

System Control

7. Control System Design by the Root-Locus Method

Professor Kyongsu Yi

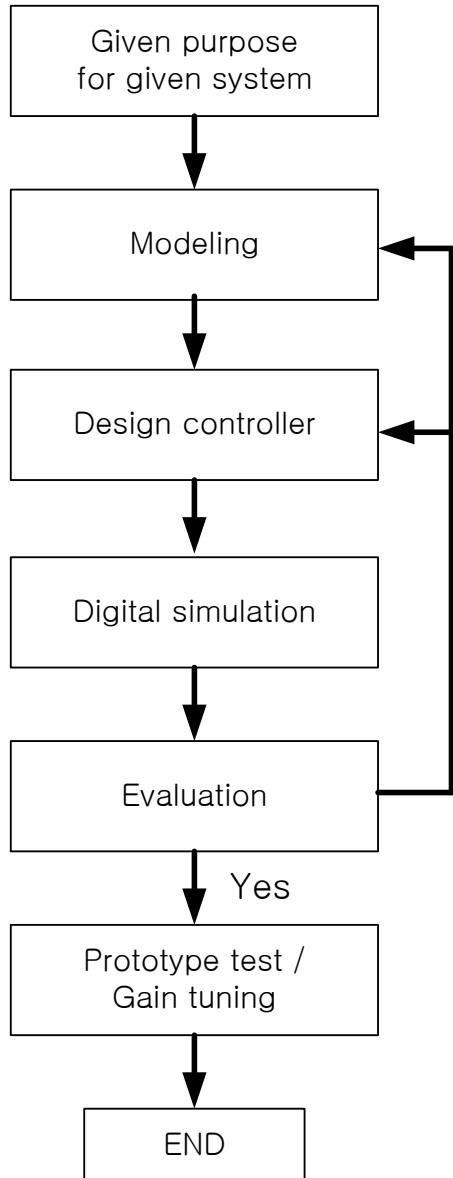
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Vehicle Dynamics and Control Laboratory
Seoul National University

Control system design

- Control System Design ; to perform specific tasks
- requirements ; performance specifications
 - accuracy (steady state error)
 - relative stability (ζ , damping ratio)
 - speed of response (T , $e^{-\zeta\omega_n t}$, ω_n : natural frequency)
- Given purpose → precise performance specifications
 - an optimal control system
- Controller ;
 - digital controller , in many cases
 - microprocessor based controller
 - software; control algorithm
 - hydraulic
 - pneumatic
 - electronic (analog)
 - mechanical

Design procedure



1) Build up → test

month to years

Suspension

- spring, damper
- tune the parameter
- test/evaluation (road tests)

2) Lab tests (simulator) week to months

3) Computer simulation (software) day to weeks
/ test 검증 (vehicle test/final tuning)

자동차 48개월 개발기간 ; 80년대 초반

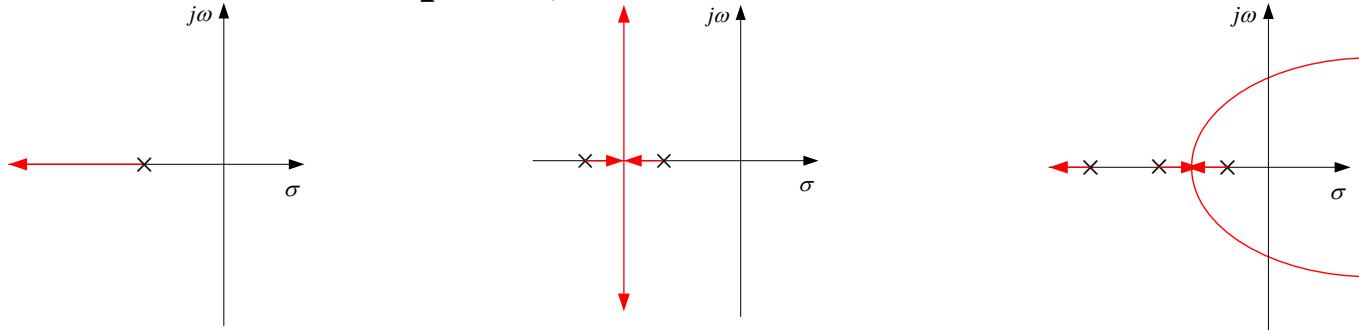
36개월 80년대 말

30개월 90년대 초반

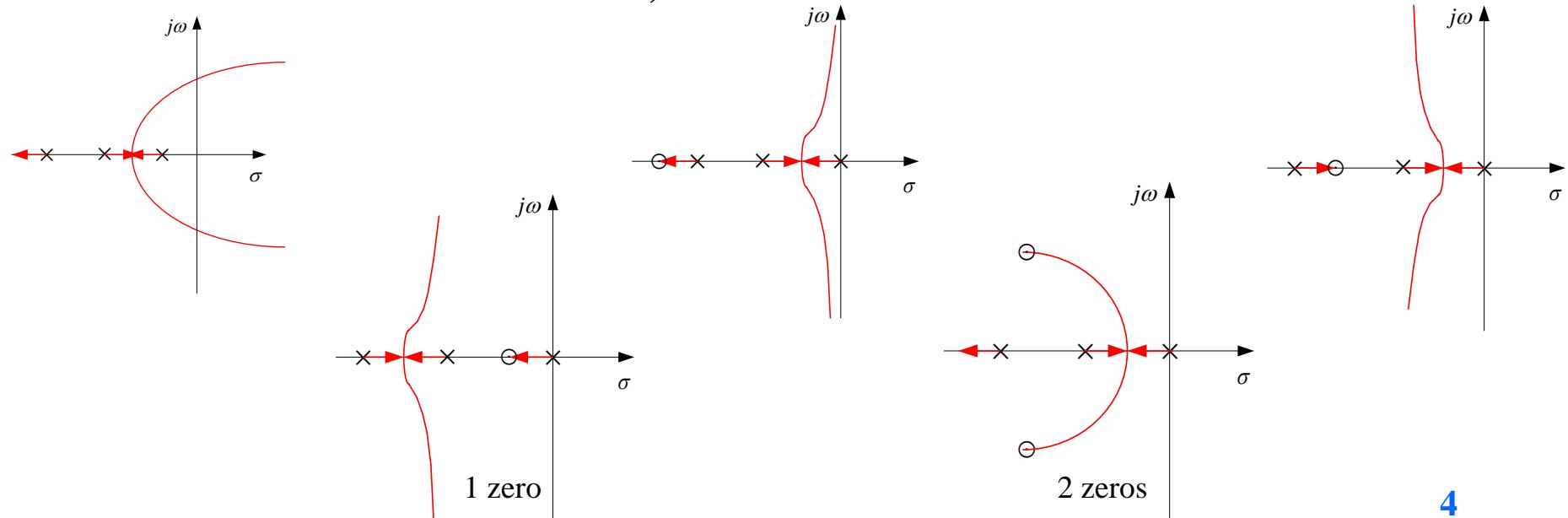
24개월 2000년대

Preliminary Design Considerations

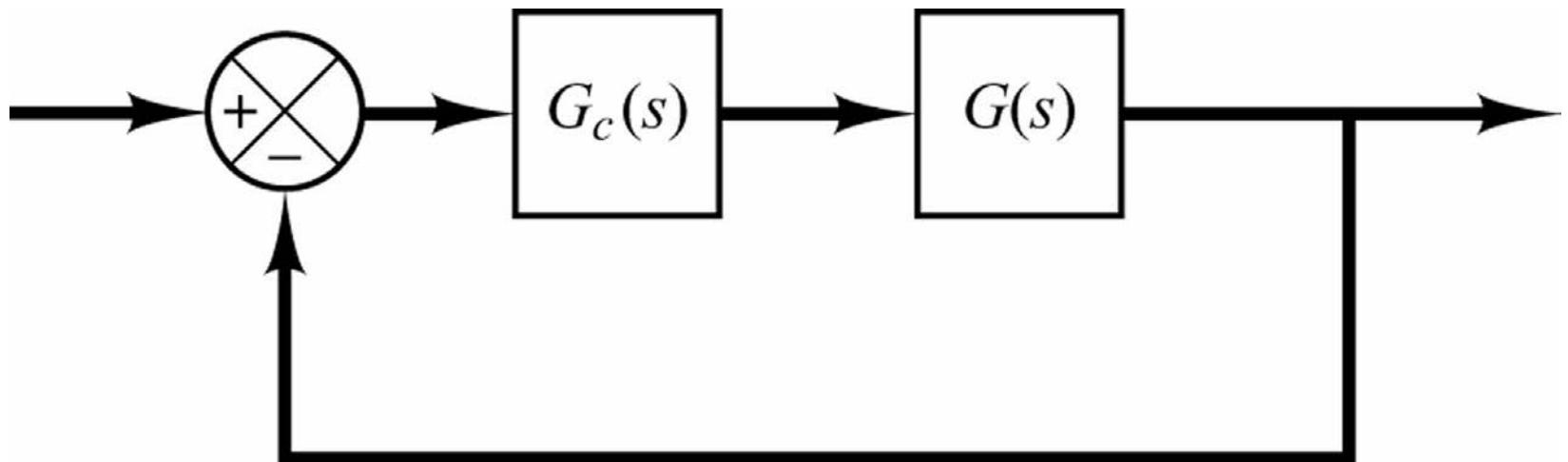
- Root – Locus approach ;
 - graphical method
 - gain or parameter variations
- Effect of the addition of poles ; **less stable**



- Effect of the addition of zeros ; **more stable**



Lead/Lag Compensation



$$G_c(s) = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}}$$

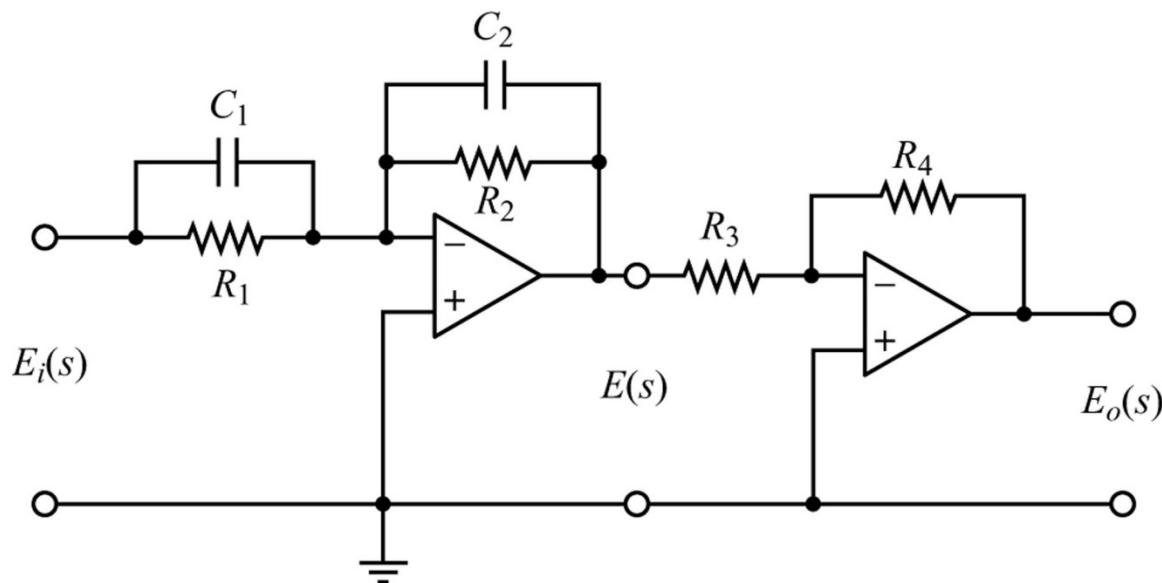
Lead/Lag Compensation

$$\frac{E_o(s)}{E_i(s)} = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}}$$

$$T = R_1 C_1$$

$$\alpha T = R_2 C_2$$

$$K_c = \frac{R_4 C_1}{R_3 C_2}$$



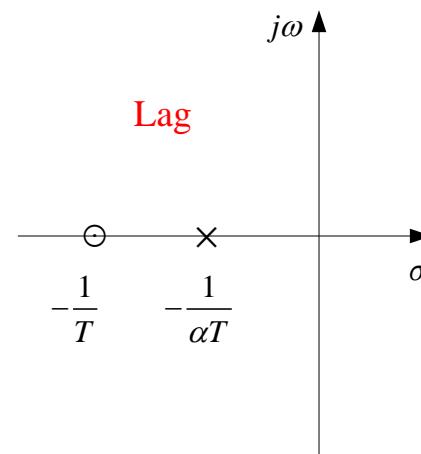
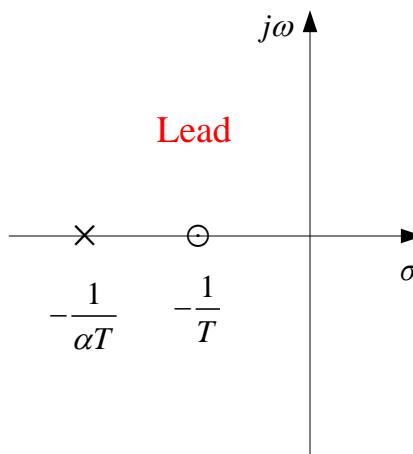
Lead/Lag Compensation

$$G_c(s) = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}}$$

When $s = j\omega$ $\angle G_c(j\omega) = \angle\left(j\omega + \frac{1}{T}\right) - \angle\left(j\omega + \frac{1}{\alpha T}\right)$

Lead Compensator \leftarrow $\frac{1}{T} < \frac{1}{\alpha T}$ $\angle G_c(j\omega) > 0$ $0 < \alpha < 1$

Lag Compensator \leftarrow $\frac{1}{T} > \frac{1}{\alpha T}$ $\angle G_c(j\omega) < 0$ $1 < \alpha$



Root Locus / Lead/Lag Compensator

- Root locus lead/lag compensator : powerful tool

when ; specification – time domain spec.

- • damping ratio
• natural frequency
• dominant closed loop poles
• rise time etc.

① Time domain spec

② unstable or
undesirable transient-response characteristics

→ Lead Compensators (relocate dominant closed loop poles)

Example

Ex.

$$G(s) = \frac{4}{s(s+2)}$$

$$\frac{C(s)}{R(s)} = \frac{4}{s^2 + 2s + 4} \quad , \text{closed loop poles : } s = -1 \pm \sqrt{3}j$$

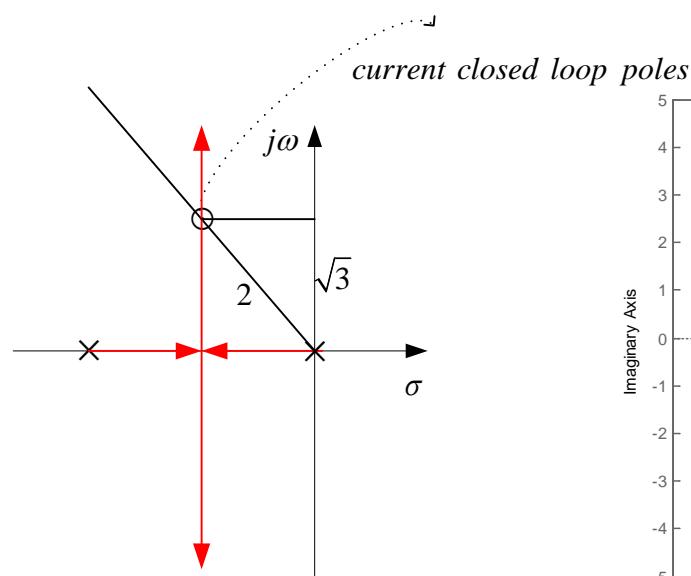
$$\begin{cases} \zeta = 0.5 \\ \omega_n = 2 \end{cases}$$

The static velocity error constant $K_v = 2$

$$E(s) = \frac{1}{1+G(s)} R(s)$$

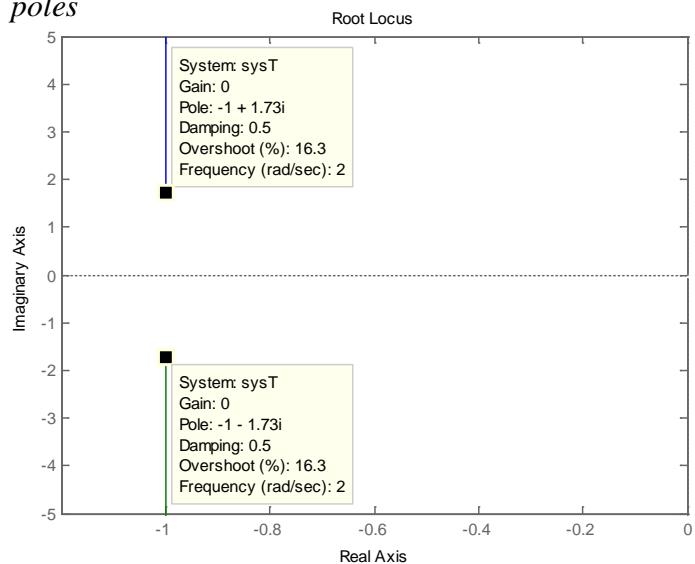
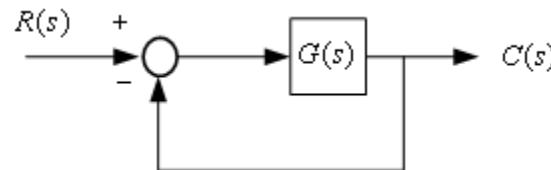
$$e_{ss}(t) = \lim_{s \rightarrow 0} s \frac{1}{1+G(s)} \frac{1}{s^2}$$

$$= \lim_{s \rightarrow 0} \frac{1}{sG(s)} = \frac{1}{K_v} = \frac{1}{2} = 0.5$$



Desired : $\omega_n = 4, \zeta = 0.5$

$$\Rightarrow s = -2 \pm 2\sqrt{3}j$$



Example

Desired : $\omega_n = 4, \zeta = 0.5$

$$\Rightarrow s = -2 \pm 2\sqrt{3}j$$

1) Angle of deficiency ϕ

$$\angle \left. \frac{4}{s(s+2)} \right|_{s=-2 \pm 2\sqrt{3}j} = -210^\circ$$

$$\phi = 30^\circ, \quad = \angle K \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}} = 30^\circ, \quad 0 < \alpha < 1$$

→ Lead Compensator

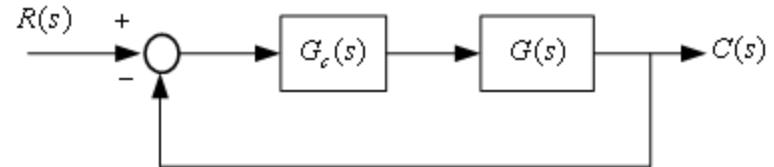
2) Choose $\frac{1}{T}, \frac{1}{\alpha T}$ **such that** $\angle \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}} = 30^\circ$

가능한한 α 가 크게 → K_v 증가 (Good)

Text 방법 → pole = -5.4 zero = -2.9 $\alpha = 0.536$

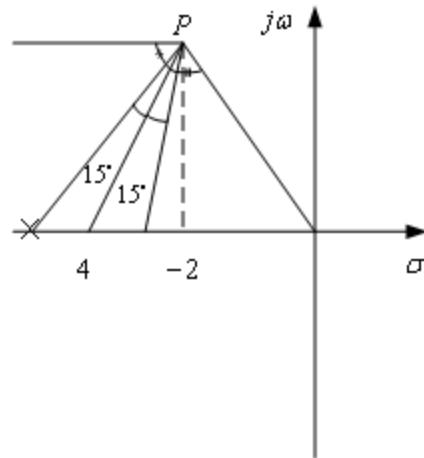
$$T = \frac{1}{2.9} = 0.345$$

$$\alpha T = \frac{1}{5.4} = 0.185$$



Example

Pole-zero location for large α



$$e_{ss} = \lim_{s \rightarrow 0} s \frac{1}{1 + G_c(s)G(s)} \frac{1}{s^2}$$

$$= \lim_{s \rightarrow 0} \frac{1}{s G_c(s) G(s)} = \frac{1}{K_v}$$

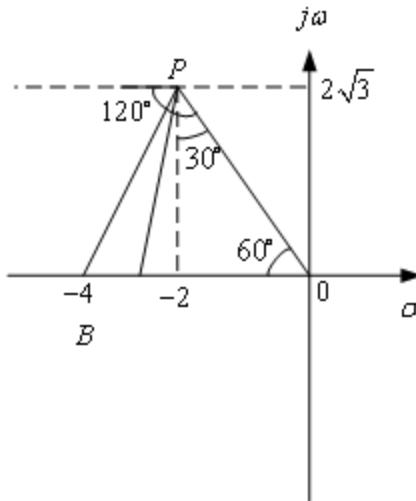
$$K_v = \lim_{s \rightarrow 0} s G_c(s) G(s)$$

$$= \lim_{s \rightarrow 0} K \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}} \frac{4}{s + 2}$$

$$= K \cdot \alpha \cdot 2$$

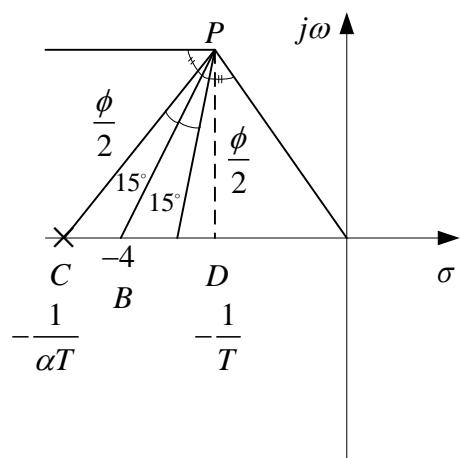
Example

Lead Compensator : pole-zero selection for large α



P : desired pole

$$-2 + 2\sqrt{3}j$$



C : pole : $-\frac{1}{\alpha T}$

D : zero : $-\frac{1}{T}$

Lead Compensator

Fig 7-9 Ogata

Example

3) Magnitude Condition

$$G_c(s)G(s) = K_c \frac{s+2.9}{s+5.4} \frac{4}{s(s+2)}$$

$$1 + G_c(s)G(s) \Big|_{s=-2+2\sqrt{3}j} = 0$$

$$|G_c(s)G(s)| = 1 = K_c \left| \frac{s+2.9}{s+5.4} \right| \left| \frac{4}{s(s+2)} \right|_{s=-2+2\sqrt{3}j}$$

→ $K_c = 4.68$

→ Lead Compensator

$$G_c(s) = 4.68 \frac{s+2.9}{s+5.4} = K_c \frac{\frac{s+2.9}{T}}{\frac{s+5.4}{\alpha T}} = K_c \alpha \frac{Ts+1}{\alpha Ts+1} = 2.51 \frac{0.345s+1}{0.185s+1}$$

Analog controller

$$\frac{E_o(s)}{E_i(s)} = \frac{R_2 R_4}{R_1 R_3} \frac{R_1 C_1 s + 1}{R_2 C_2 s + 1}$$

Arbitrarily chosen $\begin{cases} C_1 = C_2 = 10\mu F \\ R_3 = 10k\Omega \end{cases}$

Digital controller

$$\frac{u}{e} = G_c(s) = K_1 + \frac{a}{0.185s+1}$$

$$u = u_1 + u_2, \begin{cases} u_1 = K_1 e \\ 0.185\dot{u}_2 + u_2 = ae \\ \sim > u_2 \end{cases}$$

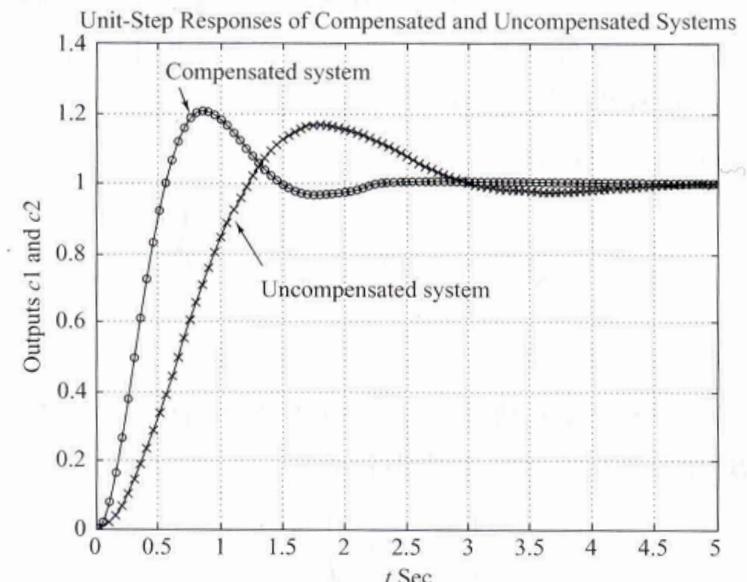
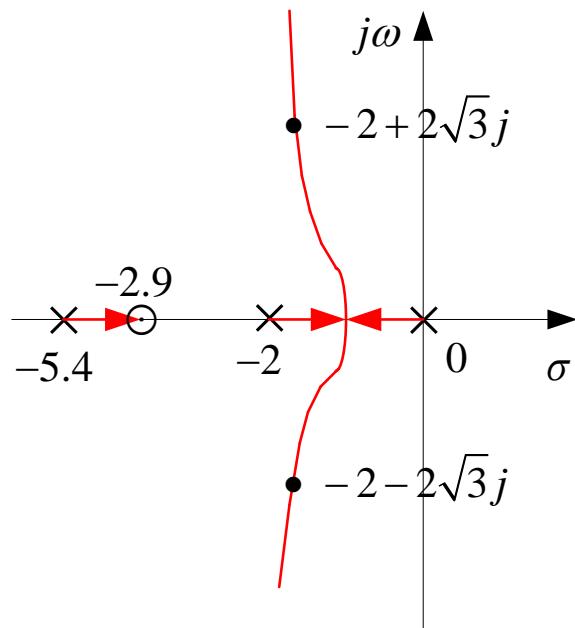


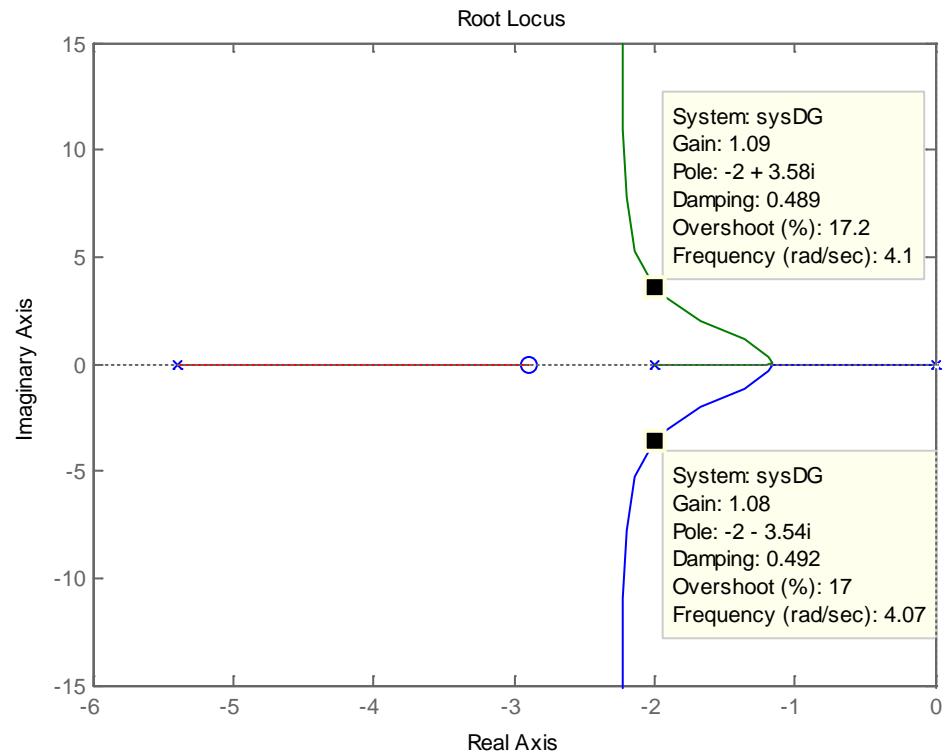
그림 7-11 보상된 시스템과 보상되지 않은 시스템의 단위계단응답

Example

Root locus of the compensated system



$$K_c \frac{s + 2.9}{s + 5.4} \frac{4}{s(s + 2)}$$



- Comparison of step responses
 - original system
 - compensated system

Example

Root locus of the compensated system

$$K_c \frac{s + 2.9}{s + 5.4} \frac{4}{s(s + 2)}$$

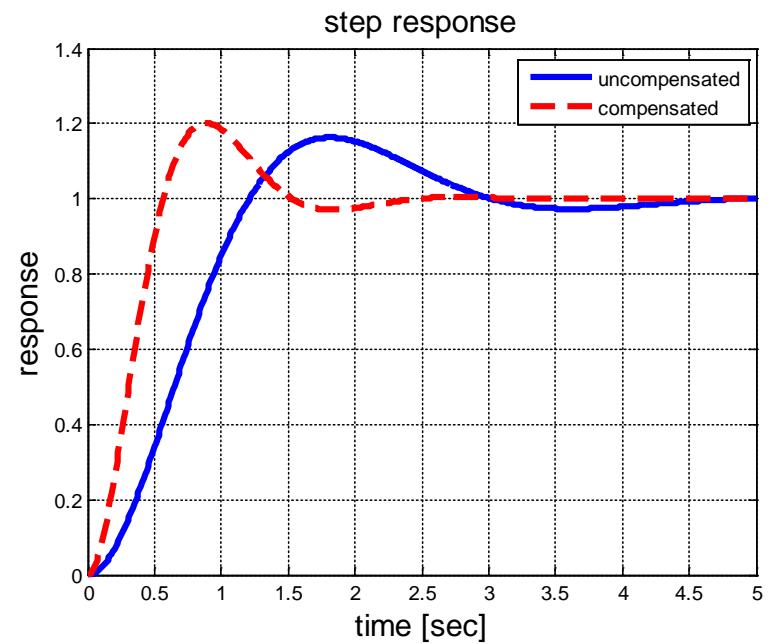
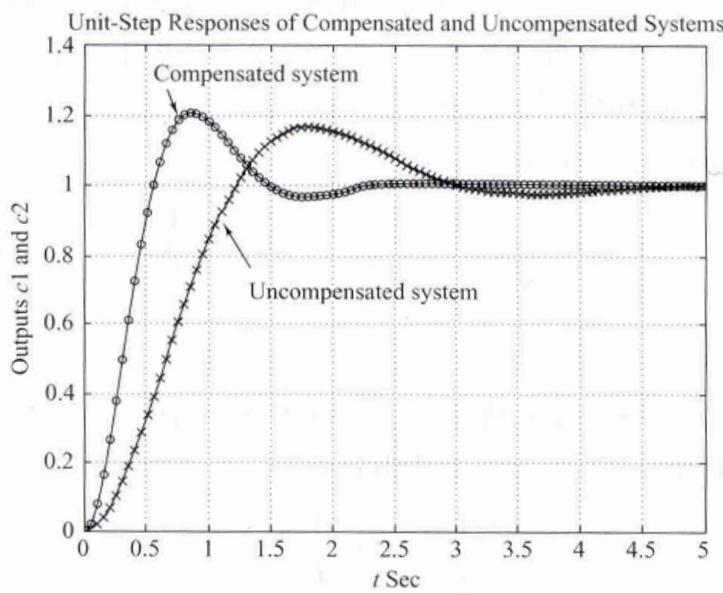


그림 7-11 보상된 시스템과 보상되지 않은 시스템의 단위계단응답

Example

4) Static velocity error constant ;

→ 가능한한 큰 α 가 K_v 증가에 기여 , K_v 가 lead Compensator로 충분히 증가하지 못한 경우 Lag compensator 추가 → Lead-Lag Compensator

$$\begin{aligned} e_{ss}(t) &= \lim_{s \rightarrow 0} s \frac{1}{1 + G_c(s)G(s)} R(s) = \lim_{s \rightarrow 0} s \frac{1}{1 + G_c(s)G(s)} \frac{1}{s^2} = \lim_{s \rightarrow 0} \frac{1}{sG_c(s)G(s)} = \frac{1}{s \cdot 2.51 \left(\frac{0.345s+1}{0.185s+1} \right) \frac{4}{s(s+2)}} \\ &= \frac{1}{2.52 \times 2} = 0.1984 \end{aligned}$$

$$K_v = 5.04 \text{ (old } K_v = 2\text{)}$$

The Procedure for design a Lead compensator

1) Performance Spec.

→ desired locations for the dominant closed-loop poles

2) Draw the root locus

(1) Check whether or not the gain adjustment alone → satisfactory results

(2) If not calculate the angle deficiency ϕ

$$3) \quad G_c(s) = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\alpha T}} = K_c \alpha \frac{Ts + 1}{\alpha Ts + 1}$$

dc gain ; $K_c \alpha$

α, T ; compensate angle deficiency

4) Tune α, T to locate the closed – loop poles at the desired locations

$-\alpha$; as large as possible

5) Tune K_c from the magnitude condition

Lag Compensation

$$G_c(s) = \hat{K}_c \frac{s + \frac{1}{T}}{s + \frac{1}{\beta T}}, \beta > 1$$

- ① satisfactory transient response
 - ② unsatisfactory steady state characteristics
 - i) closed loop poles : no change
 $\beta > 1$
 - ii) open loop gain increase
- Lag compensator

Procedure

1) Draw the root-locus plot for the uncompensated system

→ locate the dominant closed loop poles

2)

$$G_c(s) = K_c \frac{s + \frac{1}{T}}{s + \frac{1}{\beta T}}$$

calculate $\angle G_c(s)$

3) Evaluate the particular static error constant specified ;

The static velocity error constant

4) Determine pole and zero of the lag compensator s.t.

- ① the static error constant is sufficiently large
- ② without altering the original root loci.

5) Draw a new root-locus plot

6) Adjust \hat{K}_c from the magnitude condition

$$\left| \frac{s + \frac{1}{T}}{s + \frac{1}{\beta T}} \right| \approx 1$$

Angle $\angle G_c(s) \leq 50^\circ$
pole, zero close together and near the origin of the s-plane

Lag Compensation

The static velocity gain ;

Uncompensated system $K_v = \lim_{s \rightarrow 0} sG(s)$

Compensated system $\hat{K}_v = \lim_{s \rightarrow 0} sG_c(s)G(s) = \lim_{s \rightarrow 0} G_c(s)K_v = \underbrace{\hat{K}_c \cdot \beta}_{\beta = \text{factor}} \cdot K_v$

$\hat{K}_c \approx 1$

Increased by a factor of $\hat{K}_c \cdot \beta$

Example

Ex.

$$G(s) = \frac{1.06}{s(s+1)(s+2)}$$

$$\frac{C(s)}{R(s)} = \frac{1.06}{s(s+1)(s+2) + 1.06}$$

The dominant closed-loop poles ; $s = -0.3307 \pm 0.5864j$

$$\zeta = 0.491$$

$$\omega_n = 0.673 \text{ rad/sec}$$

$$K_v = 0.53 \text{ sec}^{-1}$$

Increase $K_v \rightarrow 5 \text{ sec}^{-1}$ without change of the location of dominant poles \rightarrow Lag compensator

1)

$$G_c(s) = \hat{K}_c \frac{s + \frac{1}{T}}{s + \frac{1}{\beta T}} \quad \hat{K}_v = \hat{K}_c \beta K_v$$

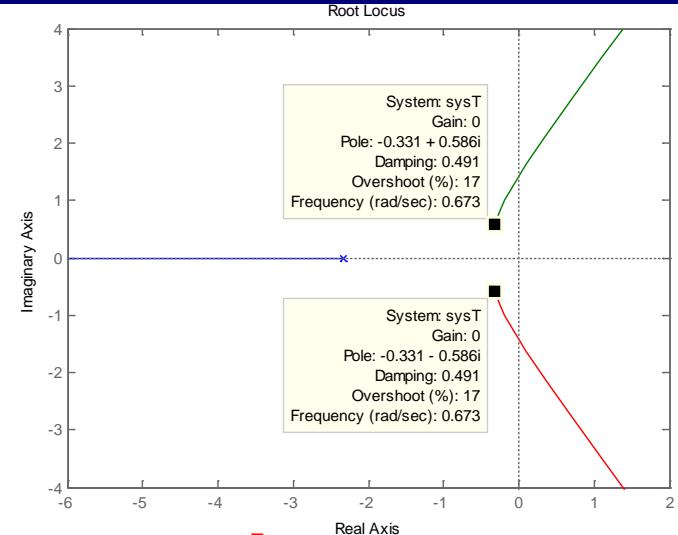
2) Let $\beta = 10, \frac{1}{T} = 0.05, \frac{1}{\beta T} = 0.005$

$$G_c(s) = \hat{K}_c \frac{s + 0.05}{s + 0.005}$$

Angle contribution near a dominant closed loop poles

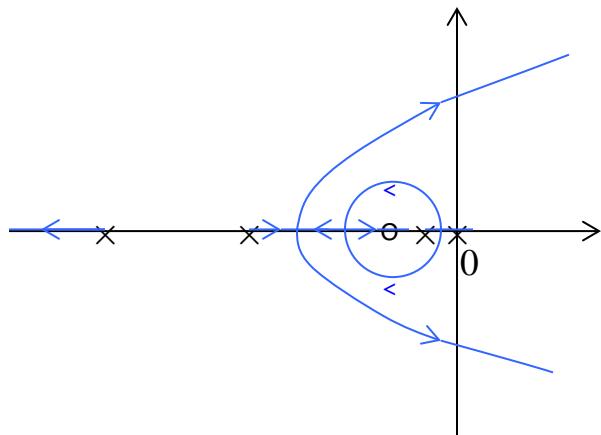
$$\angle \hat{K}_c \frac{s + 0.05}{s + 0.005} \Big|_{s=-0.3307 \pm j0.5864} \simeq 4^\circ$$

\rightarrow No significant change



Example

$$3) G_c(s)G(s) = \hat{K}_c \frac{s+0.05}{s+0.005} \cdot \frac{1.06}{s(s+1)(s+2)}$$

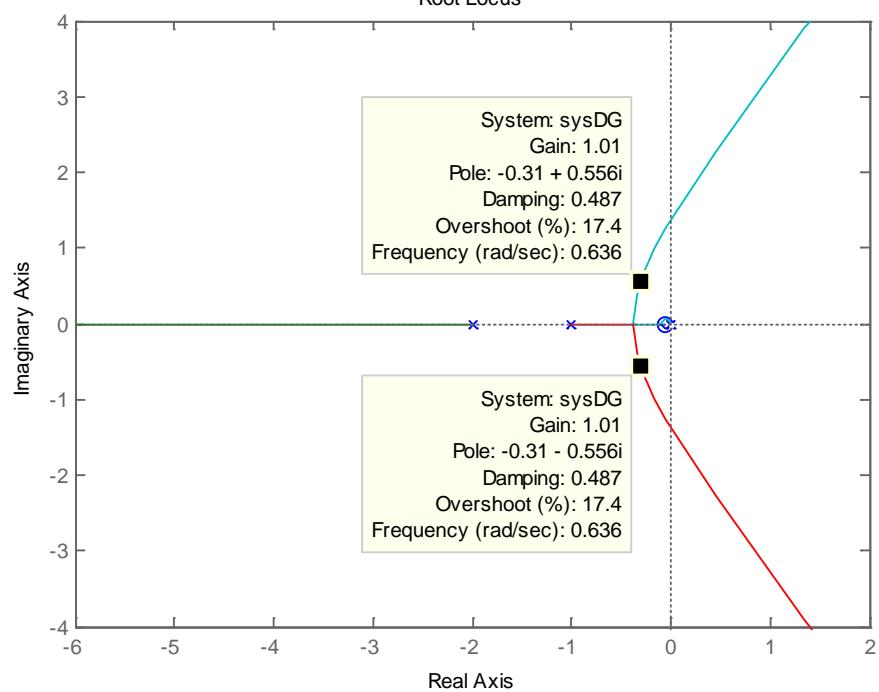
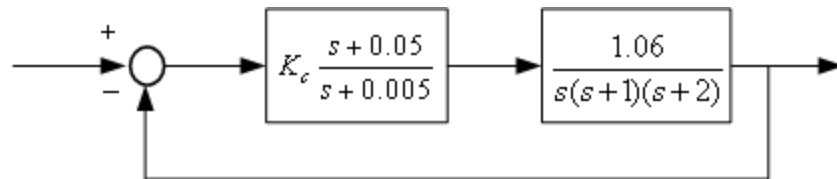


- dominant closed loop poles same damping ratio
→ $s = -0.31 \pm j0.55$

4) Magnitude condition

$$\left| \hat{K}_c \frac{s+0.05}{s+0.005} \cdot \frac{1.06}{s(s+1)(s+2)} \right|_{s=-0.31 \pm j0.55} = 1$$

$$\Rightarrow \hat{K}_c = 0.9656$$



Example

Verification ;

$$\begin{aligned}\frac{1}{\hat{K}_v} &= \lim_{s \rightarrow 0} s \frac{1}{1 + G_c(s)G(s)} \frac{1}{s^2} \\ \hat{K}_v &= \lim_{s \rightarrow 0} s G_c(s)G(s) \\ &= 0.9656 \cdot \frac{s + 0.05}{s + 0.005} \frac{1.06}{(s+1)(s+2)} \\ &= 5.12 \text{ sec}^{-1} \approx \beta K_{v,old}\end{aligned}$$

5) $s_3 = -2.326$ $s_4 = -0.0549$

A long tail of small amplitude

Example

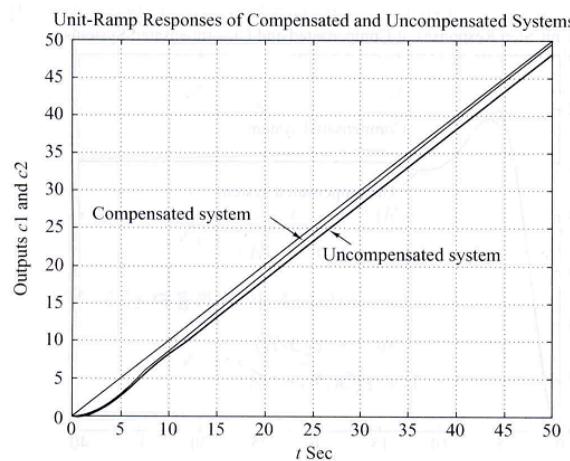


그림 7-16 보상된 시스템과 보상되지 않은 시스템의 단위램프응답 [보상기는 식 (7-3)으로 주어짐]

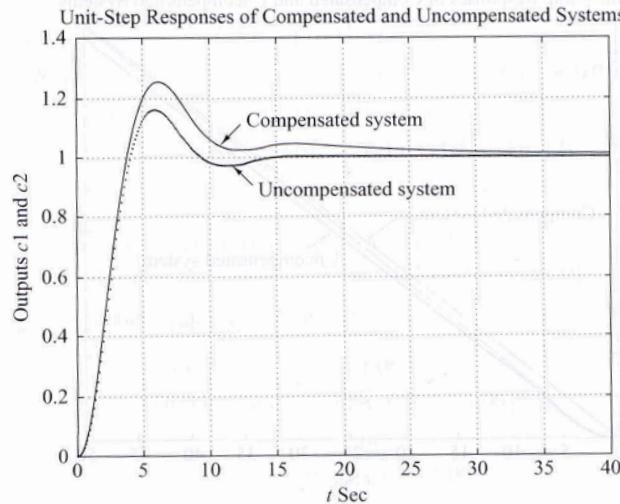
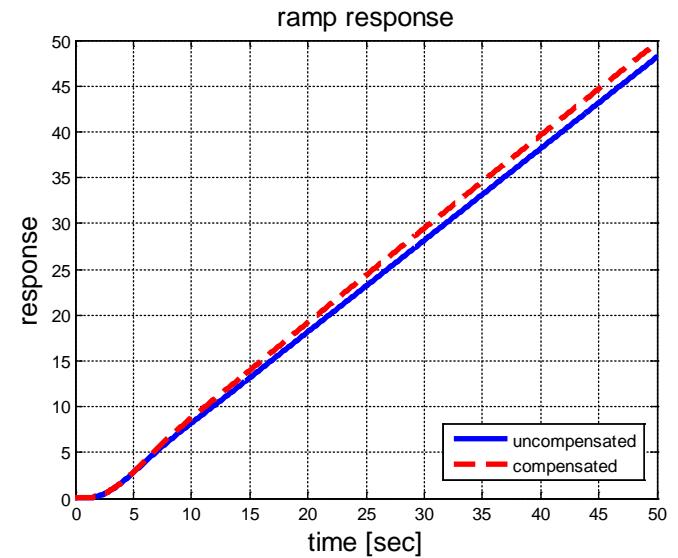
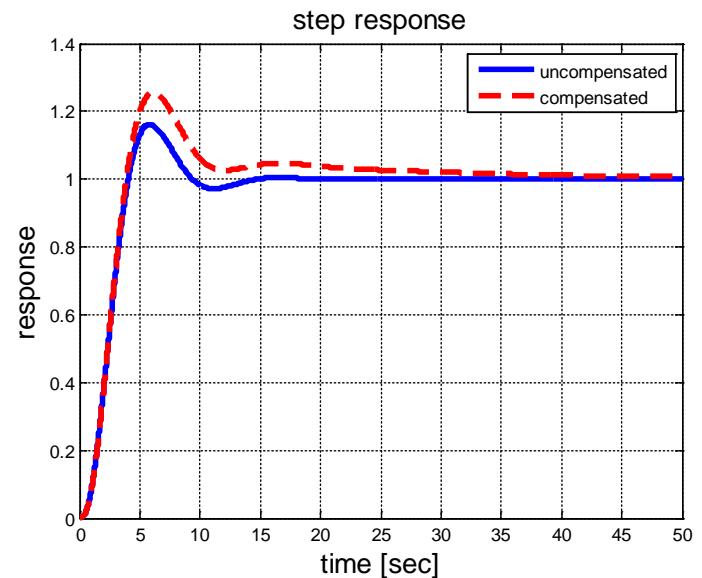


그림 7-17 보상된 시스템과 보상되지 않은 시스템에 대한 단위계단응답 [보상기는 식 (7-3)으로 주어짐]



Lag-Lead Compensation

Lead compensator → speeds up, increase the stability

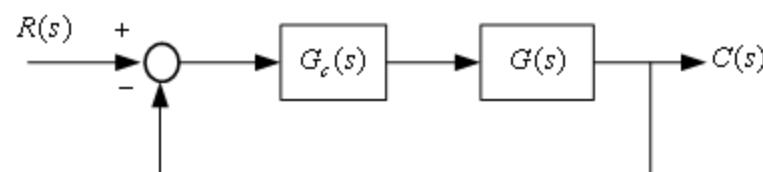
Lag compensator → improves the steady state accuracy but reduce the speed

→ Lag-Lead compensators

Design procedure

- 1) Design lead compensator to relocate the dominant poles
- 2) Design lag compensator to improve the s.s. gain

$$G_c(s) = K_c \underbrace{\left(\frac{s + \frac{1}{T_1}}{s + \frac{\gamma}{T_1}} \right)}_{\substack{\text{Lead} \\ \gamma > 1}} \underbrace{\left(\frac{s + \frac{1}{T_2}}{s + \frac{1}{\beta T_2}} \right)}_{\substack{\text{Lag} \\ \beta > 1}}$$



Lag-Lead Compensation

Spec. 1) dominant poles

2) K_v (steady state velocity error constant)

Step 1. Lead Compensator

1) choose desired poles s_1

2) angle condition

$$\angle K_c \left(\frac{s + \frac{1}{T_1}}{s + \frac{\gamma}{T_1}} \right) (G(s_1)) \Bigg|_{s=s_1} = 180^\circ (2k+1)$$

→ determine the angle deficiency ϕ

$$\angle \left(\frac{s + \frac{1}{T_1}}{s + \frac{\gamma}{T_1}} \right) = \phi = 180^\circ (2k+1) - \angle G(s_1) \quad (\text{infinitely many } \gamma, T) ; \text{choose one}$$

3) magnitude condition

$$\left| K_c \frac{s + \frac{1}{T_1}}{s + \frac{\gamma}{T_1}} G(s_1) \right| = 1$$

→ K_c

Lag-Lead Compensation

Step 2. Lag Compensator, K_v spec

$$1) K_v = \lim_{s \rightarrow 0} sG_c(s)G(s) = \lim_{s \rightarrow 0} sK_c \left(\frac{s + \frac{1}{T_1}}{s + \frac{\gamma}{T_1}} \right) \left(\frac{s + \frac{1}{T_2}}{s + \frac{1}{\beta T_2}} \right) G(s) = \lim_{s \rightarrow 0} sK_c \frac{\beta}{\gamma} G(s)$$

$\Rightarrow \beta$

2) choose T_2 such that

i)
$$\left| \frac{s + \frac{1}{T_2}}{s + \frac{1}{\beta T_2}} \right| \doteq 1$$

ii)
$$-5^\circ < \angle \underbrace{\frac{s + \frac{1}{T_2}}{s + \frac{1}{\beta T_2}}}_{< 0^\circ}$$

Example

Ex

$$G(s) = \frac{4}{s(s+0.5)}$$

The closed-loop poles ;

$$s = -0.25 \pm 1.9843j$$

$$\zeta = 0.125$$

$$\omega_n = 2 \text{ rad/sec}$$

$$K_v = 8 \text{ sec}^{-1}$$

Desired spec :

$$\begin{cases} \zeta = 0.5 \\ \omega_n = 5 \\ K_v = 80 \end{cases}$$

→ Lead – Lag compensator

$$G_c(s) = K_c \left(\frac{s + \frac{1}{T_1}}{s + \frac{\gamma}{T_1}} \right) \left(\frac{s + \frac{1}{T_2}}{s + \frac{1}{\beta T_2}} \right), \quad \gamma > 1, \quad \beta > 1$$

Example

Step 1. Lead Compensator

1) choose desired poles $s_1 = -2.50 \pm j4.33$

2) angle condition

$$\angle \frac{4}{s(s+0.5)} \Big|_{s=s_1} = -235^\circ$$

→ the angle deficiency = 55° $\angle G_c(s) + \angle G(s) = -180^\circ(2k+1)$

choose T_1 , such that pole-zero cancellation happens

$$\text{let } s + \frac{1}{T_1} = s + 0.5 \Rightarrow T_1 = 2$$

→ angle condition

$$\gamma = 10.04$$

$$\angle(s_1 + 0.5) + \angle(s_1 + \gamma 0.5) = 55^\circ$$

3) magnitude condition

$$\left| K_c \frac{s+0.5}{s+5.021} \frac{4}{s(s+0.5)} \right|_{s=s_1} = 1$$

$$\Rightarrow K_c = 6.26$$

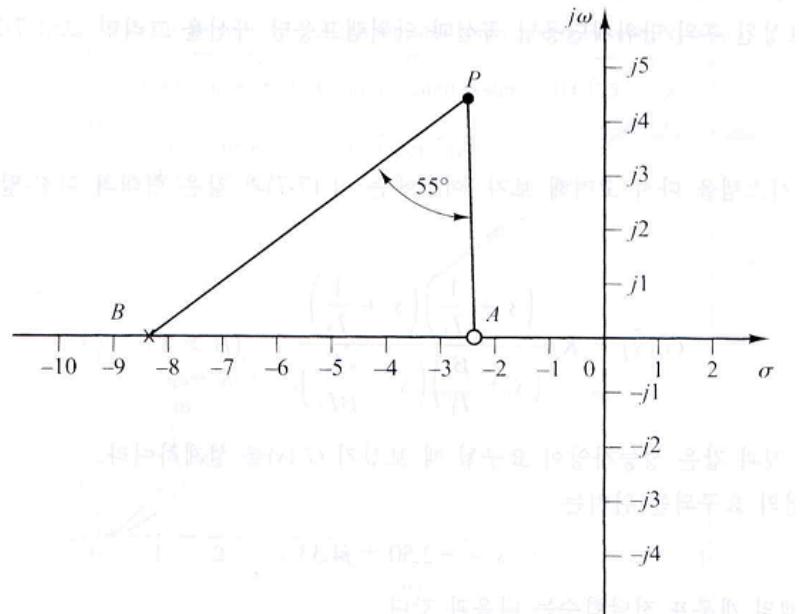


그림 7-23 요구되는 극점-영점 위치의 결정

Example

Step 2. Lag Compensator

$$\begin{aligned}
 1) \quad K_v &= \lim_{s \rightarrow 0} sG_c(s)G(s) = \lim_{s \rightarrow 0} sK_c \frac{\beta}{\gamma} G(s) \\
 &= \lim_{s \rightarrow 0} s(6.26) \frac{\beta}{10.04} \frac{4}{s(s+0.5)} = 4.988\beta = 80 \\
 \Rightarrow \beta &= 16.04
 \end{aligned}$$

2) choose T_2 such that

$$\text{i) } \left| \frac{s + \frac{1}{T_2}}{s + \frac{1}{\beta T_2}} \right|_{s=s_1} \doteq 1$$

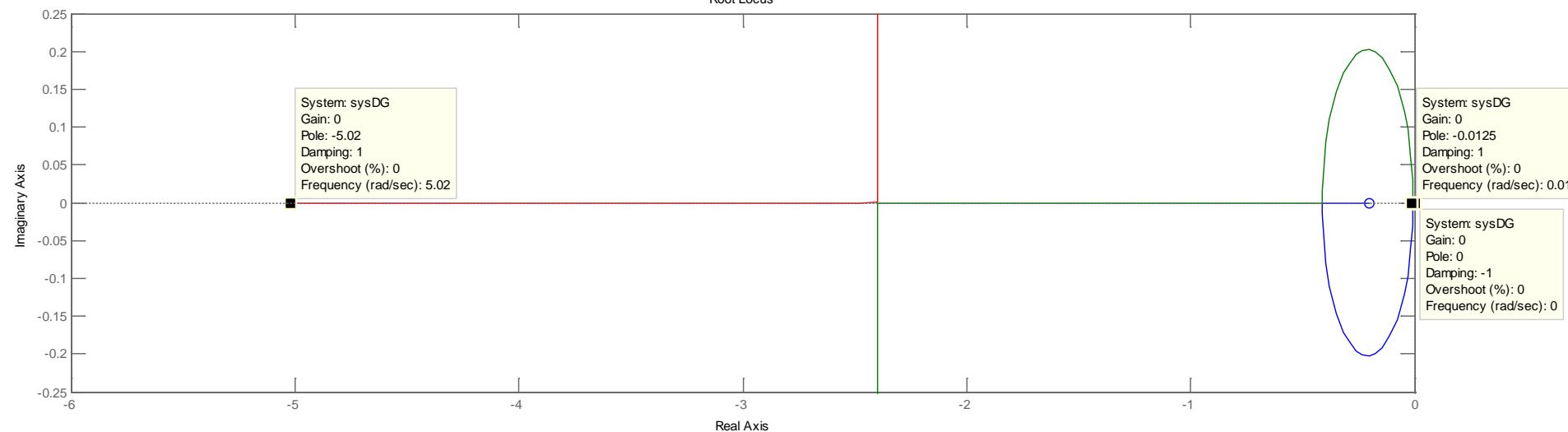
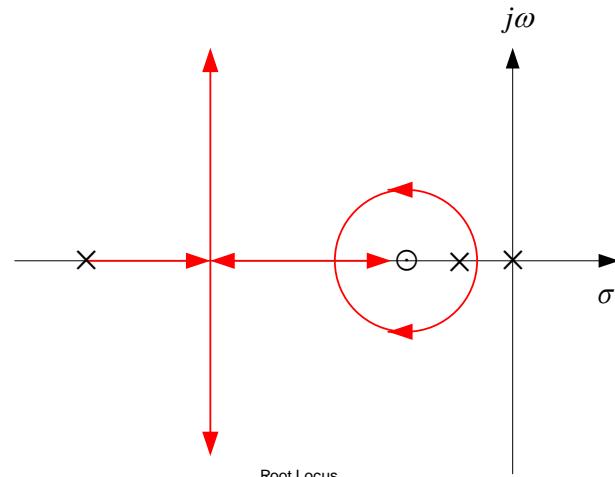
$$\text{ii) } -5^\circ < \angle \frac{s + \frac{1}{T_2}}{s + \frac{1}{\beta T_2}} < 0$$

$$\Rightarrow T_2 \geq 5 \Rightarrow \text{let } T_2 = 5$$

$$\begin{aligned}
 G_c(s) &= 6.26 \left(\frac{s + \frac{1}{2}}{s + \frac{10.04}{2}} \right) \left(\frac{s + \frac{1}{5}}{s + \frac{1}{16.04 \times 5}} \right) \\
 G_c(s)G(s) &= \frac{25.04(s+0.2)}{s(s+5.02)(s+0.01247)}
 \end{aligned}$$

Example

Root locus of the compensated system



Example

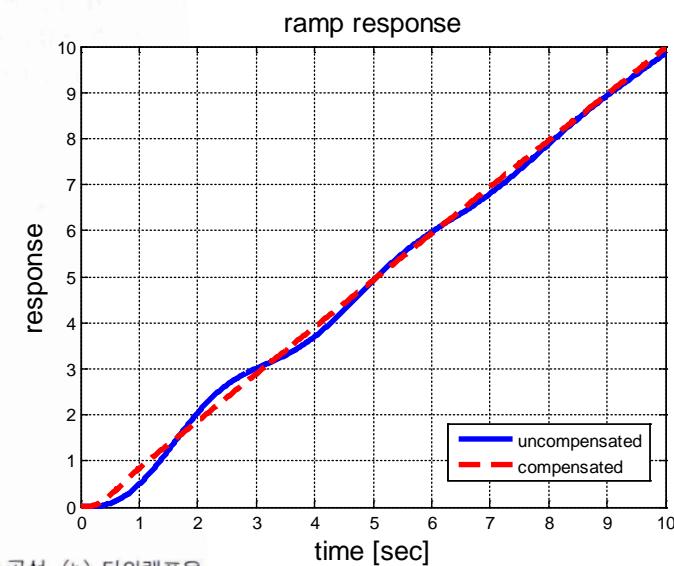
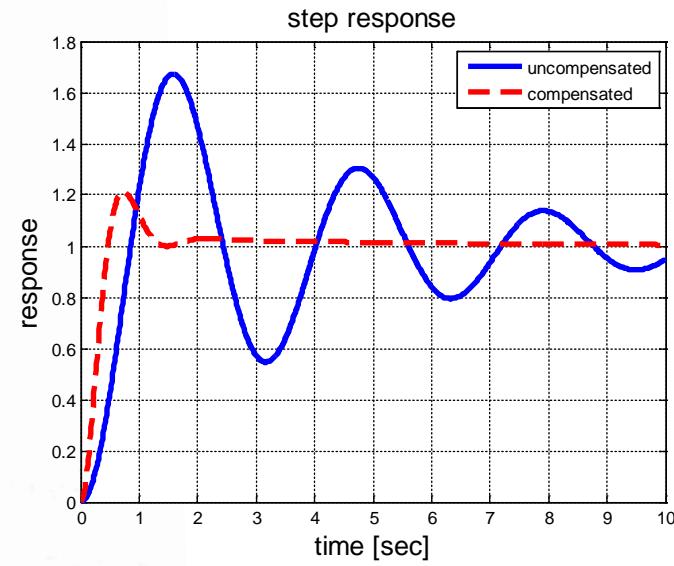
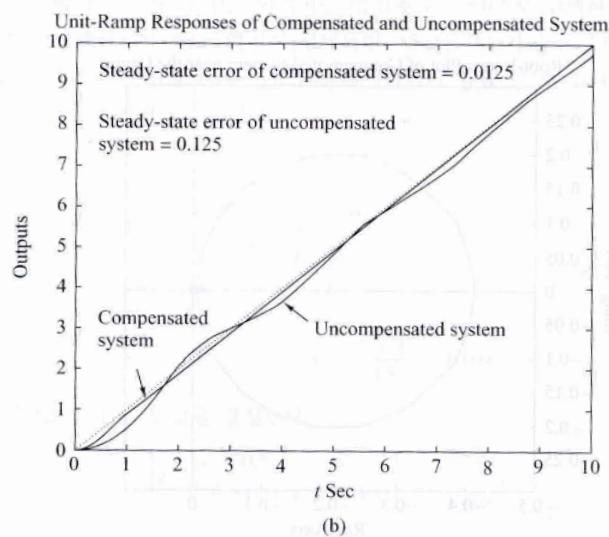
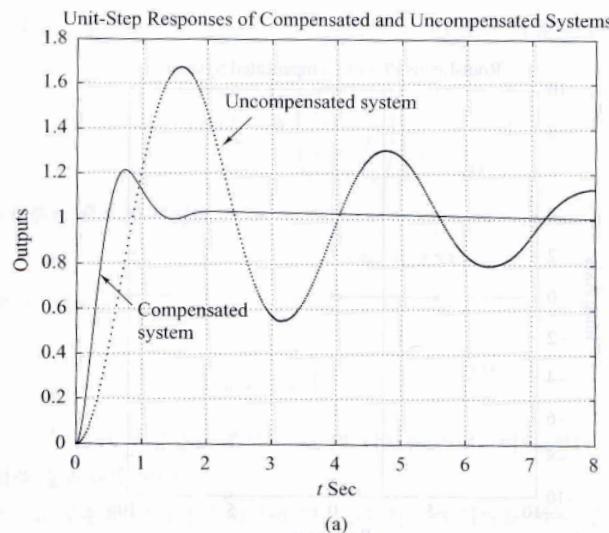


그림 7-22 보상된 시스템과 보상되지 않은 시스템의 과도응답 곡선: (a) 단위계단응답 곡선, (b) 단위램프응답 곡선.

End of lecture note 7