_B' \cdot \sin \phi - \delta z_G' \cdot \sin \phi$

$KG = \delta z_G'$
 $GG_1 = \delta y_G'$
 $G_1Z_1 = KN - KG' - G_1G_1'$
 $= KB \cdot \sin \phi + \delta y_B' \cdot \cos \phi + \delta z_B' \cdot \sin \phi - \delta z_G' \cdot \sin \phi - \delta y_G' \cdot \cos \phi$

This term has negative effect to the restoring moment arm.

Derivation of Inclining Test Formula (4/5)

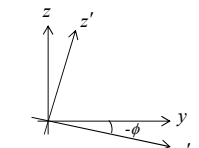
✓ Rotational transformation matrix (b to n frame)



$${}^n \mathbf{r}_p = {}^n \mathbf{R}_b {}^b \mathbf{r}_p$$

$$\begin{bmatrix} \cos \phi & -\sin \phi \\ \sin \phi & \cos \phi \end{bmatrix} = {}^n \mathbf{R}_b(\phi)$$

✓ Rotational transformation matrix (b to n frame)



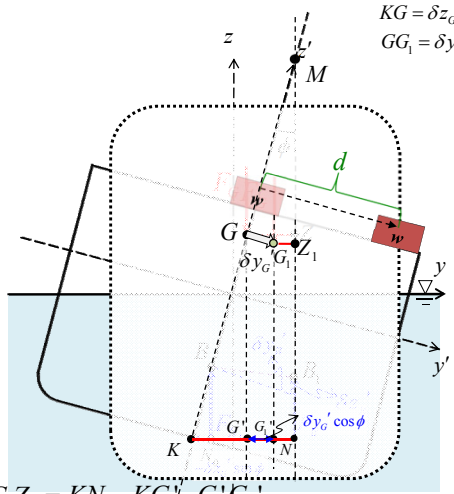
$$\begin{bmatrix} \cos(-\phi) & -\sin(-\phi) \\ \sin(-\phi) & \cos(-\phi) \end{bmatrix} = {}^n \mathbf{R}_b(-\phi)$$

✓ In n-frame, because the forces are acting on vertical direction, moment arm is **y_n-component**.

$$\begin{bmatrix} \delta y_B \\ \delta z_B \end{bmatrix} = \begin{bmatrix} \cos \phi & \sin \phi \\ -\sin \phi & \cos \phi \end{bmatrix} \begin{bmatrix} \delta y'_B \\ \delta z'_B \end{bmatrix}$$

⇒ $\delta y_B = \delta y'_B \cos \phi + \delta z'_B \sin \phi$

⇒ $\delta y_G = \delta y'_G \cos \phi + \delta z'_G \sin \phi$



$KG = \delta z'_G$
 $GG_1 = \delta y'_G$

$$G_1 Z_1 = KN - KG' - G' G_1'$$

$$= KB \cdot \sin \phi + \delta y'_B \cdot \cos \phi + \delta z'_B \cdot \sin \phi$$

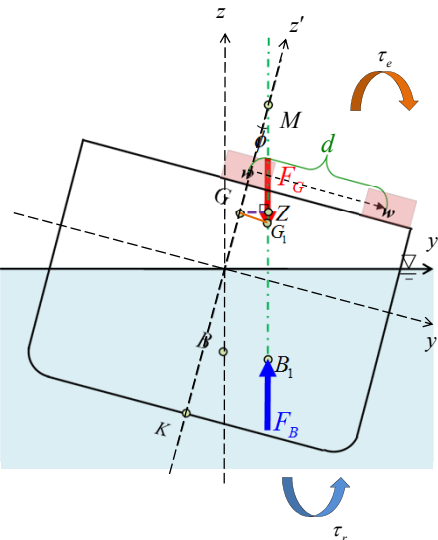
$$- \delta z'_G \cdot \sin \phi - \delta y'_G \cdot \cos \phi$$

δy_B
 $-\delta y_G$

$\tau_r = F_B \cdot GZ$
 $GZ \approx GM \cdot \sin \phi$ (at small angle ϕ)
 $GM = KB + BM - KG$

11

Derivation of Inclining Test Formula (5/5)



Calculation of moment using "GZ"

$$G_1 Z_1 = KN - KG' - G' G_1'$$

$$= KB \cdot \sin \phi + \delta y'_B \cdot \cos \phi + \delta z'_B \cdot \sin \phi$$

$$- \delta z'_G \cdot \sin \phi - \delta y'_G \cdot \cos \phi$$

$$= \underline{KN - KG \sin \phi} - GG_1 \cos \phi$$

(= GZ
(= GM sin phi : Assume that phi << 1

$$= GM \sin \phi - GG_1 \cos \phi$$

Moment produced by total weight & buoyant force

$$\delta M = \Delta \cdot G_1 Z_1$$

$$= \Delta \cdot (GM \sin \phi - GG_1 \cos \phi)$$

Static equilibrium of moment

$$GM \sin \phi = GG_1 \cos \phi$$

∴ $GM = \frac{GG_1}{\tan \phi} = \frac{w \cdot d}{F_G \cdot \tan \phi}$: Inclining test formula

$KG = \delta z'_G$ $GG_1 = \frac{w \cdot d}{F_G}$ $\tau_r = F_B \cdot GZ$
 $GG_1 = \delta y'_G$ $GZ \approx GM \cdot \sin \phi$ (at small angle ϕ)
 $GM = KB + BM - KG$

12

Method of Measuring the Angle of Inclination (1/2)

$$GM = \frac{w \cdot d}{F_G \cdot \tan \phi}$$
 Inclining test formula

How can you measure the angle of inclination when you perform the inclining test?

$\therefore \tan \phi = \frac{\text{Deflection}}{L}$

L: Length of plumb line
 Plumb: The line which is exactly vertical or perpendicular to a level horizontal line
 Batten: Long and thin strip of wood

13

Naval Architectural Calculation, Spring 2016, Myung-II Roh

Method of Measuring the Angle of Inclination (2/2)

* Reference: <http://www.mchl.fr>

14

Naval Architectural Calculation, Spring 2016, Myung-II Roh

Example	$GM = \frac{w \cdot d}{F_G \cdot \tan \phi}$	Inclining test formula
	$KG = KB + BM - GM$	

A ship is inclined by moving a weight of 40 tons a distance 8 m from the center line. A 12 m pendulum shows a deflection of 0.3 m. Displacement of the ship is 3,700 tons. If the KB is 5 m and BM is 14 m, what is the KG?

Solution)

$$\tan \phi = \frac{0.3}{12} = 0.025$$

$$GM = \frac{w \cdot d}{F_G \cdot \tan \phi} = \frac{40 \cdot 8}{3700 \cdot 0.025} = 3.46$$

$$KG = KB + BM - GM$$

$$= 5 + 14 - 3.46$$

$$= 14.54$$

$\therefore KG = 14.54[m]$

Naval Architectural Calculation, Spring 2016, Myung-II Roh

sydlab 15


Precautions to be Taken During the Inclining Test

Certain precautions must be taken to ensure that **accuracy is obtained**.

- (1) The ship must be **floating upright** and freely without restraint from ropes.
- (2) There should be **no wind** on the beam.
- (3) All **loose weights** should be **fixed**.
- (4) All cross-connections between tanks should be **closed**.
- (5) **Tanks should be empty or pressed full**. If neither of these conditions is possible, the level of liquid in the tank should be such that the **free surface effect** is readily calculable and will remain sensibly constant through the experiment.
- (6) The **number of men** on board should be kept to a minimum and they **should be on the center line**.
- (7) Any mobile equipment used to move the weights across the deck must return to a known positions for each set of readings.

Naval Architectural Calculation, Spring 2016, Myung-II Roh

sydlab 16

Various Problems Using the Inclining Test Formula	$GM = \frac{w \cdot d}{F_G \cdot \tan \phi}$	Inclining test formula
<p>The inclining test formula can be used in various problems as follows:</p>		
<p>(1) To find the angle of heel ϕ, a ship will take by moving a weight a transverse distance d.</p>		
$\tan \phi = \frac{w \cdot d}{GM \cdot F_G}$		
<p>(2) To find the weight w necessary to remove or produce a heel by moving it a transverse distance d.</p>		
$w = \frac{GM \cdot \tan \phi \cdot F_G}{d}$		
<p>(3) To find the distance d necessary to move a weight in order to remove or produce a heel.</p>		
$d = \frac{GM \cdot \tan \phi \cdot F_G}{w}$		
<small>Naval Architectural Calculation, Spring 2016, Myung-II Roh</small>		 17