

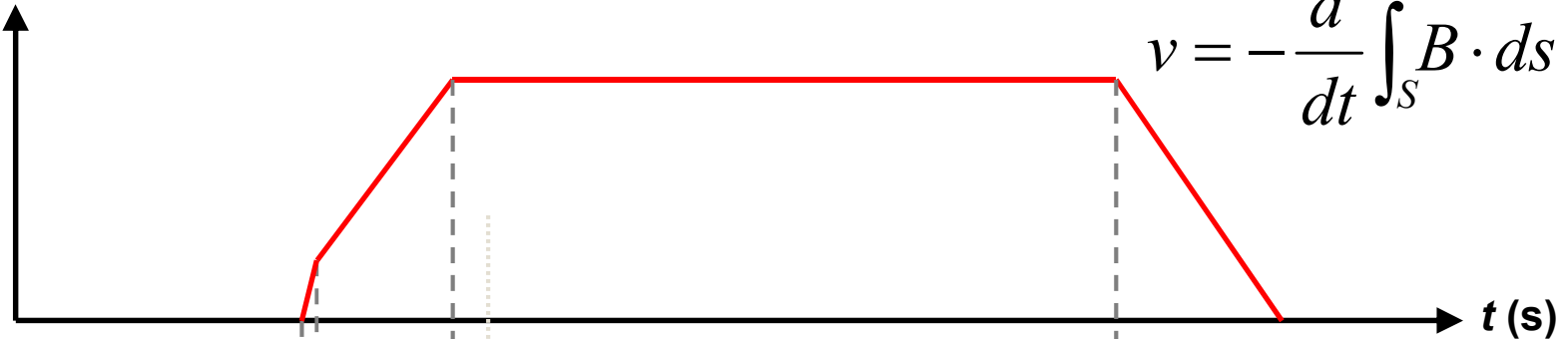
# **Fusion Reactor Technology I**

**(459.760, 3 Credits)**

**Prof. Dr. Yong-Su Na**  
(32-206, Tel. 880-7204)

# Pulsed Operation

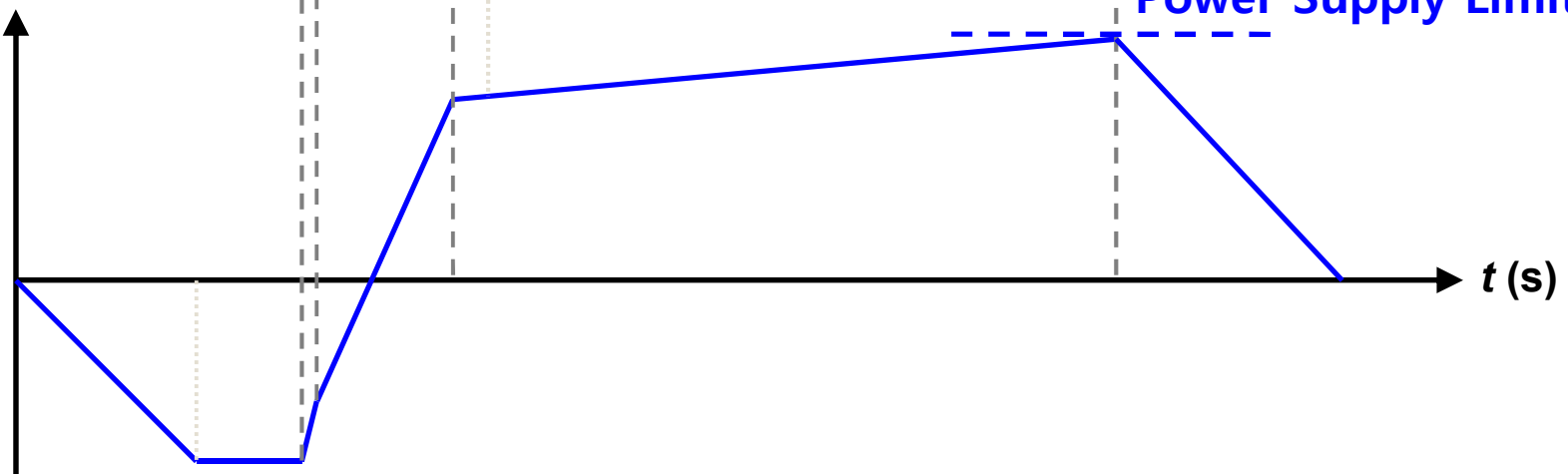
Plasma Current  
(MA)



Faraday's law

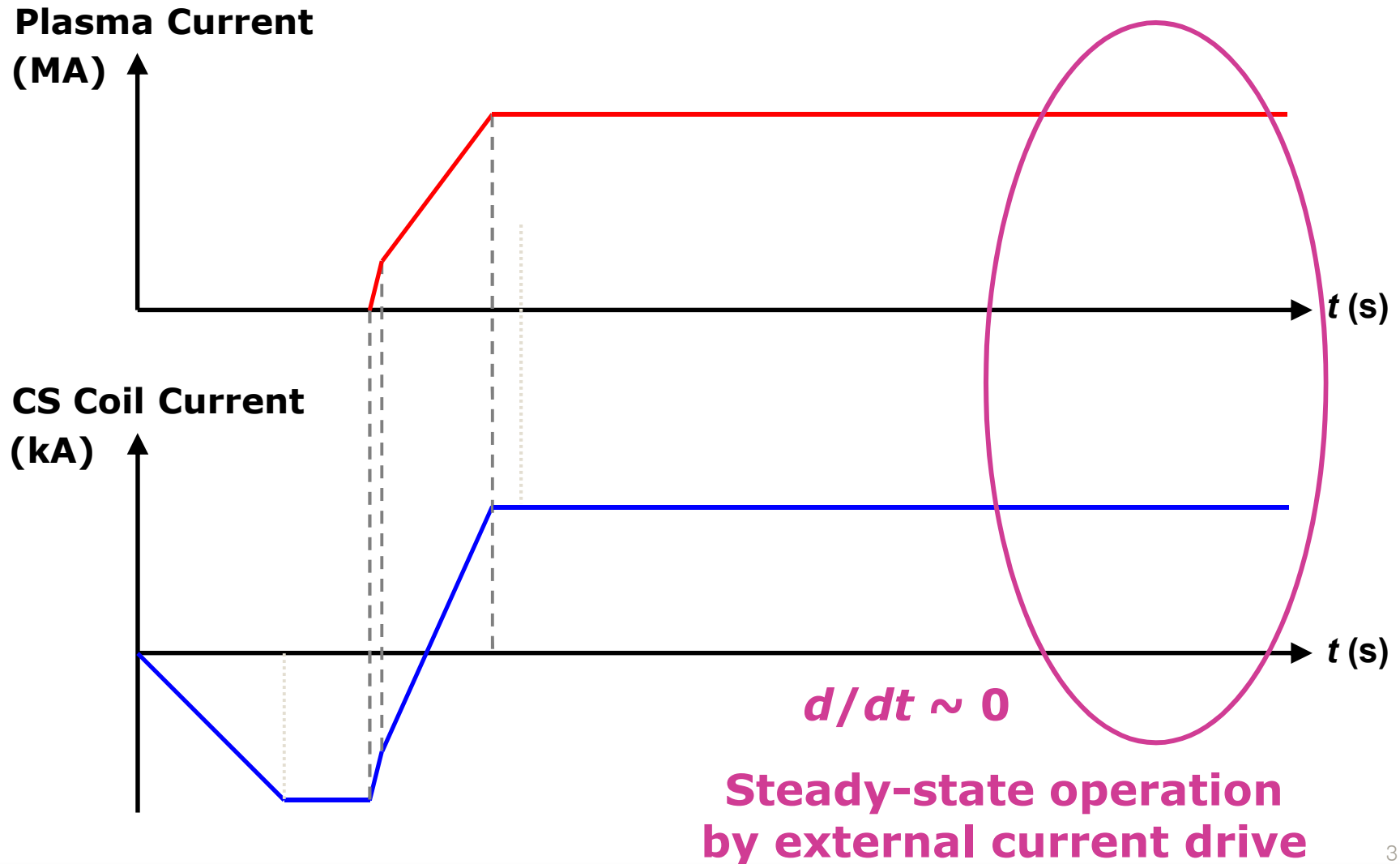
$$\mathcal{V} = -\frac{d}{dt} \int_S \mathbf{B} \cdot d\mathbf{s}$$

CS Coil Current  
(kA)



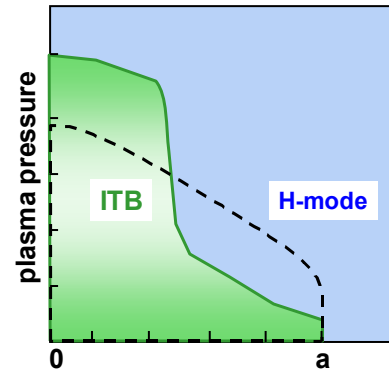
**Inherent drawback of Tokamak!**

# Steady-State Operation

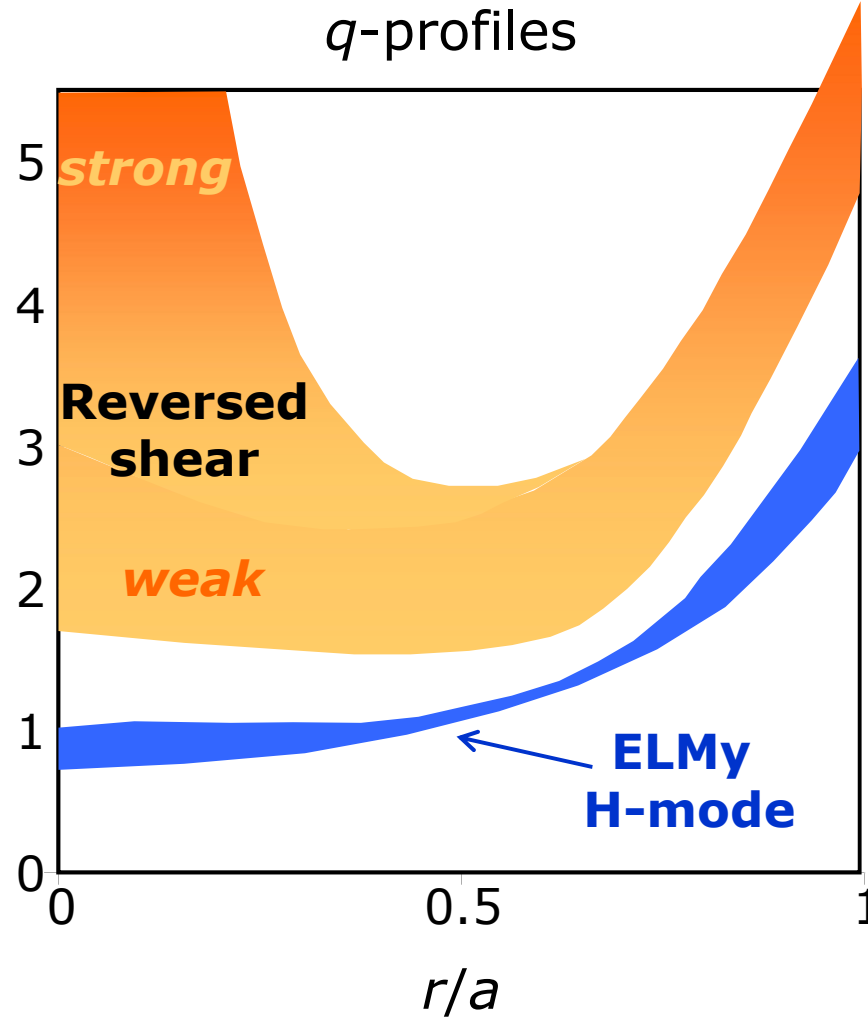




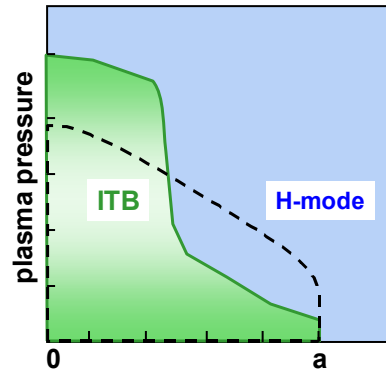
# Tokamak Operation Modes



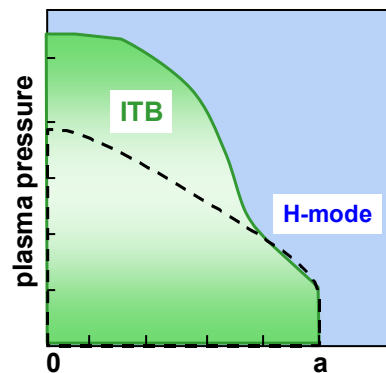
- Good confinement
- Poor stability



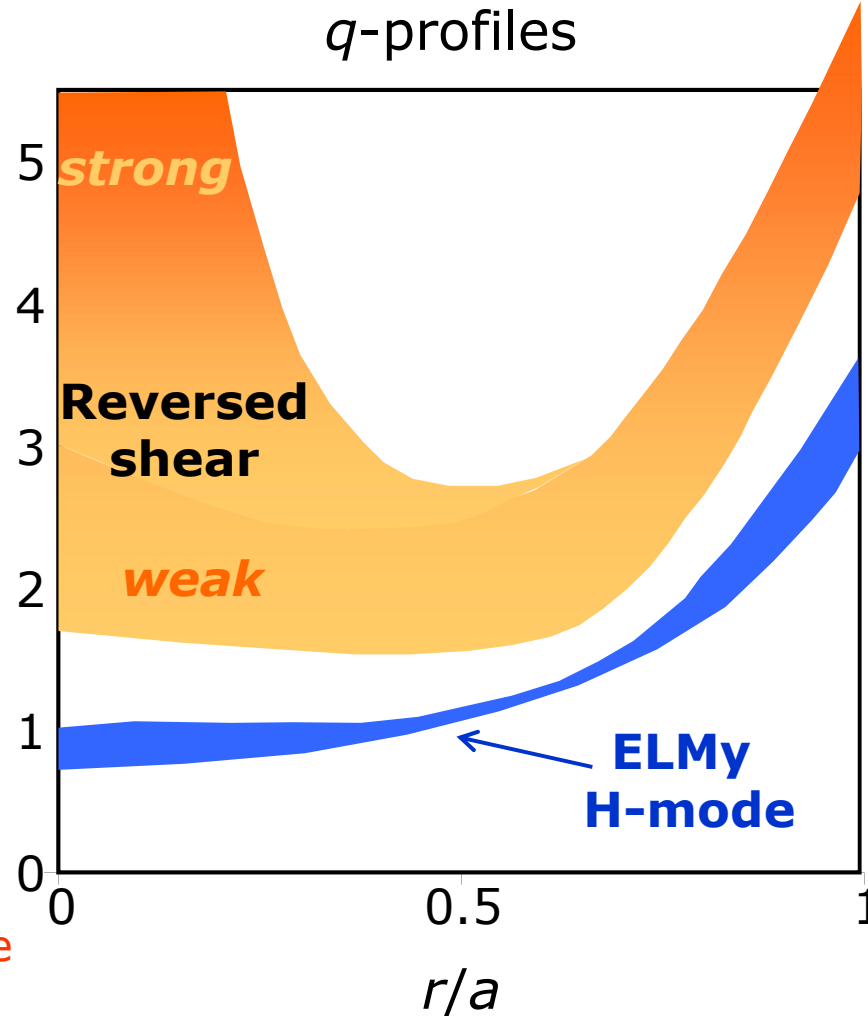
# Tokamak Operation Modes



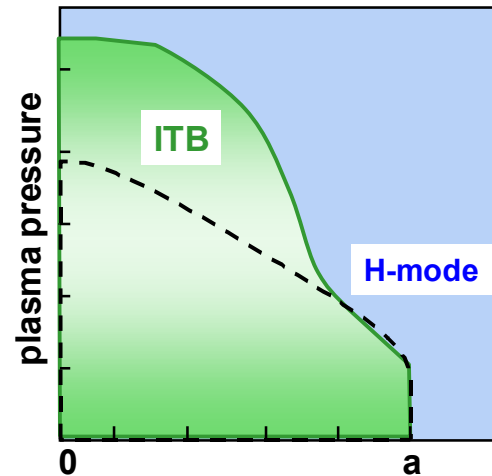
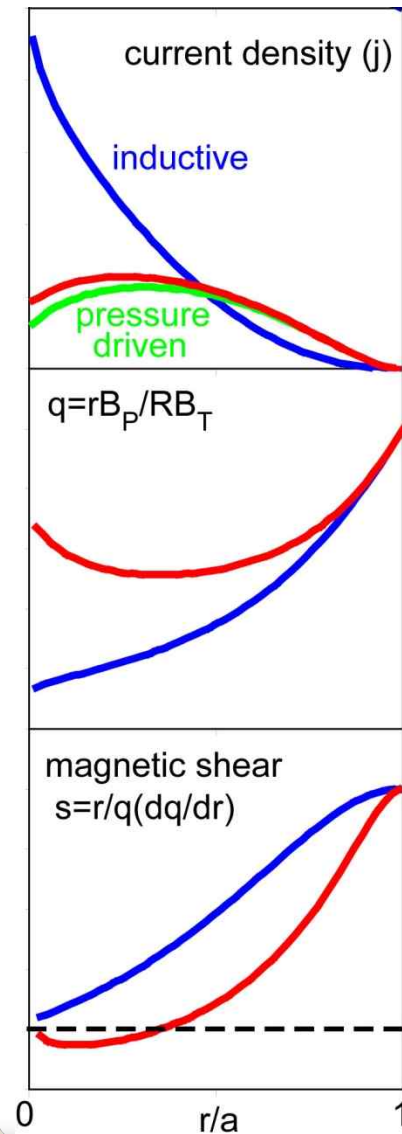
- Good confinement
- Poor stability



- Only "weak" RS plasmas are stable but they require a delicate active control



# Reversed Shear Mode



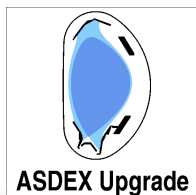
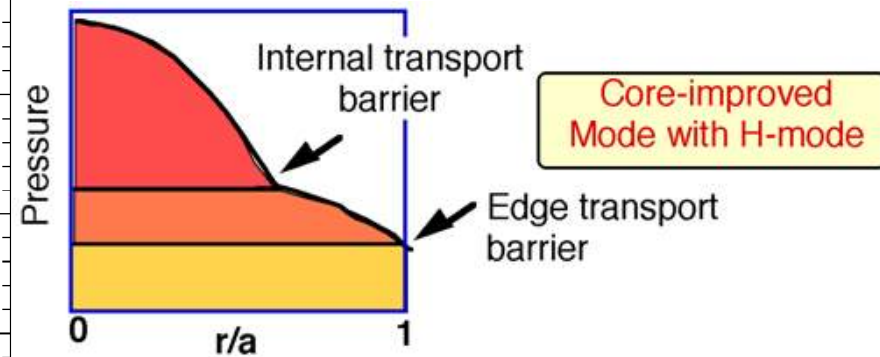
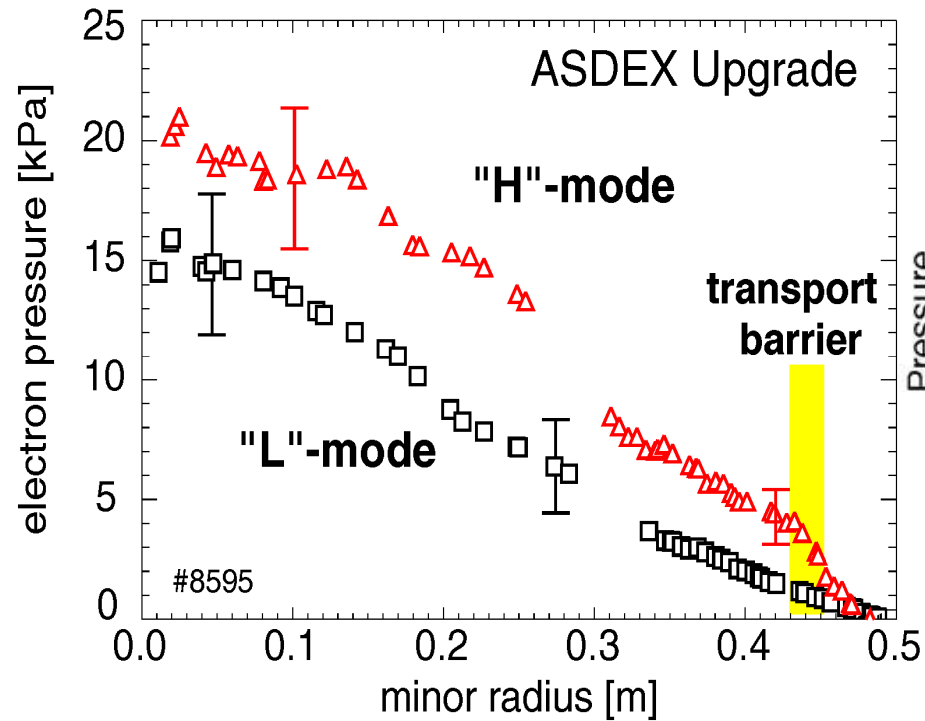
**High bootstrap current!**

- Higher pressure gradient region in the core with steep edge pedestal
- Hollow current profile
- Reversed  $q$ -profile
- With negative magnetic shear

# Reversed Shear Mode

H-mode

Reversed shear mode





# Internal Transport Barrier

Tokamak operation in the high- $\beta_p$  regime is a promising concept for a steady-state tokamak reactor [1,2].

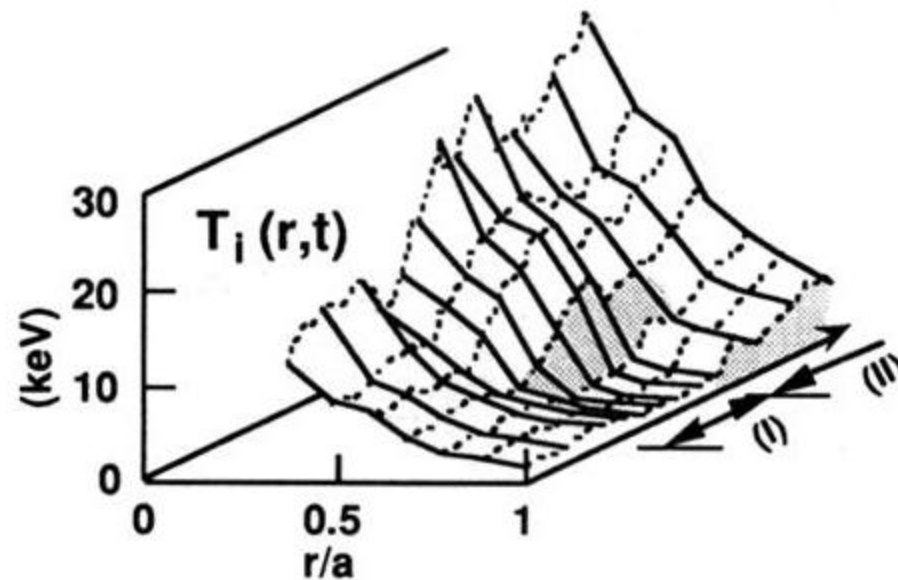
LETTERS

6 JUNE 1994

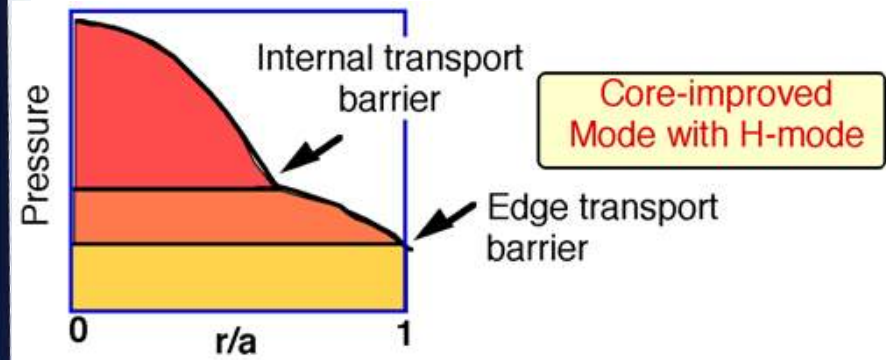
Here the poloidal beta is defined as  $\beta_p = 2\mu_0 \langle p \rangle / B_p^2$ , where  $\langle p \rangle$  is the volume-averaged plasma pressure and  $B_p$

and Poloidal Plasma Spin Up

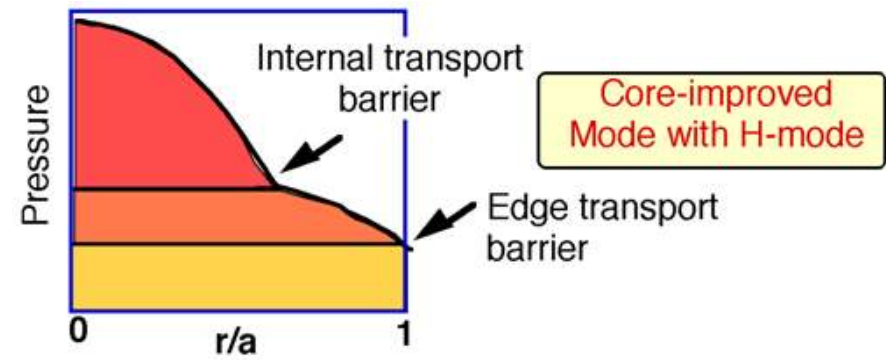
is the averaged poloidal magnetic field on the face. An energy confinement time,  $\tau_E$ , more than that for  $L$  mode (for example, ITER89-P [3] in the high- $\beta_p$  regime to reduce the plasma current and hence to achieve efficient steady-state operation [4]. Improved confinement time was achieved in the high- $\beta_p$  regime ( $\beta_p = 1-2$ ) in JT-60U, where the confinement improvement factor,  $\tau_E/\tau_{E,L}$ , increased with  $\epsilon\beta_p$  [5]. In this regime, the “high- $\beta_p$  mode” regime achieved a bootstrap-current fraction of up to 58% at an ion temperature,  $T_i(0)$ , of 38 keV were achieved. Recently the high- $\beta_p$  mode regime was shifted to a lower  $q$  regime ( $q_{\text{eff}} \sim 4.3$ ;  $q_{\text{eff}}$  is the effective safety factor defined in Ref. [6]) by using current profile control to avoid sawteeth. And high fusion performance was attained in this regime [7,8]. This Letter describes two distinctive features of this high- $\beta_p$  mode: (1) the formation of an “internal” transport barrier near the  $q=3$  rational surface and (2) the appearance of high poloidal plasma rotation velocity of  $\sim 50$  km/s in the plasma interior.



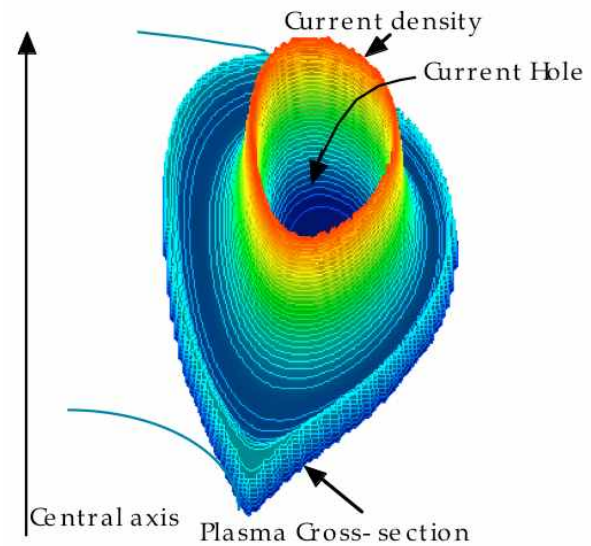
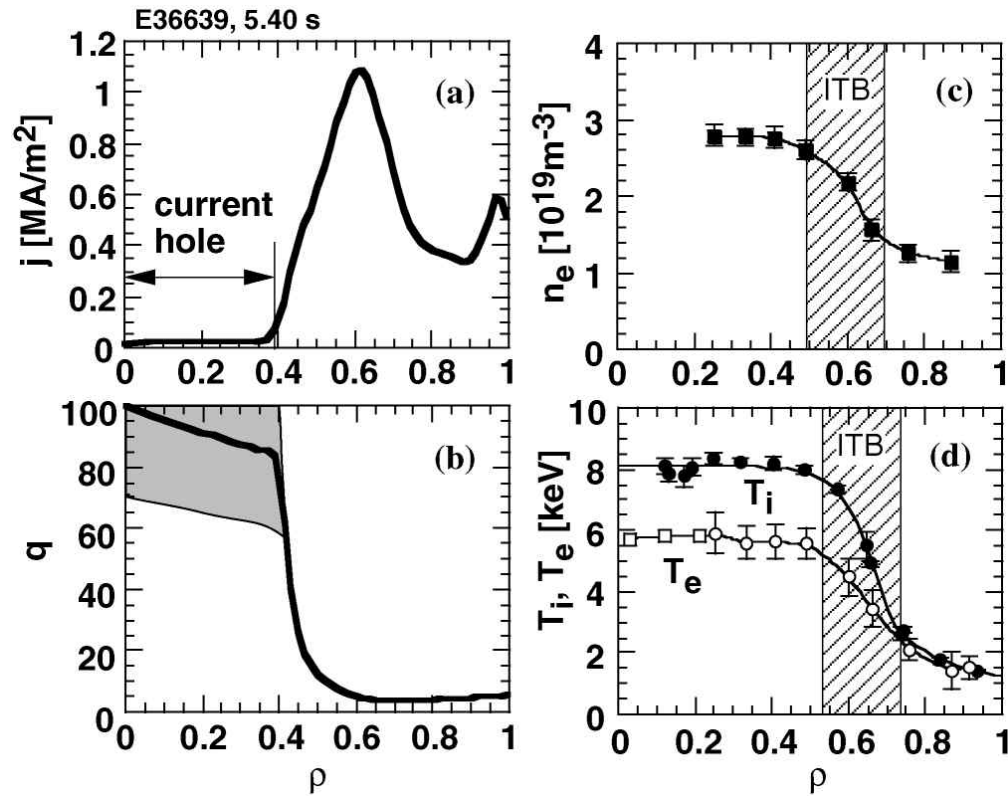
# Reversed Shear Mode



# Reversed Shear Mode

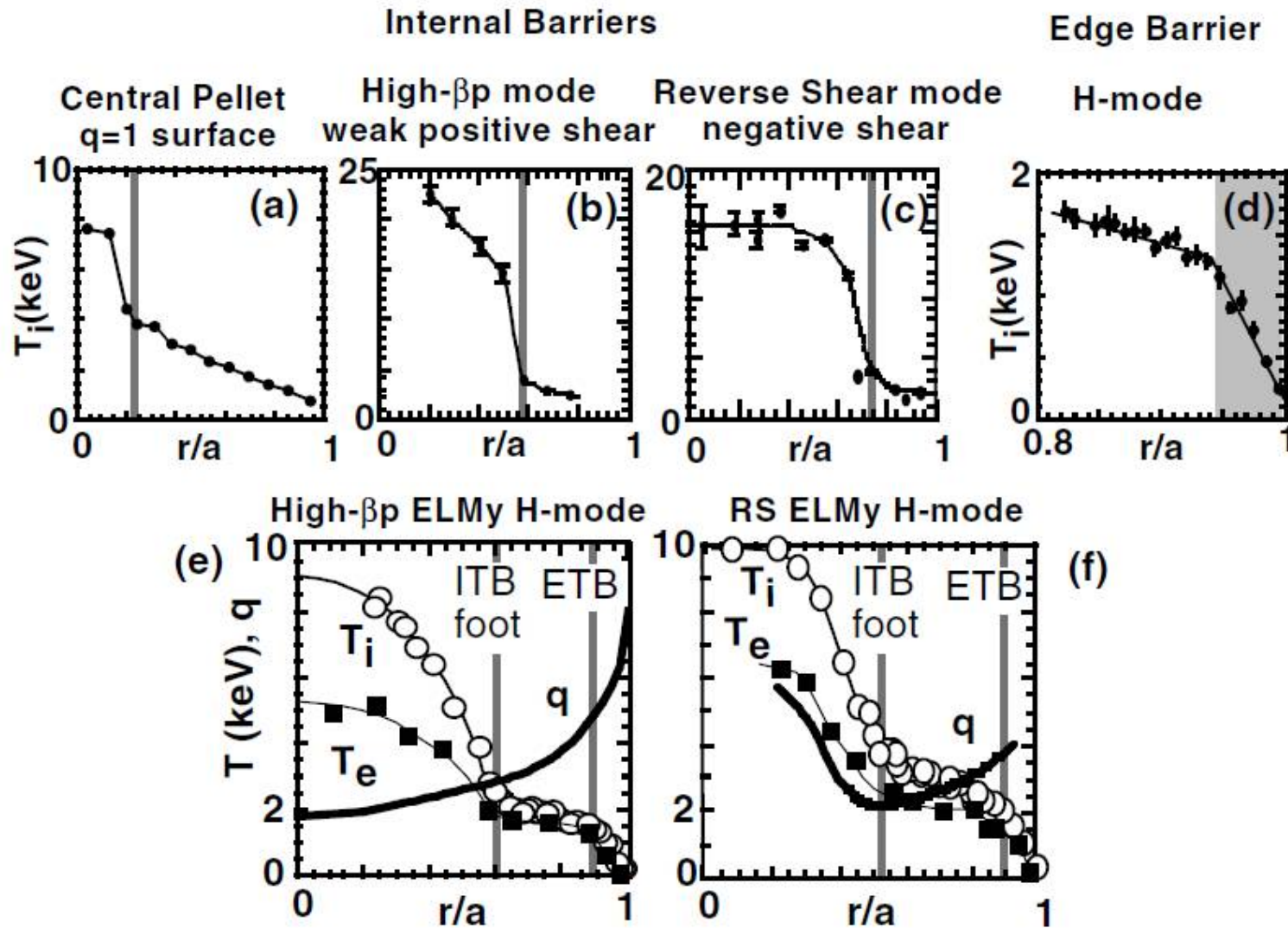


# Current Hole Regime



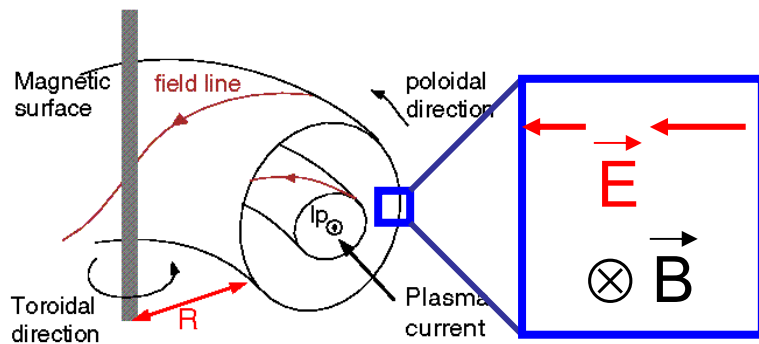
*T. Fujita et al, PRL* **87** 245001 (2001)

# Internal+Edge Transport Barrier

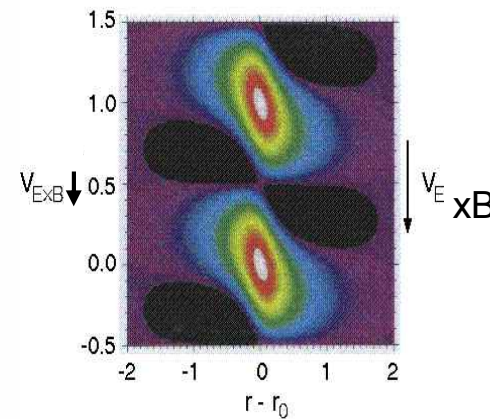
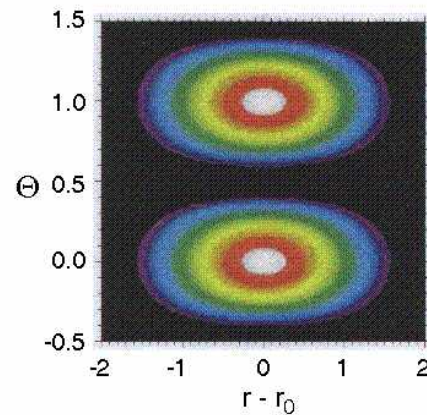


# Turbulence Stabilisation

- Formation of internal transport barriers to improve confinement
    - Reversed magnetic shear
    - Differential rotation (input power)
- } Stabilises turbulence

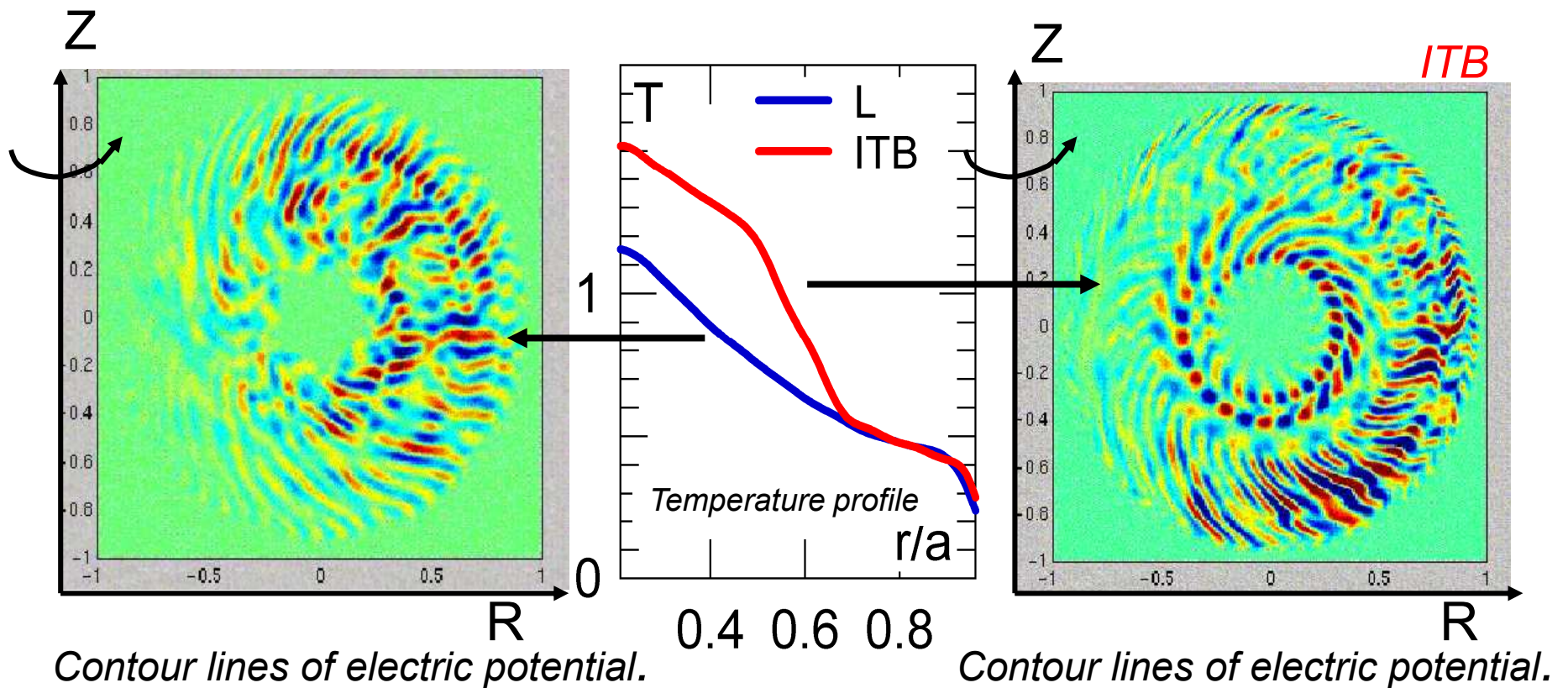


- One reason:
    - Losses of fast ions at the plasma edge
    - sheared radial electric field
    - sheared  $E \times B$  rotation
    - eddies get tilted and ripped apart
- cause turbulence suppression!**



# Turbulence Stabilisation

- Formation of internal transport barriers to improve confinement
    - Reversed magnetic shear
    - Differential rotation (input power)
- } Stabilises turbulence



# Turbulence Stabilisation

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**Gyrokinetic Simulations  
of Plasma Microinstabilities**

**simulation by**

**Zhihong Lin et al.**

**Science 281, 1835 (1998)**

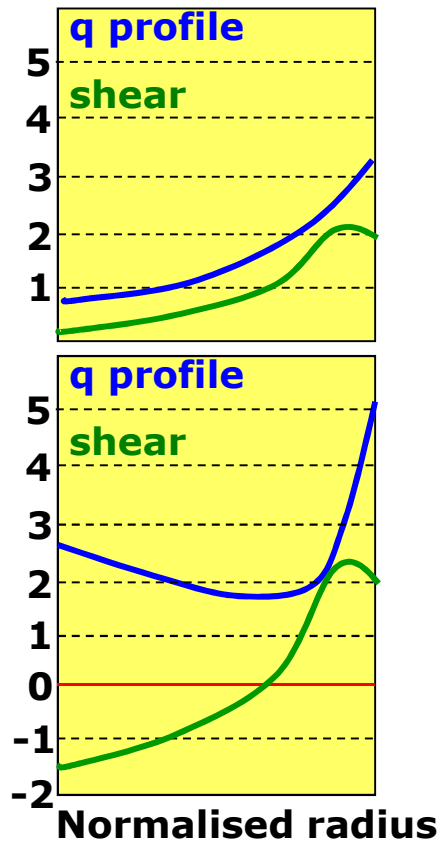
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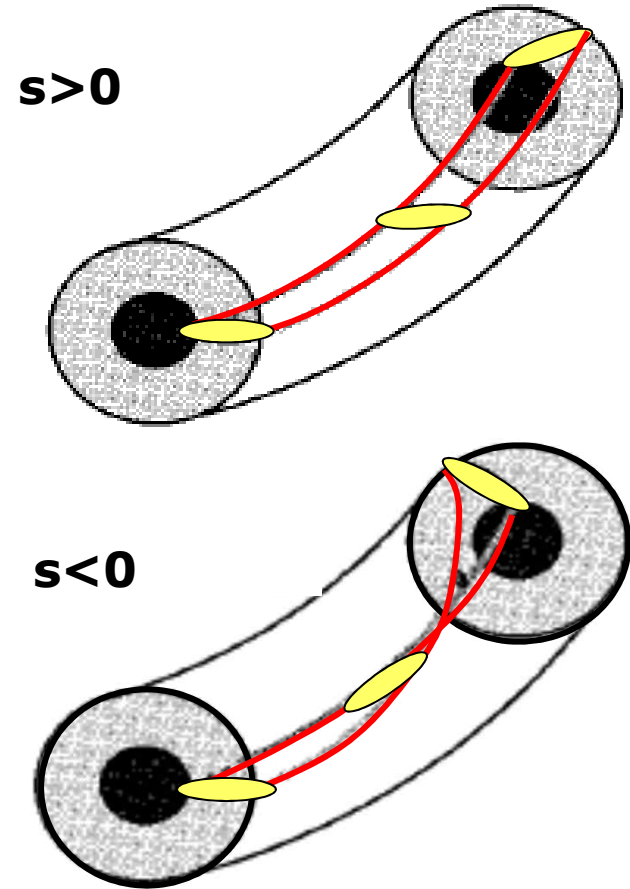
# Turbulence Stabilisation

**q & magnetic shear:  $s = r/q \, dq/dr$**

**Standard scenario**



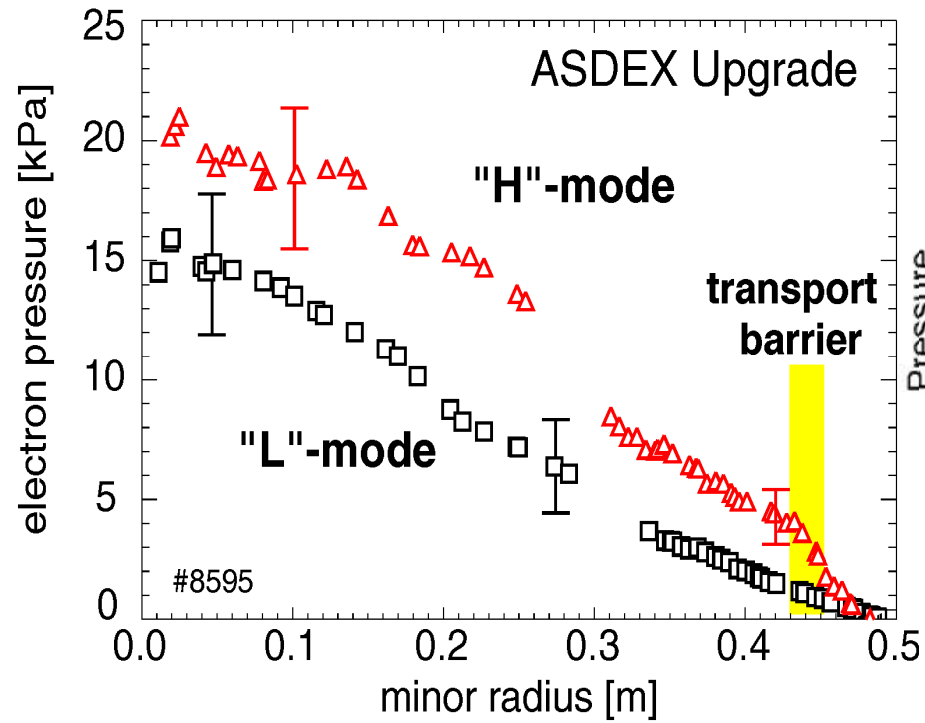
**Advanced tokamak scenario**



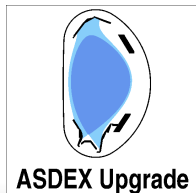
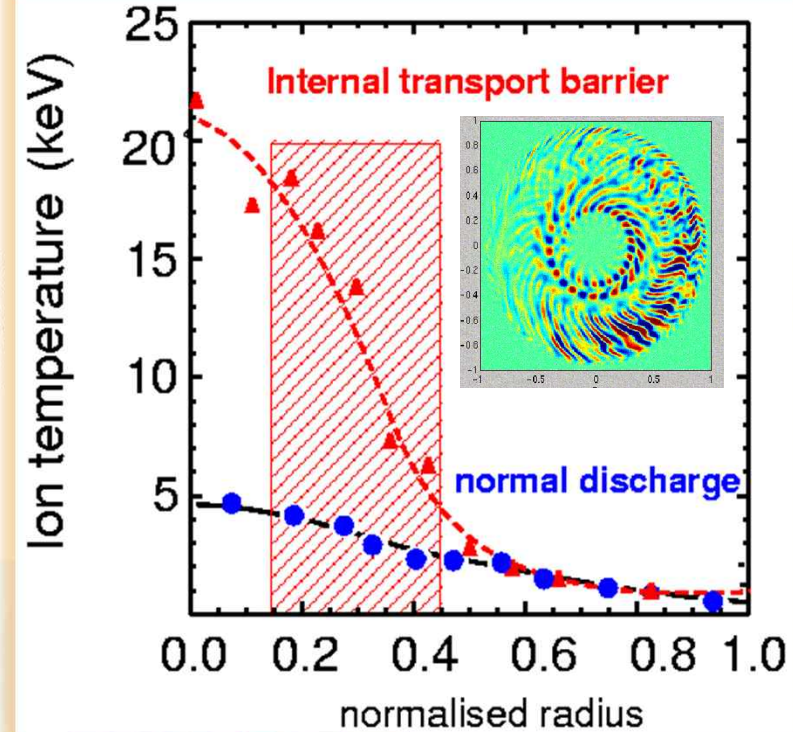
**Magnetic shear can twist plasma disturbances**

# Reversed Shear Mode

## H-mode

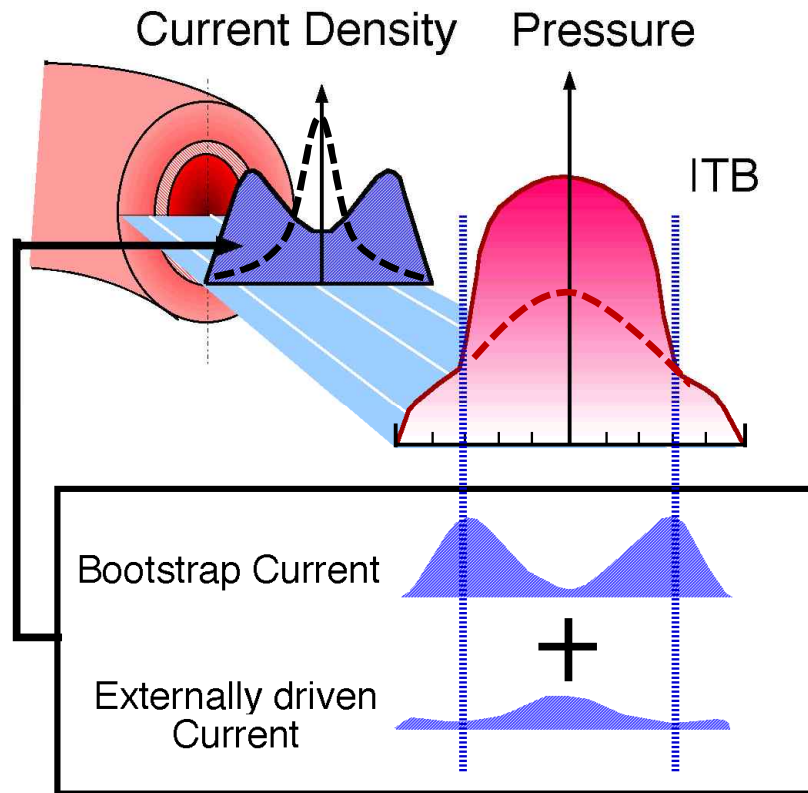


## Reversed shear mode



# Reversed Shear Mode

- Operation at lower plasma current:  $f_{BS} \sim \beta_p \sim I_p^{-2}$ 
  - Confinement degradation:  $\tau_E \sim H_{98}(y,2) I_p^{0.93}$
  - To get enough fusion power:  $H_{98}(y,2) > 1$  (advanced)



Non-monotonic current profile



Turbulence suppression



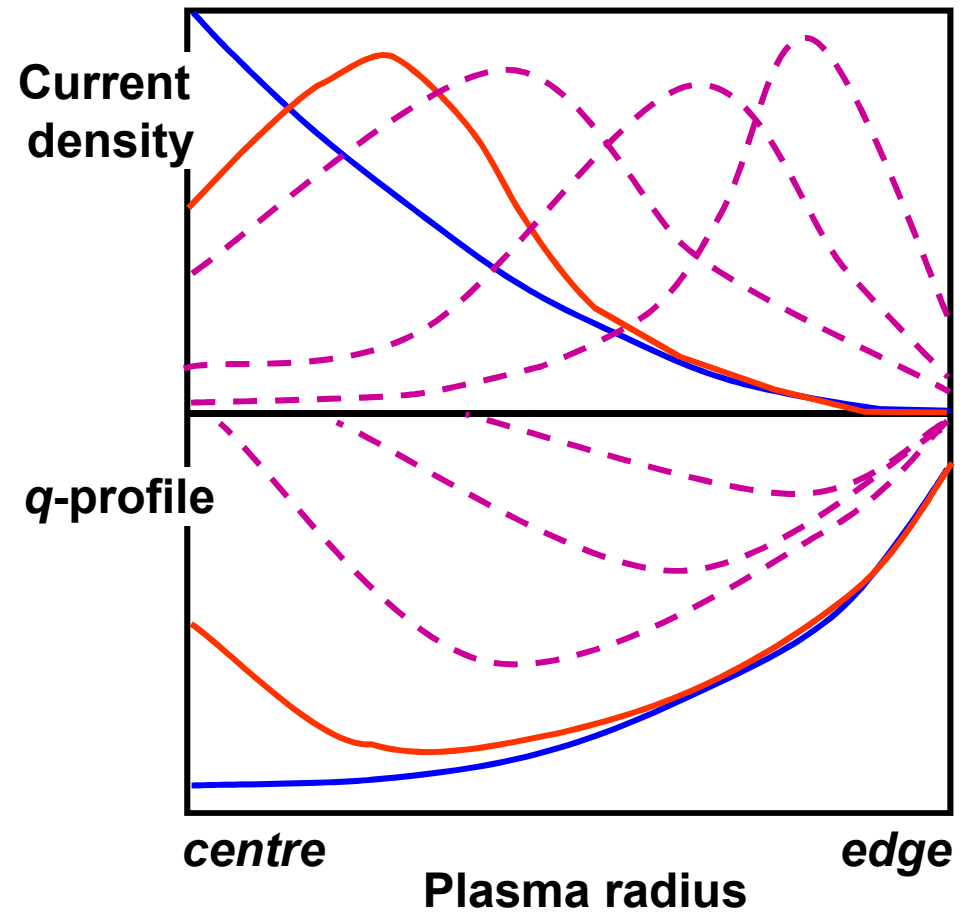
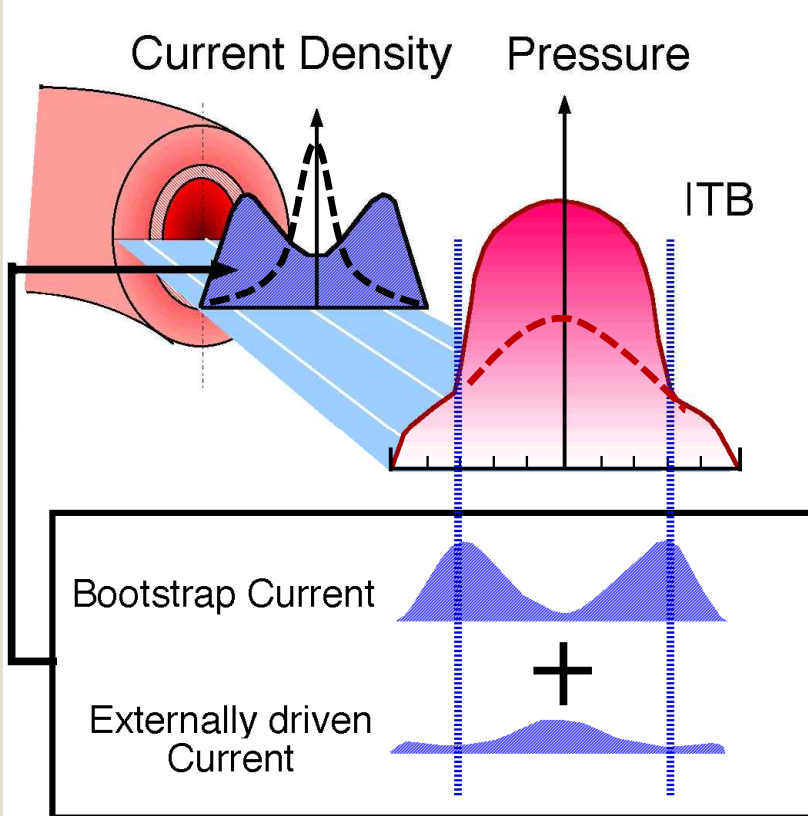
High pressure gradients



Large bootstrap current

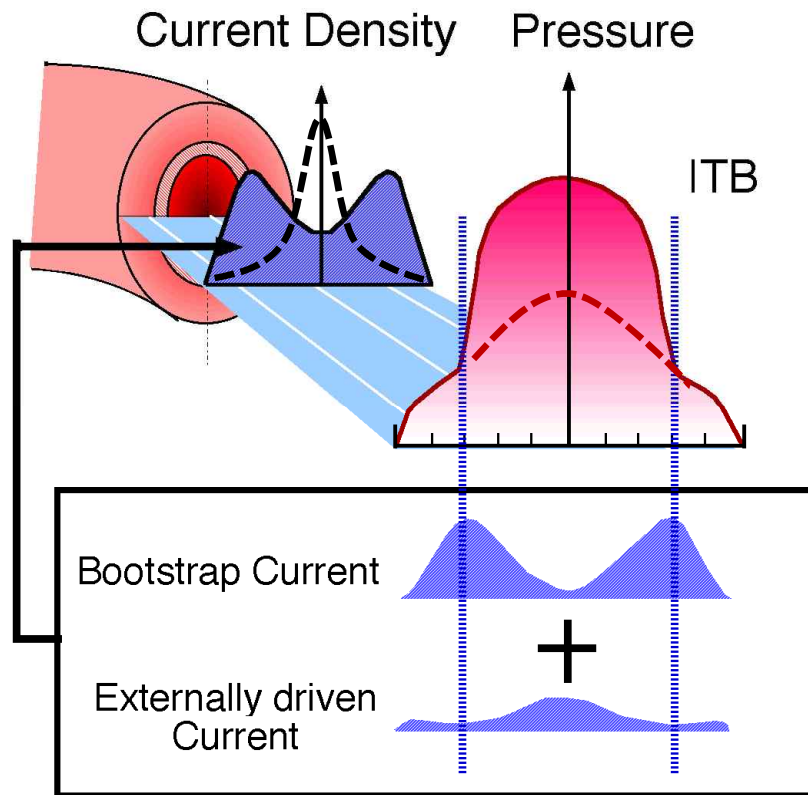
# Sustainment of Non-monotonic Current Profile

- Plasma current diffusion into the core from the edge



**Current and pressure profile control !**

# Current drive and current profile control



**Non-monotonic current profile**



**Turbulence suppression**



**High pressure gradients**



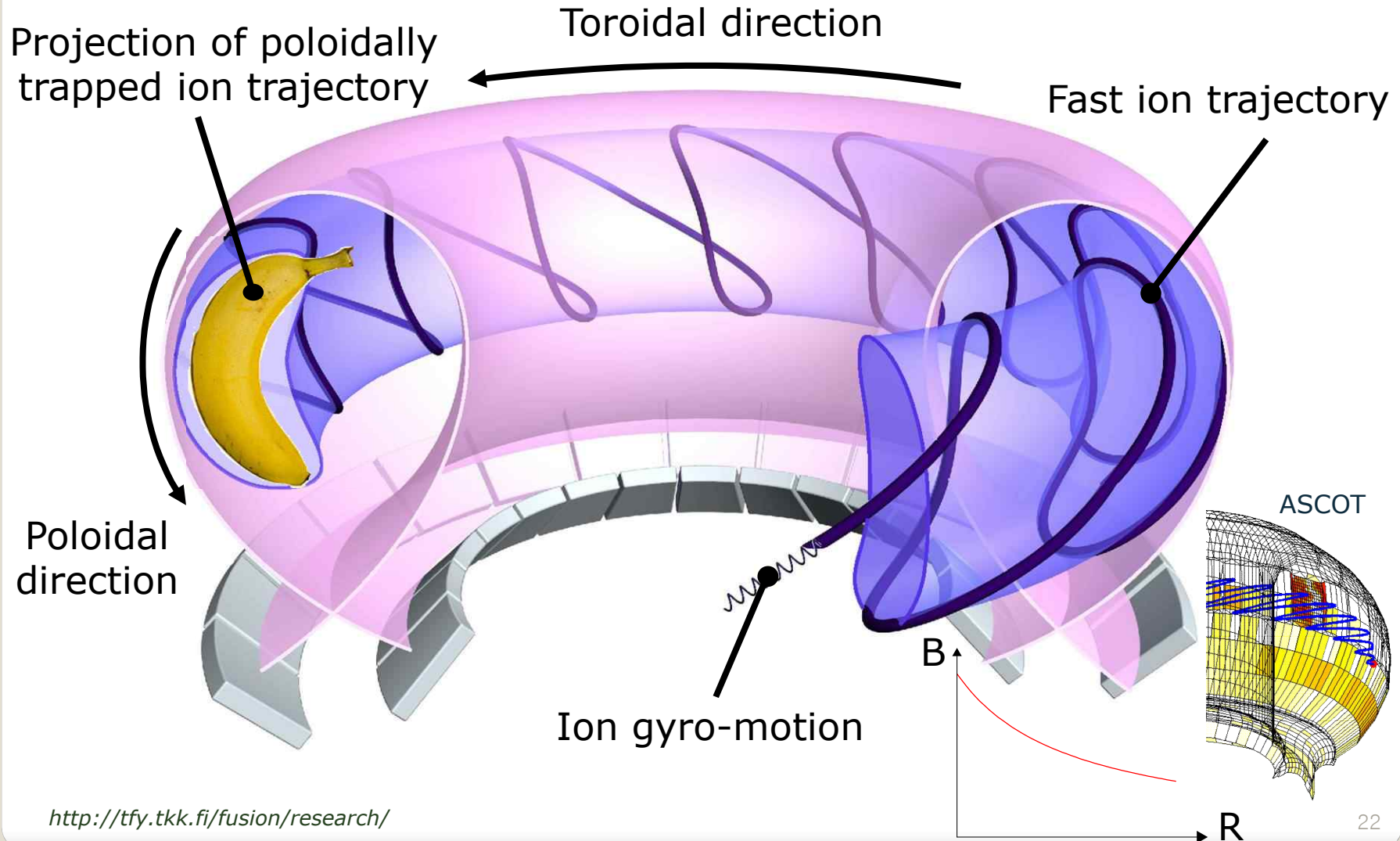
**Large bootstrap current**



**Non-inductive current drive**

# Current drive and current profile control

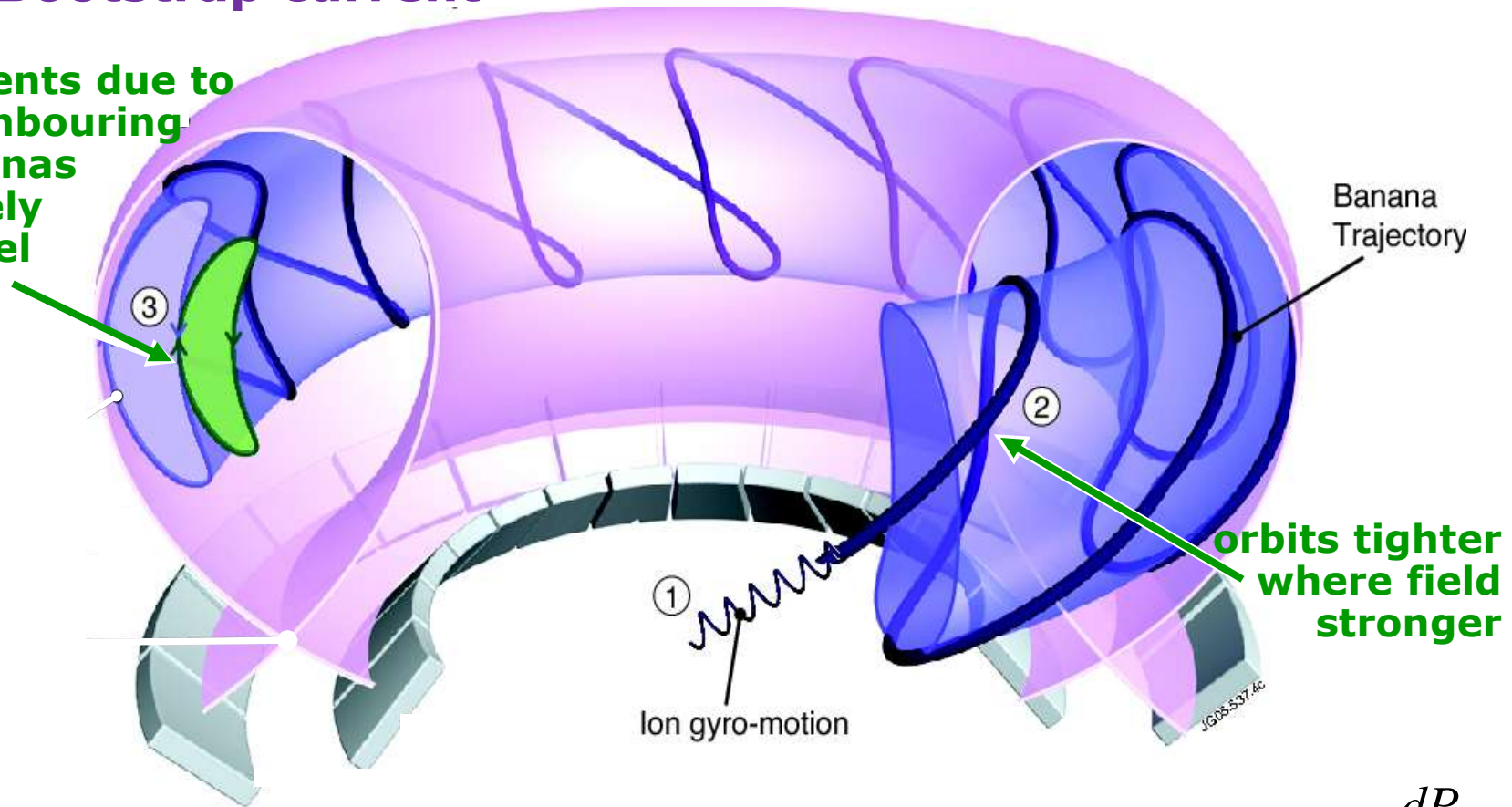
- Bootstrap current



# Current drive and current profile control

## • Bootstrap current

Currents due to neighbouring bananas largely cancel



- But more & faster particles on orbits nearer the core (green cf blue) lead to a net "banana current"

$$J_{boot} \sim \frac{dP}{dr}$$

- this is transferred to a helical bootstrap current via collisions

# Current drive and current profile control

- Bootstrap current

110

NATURE PHYSICAL SCIENCE VOL. 229 JANUARY 25 1971

## Diffusion Driven Plasma Currents and Bootstrap Tokamak

by

R. J. BICKERTON, J. W. CONNOR & J. B. TAYLOR

UKAEA Research Group, Culham Laboratory, Abingdon, Berkshire

In toroidal systems of plasma confinement the intrinsic diffusion driven toroidal current modifies estimates of the maximum ratio of plasma pressure to magnetic field pressure. This intrinsic current may also make possible a type of Tokamak machine which operates in a steady state, unlike present pulsed designs.

in what we call a “bootstrap” Tokamak. Such a machine could operate in a steady state, unlike present pulsed designs, because refuelling and thermonuclear reactions provide a continuous source of plasma to diffuse across the lines of force.

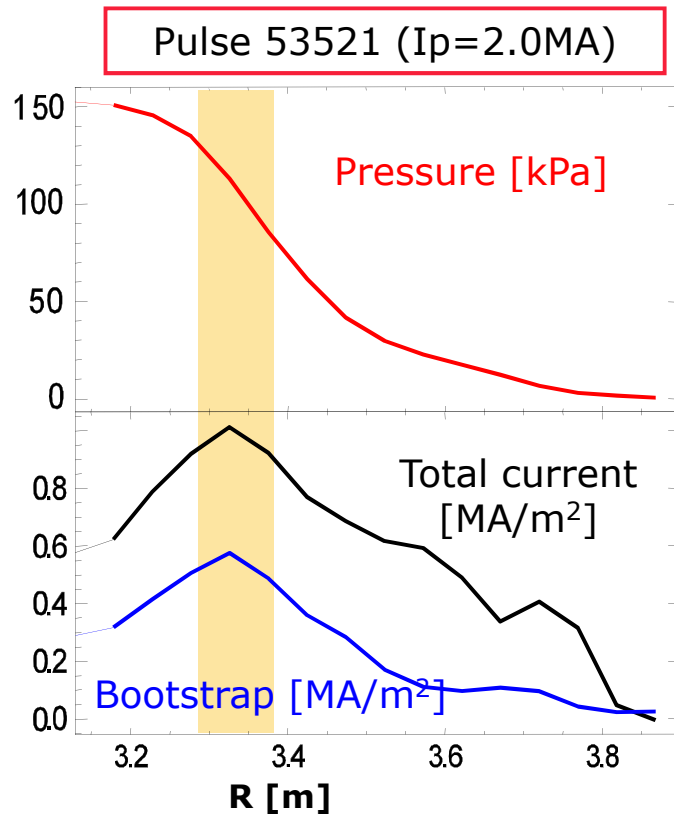
The existence of the intrinsic toroidal current is implicit in all calculations of toroidal diffusion and its value may be obtained easily from such calculations, so that only the result need be quoted here. For simplicity we consider the usual axisymmetric system with concentric magnetic surfaces  $B\varphi = B_0/h$ ,  $B_\theta = \Theta B\varphi$  with

$$\Theta = \varepsilon \frac{t}{2\pi} \ll 1, \quad h = 1 + (r/R) \cos \theta, \quad \text{and } r, \theta, \varphi$$



# Current drive and current profile control

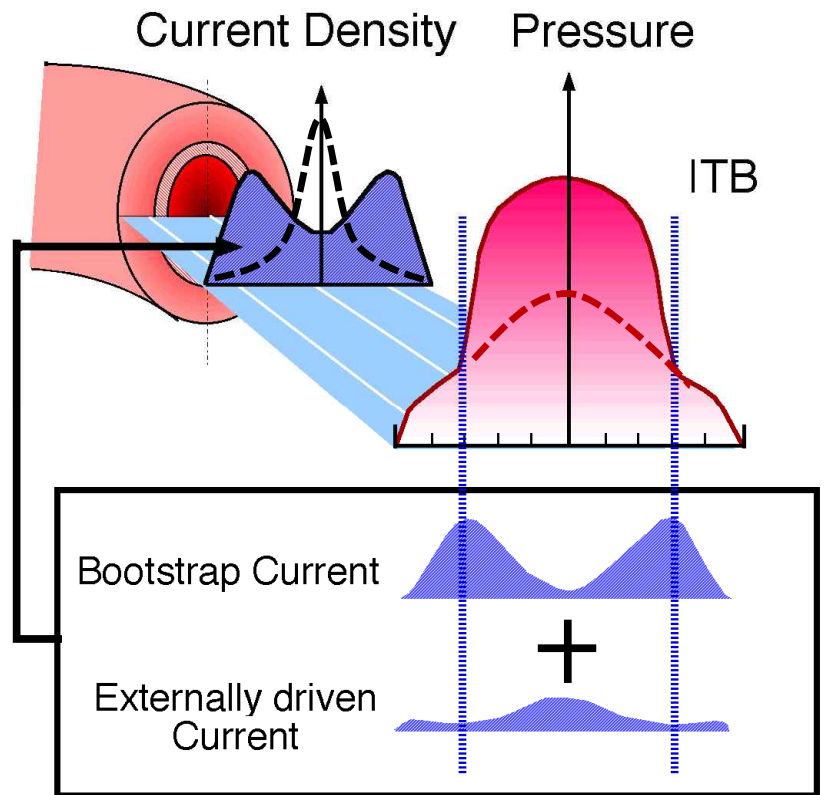
- Bootstrap current



**Bootstrap current is an off-axis current drive**

***Bickerton 1971 & Galeev 1970***

# Current drive and current profile control



Cf. NTM control

Non-monotonic current profile



Turbulence suppression



High pressure gradients



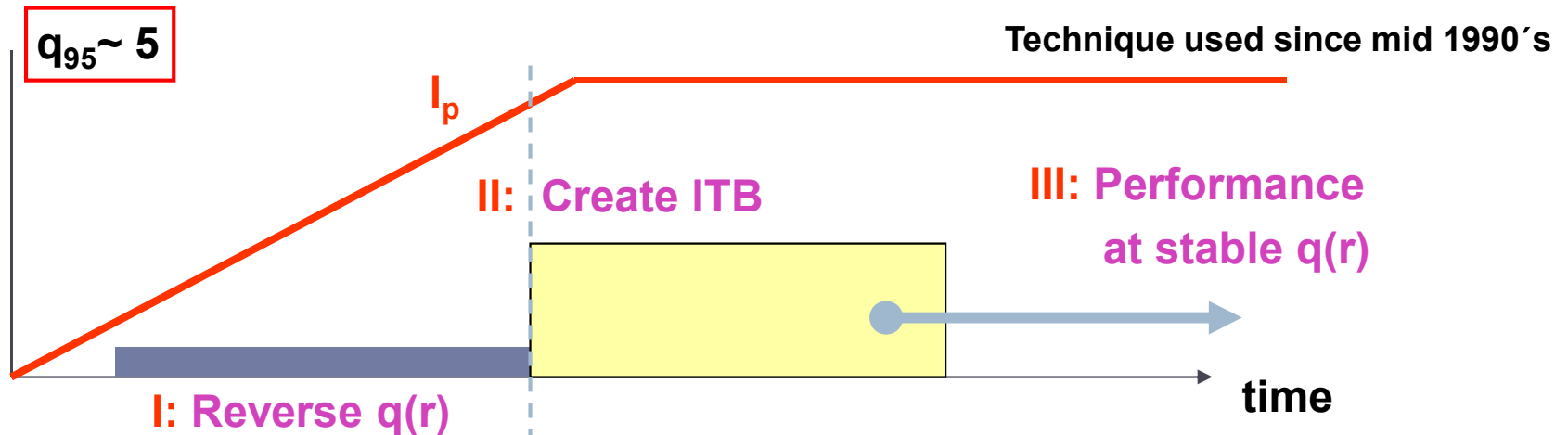
Large bootstrap current



**Non-inductive current drive**

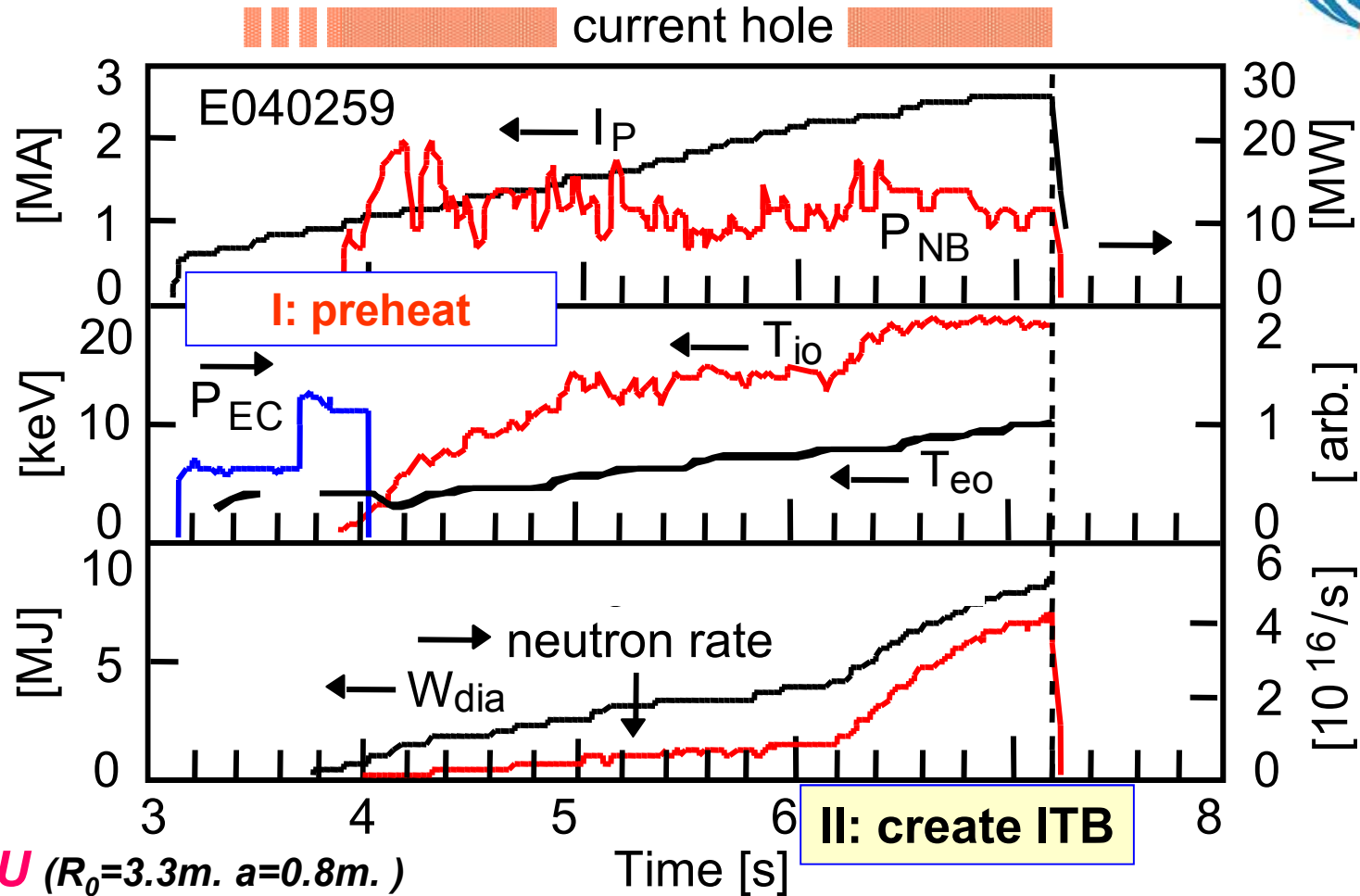
**HW: Which heating & CD sources for fusion reactors?**

# Reversed Shear Scenario



- I: Heat during current rise, external current drive (reverse  $q$ ).
- II: Increase heating power to stabilise turbulence (ITB).  
Improve plasma confinement, try to increase pressure ( $\beta_N$ )
- III: Keep going: ITER non-inductive regime:  $H_H \approx 1.6$ ;  $\beta_N \approx 3.0$   
(ITER: 9MA, 50% external current drive (73MW), 50% bootstrap fraction)

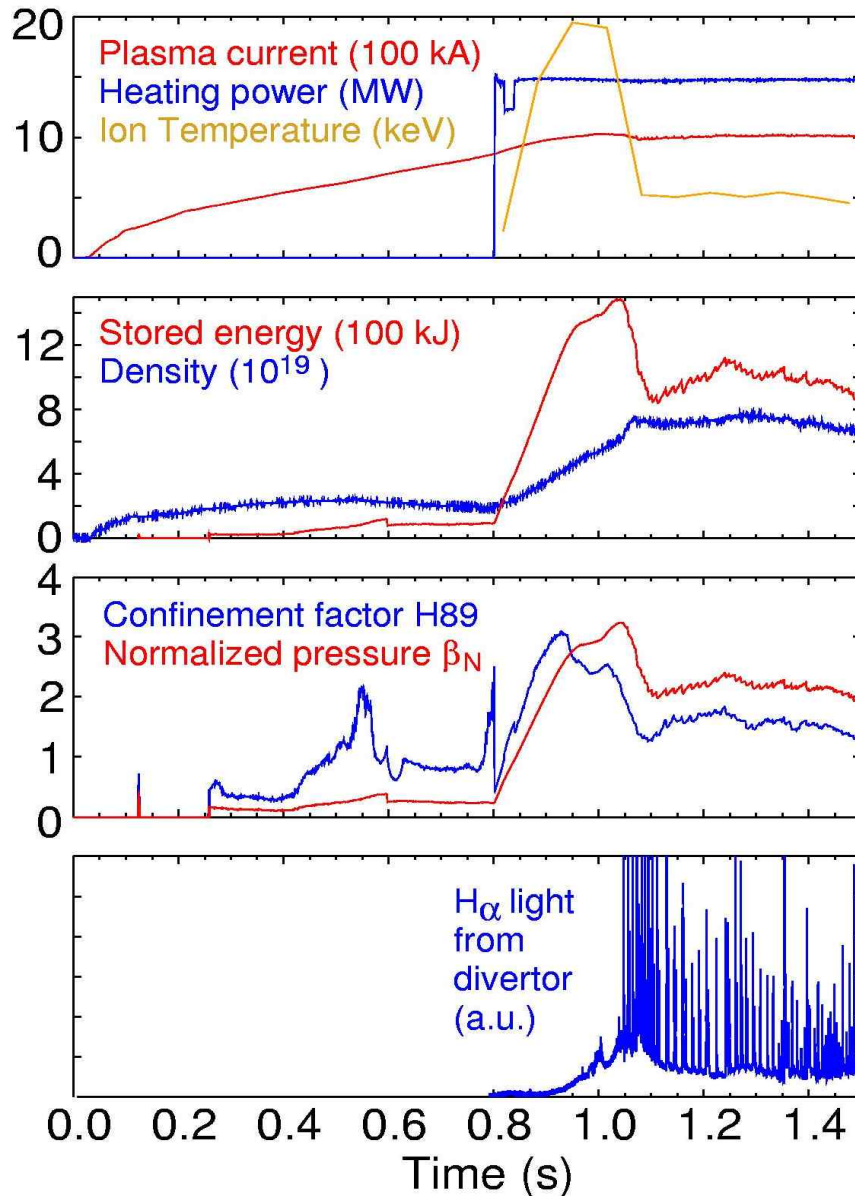
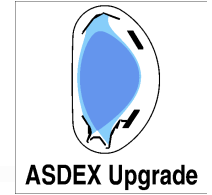
# Reversed Shear Scenario



**JT-60U** ( $R_0=3.3m.$   $a=0.8m.$ )

**I:** Form  $q(r)$ , **II:** create ITB, **III:** But discharge terminates (unstable)

# Reversed Shear Scenario

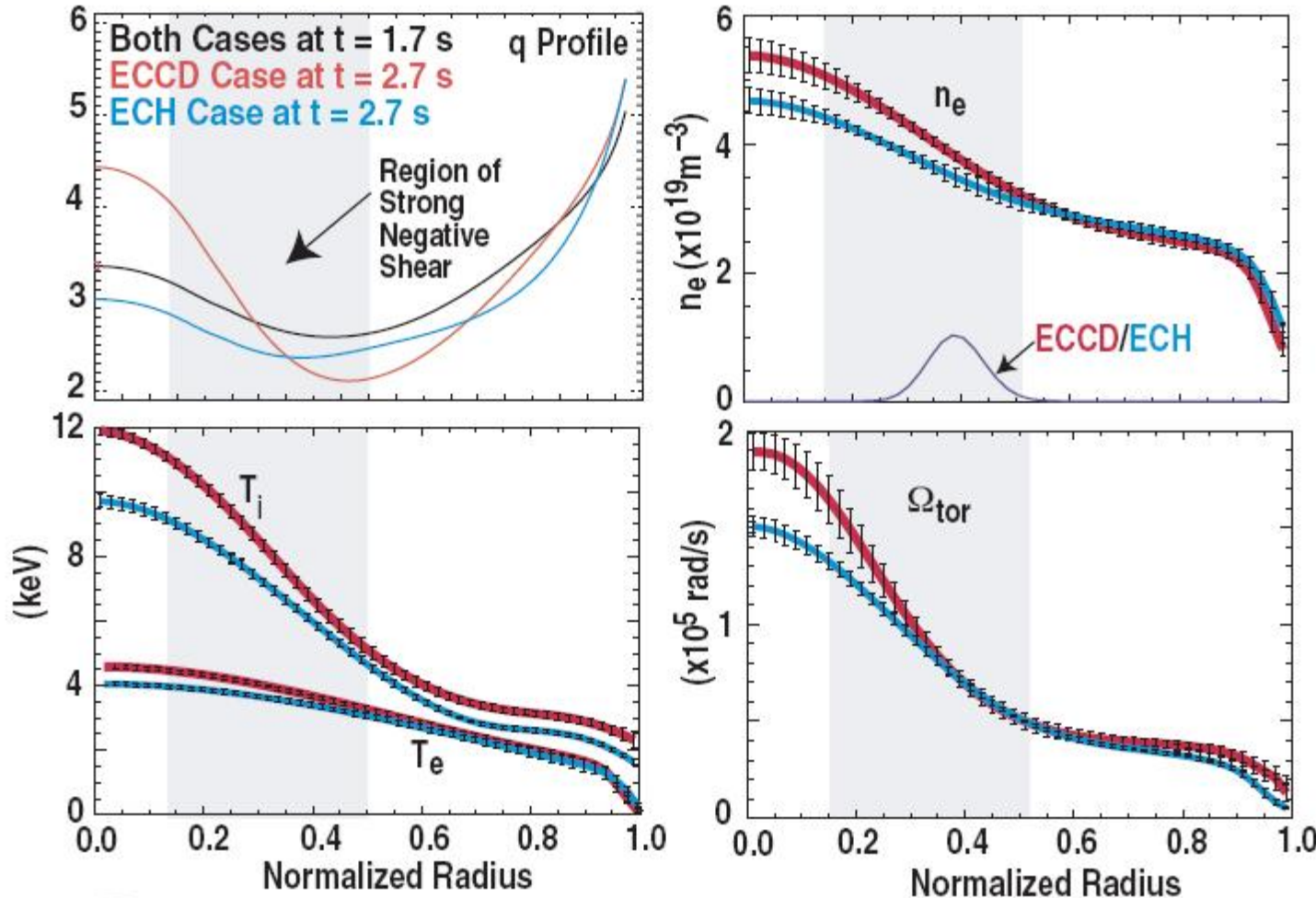


- Formation of an ITB at low  $n_e$ , with 15 MW NBI power  
 $T_i > T_e$ , high rotation shear
- ITBs are relatively short lived, only few  $\tau_E$
- Good, transient performance:  
 $H_{89} \sim 3$ ,  $\beta_N \sim 3$
- ITB not compatible with H-mode edge barrier and large ELMs

# Reversed Shear Scenario



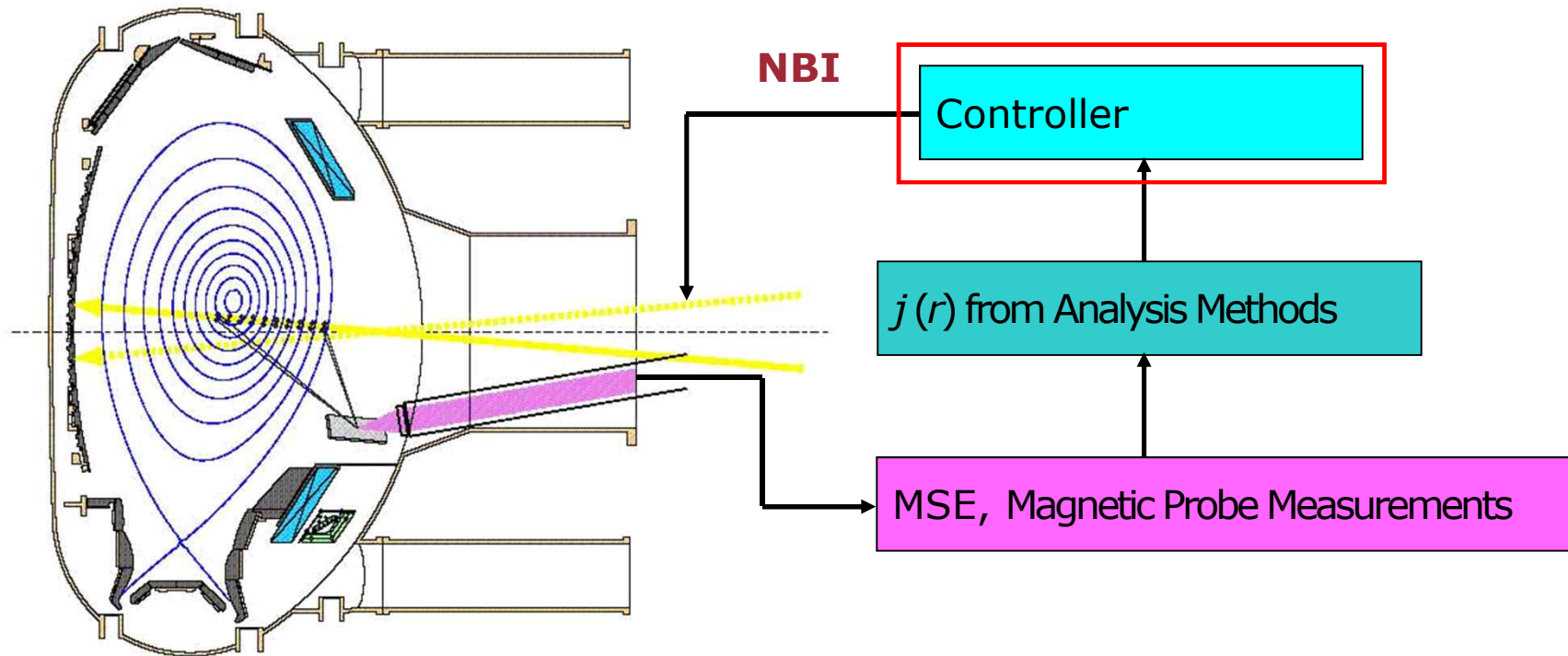
( $R_0=1.7m.$  ,  $a=0.6m.$  )



- Less RS
- $H_{H98(y,2)} = 1.37$
- $\beta_N = 2.62$
- $q_{95} = 5$
- „Weak“ ITBs

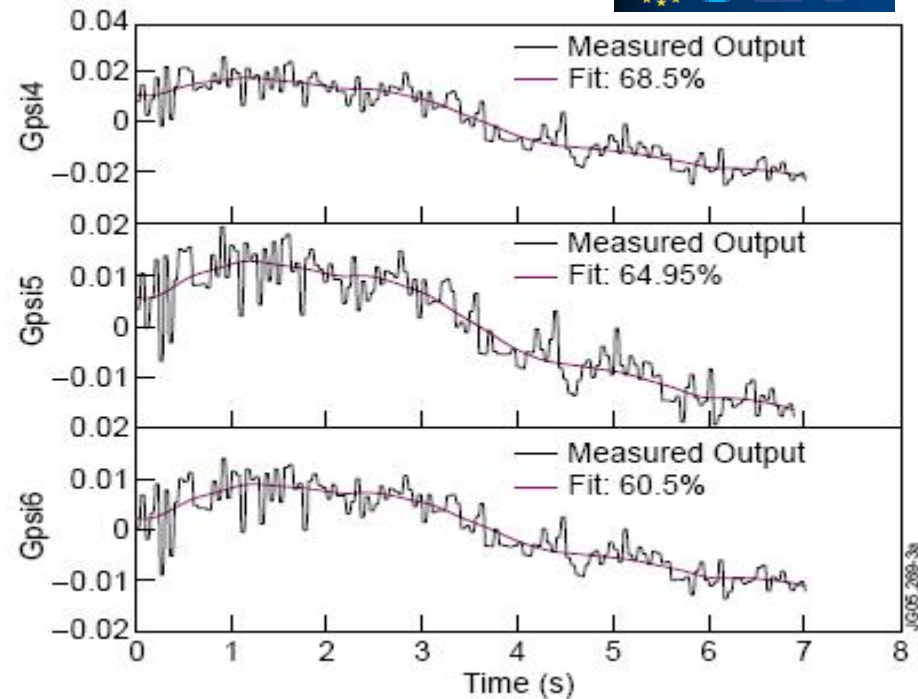
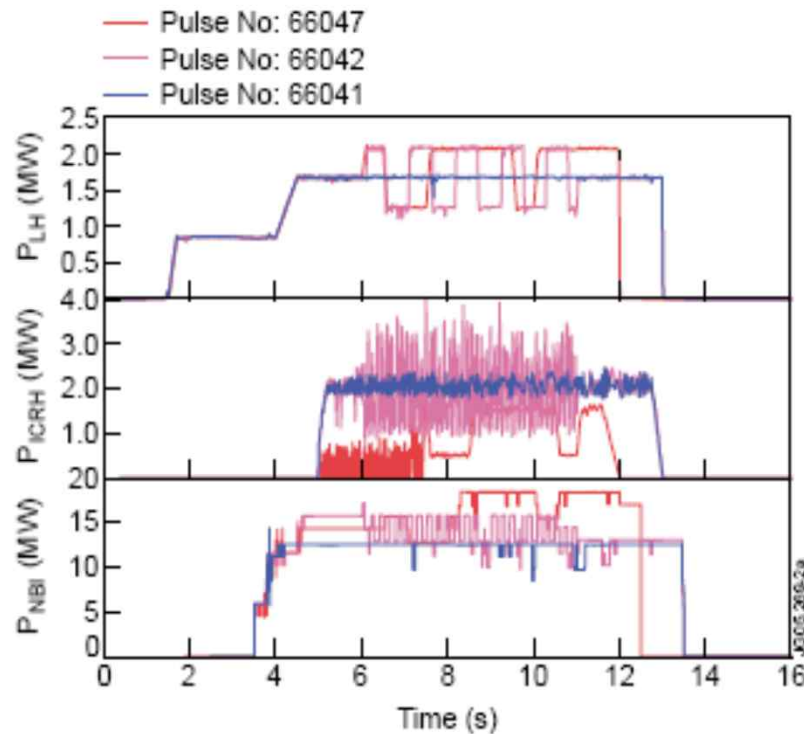
# Reversed Shear Scenario

- Current density profile control at ASDEX Upgrade



# RT Current and Pressure Profile Control

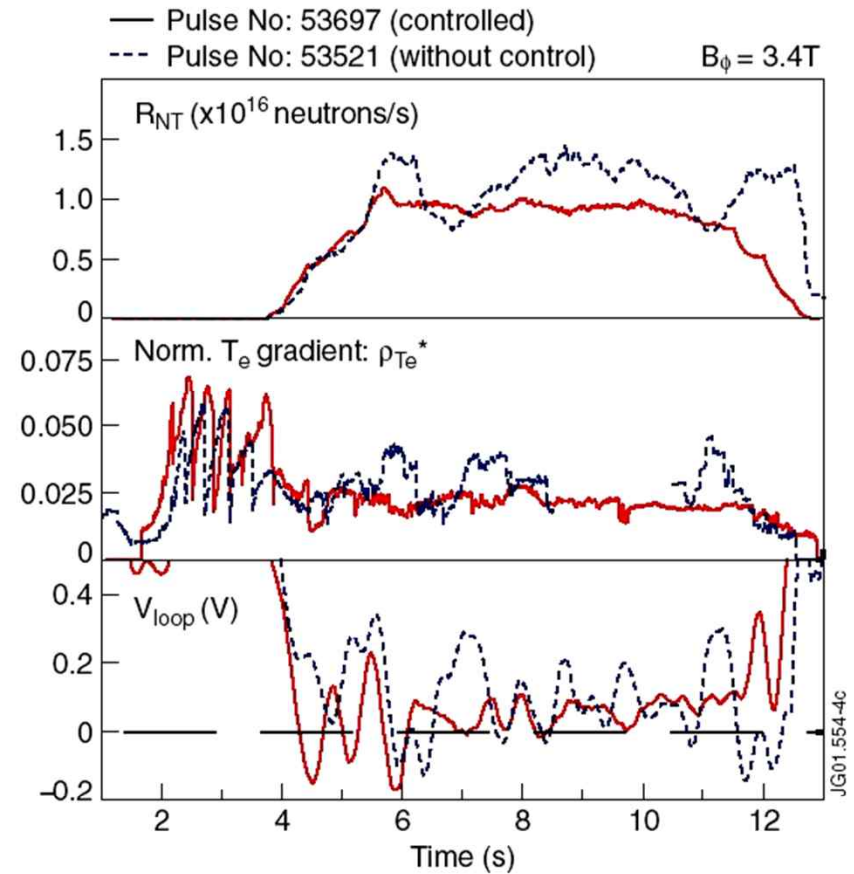
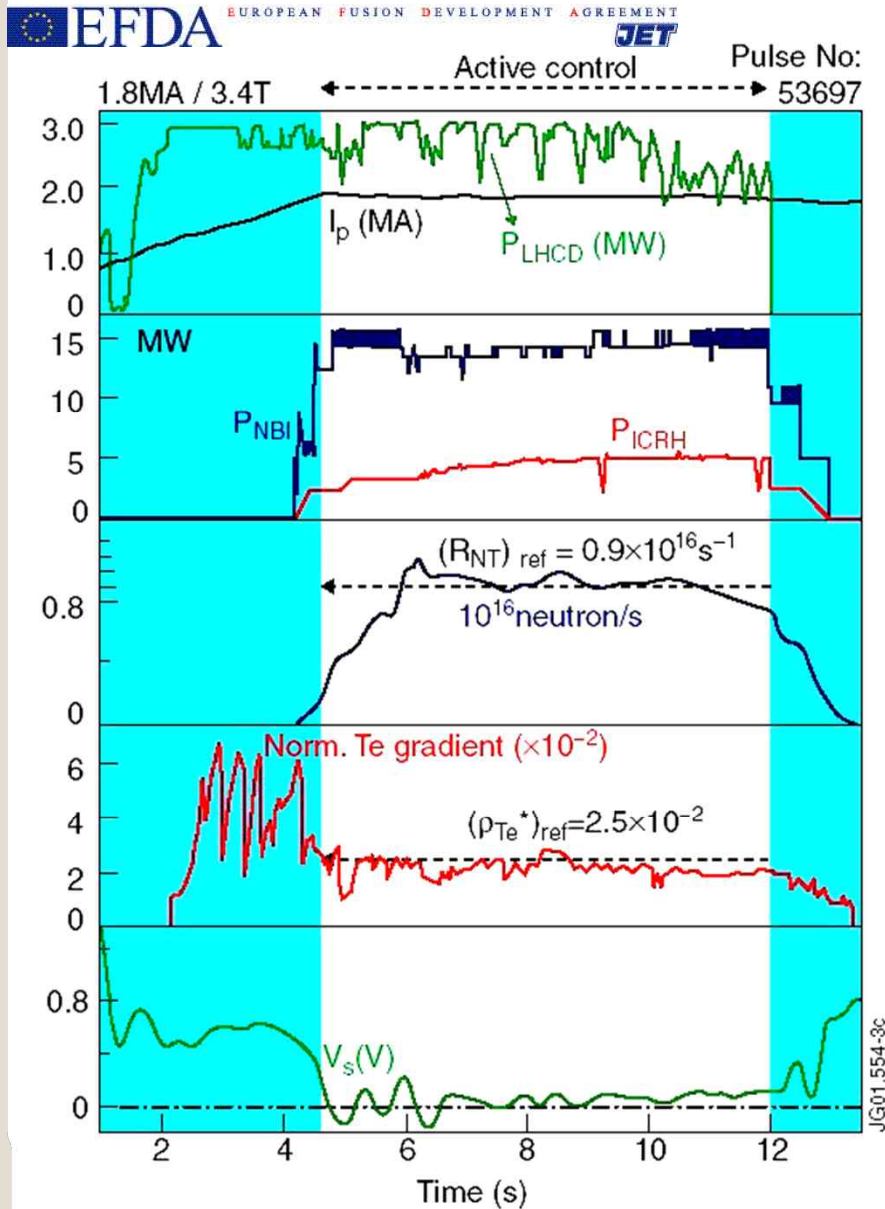
- Simultaneous control of distributed magnetic and kinetic parameters
- Dedicated experiments to identify controller coefficients



- Modulation combinations of actuators (NBI, LH, ICRH) to infer the coefficients of the state space model of the slow loop.
- Two control loops, 4 actuators (NBI, LH, ICRH, PF)



# RT Current and Pressure Profile Control

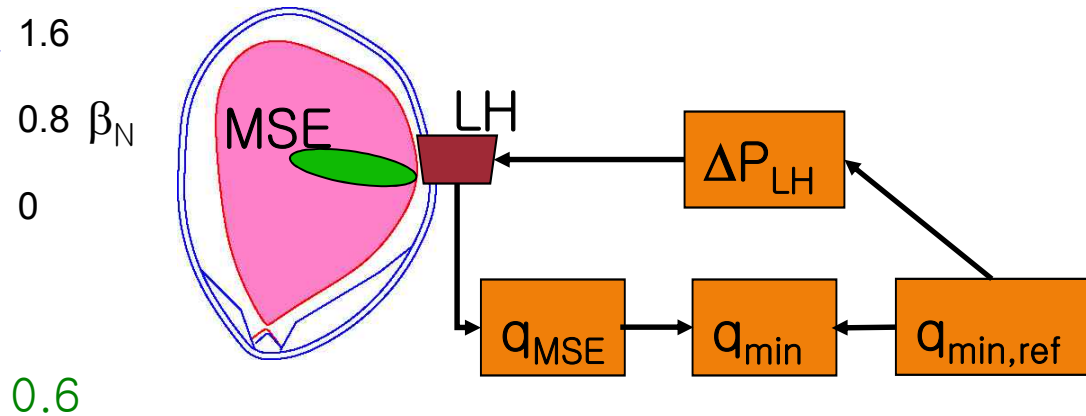
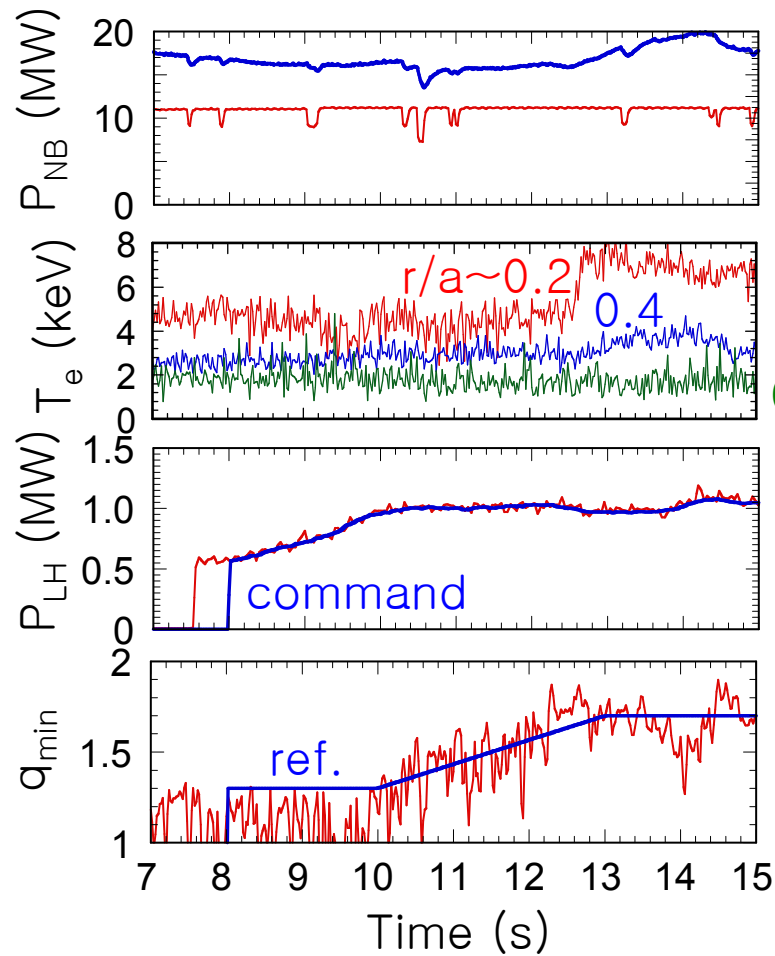


- Real time pressure profile and  $q$ -profile control to keep ITB steady

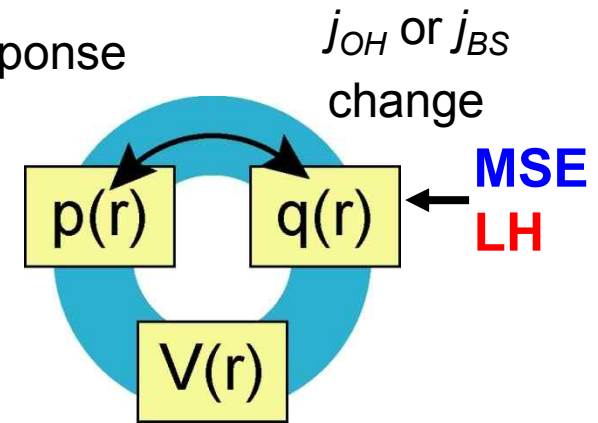
Mazon et al, PPCF 2002

# RT Current and Pressure Profile Control

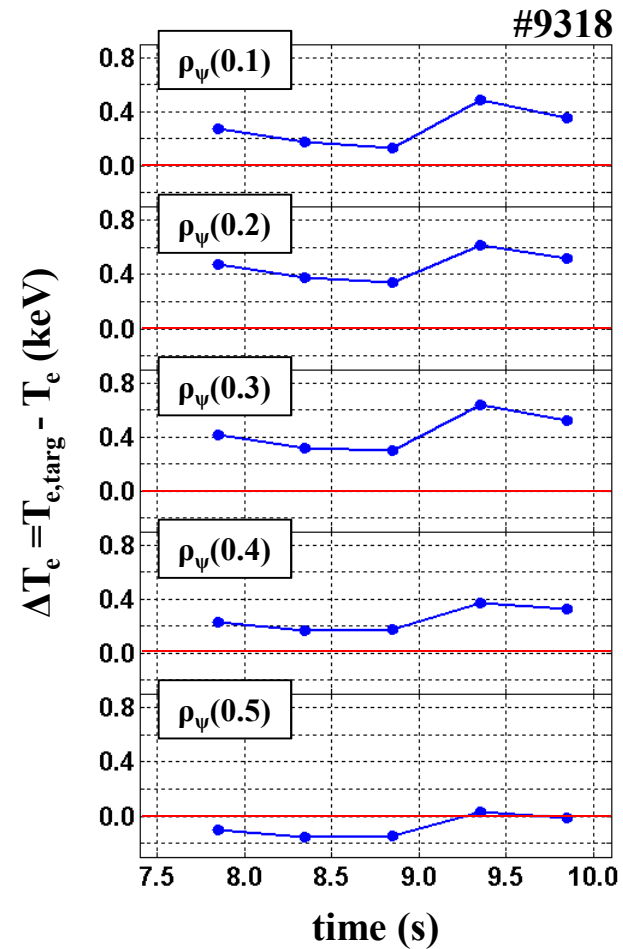
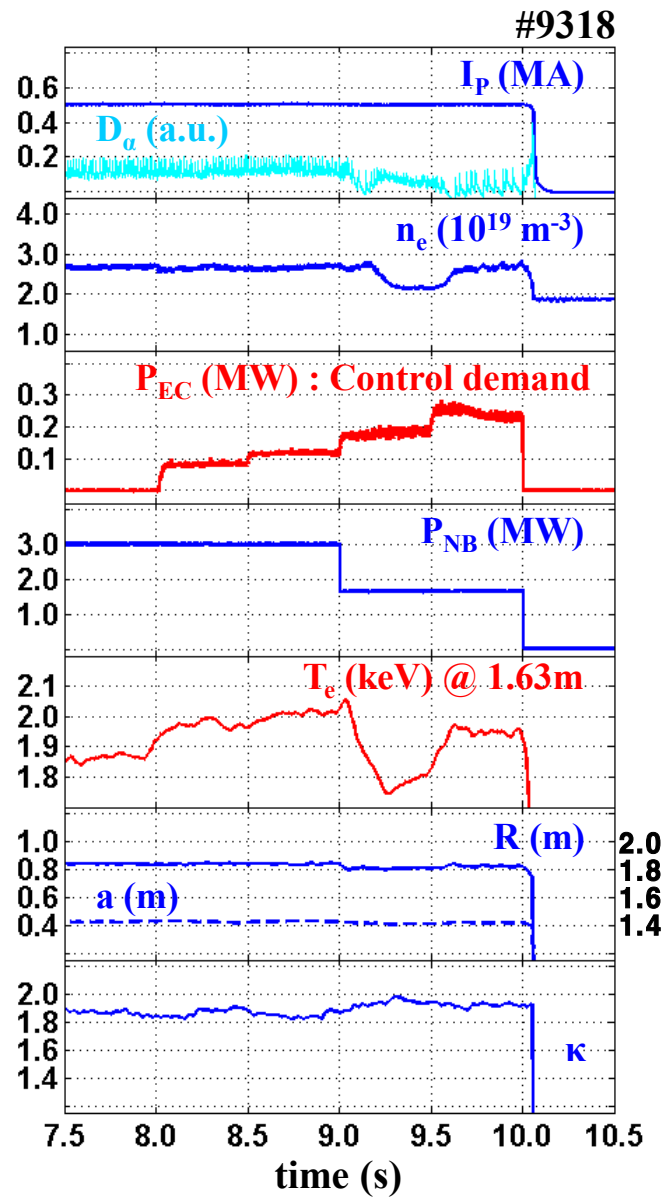
- JT60-U: Real time  $q_{min}$  control with MSE diagnostics and LHCD



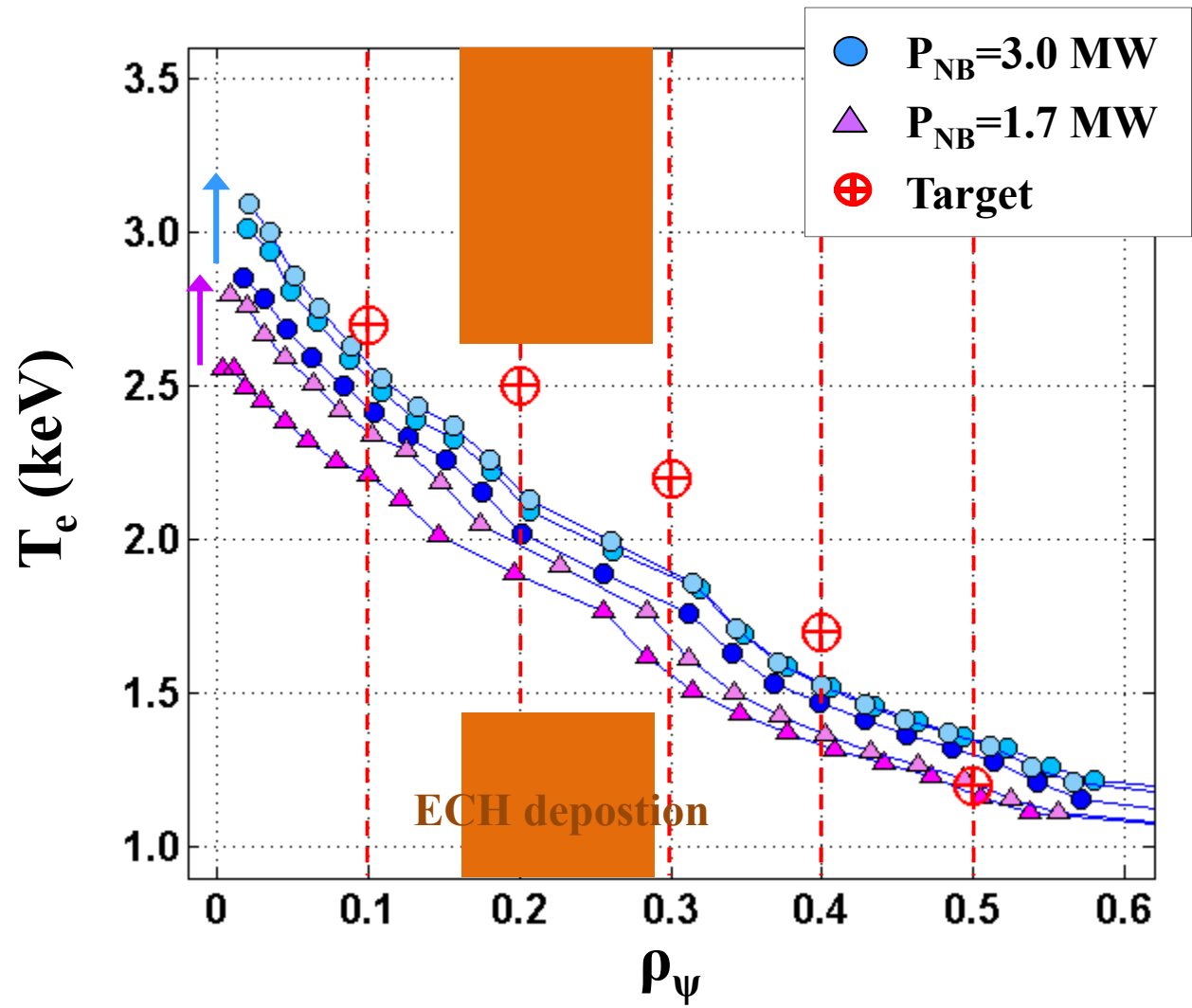
- Transport reduction at  $t = 12.4$  s
- Time delay in response of  $q_{min}$



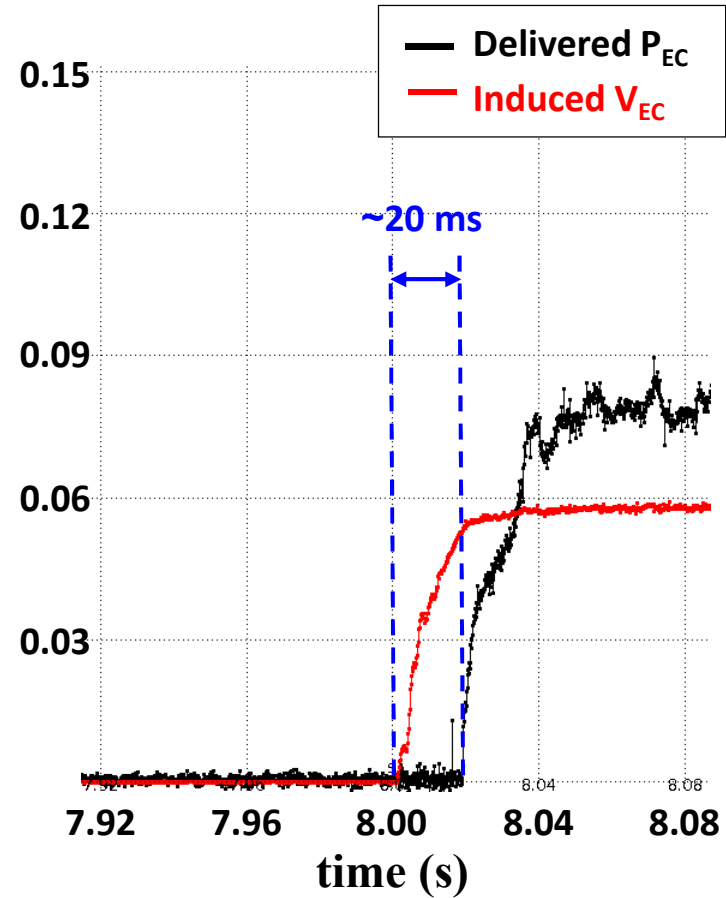
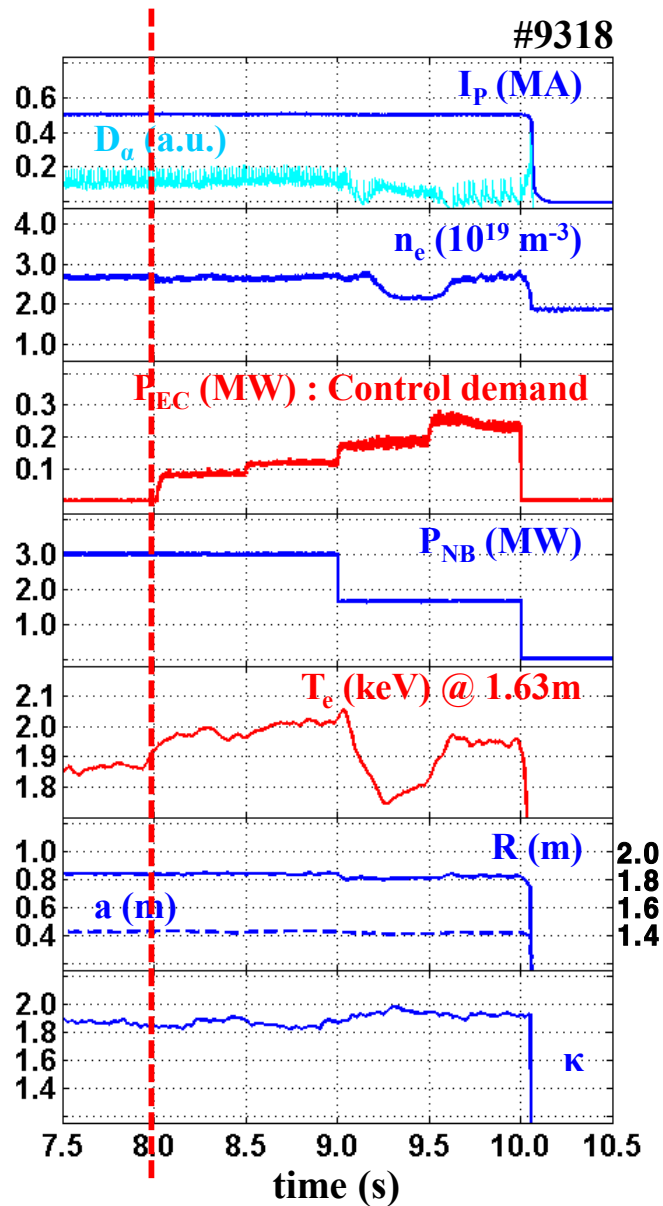
# RT- $T_e$ profile control in H-mode discharge (#9318)



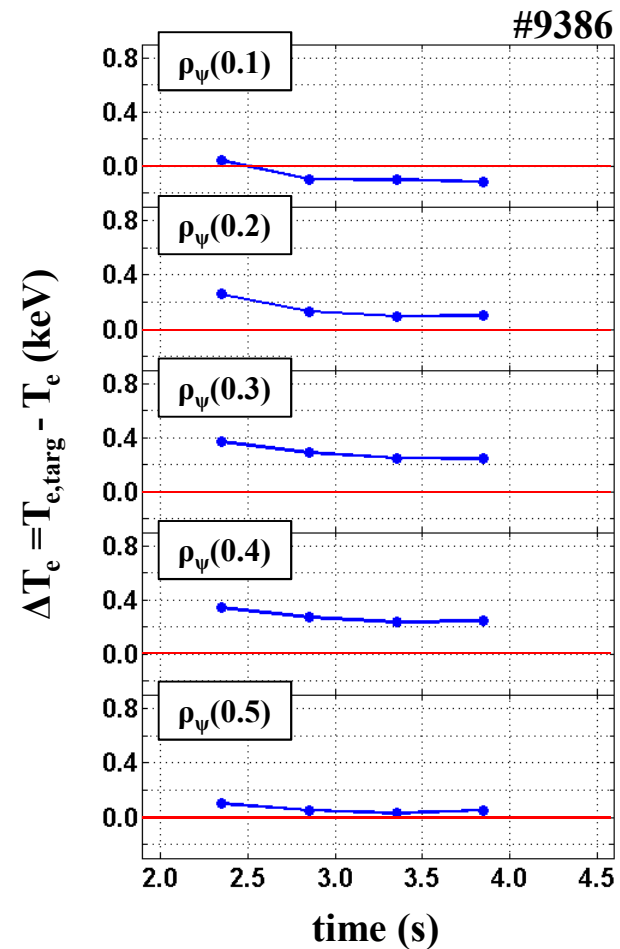
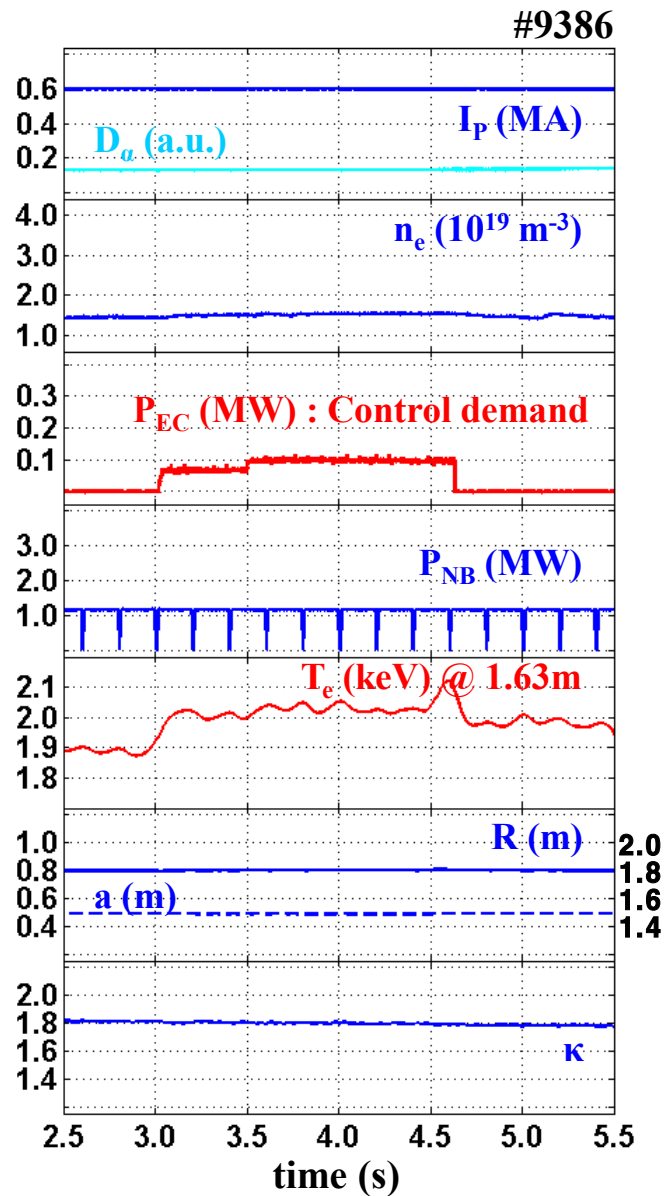
# RT- $T_e$ profile control in H-mode discharge (#9318)



# Time delay of first $P_{EC}$ injection



# RT- $T_e$ profile control in L-mode discharge (#9386)



# References

- *A. C. C. Sips*, Seminars