

• Mean flow and turb kinetic energy

$$\left\{ \begin{array}{l} \frac{\overline{D\bar{E}}}{\overline{Dt}} + \frac{\partial}{\partial x_j} \bar{T}_{ij} = \overline{P} - \bar{\epsilon} \\ \frac{\overline{Dk}}{\overline{Dt}} + \frac{\partial}{\partial x_j} T'_{ij} = P - \epsilon \end{array} \right. \quad \begin{array}{l} \bar{E} = \frac{1}{2} \langle \underline{U} \rangle \cdot \langle \underline{U} \rangle \\ k = \frac{1}{2} \langle u_i u_i \rangle \\ \bar{T}_{ij} = \dots \\ T'_{ij} = \dots \end{array}$$

$$P = - \langle u_i u_j \rangle \frac{\partial \langle U_i \rangle}{\partial x_j} : \text{production}$$

$$\bar{\epsilon} = 2\nu \overline{S_{ij} S_{ij}} = 2\nu \langle S_{ij} \rangle \langle S_{ij} \rangle$$

$$\epsilon = 2\nu \langle S_{ij} S_{ij} \rangle \quad S_{ij} = S_{ij} - \langle S_{ij} \rangle$$

↑ dissipation due to fluctuating strain-rate

• dissipation ϵ

$$\epsilon = 2\nu \langle S_{ij} S_{ij} \rangle \geq 0$$

$$2\nu \langle S_{ij} \cdot \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \rangle$$

$= 2\nu \langle s_{xy} \frac{\partial u_i}{\partial x_j} \rangle$: fluctuating vel. grads. working against the fluctuating deviatoric stresses transfer kinetic energy to internal energy.

$$\overline{P} = \frac{P}{U_0^3 / r_{1/2}} \approx \frac{-\langle uv \rangle}{U_0^2} \frac{r_{1/2}}{U_0} \frac{\partial \langle U \rangle}{\partial Y} \quad \text{self-similar}$$

$\overline{\epsilon} = \frac{\epsilon}{U_0^3 / r_{1/2}} \sim$ from k-eq are self-similar and indep. of Re.

Kolmogorov Scales : characteristic scales of the smallest turbulent motions formed from ϵ and ν .

Ch. 6

$$\text{length scale: } \eta = (\nu^3 / \epsilon)^{1/4} \qquad \eta = \epsilon^a \nu^b$$

$$\text{time scale: } \tau_\eta = (\nu / \epsilon)^{1/2}$$

$$\text{velocity scale: } u_\eta = (\nu \epsilon)^{1/4}$$

Comparison with mean flow scales (U_0 and $r_{1/2}$)

$$\frac{\eta}{r_{1/2}} = \frac{(\nu^3/\epsilon)^{1/4}}{r_{1/2}} = Re_0^{-3/4} \epsilon^{1/4}$$

$$\frac{u_\eta}{r_{1/2} U_0} = Re_0^{-1/2} \epsilon^{1/2}$$

$$\frac{u_\eta}{U_0} = Re_0^{-1/4} \epsilon^{1/4}$$

$$Re_0 = \frac{U_0 r_{1/2}}{\nu}$$

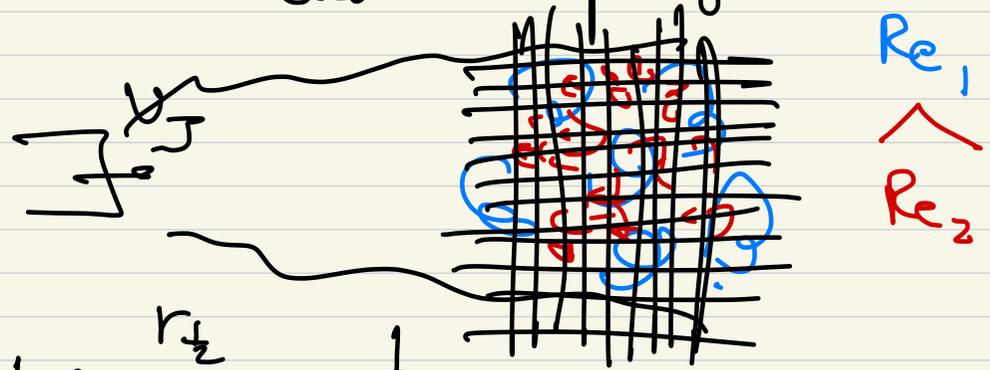
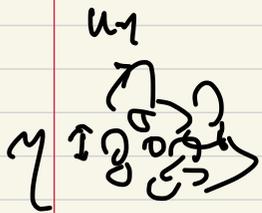
ϵ is non-dimensional and indep. of Re .

$$\eta \sim Re^{-3/4}$$

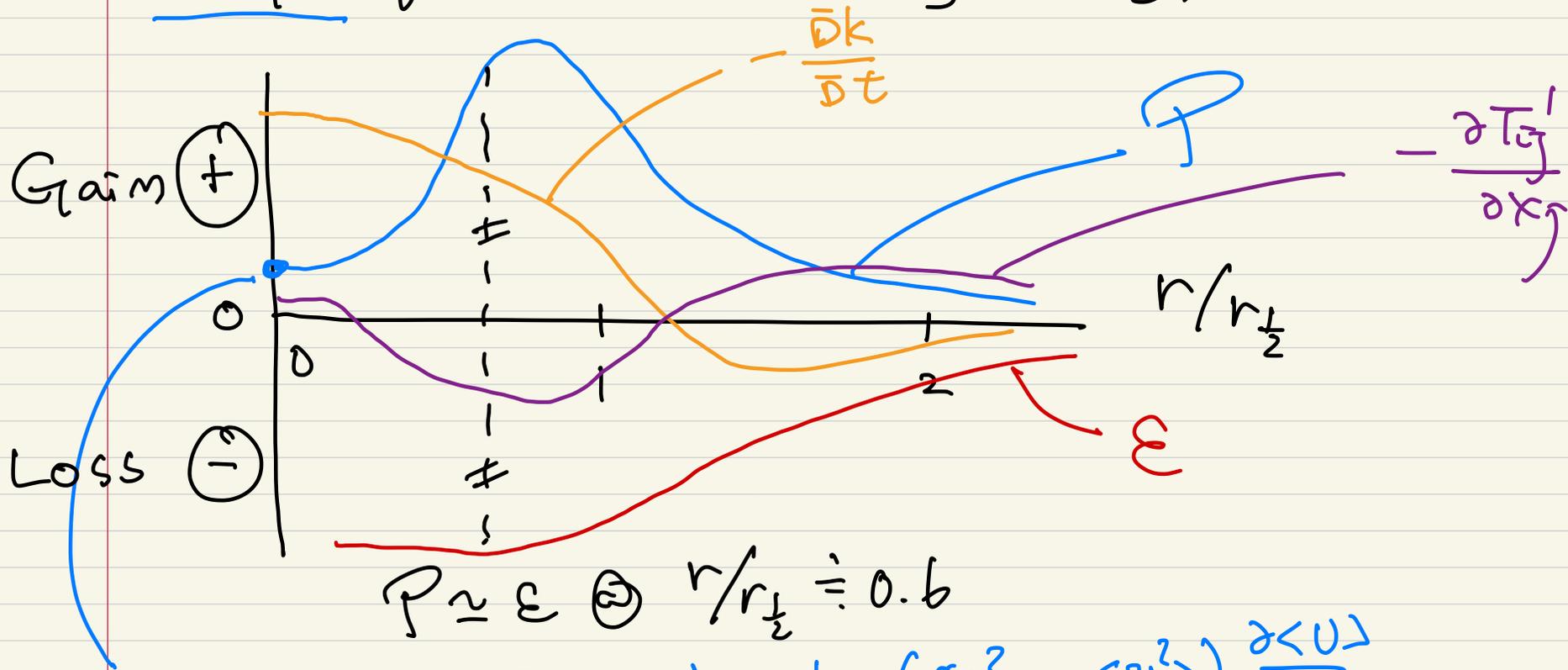
$$\Delta x \sim Re^{-3/4} \rightarrow N \sim \frac{r_{1/2}}{\Delta x} \sim \frac{1}{\Delta x}$$

$$N^3 \sim Re^{3/4} \quad (\text{DNS})$$

$\frac{\eta u_\eta}{\nu} = 1$: Reynolds number based on the Kolmogorov scales is unity \rightarrow motions on these scales are strongly affected by viscosity.



• Budget of k (normalized by $U_0^3 / r_{1/2}$)

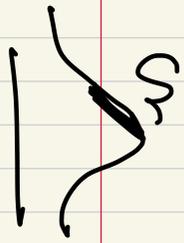


$P \approx \epsilon$ @ $r/r_{1/2} \doteq 0.6$

non-zero @ $r=0$ due to $(\langle u^2 \rangle - \langle v^2 \rangle) \frac{\partial \langle U \rangle}{\partial x}$.

- $\tau = \frac{k}{\epsilon}$: turbulence decaying time scale
or time to dissipate an amount of energy k
at constant rate ϵ .

- $\tau_p = \frac{k}{P}$: turbulence producing time scale
or time to produce k at the rate P



- $\tau \approx \tau_p \approx 3 S^{-1}$: three times the time scale
of the imposed shear S^{-1}
mean

→ turbulence is long-lived.

- Pseudo-dissipation $\tilde{\epsilon} = \nu \left\langle \frac{\partial u_i}{\partial x_j} \frac{\partial u_i}{\partial x_j} \right\rangle$

$$\epsilon = 2\nu \langle S_{ij} S_{ij} \rangle$$

$$\tilde{\epsilon} = \epsilon - \nu \frac{\partial^2}{\partial x_i \partial x_j} \langle u_i u_j \rangle$$

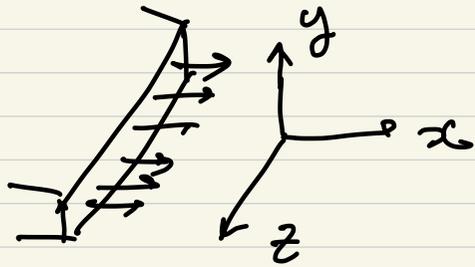
pseudo
-dissipation

true
dissipation

↑ quite small

5.4 Other self-similar flows

⊙ Plane jet



$U_0(x) = \langle U(x, y=0, z) \rangle$: centerline vel.

$y_{1/2}$: jet half width

$$\hookrightarrow \langle U(x, y=y_{1/2}, z) \rangle = \frac{1}{2} U_0(x)$$

mtm flux conservation & self similarity

$$\rightarrow \frac{dy_{1/2}}{dx} = f \approx 0.10 \rightarrow y_{1/2} \sim x$$

$$U_0(x) \sim x^{-\frac{1}{2}}$$

$$\hat{v}_T(\xi) = \frac{\nu_T}{U_0 y_{1/2}} \rightarrow \nu_T \sim x^{\frac{1}{2}} \quad \left(\xi = \frac{y}{y_{1/2}} \right)$$

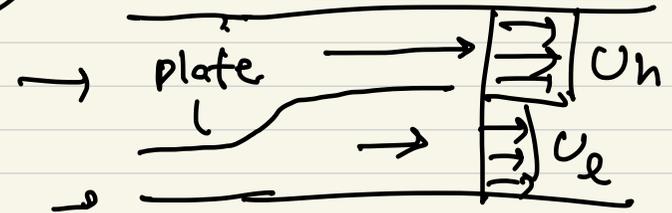
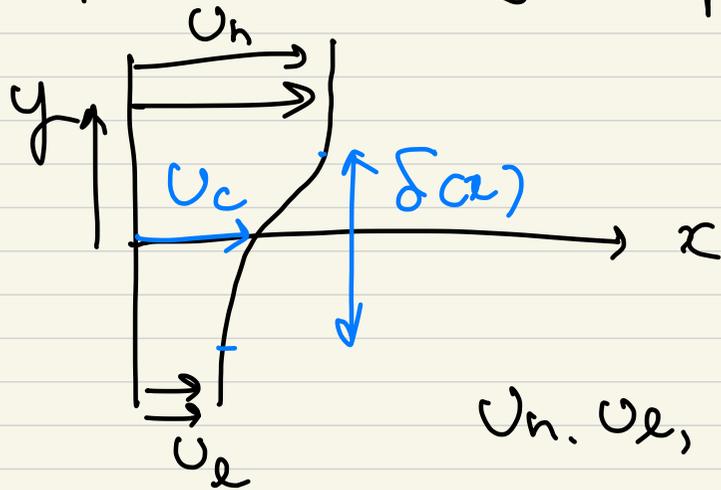
$$Re_0 = \frac{U_0(x) y_{1/2}(x)}{\nu_T} \sim x^{\frac{1}{2}} \quad (35 \text{ for round jet})$$

$$Re_T = \frac{U_0 y_{1/2}}{\nu_T} \text{ indep. of } x, \quad Re_T \approx 31$$

dry layer approx. & self-similarity

$$\rightarrow \bar{f}(\xi) = \frac{\langle U \rangle}{U_0} = \text{sech}^2(\alpha \xi)$$

Plane mixing layer



$$U_c = \frac{1}{2}(U_h + U_e) : \text{char. conv. vel.}$$

$$U_s = U_h - U_e : \text{ " vel. difference.}$$

U_h, U_e, U_c, U_s are indep. of x

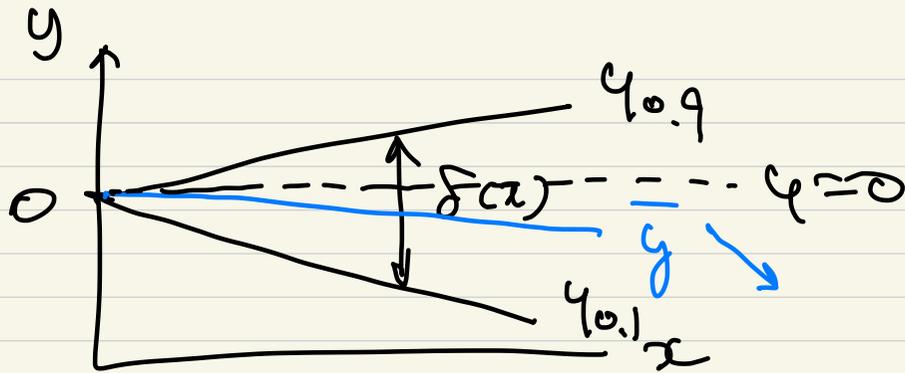
char. length $\delta(x)$?

$$y_\alpha : \langle U(x, y=y_\alpha(x), z) \rangle = U_e + \alpha(U_h - U_e)$$

$$\delta(x) \equiv y_{0.9}(x) - y_{0.1}(x)$$

$$\bar{y}(x) \equiv \frac{1}{2} [y_{0.9}(x) + y_{0.1}(x)]$$

$$\xi = \frac{y - \bar{y}(x)}{\delta(x)}, \quad f(\xi) = \frac{\langle U \rangle - U_c}{U_s}$$



$$\xi \rightarrow \infty, \langle U \rangle = U_h$$

$$f(\infty) = \frac{U_h - \frac{1}{2}(U_h + U_e)}{U_h - U_e} = \frac{1}{2}$$

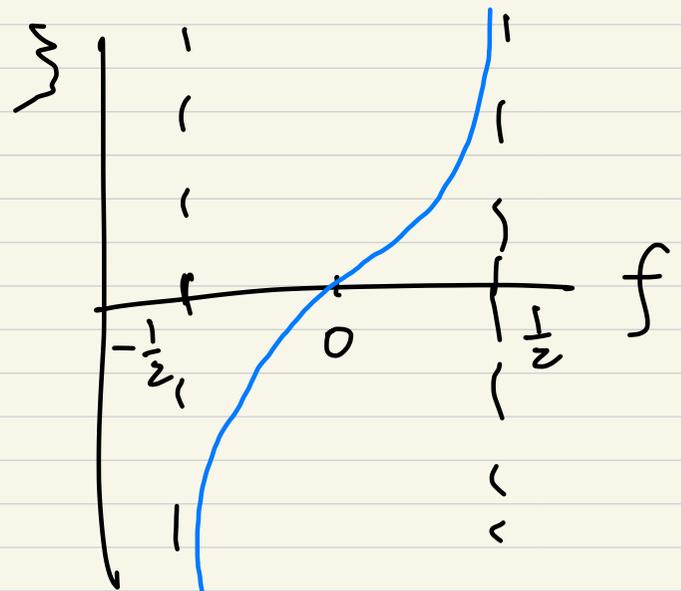
$$f(-\infty) = \frac{U_e - \text{"}}{\text{"}} = -\frac{1}{2}$$

$$\bar{y} = \frac{1}{2}(y_{0.9} + y_{0.1}) \rightarrow f(\bar{y}) = \frac{\langle U(\bar{y}) \rangle - \frac{1}{2}(U_h + U_e)}{U_h - U_e}$$

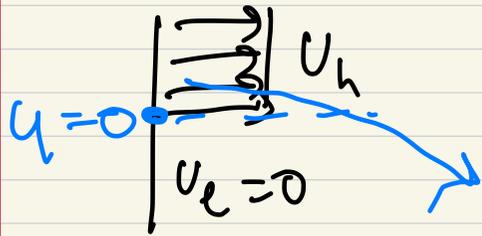
$$\langle U(\bar{y}) \rangle = \frac{1}{2} \left[\underline{U_e + 0.9(U_h - U_e)} + \underline{U_e + 0.1(U_h - U_e)} \right]$$

$$= \frac{1}{2}(U_h + U_e)$$

$$\rightarrow f(\bar{y}) = 0$$



* $U_e/U_h = 0$: exp. results confirm that the mixing layer is self-similar



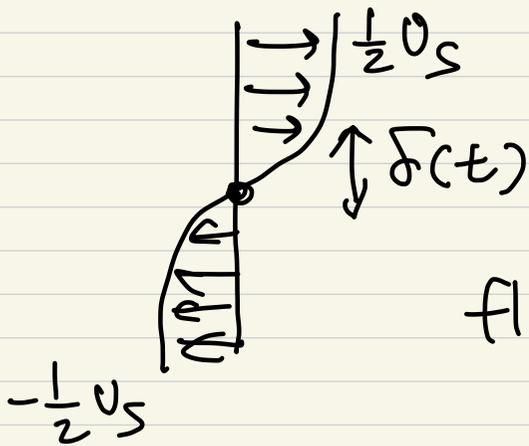
Flow is not symmetric about $y=0$ and spreads into the low-speed stream.

boundary layer eq. + self-similarity

→ $\delta \sim x$ (spreading rate)

$$S \equiv \frac{U_c}{U_s} \frac{d\delta}{dx} = \text{const} \quad (0.06 \sim 0.11)$$

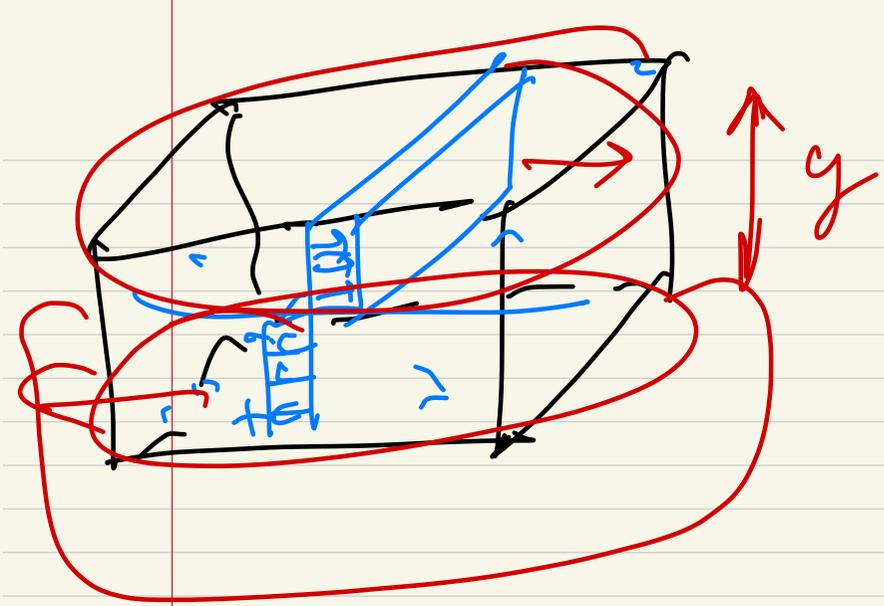
* To an observer travelling in x direction at U_c .



$$\frac{d\delta}{dt} = U_c \frac{d\delta}{dx} = S U_s = \text{const}$$

$$\rightarrow \delta \sim t$$

flow becomes statistically 1D (varying in y) and time-dependent



⇒ called 'temporal mixing layer'
 (as opposed to spatial mixing layer)

Flow is symmetric about $y=0$

Rogers & Moser (1994)

* Mixing layer

$$U_s = U_h - U_l = \text{const}, \quad \delta \sim x$$

$$Re_o = \frac{U_s \delta}{\nu} \sim x, \quad \nu_T = U_s \delta \sqrt{\nu_T} \sim x$$

$$Re_T = \frac{U_s \delta}{\nu_T} = \text{const}$$

Flow rate of k : $k(x) = \int_{-\infty}^{\infty} \langle U \rangle k dy \sim U_c U_s^2 \delta \sim x$

→ P should be bigger than ϵ .

cf. jet: $\int_0^{\infty} \langle U \rangle \cdot k \cdot 2\pi r dr \sim U_c^3 \delta^2 \sim x^{-1}$

wake: $k \sim x^{-1}$