# Chapter 5

## **AUXILIARY FUNCTIONS**

## **5.1 Introduction**

- The main power of the thermodynamic method stems from its provision of criteria for equilibrium in materials systems
- S and V are an inconvenient choice of independent variables.

## **5.1 Introduction**

 From the theoretician's point of view the most convenient choice of independent variables would be V and T

$$G = (U + PV) - TS$$
 (The Gibbs F.E.)  
= H - TS (5.2)

## 5.2 The Enthalpy, H

• For a closed system with const. P

 $U_2 - U_1 = q_p - P(V_2 - V_1)$ 

 $(U_2 + PV_2) - (U_1 + PV_1) = q_p$ 

$$\Delta H = H_2 - H_1 = q_p$$

$$(A_2 - A_1) = (U_2 - U_1) - (T_2 S_2 - T_1 S_1)$$

If the system is closed

• If the process is isothermal,  $T_2 = T_1 = T$ , then, from the  $2^{nd}$  Law

$$q \le T(S_2 - S_1)$$

• Hence

 $(A_2 - A_1) \leq -w$ 

$$(A_2 - A_1) + T\Delta S_{irr} = -w$$
 (5.3)

• For an isothermal process conducted at const. V, no P-V work,

 $(A_2-A_1) + T\Delta S_{irr}=0$ 

 $dA + TdS_{irr} = 0$ 

• For a reversible process, dA = 0, reversible means equilibrium!



constant temperature U  $A = U \cdot TS$  -TS 0  $n_v(eq,T)$  $n_v \rightarrow$ 

constant volume.

Figure 5.1 The variations of (a) internal energy, U, and (b) entropy, S, with the number of atoms in the vapor phase of a closed solidvapor system at constant temperature and constant volume.

Figure 5.2 Illustration of the criterion for equilibrium in a closed solidvapor system at constant temperature and constant volume.

$$p = \frac{n_{\nu(\text{eq.}T)}kT}{(V - V_S)}$$

$$p_{(\text{at }T_1)} = \frac{n_{v(\text{eq},T_1)}kT_1}{(V - V_{S(\text{at }T_1)})}$$

$$p_{(\text{at }T_2)} = \frac{n_{v(\text{eq},T_2)}kT_2}{(V - V_{S(\text{at }T_2)})}$$

$$\ln p \,(\text{atm}) = \frac{-3166}{T} + 16.01$$



 $\Delta A = -T\Delta S_{\rm irr}$ 

Figure 5.3 The influence of temperature on the equilibrium state of a closed solid-vapor system of constant volume.

### 5.4 THE GIBBS FREE ENERGY, G

$$(G_2 - G_1) = (H_2 - H_1) - (T_2S_2 - T_1S_1) = (U_2 - U_1) + (P_2V_2 - P_1V_1) - (T_2S_2 - T_1S_1)$$

For a closed system,  $(U_2 - U_1) = q - w$ 

If 
$$T_1 = T_2 = T$$
, and  $P_1 = P_2 = P$   
 $(G_2 - G_1) = q - w + (P_2V_2 - P_1V_1) - (T_2S_2 - T_1S_1)$  (5.6)

w is the total work

$$w = w' + P(V_2 - V_1)$$

## 5.4 THE GIBBS FREE ENERGY, G

$$(G_2 - G_1) = q - w' - T(S_2 - S_1)$$

$$q \leq T(S_2 - S_1)$$





### 5.5 SUMMARY OF THE EQ. FOR A CLOSED SYS.



## 5.6 THE VARIATION OF THE COMPO. & SIZE OF THE SYS.

 If the size & composition can vary during a process, then the specification of only two variables is no longer sufficient to fix the state of the system

$$G=G(T,P,n_i,n_j,n_k,...)$$
 (5.13)

• Differentiation of Eq.(5.13)



## 5.6 THE VARIATION OF THE COMPO. & SIZE OF THE SYS.

$$dG = -SdT + VdP$$
$$\left(\frac{\partial G}{\partial T}\right)_{P,n_{P},n_{P},\dots} = -S$$

$$\left(\frac{\partial G}{\partial P}\right)_{T,n_i,n_j,\ldots} = V$$



### **5.7 The Chemical Potential**

$$\left(\frac{\partial G}{\partial n_i}\right)_{T,P,n_j,\ldots} = \mu_i$$
 (5.16)

 $\mu_i$  is the amount by which the capacity of the system for doing work, other than the work of expansion, is increased, per mole of i added at const. T, P and  $i \neq j$ .

$$dG = -SdT + VdP + \sum_{i=1}^{k} \mu_{i} dn_{i}$$
 (5.17)

Applicable to open system which exchange matter as well as heat with surrounding, to closed system which undergoes compositional change.

To open system 
$$dU = TdS - PdV + \sum_{i=1}^{k} \left(\frac{\partial U}{\partial n_{i}}\right)_{S,V,n,\dots} dn_{i}$$
(5.18)

#### **5.7 The Chemical Potential**

$$\left(\frac{\partial G}{\partial n_i}\right)_{T,P,n_j} = \mu_i = \left(\frac{\partial U}{\partial n_i}\right)_{S,V,n_j} = \left(\frac{\partial H}{\partial n_i}\right)_{S,P,n_j} = \left(\frac{\partial A}{\partial n_i}\right)_{T,V,n_j}$$
(5.21)



From the 1<sup>st</sup> & 2<sup>nd</sup> laws

$$dU = \delta q - \delta w$$

$$\delta q = TdS$$

The comparison gives

 $\delta w = PdV + \sum \mu_i dn_i$ = w' = chemical work

### **5.8 Thermodynamic Relations**

$$T = \left(\frac{\partial U}{\partial S}\right)_{V,\text{comp}} = \left(\frac{\partial H}{\partial S}\right)_{P,\text{comp}}$$
(5.26)

$$P = -\left(\frac{\partial U}{\partial V}\right)_{S,\text{comp}} = -\left(\frac{\partial A}{\partial V}\right)_{T,\text{comp}}$$
(5.27)



If Z is a state function, then

$$Z = Z(x,y)$$

$$dZ = \left(\frac{\partial Z}{\partial x}\right)_y dx + \left(\frac{\partial Z}{\partial y}\right)_x dy$$

$$dZ = Ldx + Mdy$$



If Z is a state function, the change in Z is indep. of the order of differentiation.

$\left[\frac{\partial}{\partial Z}\right]_{-}$	[ <u>∂</u> ( à	Z ] ]	$\partial^2 Z$
$\left[\frac{\partial y}{\partial x}\left(\frac{\partial x}{\partial x}\right)_{y}\right]_{x} =$	$\left[\frac{\partial x}{\partial x}\right]$	$\left[\frac{1}{y}\right]_{x} \left[\frac{1}{y}\right]_{y} =$	$\partial x \partial y$

$$\left(\frac{\partial L}{\partial y}\right)_{x} = \left(\frac{\partial M}{\partial x}\right)_{y}$$
(5.30)

$$dU = TdS - PdV$$
(5.31) $dH = TdS + VdP$ (5.10)(5.32) $dA = -SdT - PdV$ (5.11)(5.33) $dG = -SdT + VdP$ (5.12)(5.34)

(5.33) & (5.34) are measurable quantities!

$$\left(\frac{\partial S}{\partial V}\right)_T = \left(\frac{\partial P}{\partial T}\right)_V \tag{5.33}$$

$$S = S(T, V)$$
(ii)  

$$dS = \left(\frac{\partial S}{\partial T}\right)_{V} dT + \left(\frac{\partial S}{\partial V}\right)_{T} dV$$
(i)  

$$TdS = \delta q_{v} = dU = nc_{v} dT$$
(iv)  

$$\left(\frac{\partial S}{\partial T}\right)_{V} = \frac{nc_{v}}{T}$$
(v)

For closed system of fixed composition,

$$dU = TdS - PdV$$

$$\left(\frac{\partial U}{\partial V}\right)_{T} = T\left(\frac{\partial S}{\partial V}\right)_{T} - P$$
From (5.33)
$$\left(\frac{\partial S}{\partial V}\right)_{T} = \left(\frac{\partial P}{\partial T}\right)_{V}$$

$$\left(\frac{\partial U}{\partial V}\right)_{T} = T\left(\frac{\partial P}{\partial T}\right)_{V} - P$$

Similarly, dH = TdS + VdP



### 5.10 The Upstairs-Downstairs-Inside-Out Formula

For closed system of fixed composition, with 3 state properties, x, y, & z:

x = x(y,z) $dx = \left(\frac{\partial x}{\partial y}\right)_z dy + \left(\frac{\partial x}{\partial z}\right)_y dz$ 

For an incremental change of state at const. x,

then,

or,





### 5.11 The Gibbs-Helmholtz Equation

$$G = H - TS$$

dG = -SdT + VdP (5.12) 
$$\left(\frac{\partial G}{\partial T}\right)_P = -S$$



### 5.11 The Gibbs-Helmholtz Equation



(5.36)

(5.36a)

 $\Delta G$  can be determined from an experimentally measured  $\Delta H$ ,

Similarly,

$$A = U - TS$$
  
=  $U + T \left(\frac{\partial A}{\partial T}\right)_{V}$   
$$\frac{d(A/T)}{dT} = -\frac{U}{T^{2}}$$
 (5.37)  
$$\frac{d(\Delta A/T)}{dT} = -\frac{\Delta U}{T^{2}}$$
 (5.37a)