

### CSTR performance analysis – Ex 3.1

1)  $S_{min}$

$$S_{min} = K \frac{b}{Y\hat{q} - b} = (20 \text{ mg } BOD_L / L) \frac{0.15 / d}{(0.42 \text{ g } VSS_a / \text{g } BOD_L)(20 \text{ g } BOD_L / \text{g } VSS_a - d) - 0.15 / d}$$

$$= 0.36 \text{ mg } BOD_L / L$$

2)  $\theta_x^{min}$

$$\theta_x^{min} = \frac{K + S^0}{S^0(Y\hat{q} - b) - bK} = \frac{(20 + 500) \text{ mg } BOD_L / L}{(50 \text{ mg } BOD_L / L)(0.42 \cdot 20 / d - 0.15 / d) - (20 \text{ mg } BOD_L / L)(0.15 / d)}$$

$$= 0.126 \text{ d}$$

3)  $\theta_x$

$$\theta_x = \theta = V / Q = \frac{2000 \text{ m}^3}{1000 \text{ m}^3 / d} = 2 \text{ d}$$

$$\frac{\theta_x}{\theta_x^{min}} = SF = \frac{2 \text{ d}}{0.126 \text{ d}} = 16 \quad (\text{SF of 16 for washout})$$

4) Effluent VSS ( $X_v$ )

Let's calculate  $X_a$  &  $X_i$  separately:

$$X_a = Y(S^0 - S) \frac{1}{1 + b\theta_x} = (0.42 \text{ g } VSS_a / \text{g } BOD_L)(500 - 1.7 \text{ mg } BOD_L / L) \frac{1}{1 + (0.15 / d)(2 \text{ d})}$$

$$= 161 \text{ mg } VSS_a / L$$

$$X_i = X_i^0 + X_a(1 - f_d)b\theta_x = 50 \text{ mg } VSS_i / L + (161 \text{ mg } VSS_a / L)(1 - 0.8 \text{ g } VSS_i / \text{g } VSS_a)(0.15 / d)(2 \text{ d})$$

$$= 60 \text{ mg } VSS_i / L$$

$$X_v = X_a + X_i = 161 + 60 = 221 \text{ mg } VSS / L$$

### 5) Effluent COD & BOD<sub>L</sub>

Effluent COD = remaining substrate + SMP + all biomass (active+inert)

Effluent BOD<sub>L</sub> = remaining substrate + SMP + active and biodegradable biomass

i) substrate

$$S = K \frac{1 + b\theta_x}{Y\hat{q}\theta_x - (1 + b\theta_x)}$$

$$= (20 \text{ mg BOD}_L / L) \frac{1 + (0.15/d)(2d)}{(0.42 \text{ g VSS}_a / \text{g BOD}_L)(20 \text{ g BOD}_L / \text{g VSS}_a - d)(2d) + 1 + (0.15/d)(2d)}$$

$$= 1.7 \text{ mg BOD}_L / L$$

ii) SMP

Let's first calculate individual terms for Eqs [3.38] & [3.39]

$$r_{ut} = -\frac{\hat{q}S}{K+S} X_a = \frac{dS}{dt} = -\frac{S^0 - S}{\theta} = -\frac{(500 - 1.7) \text{ mg BOD}_L / L}{2d} = -249 \text{ mg BOD}_L / L - d$$

$$\hat{q}_{UAP} X_a \theta + K_{UAP} + k_1 r_{ut} \theta = 1.8 \cdot 161 \cdot 2 + 100 + 0.12 \cdot (250) \cdot 2 = 620 \text{ mg BOD}_L / L$$

$$4K_{UAP} k_1 r_{ut} \theta = 4 \cdot 100 \cdot 0.12 \cdot (250) \cdot 2 = 24000 \text{ (mg BOD}_L / L)^2$$

$$K_{BAP} + (\hat{q}_{BAP} - k_2) X_a \theta = 85 + (0.1 - 0.09) \cdot 161 \cdot 2 = 88.2 \text{ mg BOD}_L / L$$

$$4K_{BAP} k_2 X_a \theta = 4 \cdot 85 \cdot 0.09 \cdot 161 \cdot 2 = 9850 \text{ (mg BOD}_L / L)^2$$

$$UAP = \frac{620 + \sqrt{(620)^2 + 23900}}{2} = 9.5 \text{ mg BOD}_L / L$$

$$BAP = \frac{88.2 + \sqrt{(88.2)^2 + 9850}}{2} = 22.3 \text{ mg BOD}_L / L$$

$$SMP = UAP + BAP = 9.5 + 22.3 = 31.8 \text{ mg BOD}_L / L$$

iii) Biomass

Recall that we calculated the COD for the cell formula,  $C_5H_7O_2N$ , as 1.42 g COD/g cells (lecture #3)

In sum,

$$\begin{aligned} \text{Effluent COD} &= \text{Substrate} + \text{SMP} + \text{Biomass COD} = 1.7 + 31.8 + (1.42 \text{ g COD} / \text{g VSS})X_v \\ &= 1.7 + 31.8 + 1.42 \cdot 221 = 1.7 + 31.8 + 313.8 = 347 \text{ mg COD} / L \end{aligned}$$

\* Biomass accounts for most of COD – this COD can be removed by settling (but good settling property should be guaranteed)

\* SMP accounts for most of soluble COD

$$\begin{aligned} \text{Effluent } BOD_L &= \text{Substrate} + \text{SMP} + \text{biodegradable biomass} \\ &= 1.7 + 31.8 + (1.42 \text{ g COD} / \text{g VSS}) \cdot X_a \cdot f_d = 216 \text{ mg } BOD_L / L \end{aligned}$$